

Gas Oil Composition

[Field of the Invention]

The present invention relates to gas oil compositions containing mainly an FT synthetic base oil, more particularly to gas oil compositions that can achieve environment load reduction, low temperature properties and low fuel consumption all together and are suitably used in a winter season.

[Background of the Invention]

In general, a gas oil composition is produced by blending one or more types of base oils produced by subjecting a straight gas oil or straight kerosene, produced by atmospheric distillation of crude oil to hydrorefining or hydrodesulfurization. In particular, it is often the case that the blend ratio of the foregoing kerosene base oil and gas oil base oil is adjusted in order to ensure the cold flowability during a winter season. If necessary, the base oils are blended with additives such as cetane number improvers, detergents and cold flow improvers (see, for example, Non-Patent Document No. 1 below).

Lower sulfur and aromatic contents are regarded as capable of suppressing the formation of harmful

components such as NO_x and PM in the exhaust gas from engines. From the view point of this, attention has been brought to fuels such as liquid fractions corresponding to naphtha, kerosene and gas oil, produced by subjecting a mixed gas containing mainly hydrogen and carbon monoxide produced from natural gas, coal, biomass or sludge (hereinafter may be often referred to as "synthetic gas") to a Fischer-Tropsch (FT) reaction; hydrocarbon mixtures produced by hydrorefining or hydrocracking such liquid fractions; and hydrocarbon mixtures produced by hydrorefining or hydrocracking liquid fractions and FT wax produced through a Fischer-Tropsch reaction, as fuels contributing environment load reduction.

However, since the FT reaction per se contains a wax formation process, the hydrotreated products of the FT reaction product are relatively large in the content of straight-chain saturated hydrocarbon (normal paraffins) compounds. It has been pointed out that in particular when heavy normal paraffin compounds are contained, there is the possibility that they would deposit in the form of wax. Further, the FT synthetic base oil is a hydrocarbon mixture containing predominantly the aforesaid normal paraffins and saturated hydrocarbons having a side chain

(isoparaffin) and thus is generally poor in oil solubility. Therefore, there is the possibility that additives that are dissolved in fuel oils such as gas oil, highly relying on their oil soluble groups (straight-chain alkyl groups or the like) would be hardly dissolved. Among such additives, there would be likely used conventional cold flow improvers (CFI) composed of an ethylene-vinyl acetate copolymer mixture due to the restriction on the solubility to fuel.

Patent Document No. 1 discloses in an example thereof a synthetic fuel containing a gas oil fraction produced from an FT synthetic base oil only. However, this gas oil is an extremely light fuel containing a kerosene fraction in a large amount because the document intends to solve a problem concerning low-temperature startability and thus a technique for improving low-temperature properties with a cold flow improver can not be selected. As the result, significant reductions in density, kinematic viscosity and volume calorific value can not be avoided, and furthermore it can not be denied that the reductions would result in significant deterioration in fuel consumption, seizure of injection pumps, cavitation damages and defects in high-temperature restartability.

That is, it is very difficult to design a high-quality fuel that can achieve at a high level the requirements sought for a gas oil composition having environment load reduction properties, excellent practical performances in a winter season and suppression of fuel consumption deterioration all together, and there exists no example or finding on the basis of studies of such a fuel satisfying various properties required for fuel other than the foregoing sufficiently and a practical process for producing the fuel.

(1) Patent Document No. 1: Japanese Patent
Laid-Open Publication No. 2005-529213

(2) Non-Patent Document No. 1: Konishi Seiichi,
"Nenryo Kogaku Gairon", Shokabo Publishing Co.,
Ltd., March, 1991, pages 136 to 144

[Disclosure of the Invention]

The present invention was made in view of the above-described situations and has an object to provide a gas oil composition containing mainly an FT synthetic base oil, more specifically such a gas oil composition that can achieve environment load reduction, low temperature properties and low fuel consumption all together and is suitably used in a winter season.

The present invention was completed as the result

of extensive study and research carried out by the present inventors to solve the foregoing problems. That is, the present invention relates to a gas oil composition comprising a gas oil composition selected from the group consisting of the following gas oil compositions (A) to (C) and additives added in accordance with the following Steps 1 and 2:

[I] gas oil compositions (A) comprising an FT synthetic base oil in an amount of 60 percent by volume or more on the basis of the total amount of the gas oil composition, with a sulfur content of 5 ppm by mass or less, an aromatic content of 10 percent by volume or less, an oxygen content of 100 ppm or less, a density of 760 kg/m^3 or greater and 840 kg/m^3 or less, a 90% distillation temperature of 280°C or higher and 330°C or lower and an end point of 360°C or lower in distillation characteristics, an insoluble content after an oxidation stability test of 0.5 mg/100 mL or less, an HFRR wear scar diameter (WS1.4) of 400 μm or smaller, a cloud point of -15°C or lower, a cold filter plugging point of -25°C or lower, a pour point of -32.5°C or lower, a total content of normal paraffins having 20 to 30 carbon atoms of less than 2 percent by mass, a value determined by dividing the total content of normal paraffins having 20 to 30 carbon atoms by the

total content of hydrocarbons having 20 to 30 carbon atoms other than the normal paraffins of 0.2 or greater and 0.6 or less, and a relation in the content of each of normal paraffins (CnP) having 15 to 20 carbon atoms defined by $C_{20}P < C_{19}P < C_{18}P < C_{17}P < C_{16}P < C_{15}P$;

[II] gas oil compositions (B) comprising an FT synthetic base oil in an amount of 60 percent by volume or more on the basis of the total amount of the gas oil composition, with a sulfur content of 5 ppm by mass or less, an aromatic content of 10 percent by volume or less, an oxygen content of 100 ppm or less, a density of 760 kg/m³ or greater and 840 kg/m³ or less, a 90% distillation temperature of 280°C or higher and 350°C or lower and an end point of 360°C or lower in distillation characteristics, an insoluble content after an oxidation stability test of 0.5 mg/100 mL or less, an HFRR wear scar diameter (WS1.4) of 400 µm or smaller, a cloud point of -5°C or lower, a cold filter plugging point of -20°C or lower, a pour point of -25°C or lower, a total content of normal paraffins having 20 to 30 carbon atoms of 2 percent by mass or more and less than 4 percent by mass, a value determined by dividing the total content of normal paraffins having 20 to 30 carbon atoms by the total content of hydrocarbons having 20 to 30 carbon atoms other than

the normal paraffins of 0.2 or greater and 0.6 or less, and a relation in the content of each of normal paraffins (C_nP) having 20 to 25 carbon atoms defined by C₂₀P>C₂₁P>C₂₂P>C₂₃P>C₂₄P>C₂₅P; and

[III] gas oil compositions (C) comprising an FT synthetic base oil in an amount of 60 percent by volume or more on the basis of the total amount of the gas oil composition, with a sulfur content of 5 ppm by mass or less, an aromatic content of 10 percent by volume or less, an oxygen content of 100 ppm or less, a density of 760 kg/m³ or greater and 840 kg/m³ or less, a 90% distillation temperature of 280°C or higher and 350°C or lower and an end point of 360°C or lower in distillation characteristics, an insoluble content after an oxidation stability test of 0.5 mg/100 mL or less, an HFRR wear scar diameter (WS1.4) of 400 μm or smaller, a cloud point of -3°C or lower, a cold filter plugging point of -10°C or lower, a pour point of -12.5°C or lower, a total content of normal paraffins having 20 to 30 carbon atoms of 4 percent by mass or more and less than 6 percent by mass, a value determined by dividing the total content of normal paraffins having 20 to 30 carbon atoms by the total content of hydrocarbons having 20 to 30 carbon atoms other than the normal paraffins of 0.2 or greater and 0.6 or less,

and relations in the content of each of normal paraffins (C_nP) having 20 to 25 carbon atoms defined by C₂₀P>C₂₁P>C₂₂P>C₂₃P>C₂₄P>C₂₅P and $(C_{24}P - C_{25}P) / C_{24}P > (C_{22}P - C_{23}P) / C_{22}P > (C_{20}P - C_{21}P) / C_{20}P$; (Step 1) a lubricity improver comprising a fatty acid and/or a fatty acid ester is admixed in an amount of 20 mg/L or more and 300 mg/L or less in terms of the active component with the gas oil composition by line-blending, forced-stirring or leaving to stand for a sufficient time; and (Step 2) a cold flow improver comprising an ethylene vinyl acetate copolymer and/or a compound with a surface active effect is admixed in an amount of 20 mg/L or more and 1000 mg/L or less in terms of the active component with the gas oil composition by line-blending, forced-stirring or leaving to stand for a sufficient time.

Alternatively, the gas oil composition of the present invention is preferably admixed with 200 mg/L or more and 500 mg/L or less of a detergent comprising a polyether amine compound, a polybutenyl amine compound, an alkenyl succinamide compound, or an alkenyl succinimide compound by line-blending, forced-stirring or leaving to stand for a sufficient

time, in a step added between Steps 1 and 2. Preferably, the lubricity improver, detergent and cold flow improver each contain a solvent containing no chemical substance with a melting point of 10°C or higher. Preferably, the gas oil composition has a peroxide number after an accelerated oxidation test of 50 ppm by mass or less, a kinematic viscosity at 30°C of 2.5 mm²/s or greater and 5.0 mm²/s or less, a cetane index of 45 or greater and a water content of 100 ppm by volume or less.

The intentions of the present invention are as follows. A fuel would be adversely affected if it is produced by a process wherein the wax content is extremely reduced by excessive lightening, and a fuel of low oil solubility, which is produced solely from an FT synthetic base oil would hardly dissolve additives, resulting in the possibility that they would fail to exhibit their original advantageous effects. Therefore, the present invention is intended to create and propose a quality design method required for imparting a fuel reduced in oil solubility with an effect to improve cold flowability by addition of additives such as CFI.

[Effects of the Invention]

According to the present invention, the use of a gas oil composition produced by the above-described process to satisfy the above-described requirements regarding fractions and the like renders it possible to produce easily a gas oil composition suitable for a winter season that can achieve environment load reduction, low-temperature properties and low fuel consumption all together, which have been difficult to achieve with the conventional gas oil compositions.

[Best Mode for Carrying out the Invention]

The present invention will be described in more detail below.

The gas oil composition of the present invention necessarily contains an FT synthetic base oil. The FT synthetic base oil is composed of saturated hydrocarbon compounds, and the gas oil composition of the present invention can be easily produced by adjusting the blend of the hydrocarbon compounds. There is no particular restriction on the characteristics of the FT synthetic base oil as long as the characteristics of the gas oil composition of the present invention are satisfied. There is no particular restriction on base oils other than the FT synthetic base oil as long as the

characteristics of the gas oil composition of the present invention are fulfilled. However, in order to allow the composition to exhibit sufficient environment friendly properties, it is preferable to blend the following petroleum base oil having been highly hydrotreated and animal- or vegetable-derived processed oils.

The FT synthetic base oil referred herein denotes various synthetic oils such as liquid fractions corresponding to naphtha, kerosene and gas oil, produced by subjecting a mixed gas containing mainly hydrogen and carbon monoxide (hereinafter may be often referred to as "synthetic gas") to a Fischer-Tropsch (FT) reaction; hydrocarbon mixtures produced by hydrotreating or hydrocracking such liquid fractions; and hydrocarbon mixtures produced by hydrotreating or hydrocracking liquid fractions and FT wax produced through a Fischer-Tropsch reaction.

The gas oil composition comprises preferably 60 percent by volume or more of the FT synthetic base oil. Further, the composition comprises more preferably 70 percent by volume or more, more preferably 80 percent by volume or more of the FT synthetic base oil with the objective of lessening the occasion to increase the burden to the environment caused by sulfur components

or aromatic components.

The mixed gas which will be the feedstock of the FT synthetic oil is produced by oxidizing a substance containing carbon using oxygen and/or water and/or carbon dioxide as an oxidizing agent and further if necessary by a shift reaction using water so as to be adjusted in predetermined hydrogen and carbon monoxide concentrations.

Substances containing carbon which may be used herein are generally gas components composed of hydrocarbons that are gas in normal temperatures such as natural gas, liquefied petroleum gas, and methane gas, petroleum asphalt, biomass, coke, wastes such as building materials and garbage, sludge, heavy crude oils that are difficult to be disposed in the usual manner, and mixed gas produced by exposing unconventional petroleum resources to elevated temperatures. However, in the present invention, there is no particular restriction on the feedstock as long as a mixed gas containing mainly hydrogen and carbon monoxide can be produced.

The Fischer-Tropsch reaction requires a metal catalyst. It is preferable to use metals in Group 8 of the periodic table, such as cobalt, ruthenium, rhodium, palladium, nickel and iron, more preferably

metals in Group 8, Period 4, as an active catalyst component. Alternatively, there may be used a mixed metal group containing these metals in suitable amounts. These active metals are generally used in the form of a catalyst produced by supporting them on a support such as alumina, titania and silica-alumina.

Alternatively, the use of the forgoing active metals in combination with a second metal can improve the performances of the resulting catalyst. Examples of the second metal include alkali or alkaline earth metals such as sodium, lithium and magnesium, zirconium, hafnium and titanium, which will be used depending on purposes such as increase in conversion rate of carbon monoxide or chain growth probability (α) which is an index of the production amount of wax.

The Fischer-Tropsch reaction is a synthetic method for producing liquid fractions and FT wax using a mixed gas as the feedstock. It is generally preferable to adjust the ratio of hydrogen to carbon monoxide in the mixed gas in order to carry out the synthetic method efficiently. In general, the molar mix ratio of hydrogen to carbon monoxide (hydrogen/carbon monoxide) is preferably 1.2 or greater, more preferably 1.5 or greater, more preferably 1.8 or greater. The ratio is also

preferably 3 or less, more preferably 2.6 or less, more preferably 2.2 or less.

The reaction temperature at which the Fischer-Tropsch reaction is carried out using the foregoing catalyst is preferably 180°C or higher and 320°C or lower, more preferably 200°C or higher and 300°C or lower. At a reaction temperature of lower than 180°C, carbon monoxide hardly reacts, resulting in a tendency that the hydrocarbon yield is reduced. At a reaction temperature of higher than 320°C, gas such as methane is increasingly formed, resulting in a reduction in the production efficiency of liquid fractions and FT wax.

There is no particular restriction on the gas hourly space velocity with respect to the catalyst. However, it is preferably 500 h⁻¹ or more and 4000 h⁻¹ or lower, more preferably 1000 h⁻¹ or more and 3000 h⁻¹ or lower. A gas hourly space velocity of less than 500 h⁻¹ is likely to reduce the production of the liquid fuel while a gas hourly space velocity of more than 400 h⁻¹ causes a necessity to increase the reaction temperature and increase the amount of gas to be produced, resulting in a reduction in the yield of the intended product.

There is no particular restriction on the reaction

pressure (partial pressure of a synthetic gas composed of carbon monoxide and hydrogen). However, it is preferably 0.5 MPa or greater and 7 MPa or smaller, more preferably 2 MPa or greater and 4 MPa or smaller. If the reaction pressure is smaller than 0.5 MPa, the yield of liquid fuel would tend to decrease. If the reaction pressure is greater than 7 MPa, it is not economically advantageous because the amount of capital investment in facilities would be increased.

If necessary, liquid fractions and FT wax produced through the above-described FT reaction may be hydrorefined or hydrocracked in any suitable manner so as to be adjusted in distillation characteristics or composition to achieve the purposes of the invention. Hydrorefining or hydrocracking may be selected depending on the purposes and the present invention is not limited in selection to either one or both of them to such an extent that the gas oil composition of the present invention is produced.

Catalysts used for hydrorefining are generally those comprising a hydrogenation active metal supported on a porous support, but the present invention is not limited thereto as long as the same effects are obtained.

The porous support is preferably an inorganic

oxide. Specific examples include alumina, titania, zirconia, boria, silica, zeolite and the like.

Zeolite is crystalline aluminosilicate, examples of which include faujasite, pentasil and mordenite type zeolites. Preferred are faujasite, beta and mordenite type zeolites and particularly preferred are Y-type and beta-type zeolites. Y-type zeolites are preferably ultra stable.

Preferred for the active metal are those of the following two types (active metal A type and active metal B type).

The active metal A type is at least one type of metal selected from the group consisting of those in Group 8 of the periodic table. It is preferably at least one type selected from the group consisting of Ru, Rh, Ir, Pd and Pt, and is more preferably Pd and/or Pt. The active metal may be a combination of these metals, such as Pt-Pd, Pt-Rh, Pt-Ru, Ir-Pd, Ir-Rh, Ir-Ru, Pt-Pd-Rh, Pt-Rh-Ru, Ir-Pd-Rh, and Ir-Rh-Ru. A noble metal catalyst formed of these metals can be used after being subjected to a pre-reduction treatment under hydrogen flow. In general, the catalyst is heated at a temperature of 200°C or higher in accordance with predetermined procedures, circulating a gas containing hydrogen so that the active metal on the

catalyst is reduced and thus exhibits hydrogenation activity.

The active metal B type contains preferably at least one type of metal selected from the group consisting of those in Groups 6A and 8 of the periodic table, desirously two or more types of metals selected therefrom. Examples of these metals include Co-Mo, Ni-Mo, Ni-Co-Mo and Ni-W. When a metal sulfide catalyst formed of these metals is used, it must undergo a pre-sulfurization process.

The metal source may be a conventional inorganic salt or complex salt compound. The supporting method may be any supporting method that has been usually used for hydrogenation catalysts, such as impregnation and ion-exchange methods. When a plurality of metals are supported, they may be supported simultaneously using a mixed solution thereof or sequentially using a single solution containing each metal. The metal solution may be an aqueous solution or a solution using an organic solvent.

The reaction temperature at which hydrorefining is carried out using a catalyst composed of the active metal A type is preferably 180°C or higher and 400°C or lower, more preferably 200°C or higher and 370°C or lower, more preferably 250°C or higher and 350°C or

lower, more preferably 280°C or higher and 350°C or lower. A reaction temperature of higher than 370°C is not preferable because the yield of the middle fraction is extremely reduced, resulting from an increase in a side reaction wherein the liquid fraction or FT wax is cracked to a naphtha fraction. A reaction temperature of lower than 270°C is not also preferable because alcohols can not be removed and thus remains in the reaction system.

The reaction temperature at which hydrotreating is carried out using a catalyst composed of the active metal B type is preferably 170°C or higher and 320°C or lower, more preferably 175°C or higher and 300°C or lower, more preferably 180°C or higher and 280°C or lower. A reaction temperature of higher than 320°C is not preferable because the yield of the middle fraction is reduced, resulting from an increase in a side reaction wherein the liquid fraction or FT wax is cracked to a naphtha fraction. A reaction temperature of lower than 170°C is not also preferable because alcohols can not be removed and thus remains in the reaction system.

The hydrogen pressure at which hydrotreating is carried out using a catalyst composed of the active metal A type is preferably 0.5 MPa or greater and 12

MPa or less, more preferably 1.0 MPa or greater and 5.0 MPa or less. Although a higher hydrogen pressure facilitates the hydrogenation reaction, there is generally an optimum point in economical sense.

The hydrogen pressure at which hydrorefining is carried out using a catalyst composed of the active metal B type is preferably 2 MPa or greater and 10 MPa or less, more preferably 2.5 MPa or greater and 8 MPa or less, more preferably 3 MPa or greater and 7 MPa or less. Although a higher hydrogen pressure facilitates the hydrogenation reaction, there is generally an optimum point in economical sense.

The liquid hourly space velocity (LHSV) at which hydrorefining is carried out using a catalyst composed of the active metal A type is preferably 0.1 h^{-1} or greater and 10.0 h^{-1} or less, more preferably 0.3 h^{-1} or greater and 3.5 h^{-1} or less. Although a lower LHSV is advantageous for the reaction, a too low LHSV is not economically preferable because it requires an extremely large reactor volume, leading to an excessive capital investment in facilities.

The liquid hourly space velocity (LHSV) at which hydrorefining is carried out using a catalyst composed of the active metal B type is preferably 0.1 h^{-1} or greater and 2 h^{-1} or less, more preferably 0.2 h^{-1} or

greater and 1.5 h^{-1} or less, more preferably 0.3 h^{-1} or greater and 1.2 h^{-1} or less. Although a lower LHSV is advantageous for the reaction, a too low LHSV is not economically preferable because it requires an extremely large reactor volume, leading to an excessive capital investment in facilities.

The hydrogen/oil ratio at which hydrorefining is carried out using a catalyst composed of the active metal A type is preferably 50 NL/L or greater and 1000 NL/L or less, more preferably 70 NL/L or greater and 800 NL/L or less. Although a higher hydrogen/oil ratio facilitates the reaction, there is generally an optimum point in economical sense.

The hydrogen/oil ratio at which hydrorefining is carried out using a catalyst composed of the active metal B type is preferably 100 NL/L or greater and 800 NL/L or less, more preferably 120 NL/L or greater and 600 NL/L or less, more preferably 150 NL/L or greater and 500 NL/L or less. Although a higher hydrogen/oil ratio facilitates the reaction, there is generally an optimum point in economical sense.

Catalysts used for hydrocracking are generally those comprising a hydrogenation active metal supported on a support with solid acidic properties, but the present invention is not limited thereto as long

as the same effects are obtained.

As for the support with solid acidic properties, there are amorphous and crystalline zeolite types. Specific examples include silica-alumina, silica-magnesia, silica-zirconia and silica-titania, which are of amorphous type and zeolites of faujasite, beta, MFI and mordenite types, preferably Y type and beta type. The Y type zeolites are preferably those that are ultra stable.

Preferred for the active metal are those of the following two types (active metal A type and active metal B type).

The active metal A type is at least one type of metal mainly selected from the group consisting of those in Groups 6A and 8 of the periodic table. It is preferably at least one type of metal selected from the group consisting of Ni, Co, Mo, Pt, Pd and W. A noble metal catalyst formed of these metals can be used after being subjected to a pre-reduction treatment under hydrogen flow. In general, the catalyst is heated at a temperature of 200°C or higher in accordance with predetermined procedures, circulating a gas containing hydrogen so that the active metal on the catalyst is reduced and thus exhibits hydrogenation activity.

The active metal B type may be a combination of

these metals, such as Pt-Pd, Co-Mo, Ni-Mo, Ni-W, and Ni-Co-Mo. When a catalyst formed of these metals is used, it must undergo a pre-sulfurization process before use.

The metal source may be a conventional inorganic salt or complex salt compound. The supporting method may be any supporting method that has been usually used for hydrogenation catalysts, such as impregnation and ion-exchange methods. When a plurality of metals are supported, they may be supported simultaneously using a mixed solution thereof or sequentially using a single solution containing each metal. The metal solution may be an aqueous solution or a solution with an organic solvent.

The reaction temperature at which hydrocracking is carried out using a catalyst composed of the active metal type A and active metal type B is preferably 200°C or higher and 450°C or lower, more preferably 250°C or higher and 430°C or lower, more preferably 300°C or higher and 400°C or lower. A reaction temperature of higher than 450°C is not preferable because the yield of the middle fraction is extremely reduced, resulting from an increase in a side reaction wherein the liquid fraction or FT wax is cracked to a naphtha fraction. A reaction temperature of lower than 200°C is not also

preferable because the activity of the catalyst is extremely reduced.

The hydrogen pressure at which hydrocracking is carried out using a catalyst composed of the active metal type A and active metal type B is preferably 1 MPa or greater and 20 MPa or less, more preferably 4 MPa or greater and 16 MPa or less, more preferably 6 MPa or greater and 13 MPa or less. Although a higher hydrogen pressure facilitates the hydrogenation reaction, the cracking reaction would rather proceed slowly and thus needs to be adjusted in the proceeding thereof by increasing the reaction temperature, leading to a short working life of the catalyst. Therefore, there is generally an optimum point in economical sense.

The liquid hourly space velocity (LHSV) at which hydrocracking is carried out using a catalyst composed of the active metal A type is preferably 0.1 h^{-1} or greater and 10.0 h^{-1} or less, more preferably 0.3 h^{-1} or greater and 3.5 h^{-1} or less. Although a lower LHSV is advantageous for the reaction, a too low LHSV is not economically preferable because it requires an extremely large reactor volume, leading to an excessive capital investment in facilities.

The liquid hourly space velocity (LHSV) at which

hydrocracking is carried out using a catalyst composed of the active metal B type is preferably 0.1 h^{-1} or greater and 2 h^{-1} or less, more preferably 0.2 h^{-1} or greater and 1.7 h^{-1} or less, more preferably 0.3 h^{-1} or greater and 1.5 h^{-1} or less. Although a lower LHSV is advantageous for the reaction, a too low LHSV is not economically preferable because it requires an extremely large reactor volume, leading to an excessive capital investment in facilities.

The hydrogen/oil ratio at which hydrocracking is carried out using a catalyst composed of the active metal A type is preferably 50 NL/L or greater and 1000 NL/L or less, more preferably 70 NL/L or greater and 800 NL/L or less, more preferably 400 NL/L or greater and 1500 NL/L or less. Although a higher hydrogen/oil ratio facilitates the reaction, there is generally an optimum point in economical sense.

The hydrogen/oil ratio at which hydrocracking is carried out using a catalyst composed of the active metal B type is preferably 150 NL/L or greater and 2000 NL/L or less, more preferably 300 NL/L or greater and 1700 NL/L or less, more preferably 400 NL/L or greater and 1500 NL/L or less. Although a higher hydrogen/oil ratio facilitates the reaction, there is generally an optimum point in economical sense.

The reactor for hydrogenation may be of any structure and a single or a plurality of reaction tower may be used. Hydrogen may be additionally supplied between a plurality of reaction towers. The reactor may have a facility for removing sulfurized hydrogen and a distillation tower for fractionally distilling hydrogenated products for producing desired fractions.

The reaction mode of the hydrogenation reactor may be a fixed bed mode. Hydrogen may be supplied to the feedstock in a counter or parallel flow mode.

Alternatively, the reaction mode may be a combination of counter and parallel flow modes, with a plurality of reaction towers. The supply mode of the feedstock is generally down flow and is preferably a gas-liquid cocurrent flow mode. Hydrogen gas may be supplied as quencher into a middle portion of a reactor for the purposes of removing the reaction heat or increasing the hydrogen partial pressure.

The above-mentioned petroleum-based base oil is a hydrocarbon base oil produced by processing crude oil. Examples include straight base oils produced through an atmospheric distillation unit; vacuum base oils produced by processing straight heavy oil or residue produced through an atmospheric distillation unit, in a vacuum distillation unit; catalytically cracked or

hydrocracked base oils produced by catalytically cracking or hydrocracking vacuum heavy base oil or desulfurized fuel oil; and hydrorefined or hydrodesulfurized base oils produced by hydrorefining any of these petroleum hydrocarbons. Alternatively, other than crude oil, base oils produced by subjecting to resources referred to as unconventional petroleum resources, such as oil shale, oil sand and Orinoco tar to suitable processing to have properties equivalent to those of the foregoing base oils may be used as the base oil in the present invention.

The above-mentioned highly hydrogenated petroleum-based base oil is a kerosene or gas oil fraction produced by hydrorefining and then hydrotreating a predetermined feedstock. Examples of the feedstock include straight kerosene or gas oils produced through an atmospheric distillation unit for crude oil; vacuum kerosene or gas oils produced by processing straight heavy oil or residue produced through an atmospheric distillation unit, in a vacuum distillation unit; and hydrorefined and hydrodesulfurized kerosene or gas oils produced by hydrotreating catalytically cracked kerosene or gas oils produced by catalytically cracking desulfurized or undesulfurized vacuum kerosene or gas oils, vacuum

heavy gas oil or desulfurized fuel oil.

When the feedstock is a gas oil fraction, conditions for hydrotreating may be those determined when a hydrodesulfurizing unit is generally used for petroleum refining. Generally, hydrotreating of a gas oil fraction is carried out under conditions where the reaction temperature is from 300 to 380°C, the hydrogen pressure is from 3 to 8 MPa, the LHSV is from 0.3 to 2 h⁻¹, and the hydrogen/oil ratio is from 100 to 500 NL/L. When the feedstock is a kerosene fraction, conditions for hydrotreating may be those determined when a hydrodesulfurizing unit is generally used for petroleum refining. Generally, hydrotreating of a kerosene fraction is carried out under conditions where the reaction temperature is from 220 to 350°C, the hydrogen pressure is from 1 to 6 MPa, the LHSV is from 0.1 to 10 h⁻¹, and the hydrogen/oil ratio is from 10 to 300 NL/L, preferably conditions where the reaction temperature is from 250 to 340°C, the hydrogen pressure is from 2 to 5 MPa, the LHSV is from 1 to 10 h⁻¹, and the hydrogen/oil ratio is from 30 to 200 NL/L, more preferably under conditions where the reaction temperature is from 270 to 330°C, the hydrogen pressure is from 2 to 4 MPa, the LHSV is from 2 to 10 h⁻¹, and the hydrogen/oil ratio is from 50 to 200 NL/L.

A lower reaction temperature is advantageous for hydrogenation reaction but is not preferable for desulfurization reaction. A higher hydrogen pressure and a higher hydrogen/oil ratio facilitate desulfurization and hydrogenation reactions but there is an optimum point in economical sense. Although a lower LHSV is advantageous for the reaction, a too low LHSV is not economically preferable because it requires an extremely large reactor volume, leading to an excessive capital investment in facilities.

A catalyst used for the hydrorefining may be any of the conventional hydrodesulfurization catalysts. Preferably, the active metals of the catalyst are the Groups 6A and 8 metals of the periodic table. Examples of these metals include Co-Mo, Ni-Mo, Co-W, and Ni-W. The support may be an porous inorganic oxide containing alumina as the main component. These conditions and the catalyst are not particularly restricted as long as the characteristics of the feedstock are satisfied.

The feedstock used in the present invention is produced through the above-described hydrorefining process and has preferably a sulfur content of 5 ppm by mass or more and 10 ppm by mass or less and a boiling point of 130°C or higher and 380°C or lower. The feed stock having a sulfur content and a boiling point within

these ranges can ensure the easy achievement of the characteristics defined for the following high hydrogenation process.

The highly hydrotreated base oil is produced by hydrotreating the above-described hydrogenated kerosene or gas oil as the feedstock in the presence of a hydrogenation catalyst.

Conditions for the highly hydrogenation are those where the reaction temperature is from 170 to 320°C, the hydrogen pressure is from 2 to 10 MPa, the LHSV is from 0.1 to 2 h⁻¹, and the hydrogen/oil ratio is from 100 to 800 NL/L, preferably conditions where the reaction temperature is from 175 to 300°C, the hydrogen pressure is from 2.5 to 8 MPa, the LHSV is from 0.2 to 1.5 h⁻¹, and the hydrogen/oil ratio is from 150 to 600 NL/L, more preferably under conditions where the reaction temperature is from 180 to 280°C, the hydrogen pressure is from 3 to 7 MPa, the LHSV is from 0.3 to 1.2 h⁻¹, and the hydrogen/oil ratio is from 150 to 500 NL/L. A lower reaction temperature is advantageous for hydrogenation reaction but is not preferable for desulfurization reaction. A higher hydrogen pressure and a higher hydrogen/oil ratio facilitate desulfurization and hydrogenation reactions but there is an optimum point in economical sense. Although a

lower LHSV is advantageous for the reaction, a too low LHSV is not economically preferable because it requires an extremely large reactor volume, leading to an excessive capital investment in facilities.

A unit for hydrotreating the feedstock having been hydrorefined may be of any structure, and a single or a plurality of reactors in combination may be used. Hydrogen may be additionally introduced into the spaces between a plurality of reactors. The hydrorefining unit may be provided with a gas-liquid separation system or a hydrogen sulfide removal system.

The reaction mode of the hydrogenation reactor may be a fixed bed mode. Hydrogen may be supplied to the feedstock in a counter or parallel flow mode. Alternatively, the reaction mode may be a combination of counter and parallel flow modes, with a plurality of reaction towers. The supply mode of the feedstock is generally down flow and is preferably a gas-liquid cocurrent flow mode. Hydrogen gas may be supplied as quencher into a middle portion of a reactor for the purposes of removing the reaction heat or increasing the hydrogen partial pressure.

A catalyst used for hydrotreating comprises a hydrogenation active metal supported on a porous support. The porous support may be an inorganic oxide

such as alumina. Examples of the inorganic oxide include alumina, titania, zirconia, boria, silica, and zeolite. In the present invention, the support is preferably composed of alumina and at least one selected from titania, zirconia, boria, silica, and zeolite. There is no particular restriction on the method of producing the support. Therefore, there may be employed any method using raw materials in the form of sols or salt compounds each containing any of the elements. Alternatively, the support may be prepared by forming a complex hydroxide or oxide such as silica alumina, silica zirconia, alumina titania, silica titania, and alumina boria and then adding at any step alumina in the form of alumina gel, a hydroxide, or a suitable solution. Alumina can be contained in any ratio to the other oxides on the basis of the porous support. However, the content of alumina is preferably 90 percent by mass or less, more preferably 60 percent by mass or less, and more preferably 40 percent by mass or less, of the mass of the porous support.

Zeolite is a crystalline alumino silicate. Examples of the crystalline structure include faujasite, pentasil, and mordenite. These zeolites may be those ultra-stabilized by a specific hydrothermal treatment and/or acid treatment or those

whose alumina content is adjusted. Preferred zeolites are those of faujasite, beta and mordenite types, and particularly preferred zeolites are those of Y and beta types. The zeolites of Y type are preferably ultra-stabilized. The ultra-stabilized zeolite have a micro porous structure peculiar thereto, so-called micro pores of 20 Å or smaller and also newly formed pores in the range of 20 to 100 Å. The hydrothermal treatment may be carried out under known conditions.

The active metal of the catalyst used for hydrotreating is at least one metal selected from the Group 8 metals of the periodic table, preferably at least one metal selected from Ru, Rh, Ir, Pd, and Pt, and more preferably Pd and/or Pt. These metals may be used in combination such as Pt-Pd, Pt-Rh, Pt-Ru, Ir-Pd, Ir-Rh, Ir-Ru, Pt-Pd-Rh, Pt-Rh-Ru, Ir-Pd-Rh, and Ir-Rh-Ru. The metal sources of these metals may be inorganic salts or complex salt compounds which have been conventionally used. The method of supporting the metal may be any of methods such as immersion and ion exchange which are used for a hydrogenation catalyst. When a plurality of metals are supported, they may be supported using a mixed solution thereof at the same time. Alternatively, a plurality of metals may be supported using solutions each containing any of the

metals one after another. These metal solutions may be aqueous solutions or those produced using an organic solvent.

The metal(s) may be supported on the porous support after completion of all the steps for preparing the porous support. Alternatively, the metal(s) may be supported on the porous support in the form of a suitable oxide, complex oxide or zeolite produced at the intermediate stage of the preparation of the porous support and then may proceed to gel-preparation or be subjected to heat-concentration and kneading.

There is no particular restriction on the amount of the active metal(s) to be supported. However, the amount is from 0.1 to 10 percent by mass, preferably from 0.15 to 5 percent by mass, and more preferably from 0.2 to 3 percent by mass on the basis of the catalyst mass.

The catalyst is preferably used after it is subjected to a pre-reduction treatment under a hydrogen stream. In general, the active metal(s) are subjected to heat at 200°C or higher in accordance with the predetermined procedures, circulating gas containing hydrogen and then reduced, thereby exerting catalytic activity.

The animal- or vegetable-derived processed oils

referred above are base oils composed of hydrocarbons produced by applying chemical reaction processes applied to produce the above-described petroleum-based base oils, to oils or fats yielded or produced animal or vegetable raw materials. More specifically, the animal- or vegetable-derived processed oils are hydrocarbon-containing mixed base oils produced by contacting an animal or vegetable fat and a component derived therefrom used as a feedstock with a hydrocracking catalyst containing at least one or more metals selected from the Groups 6A and 8 metals of the periodic table and an inorganic oxide with acidic properties, under hydrogen pressure. The feedstock of the animal- or vegetable-derived processed oil is necessarily an animal or vegetable fat or a component derived therefrom. Examples of the animal or vegetable fat or the component originating therefrom used herein include natural or artificially made or produced animal or vegetable fats and animal or vegetable fat components originating therefrom. Examples of raw materials of the animal fats and animal oils include beef tallow, milk fat (butter), lard, mutton tallow, whale oil, fish oil, and liver oil. Examples of raw materials of the vegetable fats and vegetable oils include the seeds and other parts of coconut, palm tree,

olive, safflower, rape (rape blossoms), rice bran, sunflower, cotton seed, corn, soy bean, sesame, and flaxseed. Fats or oils other than those produced from these materials may also be used in the present invention. The feedstocks may be of solid or liquid but are preferably produced from vegetable fats or vegetable oils with the objective of easy handling, carbon dioxide absorptivity, and high productivity. Alternatively, waste oils resulting from the use of these animal and vegetable oils for household, industry and food preparation purposes may be used as the feedstock after the residual matters are removed from these oils.

Examples of the typical composition of the fatty acid part of the glyceride compounds contained in these feedstocks include fatty acids, so-called saturated fatty acids having no unsaturated bond in the molecules, such as butyric acid (C_3H_7COOH), caproic acid ($C_5H_{11}COOH$), caprylic acid ($C_7H_{15}COOH$), capric acid ($C_9H_{19}COOH$), lauric acid ($C_{11}H_{23}COOH$), myristic acid ($C_{13}H_{27}COOH$), palmitic acid ($C_{15}H_{31}COOH$), stearic acid ($C_{17}H_{35}COOH$), and so-called unsaturated fatty acids having one or more unsaturated bonds in the molecules, such as oleic acid ($C_{17}H_{33}COOH$), linoleic acid ($C_{17}H_{31}COOH$), linolenic acid ($C_{17}H_{29}COOH$) and ricinoleic

acid ($C_{17}H_{32}(OH)COOH$). In general, the hydrocarbon parts of these fatty acids contained in substances existing in nature are mostly of straight chain. However, the fatty acid may be any of those having a side chain structure, i.e., isomers as long as the properties defined by the present invention are satisfied. The unsaturated fatty acid may be any of those existence of which are generally recognized in nature as well as those having an unsaturated bond per molecule, the position of which is adjusted through chemical synthesis as long as the properties defined by the present invention are satisfied.

The above-described feedstocks (animal or vegetable fats and components derived therefrom) contain one or more of these fatty acids, which vary depending on the raw materials. For example, coconuts oil contains a relatively large amount of saturated fatty acids such as lauric acid and myristic acid while soy bean oil contains a large amount of unsaturated fatty acids such as oleic acid and linoleic acid.

The feedstock contains a fraction whose boiling point is preferably $250^{\circ}C$ or higher, more preferably a fraction whose boiling point is $300^{\circ}C$ or higher, and more preferably a fraction whose boiling point is $360^{\circ}C$ or higher. If the feedstock contains no fraction whose

boiling point is 230°C or higher, the yield of a liquid product would be decreased due to an increase in gas formed during the production, possibly resulting in an increase in life cycle carbon dioxide.

Alternatively, the feedstock of the animal or vegetable-derived processed oil may be a mixture of an animal or vegetable fat and a component derived therefrom, with a petroleum hydrocarbon fraction. In this case, the ratio of the petroleum hydrocarbon fraction is preferably from 10 to 99 percent by volume, more preferably from 30 to 99 percent by volume, and more preferably from 60 to 98 percent by volume, of the total volume of the feedstock. If the ratio is less than the lower limit, there may arise the necessity of facilities for disposal of by-produced water. If the ratio exceeds the upper limit, it is not preferable in view of life cycle carbon dioxide reduction.

Conditions of hydrocracking the feedstock during the hydrotreating are those desirously wherein the hydrogen pressure is from 6 to 20 MPa, the liquid hourly space velocity (LHSV) is from 0.1 to 1.5 h⁻¹, and the hydrogen/oil ratio is from 200 to 2000 NL/L, more desirously wherein the hydrogen pressure is from 8 to 17 MPa, the liquid hourly space velocity (LHSV) is from 0.2 to 1.1 h⁻¹, and the hydrogen/oil ratio is from 300

to 1800 NL/L, more desirously wherein the hydrogen pressure is from 10 to 16 MPa, the liquid hourly space velocity (LHSV) is from 0.3 to 0.9 h⁻¹, and the hydrogen/oil ratio is from 350 to 1600 NL/L. Each of the conditions is a factor exerting an influence on the reaction activity. For example, if the hydrogen pressure and hydrogen/oil ratio are less than the lower limits, the reactivity tends to reduce, and the activity tends to reduce rapidly. If the hydrogen pressure and hydrogen/oil ratio exceed the upper limits, an enormous plant investment for a compressor may be required. A lower liquid hourly space velocity tends to be more advantageous for the reactions. However, if the liquid hourly space velocity is lower than 0.1 h⁻¹, an enormous plant investment for construction of a reactor with an extremely large volume may be required. If the liquid hourly space velocity exceeds 1.5 h⁻¹, the reaction tends to proceed insufficiently.

The gas oil composition of the present invention necessarily contains mainly an FT synthetic base oil and has the characteristics described below.

The gas oil composition of the present invention comprises a gas oil composition selected from the group consisting of the following gas oil compositions (A) to (C) and additives added in accordance with the

following Steps 1 and 2:

[I] gas oil compositions (A) comprising an FT synthetic base oil in an amount of 60 percent by volume or more on the basis of the total amount of the gas oil composition, with a sulfur content of 5 ppm by mass or less, an aromatic content of 10 percent by volume or less, an oxygen content of 100 ppm or less, a density of 760 kg/m^3 or greater and 840 kg/m^3 or less, a 90% distillation temperature of 280°C or higher and 330°C or lower and an end point of 360°C or lower in distillation characteristics, an insoluble content after an oxidation stability test of 0.5 mg/100 mL or less, an HFRR wear scar diameter (WS1.4) of $400 \text{ }\mu\text{m}$ or smaller, a cloud point of -15°C or lower, a cold filter plugging point of -25°C or lower, a pour point of -32.5°C or lower, a total content of normal paraffins having 20 to 30 carbon atoms of less than 2 percent by mass, a value determined by dividing the total content of normal paraffins having 20 to 30 carbon atoms by the total content of hydrocarbons having 20 to 30 carbon atoms other than the normal paraffins of 0.2 or greater and 0.6 or less, and a relation in the content of each of normal paraffins (C_nP) having 15 to 20 carbon atoms defined by $\text{C}_{20}\text{P} < \text{C}_{19}\text{P} < \text{C}_{18}\text{P} < \text{C}_{17}\text{P} < \text{C}_{16}\text{P} < \text{C}_{15}\text{P}$;

[II] gas oil compositions (B) comprising an FT

synthetic base oil in an amount of 60 percent by volume or more on the basis of the total amount of the gas oil composition, with a sulfur content of 5 ppm by mass or less, an aromatic content of 10 percent by volume or less, an oxygen content of 100 ppm or less, a density of 760 kg/m³ or greater and 840 kg/m³ or less, a 90% distillation temperature of 280°C or higher and 350°C or lower and an end point of 360°C or lower in distillation characteristics, an insoluble content after an oxidation stability test of 0.5 mg/100 mL or less, an HFRR wear scar diameter (WSI.4) of 400 µm or smaller, a cloud point of -5°C or lower, a cold filter plugging point of -20°C or lower, a pour point of -25°C or lower, a total content of normal paraffins having 20 to 30 carbon atoms of 2 percent by mass or more and less than 4 percent by mass, a value determined by dividing the total content of normal paraffins having 20 to 30 carbon atoms by the total content of hydrocarbons having 20 to 30 carbon atoms other than the normal paraffins of 0.2 or greater and 0.6 or less, and a relation in the content of each of normal paraffins (CnP) having 20 to 25 carbon atoms defined by C20P>C21P>C22P>C23P>C24P>C25P; and

[III] gas oil compositions (C) comprising an FT synthetic base oil in an amount of 60 percent by volume

or more on the basis of the total amount of the gas oil composition, with a sulfur content of 5 ppm by mass or less, an aromatic content of 10 percent by volume or less, an oxygen content of 100 ppm or less, a density of 760 kg/m^3 or greater and 840 kg/m^3 or less, a 90% distillation temperature of 280°C or higher and 350°C or lower and an end point of 360°C or lower in distillation characteristics, an insoluble content after an oxidation stability test of 0.5 mg/100 mL or less, an HFRR wear scar diameter (WS1.4) of $400 \text{ }\mu\text{m}$ or smaller, a cloud point of -3°C or lower, a cold filter plugging point of -10°C or lower, a pour point of -12.5°C or lower, a total content of normal paraffins having 20 to 30 carbon atoms of 4 percent by mass or more and less than 6 percent by mass, a value determined by dividing the total content of normal paraffins having 20 to 30 carbon atoms by the total content of hydrocarbons having 20 to 30 carbon atoms other than the normal paraffins of 0.2 or greater and 0.6 or less, and relations in the content of each of normal paraffins (C_nP) having 20 to 25 carbon atoms defined by $\text{C}_{20}\text{P} > \text{C}_{21}\text{P} > \text{C}_{22}\text{P} > \text{C}_{23}\text{P} > \text{C}_{24}\text{P} > \text{C}_{25}\text{P}$ and $(\text{C}_{24}\text{P} - \text{C}_{25}\text{P}) / \text{C}_{24}\text{P} > (\text{C}_{22}\text{P} - \text{C}_{23}\text{P}) / \text{C}_{22}\text{P} > (\text{C}_{20}\text{P} - \text{C}_{21}\text{P}) / \text{C}_{20}\text{P}$; (Step 1) a lubricity improver comprising a fatty acid and/or a fatty acid ester is admixed in an amount of

20 mg/L or more and 300 mg/L or less in terms of the active component with the gas oil composition by line-blending, forced-stirring or leaving to stand for a sufficient time; and
(Step 2) a cold flow improver comprising an ethylene vinyl acetate copolymer and/or a compound with a surface active effect is admixed in an amount of 20 mg/L or more and 1000 mg/L or less in terms of the active component with the gas oil composition by line-blending, forced-stirring or leaving to stand for a sufficient time.

Alternatively, the gas oil composition of the present invention is preferably admixed with 200 mg/L or more and 500 mg/L or less of a detergent comprising a polyether amine compound, a polybutenyl amine compound, an alkenyl succiniamide compound, or an alkenyl succiniimide compound by line-blending, forced-stirring or leaving to stand for a sufficient time, in a step added between Steps 1 and 2. Preferably, the lubricity improver, detergent and cold flow improver each contain a solvent containing no chemical substance with a melting point of 10°C or higher. Preferably, the gas oil composition has a peroxide number after an accelerated oxidation test of 50 ppm

by mass or less, a kinematic viscosity at 30°C of 2.5 mm²/s or greater and 5.0 mm²/s or less, a cetane index of 45 or greater and a water content of 100 ppm by volume or less.

The sulfur content of the gas oil composition of the present invention is necessarily 5 ppm by mass or less, preferably 3 ppm by mass or less, more preferably 1 ppm by mass or less, with the objective of reducing poisonous substances exhausted from an engine and improving exhaust-gas post-processing system performances. The sulfur content used herein denotes the mass content of the sulfur components on the basis of the total mass of a gas oil composition measured in accordance with JIS K 2541 "Crude oil and petroleum products-Determination of sulfur content".

The aromatic content of the gas oil composition of the present invention is necessarily 10 percent by volume or less, preferably 8 percent by volume or less, more preferably 5 percent by volume or less, more preferably 3 percent by volume or less, most preferably 1 percent by volume or less. When the composition has an aromatic content of 10 percent by volume or less, it can suppress the formation of PM, exhibit environment friendly properties and achieve easily and

certainly characteristics defined in the present invention. The aromatic content used herein denotes the volume percentage (volume %) of the aromatic component content measured in accordance with JPI-5S-49-97 "Petroleum Products-Determination of Hydrocarbon Types-High Performance Liquid Chromatography" prescribed in JPI Standard and Manuals Testing Method for Petroleum Products published by Japan Petroleum Inst.

The oxygen content of the gas oil composition of the present invention is necessarily 100 ppm by mass or less, preferably 80 ppm by mass or less, more preferably 60 ppm by mass or less, with the objective of improving oxidation stability. The oxygen content can be measured with a conventional elemental analysis device. For example, the oxygen content is measured by converting a sample to CO or further to CO₂ on platinum carbon and measuring the amount thereof using a thermal conductivity detector.

The density at 15°C of the gas oil composition of the present invention is preferably 760 kg/m³ or higher, more preferably 765 kg/cm³ or higher, and more preferably 770 kg/cm³ or higher with the objective of maintaining the calorific value. The density is preferably 840 kg/cm³ or lower, more preferably 835

kg/cm³ or lower, and more preferably 830 kg/cm³ or lower with the objective of reducing NOx and PM emission. The density used herein denotes the density measured in accordance with JIS K 2249 "Crude petroleum and petroleum products-Determination of density and petroleum measurement tables based on a reference temperature (15°C)".

With regard to distillation characteristics, the 90% distillation temperature of the gas oil composition (A) is necessarily 330°C or lower. If the 90% distillation temperature is in excess of 330°C, emission of PM or fine particles would be likely increased. Therefore, the 90% distillation temperature is preferably 327°C or lower, more preferably 325°C or lower. If the 90% distillation temperature is too low, it would induce deterioration of fuel consumption or reduction of engine output. Therefore, the lower limit 90% distillation temperature is necessarily 280°C or higher, preferably 285°C or higher, more preferably 290°C or higher. For the gas oil compositions (B) and (C), the 90% distillation temperature is necessarily 350°C or lower. If the 90% distillation temperature is in excess of 350°C, emission of PM or fine particles would be likely increased. Therefore, the 90% distillation

temperature is preferably 345°C or lower, more preferably 340°C or lower, more preferably 335°C or lower. If the 90% distillation temperature is too low, it would induce deterioration of fuel consumption or reduction of engine output. Therefore, the lower limit 90% distillation temperature is necessarily 280°C or higher, preferably 285°C or higher, more preferably 290°C or higher.

The initial boiling point of the gas oil composition of the present invention is necessarily 140°C or higher. If the initial boiling point is lower than 140°C, the engine output and high-temperature startability would tend to be extremely reduced and deteriorated. Therefore, the initial boiling point is preferably 145°C or higher, more preferably 150°C or higher. The end point is preferably 360°C or lower. If the end point is in excess of 360°C, emission of PM or fine particles would be likely increased. Therefore, the end point is preferably 368°C or lower, more preferably 366°C or lower.

There is no particular restriction on the 10% distillation temperature. However, the lower limit is preferably 160°C or higher, more preferably 170°C or higher, more preferably 180°C or higher with the objective of suppressing reduction of engine output and

deterioration of fuel consumption. The upper limit is preferably 250°C or lower, more preferably 245°C or lower, more preferably 230°C or lower with the objective of suppressing deterioration of exhaust gas properties. The initial boiling point, 10% distillation temperature, 90% distillation temperature and end point used herein denote the values measured in accordance with JIS K 2254 "Petroleum products-Determination of distillation characteristics".

The total insoluble content of the gas oil composition of the present invention after an oxidation stability test is necessarily 1.0 mg/100 mL or less, more preferably 0.8 mg/100 mL or less, more preferably 0.5 mg/100 mL or less in view of storage stability. The oxidation stability test used herein is carried out at a temperature of 95°C under oxygen bubbling for 16 hours in accordance with ASTM D2274-94. The total insoluble content after an oxidation stability test referred herein denotes the value measured in accordance with the foregoing oxidation stability test.

The gas oil composition of the present invention have necessarily such a lubricity that the HFRR wear scar diameter (WS1.4) is 400 μm or smaller. If the lubricity is too low, the composition would cause a

diesel engine equipped with a distribution type injection pump in particular to be increased in driving torque and in wear on each part of the pump while the engine is driven, possibly leading not only to degradation of the exhaust gas properties but also to the breakdown of the engine itself. Also in an electronically controlled fuel injection pump enabling a high pressure injection, wear on the sliding parts would likely occur. Therefore, with respect to the lubricity, the HFRR wear scar diameter (WS1.4) of the gas oil composition is necessarily 400 μm or smaller, preferably 380 μm or smaller, more preferably 360 μm or smaller. The lubricity, i.e., HFRR wear scar diameter (WS1.4) used herein denotes the lubricity measured in accordance with JPI-5S-50-98 "Gas oil -Testing Method for Lubricity" prescribed in JPI Standard and Manuals Testing Method for Petroleum Products published by Japan Petroleum Inst.

With regard to the cloud point of the gas oil composition of the present invention, the cloud point of the gas oil composition (A) is necessarily -15°C or lower, more preferably -16°C or lower, more preferably -17°C or lower with the objective of securing low-temperature startability and drivability and with the objective of maintaining the injection performance

of an electronically controlled fuel injection pump. The cloud point of the gas oil composition (B) is necessarily -5°C or lower, preferably -6°C or lower, more preferably -8°C or lower with the objective of securing low-temperature startability and drivability and with the objective of maintaining the injection performance of an electronically controlled fuel injection pump. The cloud point of the gas oil composition (C) is necessarily -3°C or lower, preferably -4°C or lower, more preferably -5°C or lower with the objective of securing low-temperature startability and drivability and with the objective of maintaining the injection performance of an electronically controlled fuel injection pump.

The cloud point used herein denotes the pour point measured in accordance with JIS K 2269 "Testing Method for Pour Point and Cloud Point of Crude Oil and Petroleum Products".

With regard to the cold filter plugging point of the gas oil composition of the present invention, the cold filter plugging point of the gas oil composition (A) is necessarily -25°C or lower. Further, the cold filter plugging point is preferably -26°C or lower, more preferably -27°C or lower with the objective of preventing plugging of the pre-filter of a diesel

powered automobile and maintaining the injection performance of an electronically controlled fuel injection pump. The cold filter plugging point of the gas oil composition (B) is necessarily -20°C or lower. Further, the cold filter plugging point is preferably -21°C or lower, more preferably -22°C or lower with the objective of preventing plugging of the pre-filter of a diesel powered automobile and maintaining the injection performance of an electronically controlled fuel injection pump. The cold filter plugging point of the gas oil composition (C) is necessarily -10°C or lower. Further, the cold filter plugging point is preferably -11°C or lower, more preferably -12°C or lower with the objective of preventing plugging of the pre-filter of a diesel powered automobile and maintaining the injection performance of an electronically controlled fuel injection pump.

The cold filter plugging point used herein denotes the cold filter plugging point measured in accordance with JIS K 2288 "Gas oil-Determination of cold filter plugging point".

With regard to the pour point of the gas oil composition of the present invention, the pour point of the gas oil composition (A) is necessarily -32.5°C or lower. Further, the pour point is preferably -35°C

or lower with the objective of securing low-temperature startability or drivability and maintaining the injection performance of an electronically controlled fuel injection pump. The pour point of the gas oil composition (B) is necessarily -25°C or lower. Further, the pour point is preferably -22.5°C or lower with the objective of securing low-temperature startability or drivability and maintaining the injection performance of an electronically controlled fuel injection pump. The pour point of the gas oil composition (C) is necessarily -12.5°C or lower. Further, the pour point is preferably -15°C or lower with the objective of securing low-temperature startability or drivability and maintaining the injection performance of an electronically controlled fuel injection pump.

The pour point used herein denotes the pour point measured in accordance with JIS K 2269 "Testing Method for Pour Point and Cloud Point of Crude Oil and Petroleum Products".

In the present invention, the total content of normal paraffins having 20 to 30 carbon atoms in the gas oil composition (A) is necessarily less than 2 percent by mass of the total mass of the gas oil composition. If the total content of these heavy

normal paraffins is 2 percent by mass or more, deposition of wax would be induced at low temperatures. Therefore, the total content is preferably 1.8 percent by mass or less, more preferably 1.6 percent by mass or less. Further, the value determined by dividing the total content of normal paraffins having 20 to 30 carbon atoms by the total content of hydrocarbons having 20 to 30 carbon atoms other than the normal paraffins is necessarily 0.2 or greater and 0.6 or less, preferably 0.22 or greater and 0.57 or less, more preferably 0.25 or greater and 0.55 or less in order to improve the additive solubility of the gas oil base oil. If the value is less than 0.2, the additive solubility would be extremely reduced. If the value is greater than 0.6, the cold flowability would be impaired. Further, the content of each of normal paraffins (C_nP) within the carbon number (n) range from 15 to 20 necessarily satisfies the relation defined by $C_{20}P < C_{19}P < C_{18}P < C_{17}P < C_{16}P < C_{15}P$. As long as this relation is satisfied, the resulting composition will have a stable wax deposition rate correspondingly to temperature changes such as the out door temperature at which the composition is cooled and be able to ensure the cold flow improver to exhibit its properties stably due to the effects of the normal paraffins present in

the aforesaid content.

The total content of the straight-chain saturated hydrocarbons having 20 to 30 carbon atoms and content of the straight-chain saturated hydrocarbons having 15 to 20 carbon atoms are the values measured using GC-FID wherein the column is a capillary column formed of methyl silicone (ULTRA ALLOY-1), the carrier gas is helium and the detector is a flame ionization detector (FID), under conditions wherein the column length is 30 m, the carrier gas flow rate is 1.0 mL/min, the ratio of division is 1:79, the sample injection temperature is 360°C, the column is heated up from 140°C to 355°C (8°C/min), and the detector temperature is 360°C.

For the gas oil composition (B), the total content of normal paraffins having 20 to 30 carbon atoms thereof is necessarily 2 percent by mass or more and less than 4 percent by mass of the total mass of the gas oil composition. If the total content of these heavy normal paraffins is 4 percent by mass or more, deposition of wax would be induced at low temperatures. If the total content is less than 2 percent by mass, the amount of the heavy normal paraffins would be reduced, resulting in a reduction in the performance efficiency of the cold flow improver, which utilizes

the heavy paraffins as a growth core. Further, the value determined by dividing the total content of normal paraffins having 20 to 30 carbon atoms by the total content of hydrocarbons having 20 to 30 carbon atoms other than the normal paraffins is necessarily 0.2 or greater and 0.6 or less, preferably 0.22 or greater and 0.57 or less, more preferably 0.25 or greater and 0.55 or less in order to improve the additives solubility of the gas oil base oil. If the value is less than 0.2, the additive solubility would be extremely reduced. If the value is greater than 0.6, the cold flowability would be impaired. Further, the content of each of normal paraffins (C_nP) within the carbon number (n) range from 20 to 25 necessarily satisfies the relation defined by C₂₀P>C₂₁P>C₂₂P>C₂₃P>C₂₄P>C₂₅P. As long as this relation is satisfied, the resulting composition will have a stable wax deposition rate correspondingly to temperature changes such as the out door temperature at which the composition is cooled and be able to ensure the cold flow improver to exhibit its properties stably due to the effects of the normal paraffins present in the aforesaid content.

The total content of the straight-chain hydrocarbons having 20 to 30 carbon atoms and content

of the straight-chain saturated hydrocarbons having 20 to 25 carbon atoms are the values measured using GC-FID wherein the column is a capillary column formed of methyl silicone (ULTRA ALLOY-1), the carrier gas is helium and the detector is a flame ionization detector (FID), under conditions wherein the column length is 30 m, the carrier gas flow rate is 1.0 mL/min, the ratio of division is 1:79, the sample injection temperature is 360°C, the column is heated up from 140°C to 355°C (8°C/min), and the detector temperature is 360°C.

For the gas oil composition (C), the total content of normal paraffins having 20 to 30 carbon atoms thereof is necessarily 4 percent by mass or more and less than 6 percent by mass of the total mass of the gas oil composition. If the total content of these heavy normal paraffins is 6 percent by mass or more, deposition of wax would be induced at low temperatures. If the total content is less than 4 percent by mass, the amount of the heavy normal paraffins would be reduced, resulting in a reduction in the performance efficiency of the cold flow improver, which utilizes the heavy paraffins as a growth core. Further, the value determined by dividing the total content of normal paraffins having 20 to 30 carbon atoms by the

total content of hydrocarbons having 20 to 30 carbon atoms other than the normal paraffins is necessarily 0.2 or greater and 0.6 or less, preferably 0.22 or greater and 0.57 or less, more preferably 0.25 or greater and 0.55 or less in order to improve the additive solubility of the gas oil base oil. If the value is less than 0.2, the additive solubility would be extremely reduced. If the value is greater than 0.6, the cold flowability would be impaired. Further, the content of each of normal paraffins (C_nP) within the carbon number (n) range from 20 to 25 necessarily satisfies the relation defined by C₂₀P>C₂₁P>C₂₂P>C₂₃P>C₂₄P>C₂₅P and also the relation defined by

$$(C_{24}P - C_{25}P) / C_{24}P > (C_{22}P - C_{23}P) / C_{22}P > (C_{20}P - C_{21}P) / C_{20}P.$$

Herein, " $(C_{24}P - C_{25}P) / C_{24}P > (C_{22}P - C_{23}P)$ " is the value determined by dividing the content of normal paraffins having 24 and 25 carbon atoms by the content of a normal paraffin having 24 carbon atoms. Also, " $(C_{22}P - C_{23}P) / C_{22}P > (C_{20}P - C_{21}P) / C_{20}P$ " is calculated in the same manner. These relations were obtained as the results of extensive research and study by the inventor of the present invention. What is meant by the relations is to express the deposition rate of the heavy normal paraffins with respect to temperature in a

simple manner. As long as these relations are satisfied, the resulting composition will have a stable wax deposition rate correspondingly to temperature changes such as the out door temperature at which the composition is cooled and be able to ensure the cold flow improver to exhibit its properties stably, due to the effects of the normal paraffins present in the aforesaid content.

The total content of the straight-chain saturated hydrocarbons having 20 to 30 carbon atoms and content of the straight-chain saturated hydrocarbon having 20 to 25 carbon atoms are the values measured using GC-FID wherein the column is a capillary column formed of methyl silicone (ULTRA ALLOY-1), the carrier gas is helium and the detector is a flame ionization detector (FID), under conditions wherein the column length is 30 m, the carrier gas flow rate is 1.0 mL/min, the ratio of division is 1:79, the sample injection temperature is 360°C, the column is heated up from 140°C to 355°C (8°C/min), and the detector temperature is 360°C.

The peroxide number of the gas oil composition of the present invention after an accelerated oxidation test (oxidation stability test) is preferably 50 ppm by mass or less, more preferably 40 ppm by mass or less,

30 ppm by mass or less in view of storage stability and compatibility to parts. The peroxide number after an accelerated oxidation test used herein denotes the value measured in accordance with JPI-5S-46-96 prescribed in JPI Standard after an accelerated oxidation test is carried out at a temperature of 95°C under oxygen bubbling for 16 hours in accordance with ASTM D2274-94. If necessary, the gas oil compositions of the present invention may be blended with additives such as anti-oxidants or metal deactivators in order to reduce the peroxide number.

The kinematic viscosity at 30°C of the gas oil composition of the present invention is preferably 2.5 mm²/s or higher, more preferably 2.55 mm²/s or higher, more preferably 2.6 mm²/s or higher. If the kinematic viscosity is lower than 2.5 mm²/s, it would be difficult to control the fuel injection timing at the fuel injection pump side, and lubricity at each part of the fuel injection pump installed in an engine would be reduced. There is no particular restriction on the upper limit kinematic viscosity at 30°C. However, the kinematic viscosity is preferably 5.0 mm²/s or lower, more preferably 4.8 mm²/s or lower, more preferably 4.5 mm²/s or lower with the objective of suppressing increase of the NO_x and PM concentrations in the exhaust

gas, caused by destabilization of the fuel injection system due to an increase in resistance therein. The kinematic viscosity used herein denotes the value measured in accordance with JIS K 2283 "Crude petroleum and petroleum products-Determination of kinematic viscosity and calculation of viscosity index from kinematic viscosity".

The cetane index of the gas oil composition of the present invention is preferably 45 or greater. If the cetane index is lower than 45, the concentrations of PM, aldehydes, and NO_x in exhaust gas would likely be increased. For the same reason, the cetane index is more preferably 47 or greater, more preferably 50 or greater. There is no particular restriction on the upper limit of the cetane index. However, if the cetane index is greater than 80, discharge of soot would likely be increased during the acceleration of a vehicle. Therefore, the cetane index is preferably 78 or lower, more preferably 75 or lower, more preferably 73 or lower. The cetane index used herein denotes the value calculated in accordance with "8.4 cetane index calculation method using variables equation" prescribed in JIS K 2280 "Petroleum products-Fuels-Determination of octane number, cetane number and calculation of cetane index". The cetane

index defined by the JIS standards is generally applied to gas oil containing no cetane number improver. However, in the present invention, "8.4 cetane index calculation method using variables equation" is applied to a gas oil containing a cetane number improver, and the value obtained thereby is also defined as cetane index.

There is no particular restriction on the cetane number of the gas oil compositions of the present invention as long as the above-described characteristics are satisfactorily obtained. However, the cetane number is preferably 45 or greater, more preferably 47 or greater, more preferably 50 or greater with the objective of inhibiting knocking during diesel combustion and reducing the discharge of NO_x, PM and aldehydes in the exhaust gas. With the objective of reducing black smoke in the exhaust gas, the cetane number is preferably 80 or lower, more preferably 78 or lower, more preferably 75 or lower. The cetane number used herein denotes the cetane number measured in accordance with "7. Cetane number test method" prescribed in JIS K 2280 "Petroleum products-Fuels-Determination of octane number, cetane number and calculation of cetane index".

The water content of the gas oil composition of

the present invention is preferably 100 ppm by volume, more preferably 50 ppm by volume, more preferably 20 ppm by volume with the objective of preventing the compositions from freezing and the engine interior from corroding. The water content used herein denotes the value measured in accordance with JIS K 2275 "Crude oil and petroleum products-Determination of water content-Potentiometric Karl Fischer titration method".

The flash point of the gas oil composition of the present invention is preferably 45°C or higher. A flash point of lower than 45°C is not preferable in view of safety. Therefore, the flash point is preferably 47°C or higher, more preferably 50°C or higher. The flash point used herein denotes the value measured in accordance with JIS K 2265 "Crude oil and petroleum products-Determination of flash point".

There is no particular restriction on the carbon residue of the 10% distillation residue of the gas oil composition of the present invention. However, the carbon residue of the 10% distillation residue is preferably 0.1 percent by mass or less, more preferably 0.08 percent by mass or less, more preferably 0.05 percent by mass or less with the objective of reducing fine particles and PM, maintaining the performances of the exhaust-gas post-processing system installed in an

engine and preventing sludge from plugging a filter. The carbon residue of the 10% distillation residue used herein denotes that measured in accordance with JIS K 2270 "Crude petroleum and petroleum products-Determination of carbon residue".

In the present invention, it is necessary that the gas oil composition is first admixed with a lubricity improver by line-blending, forced-stirring or leaving to stand for a sufficient time (Step 1) and then admixed with a cold flow improver by line-blending, forced-stirring or leaving to stand for a sufficient time (Step 2). Alternatively, depending on properties required for fuel, between Steps 1 and 2 may be provided a step wherein a detergent is admixed with the gas oil composition by line-blending, forced-stirring or leaving to stand for a sufficient time. Further, according to the situations, other additives such as cetane number improvers may be blended in a suitable amount.

The line-blending referred to as a method of mixing the gas oil composition with additives denotes a method wherein the additives are added to the gas oil composition on the pathway of transfer thereof under pressure between, for example, a storage tank and a storage tank, a production unit and a production unit

or a production unit and a storage tank to be diffused and mixed until the composition passes from the upstream to the downstream. The forced-stirring denotes a method wherein while the gas oil composition is present in a storage tank or a production unit, the additives are added thereto and forcedly diffused and mixed by forced circulation with a pump and stirring with a stirrer. The leaving to stand denotes a method wherein the gas oil composition to which the additives are added by any of various methods or in a storage tank or a production unit is left to stand there for a sufficient period to be diffused and mixed through natural diffusion and natural convection. In any of the mixing methods, the gas oil may be heated so as to improve the mixing efficiency.

With regard to Steps 1 and 2, there is no particular restriction thereon as long as the gas oil composition of the present invention can be prepared by complying with the order of adding the additives and the method of mixing the gas oil composition and the additives. Therefore, there may be used any adding method used for producing a gas oil composition in a refinery. With regard to a method of adding a cold flow improver, a method has been used frequently wherein it is added to a gas oil to be produced after diluted with

a solvent, kerosene or gas oil or wherein it is added after heated at a temperature which is 10°C higher than the environment temperature.

Preferably, the additives used in the present invention contain no solvent containing a chemical substance the melting point of which is 10°C or higher. If a solvent with a melting point of 10°C or higher is used, the solvent would deposit earlier than the wax of the gas oil, resulting in deterioration of the low-temperature properties thereof. Examples of solvents with a melting point of 10°C or higher include saturated alcohols wherein hydroxyl groups bond to a straight-chain alkyl group having 11 or more carbon atoms and the terminal groups (for example, dodecyl alcohol) and compounds having a phenol group. With the objective of reducing load to the environment, it is preferable not to use so-called endocrine disrupter or substances, the use of which are prohibited from the view of the environment protection, in these additives or solvents therefore.

It is necessary to add a lubricity improver to the gas oil composition of the present invention. With the objective of preventing a fuel injection pump from wearing, the amount of the lubricity improver is necessarily 20 mg/L or more and 300 mg/L or less,

preferably 50 mg/L or more and 200 mg/L or less, in terms of the concentration of the active component. When the lubricity improver is blended in an amount within these ranges, the lubricity improver can effectively exhibit its efficacy. For example, in a diesel engine equipped with a distribution type injection pump, the lubricity improver can suppress the driving torque from increasing and can reduce wear on each part of the pump while the engine is driven.

The lubricity improvers must be those of type containing a compound with a polar group, comprising a fatty acid and/or a fatty acid ester. There is no particular restriction on the specific name of the compound. The lubricity improver may, therefore, be any one or more type selected from carboxylic acid-, ester-, alcohol- and phenol-based lubricity improvers. Among these lubricity improvers, preferred are carboxylic acid- and ester-based lubricity improvers. The carboxylic acid-based lubricity improver may be linoleic acid, oleic acid, salicylic acid, palmitic acid, myristic acid or hexadecenoic acid or a mixture of two or more of these carboxylic acids. Examples of the ester-based lubricity improver include carboxylic acid esters of glycerin. The carboxylic acid forming the carboxylic acid ester may be of one or more types.

Specific examples of the carboxylic acid include linoleic acid, oleic acid, salicylic acid, palmitic acid, myristic acid or hexadecenoic acid. The average molecular weight of the active component of the lubricity improver is preferably 200 or greater and 1000 or less in order to enhance the solubility to the gas oil composition.

To the gas oil composition of the present invention must be added a cold flow improver through a predetermined step with the objective of preventing the filter of a diesel powered automobile from plugging. The amount of the cold flow improver is necessarily 20 mg/L or more and 1000 mg/L or less, preferably 300 mg/L or more and 800 mg/L or less in terms of the active component concentration.

The cold flow improver must be an ethylene-vinyl acetate copolymer and/or a compound with a surface active effect. Examples of the cold flow improver having a surface active effect include one or more types selected from copolymers of ethylene and methyl methacrylate, copolymers of ethylene and α -olefin, chlorinated methylene-vinyl acetate copolymers, alkyl ester copolymers of unsaturated carboxylic acids, esters synthesized from nitrogen-containing compounds having a hydroxyl group and saturated fatty acids and

salts of the esters, esters and amide derivatives synthesized from polyhydric alcohols and saturated fatty acids, esters synthesized from polyoxyalkylene glycol and saturated fatty acid, esters synthesized from alkyleneoxide adducts of polyhydric alcohols or partial esters thereof and saturated fatty acids, chlorinated paraffin/naphthalene condensates, alkenyl succinamides, and amine salts of sulfobenzoic acids.

Other than the above-exemplified cold flow improvers, the gas oil composition of the present invention may contain any one or more type selected from alkenyl succinamides; linear compounds such as dibehenic acid esters of polyethylene glycols; polar nitrogen compounds composed of reaction products of acids such as phthalic acid, ethylenediaminetetraacetic acid and nitriloacetic acid or acid anhydride thereof and hydrocarbyl-substituted amines; and comb polymers composed of alkyl fumarates- or alkyl itaconates-unsaturated ester copolymers.

Since commercially available products referred to as cold flow improvers are often in the form in which the active components contributing to low-temperature fluidity (active components) are diluted with a suitable solvent. Therefore, the above amount of the

cold flow improvers denotes the amount of the active components (active component concentration) when such commercially available products are added to the gas oil composition of the present invention.

To the gas oil composition of the present invention may be added a detergent if necessary. However, it is necessary that the detergent is added after addition of the lubricity improver and before addition of the cold flow improver, or simultaneously with addition of the lubricity improver. There is no particular restriction on the components of the detergent. Examples of the detergents include ashless dispersants, for example, polyether amine compounds which are reactions products of butyleneoxide and amine; polybutenyl amine compounds which are reaction products of isobutylene copolymers and amine; imide compounds; alkenyl succinimides such as polybutenyl succinimide synthesized from polybutenyl succinic anhydride and ethylene polyamines; succinic acid esters such as polybutenyl succinic acid ester synthesized from polyhydric alcohols such as pentaerythritol and polybutenyl succinic anhydride; copolymerized polymers such as copolymers of dialkylaminoethyl methacrylates, polyethylene glycol methacrylates, or vinylpyrrolidone and

alkylmethacrylates; and reaction products of carboxylic acids and amines. Among these, preferred are alkenyl succinimides and reaction products of carboxylic acids and amines. These detergents may be used alone or in combination. When an alkenyl succinimide is used, an alkenyl succinimide having a molecular weight of 1000 to 3000 may be used alone, or an alkenyl succinimide having a molecular weight of 700 to 2000 and an alkenyl succinimide having a molecular weight of 10000 to 20000 may be used in combination. Carboxylic acids constituting reaction products of carboxylic acids and amines may be of one or more types. Specific examples of the carboxylic acids include fatty acids having 12 to 24 carbon atoms and aromatic carboxylic acids having 7 to 24 carbon atoms. Examples of fatty acids having 12 to 24 carbon atoms include, but not limited thereto, linoleic acid, oleic acid, palmitic acid, and myristic acid. Examples of aromatic carboxylic acids having 7 to 24 carbon atoms include, but not limited thereto, benzoic acid and salicylic acid. Amines constituting reaction products of carboxylic acids and amines may be of one or more types. Typical examples of amines used herein include, but not limited thereto, oleic amines. Various amines may also be used.

There is no particular restriction on the amount of the detergent to be blended. However, the amount is preferably 20 mg/L or more, more preferably 50 mg/L or more, and more preferably 100 mg/L or more, on the basis of the total mass of the composition, because the detergent can perform its effect to suppress a fuel injection nozzle from plugging. The effect may not be obtained if the amount is less than 20 mg/L. On the other hand, if the detergent is blended in a too much amount, its effect as balanced with the amount is not obtained. Therefore, the amount of the detergent is preferably 500 mg/L or less, more preferably 300 mg/L or less, more preferably 200 mg/L or less because the detergent may increase the amounts of NO_x, PM and aldehydes in the exhaust gas from a diesel engine. Commercial available detergents are generally available in a state wherein the active component contributing to detergency is diluted with a suitable solvent. In the case where such products are blended with the gas oil compositions of the present invention, the content of the active component is preferably within the above-described range.

If necessary, the gas oil compositions of the present invention may be blended with a cetane number improver in a suitable amount to enhance the cetane

number of the composition.

The cetane number improver may be any of various compounds known as cetane number improvers for gas oil. Examples of such cetane number improvers include nitrate esters and organic peroxides. These cetane number improvers may be used alone or in combination. Preferred for use in the present invention are nitrate esters. Examples of the nitrate esters include various nitrates such as 2-chloroethyl nitrate, 2-ethoxyethyl nitrate, isopropyl nitrate, butyl nitrate, primary amyl nitrate, secondary amyl nitrate, isoamyl nitrate, primary hexyl nitrate, secondary hexyl nitrate, n-heptyl nitrate, n-octyl nitrate, 2-ethylhexyl nitrate, cyclohexyl nitrate, and ethylene glycol dinitrate. Particularly preferred are alkyl nitrates having 6 to 8 carbon atoms.

The content of the cetane number improver is preferably 500 mg/L or more, more preferably 600 mg/L or more, more preferably 700 mg/L or more, more preferably 800 mg/L or more, most preferably 900 mg/L or more. If the content of the cetane number improver is less than 500 mg/L, the cetane number improving effect may not be attained sufficiently, leading to a tendency that PM, aldehydes, and NO_x in the exhaust gas from a diesel engine are not reduced sufficiently.

There is no particular restriction on the upper limit content of the cetane number improver. However, the upper limit is preferably 1400 mg/L or less, more preferably 1250 mg/L or less, more preferably 1100 mg/L or less, and most preferably 1000 mg/L or less, on the basis of the total mass of the gas oil composition.

The cetane number improver may be any of those synthesized in accordance with conventional methods or commercially available products. Such products in the name of cetane number improver are available in a state wherein the active component contributing to an improvement in cetane number (i.e., cetane number improver itself) is diluted with a suitable solvent. In the case where the gas oil composition of the present invention is prepared using any of such commercially available products, the content of the effective component is preferably within the above-described range.

In order to further enhance the properties of the gas oil compositions of the present invention, other known fuel oil additives (hereinafter referred to as "other additives" for convenience) may be used alone or in combination. Examples of the other additives include phenolic- and aminic anti-oxidants; metal deactivators such as salicyliden derivatives;

anti-corrosion agents such as aliphatic amines and alkenyl succinic acid esters; anti-static additives such as anionic, cationic, and amphoteric surface active agents; coloring agents such as azo dye; silicone-based defoaming agents and anti-icing agents such as 2-methoxyethanol, isopropyl alcohol and polyglycol ethers.

The amounts of the other additives may be arbitrarily selected. However, the amount of each of the other additives is preferably 0.5 percent by mass or less, more preferably 0.2 percent by mass or less, on the basis of the total mass of the composition.

There is no particular restriction on the other specification of a diesel engine where the gas oil composition of the present invention is used, the applications thereof, the environment where the gas oil composition is used.

As described above, according to the present invention, the use of a gas oil composition produced by the above-described process to satisfy requirements regarding fraction and the like renders it possible to produce easily a gas oil composition suitable for a winter season that can achieve environment load reduction, low-temperature properties and low fuel consumption all together, which have been difficult to

achieve with the conventional gas oil compositions even though the gas oil composition of the present invention contains mainly an FT synthetic base oil.

[Applicability in the Industry]

The present invention can provide a gas oil composition suitable for a winter season that can achieve environment load reduction, low-temperature performance and low fuel consumption all together.

[Examples]

Hereinafter, the present invention will be described in more detail by way of the following examples and comparative examples, which should not be construed as limiting the scope of the invention.

The characteristics of gas oil compositions were measured by the following methods. The component ratio of each fraction and cetane number thereof were measured after base oils were blended and distilled.

The density referred herein denotes the density measured in accordance with JIS K 2249 "Crude petroleum and petroleum products-Determination of density and petroleum measurement tables based on a reference temperature (15°C)".

The kinematic viscosity referred herein denotes

the viscosity measured in accordance with JIS K 2283 "Crude petroleum and petroleum products-Determination of kinematic viscosity and calculation of viscosity index from kinematic viscosity".

The flash point referred herein denotes the value measured in accordance with JIS K 2265 "Crude oil and petroleum products-Determination of flash point".

The sulfur content referred herein denotes the mass content of the sulfur components on the basis of the total mass of the composition, measured in accordance with JIS K 2541 "Crude oil and petroleum products-Determination of sulfur content".

The oxygen content referred herein denotes the value measured with a thermal conductivity detector after the samples were converted to CO or alternatively further to CO₂, on platinum carbon.

All of the distillation characteristics referred herein denotes the values measured in accordance with JIS K 2254 "Petroleum products-Determination of distillation characteristics".

The content of normal paraffins every carbon number (hereinafter referred to as "CnP"), content of normal paraffins having 20 to 30 carbon atoms (hereinafter referred to as "C20-C30P") and content of hydrocarbons having 20 to 30 carbon atoms other than

the normal paraffins having 20 to 30 carbon atoms (hereinafter referred to as "C20-C30 hydrocarbon content other than C20-C30P") and the value determined by dividing the total content of normal paraffins having 20 to 30 carbon atoms by the total content of hydrocarbons having 20 to 30 carbon atoms other than the normal paraffins having 20 to 30 carbon atoms (C20-C30P/C20-C30 hydrocarbon content other than C20-C30P) are the values (mass%) measured with GC-FID or the values calculated therefrom, that is, those measured under conditions wherein the column is a capillary column formed of methyl silicone (ULTRA ALLOY-1), the carrier gas is helium and the detector is a flame ionization detector (FID), under conditions wherein the column length is 30 m, the carrier gas flow rate is 1.0 mL/min, the ratio of division is 1:79, the sample injection temperature is 360°C, the column is heated up from 140°C to 355°C (8°C/min), and the detector temperature is 360°C.

The cetane index and cetane number referred herein denote the values calculated in accordance with "8.4 cetane number calculation method using variables equation" prescribed in JIS K 2280 "Petroleum products-Fuels-Determination of octane number, cetane number and calculation of cetane number".

The cloud point referred herein denotes that measured in accordance with JIS K 2269 "Testing Method for Pour Point and Cloud Point of Crude Oil and Petroleum Products".

The cold filter plugging point referred herein denotes that measured in accordance with JIS K 2288 "Gas oil-Determination of cold filter plugging point".

The pour point referred herein denotes that measured in accordance with JIS K 2269 "Testing Method for Pour Point and Cloud Point of Crude Oil and Petroleum Products".

The carbon residue content of the 10% distillation residue referred herein denotes that measured in accordance with JIS K 2270 "Crude petroleum and petroleum products-Determination of carbon residue".

The aromatic content referred herein denotes the volume percentage (volume %) of the aromatic component content measured in accordance with JPI-5S-49-97 "Petroleum Products-Determination of Hydrocarbon Types-High Performance Liquid Chromatography" prescribed in JPI Standard and Manuals Testing Method for Petroleum Products published by Japan Petroleum Inst.

The peroxide number after an oxidation stability test referred herein denotes the value measured in

accordance with JPI-5S-46-96 prescribed in JPI Standard and Manuals Testing Method for Petroleum Products published by Japan Petroleum Inst after the compositions are subjected to an accelerated oxidation at a temperature of 95°C under oxygen bubbling for 16 hours in accordance with ASTM D2274-94.

The insoluble content after an oxidation stability test referred herein denotes the value measured after the compositions are subjected to an accelerated oxidation at a temperature of 95°C under oxygen bubbling for 16 hours in accordance with ASTM D2274-94.

The lubricity, i.e., HFRR wear scar diameter (WS1.4) referred herein denotes lubricity measured in accordance with JPI-5S-50-98 "Gas oil -Testing Method for Lubricity" prescribed in JPI Standard and Manuals Testing Method for Petroleum Products published by Japan Petroleum Inst.

The water content referred herein denotes that measured in accordance with JIS K 2275 "Crude oil and petroleum products-Determination of water content-Potentiometric Karl Fischer titration method".

(Examples 1 and 2, and Comparative Example 1)

Base oils with characteristics set forth in Table

1 were blended to produce gas oil compositions set forth in Table 2 (Examples 1 and 2 and Comparative Example 1). FT synthetic base oils 1 and 2 are hydrocarbon mixtures produced by converting natural gas to wax or a middle fraction through FT reaction, followed by hydrotreating. The reaction conditions for each FT synthetic base oil varied. FT synthetic base oil 1 is a base oil produced by isomerization positively carried out. FT synthetic base oil 2 is a base oil resulting from a treatment wherein too much emphasis was not placed on isomerization. The highly hydrotreated base oil is a hydrocarbon base oil produced by further hydrotreating a gas oil base oil to further reduce the sulfur and aromatic contents. The processed oil derived from an animal or vegetable oil is an oil produced by hydrotreating palm oil (whole component) used as the raw material to remove the foreign substance. The hydrefined gas oil corresponds to a commercially available JIS No. 2 gas oil which is used in a winter season. The gas oil compositions of Examples 1 and 2 and Comparative Example 1 were produced by blending these base oils in suitable amounts or using any of the base oils as the whole.

The additives used in these examples are as follows:

Lubricity improver: Infineum R 655 manufactured by Infineum Japan Ltd. (active component: straight-chain alkylester mixture containing a fatty acid as the raw material, average molecular weight: 250 MW)

Detergent: alkenyl succinimide mixture

Cold flow improver: Infineum R240 manufactured by Infineum Japan Ltd. (active component: ethylene-vinyl acetate copolymer mixture, solvent: alkylbenzene) (melting point: -50°C or lower)

In Example 1, additives were added through predetermined steps, i.e., steps wherein the lubricity improver was added and then sufficiently mixed and forced-stirred, and the cold flow improver was added and then sufficiently mixed and forced-stirred. Also in Example 2, additives were added through predetermined steps, i.e., steps wherein the lubricity improver and the detergent were added and then sufficiently mixed and forced-stirred, and the cold flow improver was added and then sufficiently mixed and forced-stirred. In Comparative Example 1, only the cold flow improver was added. It was confirmed that these additives used in these examples contained no solvent with a boiling point of 10°C or higher.

Table 2 sets forth the blend ratio of the gas oil compositions thus prepared and the 15°C density, 30°C kinematic viscosity, flash point, sulfur content, oxygen content, distillation characteristics, content of normal paraffins every carbon number (CnP), content of normal paraffins having 20 to 30 carbon atoms (C20-C30P), value determined by dividing the total content of normal paraffins having 20 to 30 carbon atoms by the total content of hydrocarbons having 20 to 30 carbon atoms other than the normal paraffins, cetane index, cetane number, aromatic content, cloud point, cold filter plugging point, pour point, carbon residue content of the 10% distillation residue, insoluble content and peroxide number after an oxidation stability test, wear scar diameter and water content of each composition.

The gas oil composition used in Examples 1 and 2 were produced by blending 60 percent by mass or more of the FT synthetic base oils as set forth in Table 2. Further, as apparent from Table 2, gas oil compositions satisfying the characteristics as defined herein were easily produced without fail, in Examples 1 and 2 wherein the FT synthetic base oils were blended within the range defined herein. On the other hand, as apparent from Comparative Example 1, where the

composition did not have the characteristics prescribed in the present invention or was not admixed with the predetermined additives as defined in Steps 1 and 2 of the present invention, the gas oil composition as intended by the present invention was not produced.

Next, the following various tests were carried out using the gas oil compositions of Examples 1 and 2 and Comparative Example 1. All results are set forth in Table 3. As apparent from Table 3, the gas oil compositions of Examples 1 and 2 are those with environment load reducing properties, which are excellent in fuel consumption properties and low-temperature startability, compared with the gas oil composition of Comparative Example 1 and thus are high quality fuels that can achieve at a high level excellent fuel consumption properties and low-temperature startability in a winter season, that were difficult to achieve with the conventional gas oil compositions.

(Diesel combustion test)

A vehicle 1 was driven using each gas oil composition under a test mode shown in Fig. 1 to measure NO_x, smoke and fuel consumption. The results obtained using the fuel in Comparative Example 1 were defined as 100, and the results of the other fuels were

relatively evaluated by comparison with the results of Comparative Example 1 (smaller values indicate better results).

(Low-temperature startability test)

Using the vehicle 1' and on a chassis dynamometer capable of controlling the environment temperature, each of the gas oil compositions was subjected to a test carried out at room temperature by (1) flashing (washing) the fuel system of a test diesel vehicle with a fuel to be evaluated; (2) draining out the flashing fuel; (3) replacing the main filter with new one; and (4) feeding the fuel tank with the fuel to be evaluated in a specific amount (1/2 of the tank volume of the test vehicle). The test was continued by (5) cooling rapidly the environment temperature from room temperature to -15°C ; (6) keeping the temperature at -15°C for one hour; (7) cooling gradually at a rate of 1°C/h till reaching to the predetermined temperature (-25°C); and (8) starting the engine after the temperature was kept at the predetermined temperature for one hour. If the engine did not start even after 10 second cranking was repeated twice at an interval of 30 seconds, the fuel was evaluated as "Not passed" at this moment. If the engine started while 10 second cranking was repeated twice at an interval of 30 seconds,

it was idled for 3 minutes and then the vehicle was speeded up to 60 km/h over 15 seconds and driven at the low speed. When defects in operation (hunting, stumble, vehicle speed reduction or engine stop) were observed while the vehicle was speeded up to 60 km/h and driven at that speed for 20 minutes, the gas oil composition was evaluated as "Not passed" at this moment. If the engine ran until the end without any defect, the gas oil composition was evaluated as "Passed".

(Vehicle specification): Vehicle 1

Type of engine: in-line 4 cylinder intercooled
supercharged diesel engine with EGR

Displacement: 1.4 L

Internal diameter x stroke: 73 mm x 81.4 mm

Compression ratio: 18.5 (altered to 16.0)

Maximum output: 72 kW/4000 rpm

Adopted regulation: 2002 Exhaust Gas Emission

Regulation

Vehicle weight: 1060 kg

Transmission: 5-speed manual transmission

Exhaust-gas post-processing device: oxidation
catalyst

Table 1

		FT synthetic base oil 1	FT synthetic base oil 2	Highly hydrogenated processed oil	Processed oil derived from animal or vegetable oil	Hydrotreated gas oil
Density	(15°C) kg/m ³	778	771	814	765	831
Kinematic viscosity	(30°C) mm ² /s	3.0	2.8	3.4	2.3	4.4
Distillation characteristics °C	10% distillation temperature	195.0	217.0	217.5	226.5	230.0
	50% distillation temperature	243.5	264.0	272.0	249.5	292.5
	90% distillation temperature	323.5	324.5	322.5	267.0	345.0
Sulfur content	mass %	<1	<1	<1	<1	8

Table 2

		Example 1	Example 2	Comparative Example 1
FT synthetic base oil 1		100	60	
FT synthetic base oil 2				100
Highly hydrogenated processed oil			10	
Processed oil derived from animal or vegetable oil			10	
Hydrotreated gas oil			20	
Density	(15°C) kg/m ³	778	790	771
Kinematic viscosity	(30°C) mm ² /s	3.0	3.2	2.8
Flash point	°C	58	62	58
Sulfur content	mass ppm	<1	<1	<1
Oxygen content	mass ppm	<10	<10	120
Distillation characteristics °C	Initial boiling point	158.5	161.0	171.0
	10% distillation temperature	195.0	202.0	217.0
	50% distillation temperature	243.5	254.0	264.0
	90% distillation temperature	323.5	324.0	324.5
	End point	359.0	355.5	369.0
CnP mass %	C15	2.5	2.3	3.2
	C16	2.3	2.1	3.4
	C17	1.9	1.8	3.1
	C18	1.8	1.4	2.6
	C19	1.5	1.1	2.6
	C20	1.1	0.7	1.9
	C20-C30P	1.8	1.5	2.4
C20-30 hydrocarbon content other than C20-30P mass%		7.5	4.4	12.6
C20-C30P/C20-C30 hydrocarbon content other than C20-30P		0.24	0.34	0.19
Cetane index		72.0	69.6	85.7
Cetane number		65.5	64.0	80.9
Aromatic content	vol. %	<1	3.6	<1
Cloud point	°C	-17.0	-19.0	-13.0
Cold filter plugging point	°C	-28.0	-29.0	-17.0
Pour point	°C	-35.0	-37.5	-22.5
Carbon residue content of 10% distillation residue mass %		0.00	0.00	0.00
Peroxide number	mass ppm	0	15	1
Wear scar diameter	(WS 1.4) μm	360	340	460
Insoluble content	mg/100mL	0.1	0.1	0.7
Water content	vol. ppm	19	2	47
Lubricity improver	mg/L	150	150	-
Detergent	mg/L	-	100	-
Cold flow improver	mg/L	300	300	300
Cetane number improver	mg/L	-	-	-

Table 3

	Example 1	Example 2	Comparative Example 1
Fuel consumption properties	89	86	100
Vehicle exhaust gas	96	98	100
NOx			
Smoke	94	96	100
Low-temperature startability test	Passed	Passed	Not Passed
	-25°C		

(Example 3 and 4, and Comparative Example 2)

Base oils with characteristics set forth in Table 4 were blended to produce gas oil compositions set forth in Table 5 (Examples 3 and 4 and Comparative Example 2). FT synthetic base oils 3 and 4 are hydrocarbon mixtures produced by converting natural gas to wax or a middle fraction through FT reaction, followed by hydrotreating. The reaction conditions for each FT synthetic base oil varied. FT synthetic base oil 3 is a base oil produced by isomerization positively carried out. FT synthetic base oil 4 is a base oil resulting from a treatment wherein too much emphasis was not placed on isomerization. The highly hydrotreated base oil is a hydrocarbon base oil produced by further hydrotreating a gas oil base oil to further reduce the sulfur and aromatic contents. The processed oil derived from an animal or vegetable oil is an oil produced by hydrotreating palm oil (whole component) used as the raw material to remove the foreign substance. The hydrorefined gas oil corresponds to a commercially available JIS No. 2 gas oil which is used in a winter season. The gas oil compositions of Examples 3 and 4 and Comparative Example 2 were produced by blending these base oils in suitable amounts or using any of the base oils as the whole.

The additives used in these examples are as follows:

Lubricity improver: Infineum R 655 manufactured by Infineum Japan Ltd. (active component: straight-chain alkylester mixture containing a fatty acid as the raw material, average molecular weight: 250 MW)

Detergent: alkenyl succinimide mixture

Cold flow improver: Infineum R240 manufactured by Infineum Japan Ltd. (active component: ethylene-vinyl acetate copolymer mixture, solvent: alkylbenzene) (melting point: -50°C or lower)

In Example 3, additives were added through predetermined steps, i.e., steps wherein the lubricity improver was added and then sufficiently mixed and forced-stirred, and the cold flow improver was added and then sufficiently mixed and forced-stirred. Also in Example 4, additives were added through predetermined steps, i.e., steps wherein the lubricity improver and the detergent were added and then sufficiently mixed and forced-stirred, and the cold flow improver was added and then sufficiently mixed and forced-stirred. In Comparative Example 2, only the cold flow improver was added. It was confirmed that

these additives used in these examples contained no solvent with a boiling point of 10°C or higher.

Table 5 sets forth the blend ratio of the gas oil compositions thus prepared and the 15°C density, 30°C kinematic viscosity, flash point, sulfur content, oxygen content, distillation characteristics, content of normal paraffins every carbon number (CnP), content of normal paraffins having 20 to 30 carbon atoms (C20-C30P), value determined by dividing the total content of normal paraffins having 20 to 30 carbon atoms by the total content of hydrocarbons having 20 to 30 carbon atoms other than the normal paraffins, cetane index, cetane number, aromatic content, cloud point, cold filter plugging point, pour point, carbon residue content of the 10% distillation residue, insoluble content and peroxide number after an oxidation stability test, wear scar diameter and water content of each composition.

The gas oil composition used in Examples 3 and 4 were produced by blending 60 percent by mass or more of the FT synthetic base oils as set forth in Table 5. Further, as apparent from Table 5, gas oil compositions satisfying the characteristics as defined herein were easily produced without fail, in Examples 3 and 4 wherein the FT synthetic base oils were blended within

the range defined herein. On the other hand, as apparent from Comparative Example 2, where the composition did not have the characteristics prescribed in the present invention or was not admixed with the predetermined additives as defined in Steps 1 and 2 of the present invention, the gas oil compositions as intended by the present invention was not produced.

Next, the following various tests were carried out using the gas oil compositions of Examples 3 and 4 and Comparative Example 2. All results are set forth in Table 6. As apparent from Table 6, the gas oil compositions of Examples 3 and 4 are those with environment load reducing properties, which are excellent in fuel consumption properties and low-temperature startability, compared with the gas oil composition of Comparative Example 2 and thus are high quality fuels that can achieve at a high level excellent fuel consumption properties and low-temperature startability in a winter season, that were difficult to achieve with the conventional gas oil compositions.

(Diesel combustion test)

The vehicle 1 described above was driven using each gas oil composition under a test mode shown in Fig.

1 to measure NOx, smoke and fuel consumption. The results obtained using the fuel in Comparative Example 2 were defined as 100, and the results of the other fuels were relatively evaluated by comparison with the results of Comparative Example 2 (smaller values indicate better results).

(Low-temperature startability test)

Using the vehicle 1 and on a chassis dynamometer capable of controlling the environment temperature, each of the gas oil compositions was subjected to a test carried out at room temperature by (1) flashing (washing) the fuel system of a test diesel vehicle with a fuel to be evaluated; (2) draining out the flashing fuel; (3) replacing the main filter with new one; and (4) feeding the fuel tank with the fuel to be evaluated in a specific amount (1/2 of the tank volume of the test vehicle). The test was continued by (5) cooling rapidly the environment temperature from room temperature to -15°C; (6) keeping the temperature at -15°C for one hour; (7) cooling gradually at a rate of 1°C/h till reaching to the predetermined temperature (-25°C); and (8) starting the engine after the temperature was kept at the predetermined temperature for one hour. If the engine did not start even after 10 second cranking was repeated twice at an interval

of 30 seconds, the fuel was evaluated as "Not passed" at this moment. If the engine started while 10 second cranking was repeated twice at an interval of 30 seconds, it was idled for 3 minutes and then the vehicle was speeded up to 60 km/h over 15 seconds and driven at the low speed. When defects in operation (hunting, stumble, vehicle speed reduction or engine stop) were observed while the vehicle was speeded up to 60 km/h and driven at that speed for 20 minutes, the gas oil composition was evaluated as "Not passed" at this moment. If the engine ran until the end without any defect, the gas oil composition was evaluated as "Passed".

Table 4

		FT synthetic base oil 3	FT synthetic base oil 4	Highly hydrogenated processed oil	Processed oil derived from animal or vegetable oil	Hydrotreated gas oil
Density	(15°C) kg/m³	782	792	814	765	831
Kinematic viscosity	(30°C) mm²/s	3.2	3.2	3.4	2.3	4.4
Distillation characteristics °C	10% distillation temperature	189.5	196.5	217.5	226.5	230.0
	50% distillation temperature	247.0	256.0	272.0	249.5	292.5
	90% distillation temperature	323.5	324.0	322.5	267.0	345.0
Sulfur content	mass %	<1	<1	<1	<1	8

Table 5

		Example 3	Example 4	Comparative Example 2
FT synthetic base oil 3		100	60	
FT synthetic base oil 4				100
Highly hydrogenated processed oil			10	
Processed oil derived from animal or vegetable oil			10	
Hydrotreated gas oil			20	
Density	(15°C) kg/m ³	782	792	771
Kinematic viscosity	(30°C) mm ² /s	3.2	3.2	2.8
Flash point	°C	60	58	58
Sulfur content	mass ppm	<1	<1	<1
Oxygen content	mass ppm	<10	<10	120
Distillation characteristics °C	Initial boiling point	155.5	161.0	171.0
	10% distillation temperature	189.5	196.5	217.0
	50% distillation temperature	247.0	256.0	264.0
	90% distillation temperature	323.5	324.0	324.5
	End point	358.0	355.5	369.0
CnP mass %	C20	1.1	1.4	1.9
	C21	0.7	1.1	1.5
	C22	0.4	0.7	1.1
	C23	0.3	0.3	0.7
	C24	0.2	0.2	0.3
	C25	0.1	0.1	0.2
	C20-C30P	2.9	3.9	5.7
C20-30 hydrocarbon content other than C20-30P mass%		10.7	10.8	30.0
C20-C30P/C20-30 hydrocarbon content other than C20-30P		0.27	0.36	0.19
Cetane index		70.8	70.8	85.7
Cetane number		65.5	64.0	80.9
Aromatic content	vol. %	<1	3.6	<1
Cloud point	°C	-17.0	-11.0	-13.0
Cold filter plugging point	°C	-27.0	-25.0	-17.0
Pour point	°C	-35.0	-30.0	-22.5
Carbon residue content of 10% distillation residue	mass %	0.00	0.00	0.00
Peroxide number	mass ppm	0	13	1
Wear scar diameter	(WS 1.4) μm	350	330	460
Insoluble content	mg/100mL	0.1	0.1	0.6
Water content	vol. ppm	12	19	32
Lubricity improver	mg/L	150	150	-
Detergent	mg/L	-	100	-
Cold flow improver	mg/L	150	150	150
Cetane number improver	mg/L	-	-	-

Table 6

	Example 3	Example 4	Comparative Example 2
Fuel consumption properties	88	84	100
Vehicle exhaust gas	93	98	100
NOx			
Smoke	94	96	100
Low-temperature startability test	Passed	Passed	Not Passed
	-20°C		

(Example 5 and 6, and Comparative Example 3)

Base oils with characteristics set forth in Table 7 were blended to produce gas oil compositions set forth in Table 8 (Examples 5 and 6 and Comparative Example 3). FT synthetic base oils 5 and 6 are hydrocarbon mixtures produced by converting natural gas to wax or a middle fraction through FT reaction, followed by hydrotreating. The reaction conditions for each FT synthetic base oil varied. FT synthetic base oil 5 is a base oil produced by isomerization positively carried out. FT synthetic base oil 6 is a base oil resulting from a treatment wherein too much emphasis was not placed on isomerization. The highly hydrotreated base oil is a hydrocarbon base oil produced by further hydrotreating a gas oil base oil to further reduce the sulfur and aromatic contents. The processed oil derived from an animal or vegetable oil is an oil produced by hydrotreating palm oil (whole component) used as the raw material to remove the foreign substance. The hydrorefined gas oil corresponds to a commercially available JIS No. 2 gas oil which is used in a winter season. The gas oil compositions of Examples 5 and 6 and Comparative Example 3 were produced by blending these base oils in suitable amounts or using any of the base oils as the whole.

The additives used in these examples are as follows:

Lubricity improver: Infineum R 655 manufactured by Infineum Japan Ltd. (active component: straight-chain alkylester mixture containing a fatty acid as the raw material, average molecular weight: 250 MW)

Detergent: alkenyl succinimide mixture

Cold flow improver: Infineum R240 manufactured by Infineum Japan Ltd. (active component: ethylene-vinyl acetate copolymer mixture, solvent: alkylbenzene) (melting point: -50°C or lower)

In Example 5, additives were added through predetermined steps, i.e., steps wherein the lubricity improver was added and then sufficiently mixed and forced-stirred, and the cold flow improver was added and then sufficiently mixed and forced-stirred. Also in Example 6, additives were added through predetermined steps, i.e., steps wherein the lubricity improver and the detergent were added and then sufficiently mixed and forced-stirred, and the cold flow improver was added and then sufficiently mixed and forced-stirred. In Comparative Example 3, only the cold flow improver was added. It was confirmed that

these additives used in these examples contained no solvent with a boiling point of 10°C or higher.

Table 8 sets forth the blend ratio of the gas oil compositions thus prepared and the 15°C density, 30°C kinematic viscosity, flash point, sulfur content, oxygen content, distillation characteristics, content of normal paraffins every carbon number (CnP), content of normal paraffins having 20 to 30 carbon atoms (C20-C30P), value determined by dividing the total content of normal paraffins having 20 to 30 carbon atoms by the total content of hydrocarbons having 20 to 30 carbon atoms other than the normal paraffins, cetane index, cetane number, aromatic content, cloud point, cold filter plugging point, pour point, carbon residue content of the 10% distillation residue, insoluble content and peroxide number after an oxidation stability test, wear scar diameter and water content of each composition.

The gas oil composition used in Examples 5 and 6 were produced by blending 60 percent by mass or more of the FT synthetic base oils as set forth in Table 8. Further, as apparent from Table 8, gas oil compositions satisfying the characteristics as defined herein were easily produced without fail, in Examples 5 and 6 wherein the FT synthetic base oils were blended within

the range defined herein. On the other hand, as apparent from Comparative Example 3, where the composition did not have the characteristics prescribed in the present invention or was not admixed with the predetermined additives as defined in Steps 1 and 2 of the present invention, the gas oil compositions as intended by the present invention was not produced.

Next, the following various tests were carried out using the gas oil compositions of Examples 5 and 6 and Comparative Example 3. All results are set forth in Table 9. As apparent from Table 9, the gas oil compositions of Examples 5 and 6 are those with environment load reducing properties, which are excellent in fuel consumption properties and low-temperature startability, compared with the gas oil composition of Comparative Example 3 and thus are high quality fuels that can achieve at a high level excellent fuel consumption properties and low-temperature startability in a winter season, that were difficult to achieve with the conventional gas oil compositions.

(Diesel combustion test)

The vehicle 1 described above was driven using each gas oil composition under a test mode shown in Fig.

1 to measure NO_x, smoke and fuel consumption. The results using the fuel in Comparative Example 3 were defined as 100, and the results of the other fuels were relatively evaluated by comparison with the results of Comparative Example 3 (smaller values indicate better results).

(Low-temperature startability test)

Using the vehicle 1 and on a chassis dynamometer capable of controlling the environment temperature, each of the gas oil compositions was subjected to a test carried out at room temperature by (1) flashing (washing) the fuel system of a test diesel vehicle with a fuel to be evaluated; (2) draining out the flashing fuel; (3) replacing the main filter with new one; and (4) feeding the fuel tank with the fuel to be evaluated in a specific amount (1/2 of the tank volume of the test vehicle). The test was continued by (5) cooling rapidly the environment temperature from room temperature to -15°C; (6) keeping the temperature at -15°C for one hour; (7) cooling gradually at a rate of 1°C/h till reaching to the predetermined temperature (-25°C); and (8) starting the engine after the temperature was kept at the predetermined temperature for one hour. If the engine did not start even after 10 second cranking was repeated twice at an interval

of 30 seconds, the fuel was evaluated as "Not passed" at this moment. If the engine started while 10 second cranking was repeated twice at an interval of 30 seconds, it was idled for 3 minutes and then the vehicle was speeded up to 60 km/h over 15 seconds and driven at the low speed. When defects in operation (hunting, stumble, vehicle speed reduction or engine stop) were observed while the vehicle was speeded up to 60 km/h and driven at that speed for 20 minutes, the gas oil composition was evaluated as "Not passed" at this moment. If the engine ran until the end without any defect, the gas oil composition was evaluated as "Passed".

Table 7

	FT synthetic base oil 5	FT synthetic base oil 6	Highly hydrogenated processed oil	Processed oil derived from animal or vegetable oil	Hydrorefined gas oil
Density	(15°C) kg/m ³	786	782	814	765
Kinematic viscosity	(30°C) mm ² /s	3.7	4.0	3.4	2.3
Distillation characteristics °C	10% distillation temperature	200.5	229.0	217.5	226.5
	50% distillation temperature	275.5	299.0	272.0	249.5
	90% distillation temperature	329.0	339.5	322.5	267.0
Sulfur content	mass %	<1	<1	<1	<1
					8

Table 8

		Example 5	Example 6	Comparative Example 3
FT synthetic base oil 5		100	60	
FT synthetic base oil 6				100
Highly hydrogenated processed oil			10	
Processed oil derived from animal or vegetable oil			10	
Hydrotreated gas oil			20	
Density	(15°C) kg/m ³	786	793	782
Kinematic viscosity	(30°C) mm ² /s	3.2	3.3	4.0
Flash point	°C	64	62	71
Sulfur content	mass ppm	<1	<1	<1
Oxygen content	mass ppm	<10	<10	120
Distillation characteristics °C	Initial boiling point	181.0	178.5	175.5
	10% distillation temperature	200.5	196.5	229.0
	50% distillation temperature	275.5	256.0	299.0
	90% distillation temperature	329.0	323.5	339.5
	End point	359.0	358.5	369.0
CnP mass %	C20	1.6	1.7	3.2
	C21	1.3	1.5	3.4
	C22	0.9	1.2	3.1
	C23	0.5	0.7	2.6
	C24	0.2	0.4	2.6
	C25	0.1	0.1	1.9
	C20-C30P	4.8	5.9	3.1
	(C24-C25)/C24	0.50	0.75	0.27
	(C22-C23)/C22	0.44	0.42	0.16
(C20-C21)/C20		0.19	0.12	-0.06
C20-30 hydrocarbon content other than C20-30P mass%		15.5	15.1	16.3
C20-C30P/C20-C30 hydrocarbon content other than C20-30P		0.31	0.39	0.19
Cetane index		79.0	68.5	91.6
Cetane number		67.8	68.3	80.9
Aromatic content	vol. %	<1	3.6	<1
Cloud point	°C	-5.0	-7.0	-3.0
Cold filter plugging point	°C	-13.0	-12.0	-4.0
Pour point	°C	-17.5	-17.5	-5.0
Carbon residue content of 10% distillation residue mass %		0.00	0.00	0.00
Peroxide number	mass ppm	1	12	2
Wear scar diameter	(WS 1.4) µm	360	360	460
Insoluble content	mg/100mL	0.1	0.1	0.7
Water content	vol. ppm	18	18	47
Lubricity improver	mg/L	150	150	-
Detergent	mg/L	-	100	-
Cold flow improver	mg/L	150	150	150
Cetane number improver	mg/L	-	-	-

Table 9

	Example 5	Example 6	Comparative Example 3
Fuel consumption properties	92	89	100
Vehicle exhaust gas	98	97	100
NOx			
Smoke	91	97	100
Low-temperature startability test	Passed	Passed	Not Passed
-10°C			

[Brief Description of the Drawing]

Fig. 1 is a diagram illustrating a over driving mode simulating a real run.

Claims

1. A gas oil composition comprising a gas oil composition selected from the group consisting of the following gas oil compositions (A) to (C) and additives added in accordance with the following Steps 1 and 2:
[I] gas oil compositions (A) comprising an FT synthetic base oil in an amount of 60 percent by volume or more on the basis of the total amount of the gas oil composition, with a sulfur content of 5 ppm by mass or less, an aromatic content of 10 percent by volume or less, an oxygen content of 100 ppm or less, a density of 760 kg/m³ or greater and 840 kg/m³ or less, a 90% distillation temperature of 280°C or higher and 330°C or lower and an end point of 360°C or lower in distillation characteristics, an insoluble content after an oxidation stability test of 0.5 mg/100 mL or less, an HFRR wear scar diameter (WS1.4) of 400 µm or smaller, a cloud point of -15°C or lower, a cold filter plugging point of -25°C or lower, a pour point of -32.5°C or lower, a total content of normal paraffins having 20 to 30 carbon atoms of less than 2 percent by mass, a value determined by dividing the total content of normal paraffins having 20 to 30 carbon atoms by the total content of hydrocarbons having 20 to 30 carbon

atoms other than the normal paraffins of 0.2 or greater and 0.6 or less, and a relation in the content of each of normal paraffins (CnP) having 15 to 20 carbon atoms defined by $C_{20}P < C_{19}P < C_{18}P < C_{17}P < C_{16}P < C_{15}P$;

[II] gas oil compositions (B) comprising an FT synthetic base oil in an amount of 60 percent by volume or more on the basis of the total amount of the gas oil composition, with a sulfur content of 5 ppm by mass or less, an aromatic content of 10 percent by volume or less, an oxygen content of 100 ppm or less, a density of 760 kg/m³ or greater and 840 kg/m³ or less, a 90% distillation temperature of 280°C or higher and 350°C or lower and an end point of 360°C or lower in distillation characteristics, an insoluble content after an oxidation stability test of 0.5 mg/100 mL or less, an HFRR wear scar diameter (WS1.4) of 400 µm or smaller, a cloud point of -5°C or lower, a cold filter plugging point of -20°C or lower, a pour point of -25°C or lower, a total content of normal paraffins having 20 to 30 carbon atoms of 2 percent by mass or more and less than 4 percent by mass, a value determined by dividing the total content of normal paraffins having 20 to 30 carbon atoms by the total content of hydrocarbons having 20 to 30 carbon atoms other than the normal paraffins of 0.2 or greater and 0.6 or less,

and a relation in the content of each of normal paraffins (CnP) having 20 to 25 carbon atoms defined by C20P>C21P>C22P>C23P>C24P>C25P; and

[III] gas oil compositions (C) comprising an FT synthetic base oil in an amount of 60 percent by volume or more on the basis of the total amount of the gas oil composition, with a sulfur content of 5 ppm by mass or less, an aromatic content of 10 percent by volume or less, an oxygen content of 100 ppm or less, a density of 760 kg/m³ or greater and 840 kg/m³ or less, a 90% distillation temperature of 280°C or higher and 350°C or lower and an end point of 360°C or lower in distillation characteristics, an insoluble content after an oxidation stability test of 0.5 mg/100 mL or less, an HFRR wear scar diameter (WS1.4) of 400 µm or smaller, a cloud point of -3°C or lower, a cold filter plugging point of -10°C or lower, a pour point of -12.5°C or lower, a total content of normal paraffins having 20 to 30 carbon atoms of 4 percent by mass or more and less than 6 percent by mass, a value determined by dividing the total content of normal paraffins having 20 to 30 carbon atoms by the total content of hydrocarbons having 20 to 30 carbon atoms other than the normal paraffins of 0.2 or greater and 0.6 or less, and relations in the content of each of normal paraffins

(CnP) having 20 to 25 carbon atoms defined by
C20P>C21P>C22P>C23P>C24P>C25P and
 $(C24P-C25P)/C24P > (C22P-C23P)/C22P > (C20P-C21P)/C20P$;
(Step 1) a lubricity improver comprising a fatty acid
and/or a fatty acid ester is admixed in an amount of
20 mg/L or more and 300 mg/L or less in terms of the
active component with the gas oil composition by
line-blending, forced-stirring or leaving to stand for
a sufficient time; and
(Step 2) a cold flow improver comprising an ethylene
vinyl acetate copolymer and/or a compound with a
surface active effect is admixed in an amount of 20 mg/L
or more and 1000 mg/L or less in terms of the active
component with the gas oil composition by line-blending,
forced-stirring or leaving to stand for a sufficient
time.

2. The gas oil composition according to claim 1,
wherein the gas oil composition is admixed with 200 mg/L
or more and 500 mg/L or less of a detergent comprising
a polyether amine compound, a polybutenyl amine
compound, an alkenyl succinamide compound, or an
alkenyl succinimide compound by line-blending,
forced-stirring or leaving to stand for a sufficient
time, in a step added between Steps 1 and 2.

3. The gas oil composition according to claim 1 or 2, wherein the lubricity improver, detergent and cold flow improver each contain a solvent containing no chemical substance with a melting point of 10°C or higher.

4. The gas oil composition according to any one of claims 1 to 3, wherein the gas oil composition has a peroxide number after an accelerated oxidation test of 50 ppm by mass or less, a kinematic viscosity at 30°C of 2.5 mm²/s or greater and 5.0 mm²/s or less, a cetane index of 45 or greater and a water content of 100 ppm by volume or less.