

Description

This invention relates to an audio output amplifier having a stand-by circuit, and more particularly to a protection circuit for preventing output elements from being damaged at the time of short circuit of the output terminal.

In the prior art, an audio output amplifier includes a stand-by circuit for determining whether the operation condition is a stand-by mode or normal operation mode in response to a stand-by signal, a bias circuit controlled in response to an output signal of the stand-by circuit to generate a predetermined bias voltage, a protection circuit controlled by an output signal of the stand-by circuit, an amplifier circuit connected to receive an audio signal and a bias voltage from the bias circuit and amplify the audio signal, and an output stage element (transistor) driven by an output signal from the amplifier circuit. In the audio output amplifier with the construction as described above, a non-stand-by mode (operative mode) or stand-by mode is selectively set according to the stand-by signal supplied to the stand-by circuit. Transition from the operative mode to the stand-by mode is rapidly effected. This causes a voltage at an output terminal connected to the output stage element to be rapidly changed, thereby causing an impulsive sound to be generated from a load such as a speaker connected to the output terminal. The stand-by circuit is also used to attain the audio output muting function, for example.

In order to prevent the impulsive sound from being generated, it is a common practice to delay the stand-by signal supplied to the stand-by circuit by using a CR time constant circuit. When the stand-by signal is delayed, the bias voltage from the bias circuit slowly drops, and therefore the output voltage generated from the output terminal is slowly lowered. This successfully prevents occurrence of the impulsive sound.

In a case where an abnormal condition occurs, for example, when the output terminal of the audio output amplifier is grounded, the protection circuit is operated. If transition from the operative mode to the stand-by mode occurs in the abnormal condition, the output signal of the bias circuit is slowly lowered in the transition process. At this time, since the protection circuit is immediately set into the nonoperative condition, a bias voltage is supplied to the bias circuit without any protection. Therefore, in this case, the amplifier circuit amplifies the audio signal based on the bias voltage. For this reason, if the abnormal condition as described above occurs in the transition process from the operative mode to the stand-by mode, the output stage element may be damaged.

Prior art document EP-A-0 159 079 discloses an audio amplifier switch-on control circuit in which "switch-on noise" occurring during activation of a power source and deactivation of a stand-by state is decreased. In this control circuit a rise in signal for starting the switching operation thereof is delayed and slowed, and by means of two current sources which are controlled by this slowly rising signal, a rise in the output of an amplifier is slowed so that the "switch-on noise" is decreased.

Further, prior art document EP-A-0 058 005 describes a protection circuit for an output transistor. This protection circuit detects the collector current of the output transistor and the voltage between its collector and its emitter thereby protecting the output transistor over a broad operating range.

It is an object of this invention to provide an audio output amplifier in which an output stage element can be effectively protected from being damaged in the transition process from the operative mode to the stand-by mode.

To solve this object the present invention provides an audio output amplifier as specified in claim 1.

With this construction, since an output signal of the bias circuit slowly falls with a predetermined time constant in the transition process from the operative mode to the stand-by mode, rapid change in the voltage at the output terminal can be suppressed to prevent the occurrence of the impulsive sound. Further, the protection circuit is controlled to be set to a non-operative condition after an output signal from the bias circuit is interrupted, and the protection circuit is kept in an operative condition in the transition process from the operative mode to the stand-by mode. Thus, the protection circuit is kept operative in the transition process from the operative mode to the stand-by mode so as to protect the output stage element from damage. After the protection circuit is set non-operative, each circuit in the audio output amplifier is set in the stand-by condition, preventing a useless current flow.

This invention can be more fully understood from the following detailed description when taken in conjunction with the accompanying drawings, in which:

Fig. 1 is a circuit diagram of an audio output amplifier according to a first embodiment of this invention;

Fig. 2 is a circuit diagram of an audio output amplifier according to a second embodiment of this invention; and

Fig. 3 is a circuit diagram of an audio output amplifier according to a third embodiment of this invention.

Fig. 1 is a circuit diagram showing an audio output amplifier according to a first embodiment of this

invention. Portion defined by one-dot-dash line 11 indicates the circuit construction of an audio output amplifier which is integrated. In this embodiment, audio output amplifier 11 includes V_{CC} power source terminal 12, $-V_{EE}$ power source terminal 13, non-inverting input terminal 14, inverting input terminal 15, stand-by input terminal 16 and audio signal output terminal 17. Terminal 12 is connected to receive power source voltage V_{CC} and terminal 13 is connected to receive $-V_{EE}$ power source voltage. A signal generated from audio signal source 18 is amplified by amplifier 19, and an amplified output signal is set to a desired signal level adjusted by means of volume control 20. The level-adjusted signal is then supplied to input terminal 14, via DC blocking capacitor C5. Terminal 14 is circuit-grounded via resistor R13. Terminal 16 is connected to receive a stand-by signal from CPU 21, for example. Terminal 17 is connected to a load 22 such as a speaker which is driven by an audio signal generated from terminal 17.

Further, audio output amplifier 11 includes stand-by circuit 23, bias circuit 24, protection circuit 25, amplifier circuit 26 and overcurrent detection circuit 27 which are each connected between terminals 12 and 13. Stand-by circuit 23 includes input NPN transistor Q1 for stand-by control, switching PNP transistor Q2 for stand-by control and resistor R1. The base of transistor Q1 is connected to terminal 16, the emitter is connected to terminal 13 and the collector is connected to one end of resistor R1. The other end of resistor R1 is connected to the base of transistor Q2 whose emitter is connected to terminal 12.

Bias circuit 24 is used to supply a predetermined bias voltage to amplifier 26. Bias circuit 24 includes NPN transistors Q3 and Q4, resistors R2 to R4, diodes (or PNP transistors each having a collector and a base connected together) D1 to D3, and capacitor C1. One end of resistor R2 is connected to the collector of transistor Q2, and the other end is connected to the base of transistor Q3 and to one end of resistor R3 which is connected at the other end to terminal 13. The collector of transistor Q3 is connected to terminal 12 and the emitter is connected to one end of resistor R4. Capacitor C1 is connected between the base of transistor Q3 and terminal 13. The other end of resistor R4 is connected to the anode of diode D1 whose cathode is connected to the anode of diode D2 and the base of transistor Q4. The cathode of diode D2 is connected to terminal 13. The collector and emitter of transistor Q4 are respectively connected to the cathode of diode D3 and terminal 13. Further, the anode of diode D3 is connected to terminal 12.

Protection circuit 25 is used to set amplifier circuit 26 to the non-operative condition by interrupting the supply of bias voltage from bias circuit 24 when an overcurrent is detected by means of overcurrent detection circuit 27. Protection circuit 25 includes NPN transistors Q5 to Q7, PNP transistor Q8 and resistors R5 to R7. The base of transistor Q5 is connected to the base of Q3, the collector is connected to terminal 12 and the emitter is connected to one end of resistor R5. The other end of resistor R5 is connected to the emitter of transistor Q8 and one end of resistor R6. The base of transistor Q8 is connected to the other end of resistor R6 and the collector of transistor Q7, and the collector of Q8 is connected to the base of transistor Q7. The base of transistor Q7 is also connected to the base of transistor Q6 and the emitter is connected to terminal 13. The collector of transistor Q6 is connected to the base of transistor Q4 and the emitter is connected to terminal 13. Resistor R7 is connected between terminal 13 and the base connection node of transistors Q6 and Q7. Transistors Q7 and Q8 are connected to form a thyristor.

Amplifier circuit 26 includes PNP transistors Q9 to Q13, NPN transistors Q14 to Q17, resistors R8 and R9, and diodes (or PNP transistors each having a collector and a base connected together) D4 and D5. The base of transistor Q9 is connected to the cathode of diode D3, the emitter is connected to terminal 12, and the collector is connected to the emitters of transistors Q10 and Q11. The emitter of transistor Q10 is connected to the emitter of transistor Q11, the base is connected to terminal 14 and the collector is connected to the collector of transistor Q14. The base and collector of transistor Q11 are respectively connected to terminal 15 and the collector of transistor Q15. The bases of transistors Q14 and Q15 are connected together, and the base connection node is connected to the collector of transistor Q15. The emitters of transistors Q14 and Q15 are connected to terminal 13. Transistors Q10, Q11, Q14 and Q15 are connected to constitute differential amplifier section 28. Transistor Q9 functions as an operation current source for differential amplifier section 28. The base of transistor Q12 is connected to the base of transistor Q9, the emitter is connected to terminal 12 and the collector is connected to the base of transistor Q17 and the anode of diode D4. The cathode of diode D4 is connected to the anode of diode D5 whose cathode is connected to the base of transistor Q13 and the collector of transistor Q16. The base of transistor Q16 is connected to the collector of transistor Q14, and the emitter is connected to terminal 13. The base-collector of transistor Q16 is coupled via phase-compensation capacitor C6 which prevents a parasitic oscillation of amplifier circuit 26. Diodes D4 and D5 and transistor Q16 are thus connected to constitute pre-driving section 29 for amplifying an output signal of differential amplifier section 28. Each of resistors R8 and R9 is connected at one end to terminal 15. The other end of resistor R8 is connected to terminal 17, and the other end of resistor R9 is grounded. Resistors R8 and R9 are connected to constitute a negative feedback circuit 30 for feeding an audio output signal to the input terminal of differential amplifier section 28 from

terminal (audio signal output terminal) 17. The collector and emitter of transistor Q17 are respectively connected to terminals 12 and 17. The emitter and collector of transistors Q13 are respectively connected to terminals 17 and 13. Transistors Q13 and Q17 are thus connected to constitute output stage amplifier section 31 of complementary single ended push-pull (SEPP) type. Output stage amplifier section 31 is driven in a push-pull fashion by an output signal from pre-driving section 29.

Overcurrent detection circuit 27 includes diode (or PNP transistor having a collector and a base connected together) D6, NPN transistor Q18, PNP transistor Q19, and resistor R10. The base of transistor Q18 is connected to the collector of transistor Q12, the collector is connected to the cathode of diode D6 and the emitter is connected to one terminal of resistor R10. The anode of diode D6 is connected to terminal 12, and the other end of resistor R10 is connected to terminal 17. The emitter of transistor Q19 is connected to terminal 12, the base is connected to the collector of transistor Q18, and the collector is connected to the base connection node of transistors Q6 and Q7.

Next, the operation of audio output amplifier 11 shown in Fig. 1 is explained. In the normal operative mode, a stand-by signal supplied from CPU 21 to terminal 16 is set at an "H" level to render transistors Q1 and Q2 conductive. As a result, bias circuit 24 is set operative, lowering the potential at the collector of transistor Q4. This causes the base potentials of transistors Q9 and Q12 of amplifier circuit 26 to be lowered, thus turning on transistors Q9 and Q12 to set amplifier circuit 26 in an operative condition. In this condition, an audio signal supplied from terminal 14 is amplified by amplifier circuit 26 and generated from terminal 17. The amplified audio signal is supplied to drive load 22 such as a speaker. In the normal operation mode, overcurrent detection circuit 27 is set in the non-operative condition, and protection circuit 25 is also set in the non-operative condition.

However, if an overcurrent flows in transistor Q17, and the base-emitter voltage (V_{BE}) increases, transistors Q18 and Q19 of overcurrent detection circuit 27 are turned on. Then, the thyristor constituted by transistors Q7 and Q8 is triggered and set to a conductive state and transistor Q6 is turned on. This renders transistor Q4 of bias circuit 24 to be nonconductive and transistors Q9 and Q12 of amplifier circuit 26 are turned off. Thus, differential amplifier section 28 and pre-driving section 29 of amplifier circuit 26 are set to a non-operative condition, protecting transistors Q17 and Q13 connected at the output stage.

When a stand-by signal supplied to terminal 16 is set at an "L" level, transistors Q1 and Q2 are turned off. This changes the operating condition from the normal operative mode to the stand-by mode. At this time, base potential V_{B3} of transistor Q3 of bias circuit 24 is slowly lowered with the time constant expressed as shown in the following eq. (1):

$$V_{B3} \approx \frac{R_3}{R_2+R_3} (V_{CC}+V_{EE}) \exp\left(-\frac{t}{C_1 R_3}\right) \quad \dots (1)$$

In eq. (1), the base input resistance of transistor Q3 is sufficiently larger than that of resistor R3. Therefore, current I_3 flowing through transistor Q3, and diodes D1 and D2 is slowly lowered with the time constant which is dependent on base potential V_{B3} of transistor Q3 as shown by the following eq. (2):

$$I_3 \approx \frac{V_{B3}-3V_{BE}}{R_4} \quad \dots (2)$$

where V_{BE} denotes a voltage between the base and emitter of transistor Q3 and the forward voltage drop of diode D1 and D2.

Therefore, currents flowing in transistor Q4 connected to diode D2, diode D3 connected between the collector of transistor Q4 and terminal 12, and transistors Q9 and Q12 connected to the cathode of diode D3 are slowly reduced with the time constant as described above. Thus, the operating conditions of amplifier circuit 26, pre-driving section 29 and overcurrent detection circuit 27 are slowly transferred from the operative mode to the non-operative mode. Therefore, the output level of an audio output signal from terminal 17 is slowly lowered. When the operating conditions of amplifier circuit 26, pre-driving section 29 and overcurrent detection circuit 27 are slowly transferred from the operative mode to the non-operative mode (stand-by mode), protection circuit 25 is still set in the operative condition. Accordingly, even if terminal 17 is grounded, protection circuit 25 is operated to protect transistors Q17 and Q13. That is, base potential V_{B3} of transistor Q3 in bias circuit 24 is slowly lowered, causing the base potential of transistor Q5 of protection circuit 25 to be slowly lowered. At this time, if an overcurrent is detected by overcurrent detection circuit 27, the thyristor formed of transistors Q7 and Q8 is triggered and set to a conductive state.

This turns on transistor Q6 and turns off transistor Q4 of bias circuit 24. Therefore, supply of bias voltage from bias circuit 24 to amplifier circuit 26 is interrupted, setting amplifier circuit 26 to the non-operative state. Thus, output transistors Q17 and Q13 can be protected. In this case, transistor Q4 of bias circuit 24 is turned off when base potential V_{B3} of transistor Q3 becomes smaller than $3V_{BE}$ as shown by the following expression (3) to turn off transistor Q3:

$$V_{B3} < 3V_{BE} \quad (3)$$

Further, the thyristor is set to a cut-off state when base potential V_{B5} of transistor Q5 is set to satisfy the following expression (4):

$$V_{B5} = V_{B3} < 2V_{BE} + V_{CE8} + \left(\frac{R_5}{R_6} + \frac{R_5}{R_7}\right)V_{BE} \quad (4)$$

where V_{CE8} is a voltage between the collector and emitter of transistor Q8.

Only if the circuit constants are set to satisfy the following expression (5) based on expressions (3) and (4), it is possible to turn off transistor Q3 before the thyristor formed of transistors Q7 and Q8 is turned off in the transition process from the operative mode to the stand-by mode:

$$2V_{BE} + V_{CE8} + \left(\frac{R_5}{R_6} + \frac{R_5}{R_7}\right)V_{BE} < 3V_{BE} \quad (5)$$

Thus, amplifier circuit 26 is set to the non-operative mode before protection circuit 25 is set non-operative, making it possible to protect output transistors Q17 and Q13 even in the transition process from the operative mode to the stand-by mode.

With this construction, since an output signal of bias circuit 24 is slowly lowered with a predetermined time constant in the transition process from the operative mode to the stand-by mode, rapid variation in the voltage at output terminal 17 is suppressed, preventing generation of the impulsive sound. Further, protection circuit 25 is set to the non-operative condition after an output of bias circuit 24 is interrupted, and protection circuit 25 is kept operative in the transition process from the operative mode to the stand-by mode. Therefore, protection circuit 25 is operated in the transition process from the operative mode to the stand-by mode so as to protect the output stage elements (transistors Q17 and Q13) from being damaged. After protection circuit 25 is set in the non-operative mode, each circuit in audio output amplifier 11 is set to the stand-by mode, preventing an unwanted current flow.

Fig. 2 shows an audio output amplifier according to a second embodiment of this invention. In Fig. 2, those portions which correspond to the circuit portions in Fig. 1 are denoted by the same reference numerals and the explanation thereof is omitted. Further, amplifier circuit 26 and overcurrent detection circuit 27 are constructed in the same manner as in the circuit of Fig. 1, and therefore they are shown in a block form. In this case, external circuits connected to terminals 14 to 16 are omitted. The Fig. 2 circuit is similar to that of Fig. 1 except that bias circuit 32 exclusively used for protection circuit 25 is additionally provided in the Fig. 1 circuit. In the Fig. 1 circuit, bias circuit 24 is used for both protection circuit 25 and amplifier circuit 26. However, in the Fig. 2 circuit, a bias voltage is supplied from bias circuit 24 to amplifier circuit 26 and a bias voltage to protection circuit 25 is supplied from bias circuit 32. Bias circuit 32 includes PNP transistor Q20, resistors R11 and R12, and capacitor C2. The base of transistor Q20 is connected to the base of transistor Q2, the emitter is connected to terminal 12, and the collector is connected to one end of resistor R11. The other end of resistor R11 is connected to the base of transistor Q5 and one end of resistor R12. The other end of resistor R12 is connected to terminal 13. Further, capacitor C2 is connected between the base of transistor Q5 and terminal 13.

With the construction described above, the normal operation is effected in the same manner as in the Fig. 1 circuit. In the case where a stand-by signal supplied to terminal 16 is set to an "L" level and transistor Q1 is turned off to change the operation condition from the operative mode to the stand-by mode, transistor Q20 is turned off. As a result, a potential at the connection node between resistors R11 and R12 or the base potential of transistor Q5 is slowly lowered with the CR time constant defined by resistor R12 and capacitor C2. At the same time, turn-off of transistor Q1 causes transistor Q2 to be turned off. Therefore, the base potential of transistor Q3 is slowly lowered with the CR time constant defined by resistor R3 and capacitor C1.

In audio output amplifier 11, it is necessary to turn off transistor Q3 of bias circuit 24 prior to the turn-off of the thyristor of protection circuit 25 in the transition process from the operative mode to the stand-by mode. For this reason, the relation between time constant $C1 \cdot R3$ of bias circuit 24 and time constant $C2 \cdot R12$ of bias circuit 32 is set to satisfy the following expression (6):

$$C1 \cdot R3 < C2 \cdot R12 \quad (6)$$

The condition shown in expression (6) can be easily set in comparison with that shown in expression (5).

Fig. 3 shows an audio output amplifier according to a third embodiment of this invention. In the circuit of Fig. 3, those portions which are similar to the circuit portions of Fig. 1 are denoted by the same reference numerals and the explanation thereof is omitted. In the circuit of Fig. 3, power source voltage V_{CC} is supplied to terminal 12 and ground potential GND is supplied to terminal 13. A series circuit of resistors R14 and R15 is connected between the V_{CC} circuit and the circuit ground, and the junction between resistors R14 and R15 is coupled, via resistor R13, to the base of transistor Q10. Resistors R13-R15 constitute a bias circuit for amplifier circuit 26. Capacitor C3 is connected between resistor R9 of negative feedback 30 and the ground. Further, capacitor C4 is connected between terminal 17 and the emitter connection node of transistors Q17 and Q13. Capacitors C3 and C4 are used for DC cut-off.

With this construction, stand-by circuit 23, bias circuit 24, protection circuit 25, amplifier circuit 26 and overcurrent detection circuit 27 constituting audio output amplifier 11 are operated on a power source voltage between V_{CC} and GND. In this embodiment, a power source voltage different from that in the Fig. 1 circuit is used, but the basic operation is the same as in the Fig. 1 circuit and the same effect can be attained.

Claims

1. An audio output amplifier, comprising:

- a first power source terminal (12) connected to be set at a power source potential (V_{CC});
 - a second power source terminal (13) connected to be set at a power potential ($-V_{EE}$; GND) lower than the power source potential (V_{CC}) of said first power source terminal (12);
 - a stand-by signal input terminal (16) connected to receive a stand-by signal;
 - stand-by means (23), having an input terminal connected to said stand-by signal input terminal (16), for switching between a normal operative mode and a stand-by mode;
 - delay means (R2, R3, C1) for delaying an output of said stand-by means (23);
 - bias means (Q3, Q4, R4, D1-D3) controlled in accordance with an output signal from said delay means (R2, R3, C1); and
 - amplifier means (26) for amplifying an audio signal input thereto, and whose operating current is controlled by said bias means (Q3, Q4, R4, D1-D3);
- characterized by:
- overcurrent detection means (27) for detecting an overcurrent flowing in output elements (Q17, Q13) of said amplifier means (26); and
 - protection means (25) for protecting said amplifier means (26) by placing said bias means (Q3, Q4, R4, D1-D3) in an inoperative state when an overcurrent is detected by said overcurrent detection means (27); wherein:
 - said audio output amplifier causes an output of said amplifier means (26) to fall gradually and reduces switch noise when shifting from a normal operating state to a stand-by state by controlling the bias means (Q3, Q4, R4, D1-D3) with an output of said delay means (R2, R3, C1),
 - destruction of the output elements (Q17, Q13) of said amplifier means (26) is prevented when shifting from a normal operating state to a stand-by state by controlling said protection means (25) with the output of said delay means (R2, R3, C1).

2. An audio output amplifier according to claim 1, characterized in that said stand-by means (23) includes a first transistor (Q1) of a first conductivity type which has a base connected to said stand-by signal input terminal (16) and an emitter connected to said second power source terminal (13); a resistor (R1) connected at one end to a collector of said first transistor (Q1); and a second transistor (Q2) of a second conductivity type which has a base connected to the other end of said resistor (R1), an emitter connected to said first power source terminal (12) and a collector connected to an input terminal of said delay means.

3. An audio output amplifier according to claim 1, characterized in that said delay means includes first and second resistors (R2 and R3) serially connected between the output terminal of said stand-by means (23) and said second power source terminal (13); and a capacitor (C1) which is connected at one end



$$C1 \cdot R3 < C2 \cdot R12 \quad (6)$$

The condition shown in expression (6) can be easily set in comparison with that shown in expression (5).

Fig. 3 shows an audio output amplifier according to a third embodiment of this invention. In the circuit of Fig. 3, those portions which are similar to the circuit portions of Fig. 1 are denoted by the same reference numerals and the explanation thereof is omitted. In the circuit of Fig. 3, power source voltage V_{CC} is supplied to terminal 12 and ground potential GND is supplied to terminal 13. A series circuit of resistors R14 and R15 is connected between the V_{CC} circuit and the circuit ground, and the junction between resistors R14 and R15 is coupled, via resistor R13, to the base of transistor Q10. Resistors R13-R15 constitute a bias circuit for amplifier circuit 26. Capacitor C3 is connected between resistor R9 of negative feedback 30 and the ground. Further, capacitor C4 is connected between terminal 17 and the emitter connection node of transistors Q17 and Q13. Capacitors C3 and C4 are used for DC cut-off.

With this construction, stand-by circuit 23, bias circuit 24, protection circuit 25, amplifier circuit 26 and overcurrent detection circuit 27 constituting audio output amplifier 11 are operated on a power source voltage between V_{CC} and GND. In this embodiment, a power source voltage different from that in the Fig. 1 circuit is used, but the basic operation is the same as in the Fig. 1 circuit and the same effect can be attained.

Claims

1. An audio output amplifier, comprising:

- a first power source terminal (12) connected to be set at a power source potential (V_{CC});
 - a second power source terminal (13) connected to be set at a power potential ($-V_{EE}$; GND) lower than the power source potential (V_{CC}) of said first power source terminal (12);
 - a stand-by signal input terminal (16) connected to receive a stand-by signal;
 - stand-by means (23), having an input terminal connected to said stand-by signal input terminal (16), for switching between a normal operative mode and a stand-by mode;
 - delay means (R2, R3, C1) for delaying an output of said stand-by means (23);
 - bias means (Q3, Q4, R4, D1-D3) controlled in accordance with an output signal from said delay means (R2, R3, C1); and
 - amplifier means (26) for amplifying an audio signal input thereto, and whose operating current is controlled by said bias means (Q3, Q4, R4, D1-D3);
- characterized by:
- overcurrent detection means (27) for detecting an overcurrent flowing in output elements (Q17, Q13) of said amplifier means (26); and
 - protection means (25) for protecting said amplifier means (26) by placing said bias means (Q3, Q4, R4, D1-D3) in an inoperative state when an overcurrent is detected by said overcurrent detection means (27); wherein:
 - said audio output amplifier causes an output of said amplifier means (26) to fall gradually and reduces switch noise when shifting from a normal operating state to a stand-by state by controlling the bias means (Q3, Q4, R4, D1-D3) with an output of said delay means (R2, R3, C1),
 - destruction of the output elements (Q17, Q13) of said amplifier means (26) is prevented when shifting from a normal operating state to a stand-by state by controlling said protection means (25) with the output of said delay means (R2, R3, C1).

2. An audio output amplifier according to claim 1, characterized in that said stand-by means (23) includes a first transistor (Q1) of a first conductivity type which has a base connected to said stand-by signal input terminal (16) and an emitter connected to said second power source terminal (13); a resistor (R1) connected at one end to a collector of said first transistor (Q1); and a second transistor (Q2) of a second conductivity type which has a base connected to the other end of said resistor (R1), an emitter connected to said first power source terminal (12) and a collector connected to an input terminal of said delay means.

3. An audio output amplifier according to claim 1, characterized in that said delay means includes first and second resistors (R2 and R3) serially connected between the output terminal of said stand-by means (23) and said second power source terminal (13); and a capacitor (C1) which is connected at one end



to the connection node between said first and second resistors (R2 and R3) and to the input terminal of said protection means (25) and connected at the other end to said second power source terminal (13).

4. An audio output amplifier according to claim 1, characterized in that said bias means includes a first transistor (Q3) of a first conductivity type which has a base connected to the output terminal of said delay means and a collector connected to said first power source terminal (12); a resistor (R4) connected at one end to an emitter of said first transistor (Q3); a first diode (D1) having an anode connected to the other end of said resistor (R4); a second diode (D2) having an anode connected to the cathode of said first diode (D1) and a cathode connected to said second power source terminal (13); a second transistor (Q4) of the first conductivity type which has a base connected to the anode of said second diode (D2) and to the output terminal of said protection means (25) and an emitter connected to said second power source terminal (13); and a third diode (D3) having an anode connected to said first power source terminal (12) and a cathode connected to the collector of said second transistor (Q4) and to the control input terminal of said amplifier means (26).
5. An audio output amplifier according to claim 1, characterized in that said protection means (25) includes a first transistor (Q5) of a first conductivity type which has a base connected to an output terminal of said delay means and a collector connected to said first power source terminal (12); a first resistor (R5) connected at one end to an emitter of said first transistor (Q5); a second transistor (Q8) of a second conductivity type which has an emitter connected to the other end of said first resistor (R5); a second resistor (R6) connected between the base and emitter of said second transistor (Q8); a third transistor (Q7) of the first conductivity type which has a base connected to the collector of said second transistor (Q8), a collector connected to the base of said second transistor (Q8) and an emitter connected to said second power source terminal (13); a fourth transistor (Q6) of the first conductivity type which has a base connected to the base of said third transistor (Q7) and the output terminal of said overcurrent detection means (27), a collector connected to said bias means and an emitter connected to said second power source terminal (13); a third resistor (R7) connected between the base connection node of said third and fourth transistors (Q7 and Q6) and said second power source terminal (13).
6. An audio output amplifier according to claim 1, characterized in that said amplifier means (26) includes a differential amplifier section (28) having one input terminal connected to said audio signal input terminal (14); a first current source (Q9) controlled by a bias voltage generated from said bias means and supplying an operation current to said differential amplifier section (28); a pre-driving section (29) connected to receive an amplified audio signal supplied from said differential amplifier section (28); a second current source (Q12) controlled by a bias voltage generated from said bias means and supplying an operation current to said pre-driving section (29) and said overcurrent detection means (27); an output stage amplifier section (31) driven by an output from said pre-driving section (29); and a negative feedback circuit (30) for feeding back an audio signal from said signal output terminal (17) to the other input terminal of said differential amplifier section (28).
7. An audio output amplifier according to claim 6, characterized in that said differential amplifier section (28) includes a first transistor (Q14) of a first conductivity type which has an emitter connected to said second power source terminal (13); a second transistor (Q15) of the first conductivity type which has an emitter connected to said second power source terminal (13) and a base connected to the base of said first transistor (14); a third transistor (Q10) of a second conductivity type which has a collector connected to the collector of said first transistor (Q14) and the input terminal of said pre-driving section (29) and a base connected to said audio signal input terminal (14); and a fourth transistor (Q11) of the second conductivity type which has a collector connected to the collector of said second transistor (Q15) and the base connection node of said first and second transistors (Q14 and Q15), a base connected to said negative feedback circuit (30) and an emitter connected to the emitter of said third transistor (Q10) and said first current source (Q9).
8. An audio output amplifier according to claim 6, characterized in that said pre-driving section (29) includes a transistor (Q16) which has a base connected to the output terminal of said differential amplifier section (28) and an emitter connected to said second power source terminal (13); a first diode (D5) having a cathode connected to the collector of said transistor (Q16) and the first input terminal of said output stage amplifier section (31); and a second diode (D4) having a cathode connected to the



anode of said first diode (D5) and an anode connected to the second input terminal of said output stage amplifier section (31), the input terminal of said overcurrent detection means (27) and said second current source (Q12).

- 5 9. An audio output amplifier according to claim 6, characterized in that said output stage amplifier section (31) includes a first transistor (Q17) of a first conductivity type which has a collector connected to said first power source terminal (12), a base connected to the first output terminal of said pre-driving section (29) and an emitter connected to said signal output terminal (17); and a second transistor (Q13) of a second conductivity type which has an emitter connected to said signal output terminal (17), a base connected to the second output terminal of said pre-driving section (29) and a collector connected to said second power source terminal (13).
- 10 10. An audio output amplifier according to claim 6, characterized in that said negative feedback circuit (30) includes a first resistor (R8) connected between the output terminal (17) of said audio output amplifier and the other input terminal of said differential amplifier section (28); and a second resistor (R9) connected between the other input terminal of said differential amplifier section (28) and the ground.
- 15 11. An audio output amplifier according to claim 1, characterized in that said overcurrent detection means (27) includes a first transistor (Q18) of a first conductivity type which has a base connected to said amplifier means (26); a first resistor (R10) connected between the emitter of said first transistor (Q18) and said signal output terminal (17); a diode (D6) having a cathode connected to the collector of said first transistor (Q18) and an anode connected to said first power source terminal (12); and a second transistor (Q19) of a second conductivity type which has a base connected to the collector of said first transistor (Q18), an emitter connected to said first power source terminal (12) and a collector connected to the control input terminal of said protection means (25).
- 20 25 12. An audio output amplifier according to claim 1, further comprising protection delay circuit (32) for delaying an output signal of said stand-by means (23) and supplying the delayed signal to said protection means (25), wherein the delay time by said protection delay circuit (32) is set longer than that of said delay means.
- 30 13. An audio output amplifier according to claim 12, characterized in that said protection delay means (32) includes a transistor (Q20) having a base connected to the output terminal of said stand-by means (23) and an emitter connected to said first power source terminal (12); first and second resistors (R11 and R12) serially connected between the collector of said transistor (Q20) and said second power source terminal (13); and a capacitor (C2) connected at one end to the base connection node of said first and second resistors (R11 and R12) and the input terminal of said protection means (25) and at the other end to said second power source terminal (13).
- 35 40 14. An audio output amplifier according to claim 10, further comprising a first capacitor (C4) connected between said signal output terminal (17) and output terminal of said amplifier means (26); a second capacitor (C3) connected between one end of said resistor (R9) of said negative feedback circuit (30) and the ground; and an inverting input terminal (15) connected to said amplifier means (26) and wherein said second power source terminal (13) is connected to the ground (GND) and said inverting input terminal (15) is connected to a negative voltage source (-V).
- 45

Patentansprüche

1. Audioausgangsverstärker, mit:

- 50 - einem ersten Spannungsquellenanschluß (12), der verbunden ist, um auf ein Spannungsquellenpotential (VCC) gesetzt zu sein;
- einem zweiten Spannungsquellenanschluß (13), der verbunden ist, um auf ein Spannungspotential (-VEE; GND) gesetzt zu sein, das niedriger ist als das Spannungsquellenpotential (VCC) des ersten Spannungsquellenanschlusses (12);
- 55 - einem Bereitschaftssignaleingangsanschluß (16), der verbunden ist, um ein Bereitschaftssignal zu empfangen;
- einer Bereitschaftseinrichtung (23) mit einem mit dem Bereitschaftssignaleingangsanschluß (16) verbundenen Eingangsanschluß zum Schalten zwischen einem normalen Betriebsmodus und



einem Bereitschaftsmodus;

- einer Verzögerungseinrichtung (R2, R3; C1) zum Verzögern eines Ausgangssignales der Bereitschaftseinrichtung (23);
- einer Vorspanneinrichtung (Q3, Q4, R4, D1-D3), die gemäß einem Ausgangssignal von der Verzögerungseinrichtung (R2, R3, C1) gesteuert ist; und
- einer Verstärkereinrichtung (26) zum Verstärken eines dorthin eingespeisten Audiosignales, wobei deren Betriebsstrom durch die Vorspanneinrichtung (Q3, Q4, R4, D1-D3) gesteuert ist; gekennzeichnet durch:
 - eine Überstromdetektoreinrichtung (27) zum Erfassen eines in Ausgangselementen (Q17, Q13) der Verstärkereinrichtung (26) fließenden Überstromes; und
 - eine Schutzeinrichtung (25) zum Schützen der Verstärkereinrichtung (26), indem die Vorspanneinrichtung (Q3, Q4, R4, D1-D3) in einen nichtoperativen Zustand gebracht wird, wenn ein Überstrom durch die Überstromdetektoreinrichtung (27) erfaßt wird; wobei:
 - der Audioausgangsverstärker ein Ausgangssignal der Verstärkereinrichtung (26) graduell abfallen läßt und ein Schalterrauschen vermindert, wenn ein Schieben von einem normalen Betriebszustand in einen Bereitschaftszustand erfolgt, durch Steuern der Vorspanneinrichtung (Q3, Q4, R4, D1-D3) mit einem Ausgangssignal von der Verzögerungseinrichtung (R2, R3, C1),
 - eine Zerstörung der Ausgangselemente (Q17, Q13) der Verstärkereinrichtung (26) verhindert wird, wenn ein Schieben von einem normalen Betriebszustand zu einem Bereitschaftszustand erfolgt, durch Steuern der Schutzeinrichtung (25) mit dem Ausgangssignal der Verzögerungseinrichtung (R2, R3, C1).

2. Audioausgangsverstärker nach Anspruch 1, dadurch gekennzeichnet, daß die Bereitschaftseinrichtung (23) einen ersten Transistor (Q1) eines ersten Leitfähigkeitstyps, dessen Basis mit dem Bereitschaftssignaleingangsanschluß (16) verbunden ist und dessen Emitter an den zweiten Spannungsquellenanschluß (13) angeschlossen ist, einen an einem Ende mit einem Kollektor des ersten Transistors (Q1) verbundenen Widerstand (R1) und einen zweiten Transistor (Q2) eines zweiten Leitfähigkeitstyps, dessen Basis mit dem anderen Ende des Widerstandes (R1) verbunden ist, dessen Emitter an den ersten Spannungsquellenanschluß (12) angeschlossen ist und dessen Kollektor mit einem Eingangsanschluß der Verzögerungseinrichtung verbunden ist, aufweist.

3. Audioausgangsverstärker nach Anspruch 1, dadurch gekennzeichnet, daß die Verzögerungseinrichtung einen ersten und einen zweiten Widerstand (R2 und R3), die in Reihe zwischen dem Ausgangsanschluß der Bereitschaftseinrichtung (23) und dem zweiten Spannungsquellenanschluß (13) liegen, und einen Kondensator (C1), der an einem Ende mit dem Verbindungsknoten zwischen dem ersten und dem zweiten Widerstand (R2 und R3) und mit dem Eingangsanschluß der Schutzeinrichtung (25) und am anderen Ende mit dem zweiten Spannungsquellenanschluß (13) verbunden ist, aufweist.

4. Audioausgangsverstärker nach Anspruch 1, dadurch gekennzeichnet, daß die Vorspanneinrichtung aufweist: einen ersten Transistor (Q3) eines ersten Leitfähigkeitstyps, der eine mit dem Ausgangsanschluß der Verzögerungseinrichtung verbundene Basis und einen mit dem ersten Spannungsquellenanschluß (12) verbundenen Kollektor hat, einen Widerstand (R4), der an einem Ende mit einem Emitter des ersten Transistors (Q3) verbunden ist, eine erste Diode (D1) mit einer mit dem anderen Ende des Widerstandes (R4) verbundenen Anode, eine zweite Diode (D2) mit einer mit der Kathode der ersten Diode (D1) verbundenen Anode und einer mit dem zweiten Spannungsquellenanschluß (13) verbundenen Kathode, einen zweiten Transistor (Q4) des ersten Leitfähigkeitstyps, der eine mit der Anode der zweiten Diode (D2) und dem Ausgangsanschluß der Schutzeinrichtung (25) verbundene Basis und einen mit dem zweiten Spannungsquellenanschluß (13) verbundenen Emitter hat, und eine dritte Diode (D3) mit einer mit dem ersten Spannungsquellenanschluß (12) verbundenen Anode und einer mit dem Kollektor des zweiten Transistors (Q4) und dem Steuereingangsanschluß der Verstärkereinrichtung (26) verbundenen Kathode.

5. Audioausgangsverstärker nach Anspruch 1, dadurch gekennzeichnet, daß die Schutzeinrichtung (25) aufweist: einen ersten Transistor (Q5) eines ersten Leitfähigkeitstyps, der eine mit einem Ausgangsanschluß der Verzögerungseinrichtung verbundene Basis und einen mit dem ersten Spannungsquellenanschluß (12) verbundenen Kollektor hat, einen ersten Widerstand (R5), der an einem Ende mit einem Emitter des ersten Transistors (Q5) verbunden ist, einen zweiten Transistor (Q8) eines zweiten Leitfähigkeitstyps, der einen mit dem anderen Ende des ersten Widerstandes (R5) verbundenen Emitter



5 hat; einen zwischen der Basis und dem Emitter des zweiten Transistors (Q8) liegenden zweiten Widerstand (R6); einen dritten Transistor (Q7) des ersten Leittfähigkeitstyps, der eine mit dem Kollektor des zweiten Transistors (Q8) verbundene Basis, einen mit der Basis des zweiten Transistors (Q8) verbundenen Kollektor und einen mit dem zweiten Spannungsquellenanschluß (13) verbundenen Emitter hat; einen vierten Transistor (Q6) des ersten Leittfähigkeitstyps, der eine mit der Basis des dritten Transistors (Q7) und dem Ausgangsanschluß der Überstromdetektoreinrichtung (27) verbundene Basis, einen mit der Vorspanneinrichtung verbundenen Kollektor und einen mit dem zweiten Spannungsquellenanschluß (13) verbundenen Emitter hat; einen dritten Widerstand (R7), der zwischen dem Basisverbindungsknoten des dritten und vierten Transistors (Q7 und Q6) und dem zweiten Spannungsquellenanschluß (13) verbunden ist.

10 6. Audioausgangsverstärker nach Anspruch 1, dadurch gekennzeichnet, daß die Verstärkereinrichtung (26) aufweist: einen Differenzverstärkerabschnitt (28) mit einem mit dem Audiosignaleingangsanschluß (14) verbundenen Eingangsanschluß; eine erste Stromquelle (Q9), die durch eine von der Vorspanneinrichtung erzeugte Vorspannung gesteuert ist und einen Betriebsstrom zu dem Differenzverstärkerabschnitt (28) speist; einen Voransteuerabschnitt (29), der verbunden ist, um ein verstärktes Audiosignal zu empfangen, das von dem Differenzverstärkerabschnitt (28) zugespeist ist; eine zweite Stromquelle (Q12), die durch eine von der Vorspanneinrichtung erzeugte Vorspannung gesteuert ist und einen Betriebsstrom zu dem Voransteuerabschnitt (29) und der Überstromdetektoreinrichtung (27) speist; einen Ausgangsstufenverstärkerabschnitt (31), der durch ein Ausgangssignal von dem Voransteuerabschnitt (29) angesteuert ist; und einen Gegenkopplungskreis (30) zum Rückkoppeln eines Audiosignales von dem Signalausgangsanschluß (17) zu dem anderen Eingangsanschluß des Differenzverstärkerabschnittes (28).

25 7. Audioausgangsverstärker nach Anspruch 6, dadurch gekennzeichnet, daß der Differenzverstärkerabschnitt (28) aufweist: einen ersten Transistor (Q14) eines ersten Leittfähigkeitstyps, der einen mit dem zweiten Spannungsquellenanschluß (13) verbundenen Emitter hat; einen zweiten Transistor (Q15) des ersten Leittfähigkeitstyps, der einen mit dem zweiten Spannungsquellenanschluß (13) verbundenen Emitter und eine mit der Basis des ersten Transistors (Q14) verbundene Basis hat; einen dritten Transistor (Q10) eines zweiten Leittfähigkeitstyps, der einen mit dem Kollektor des ersten Transistors (Q14) und dem Eingangsanschluß des Voransteuerabschnittes (29) verbundenen Kollektor und eine mit dem Audiosignaleingangsanschluß (14) verbundene Basis hat; und einen vierten Transistor (Q11) des zweiten Leittfähigkeitstyps, der einen mit dem Kollektor des zweiten Transistors (Q15) und dem Basisverbindungsknoten des ersten und des zweiten Transistors (Q14 und Q15) verbundenen Kollektor, eine mit dem Gegenkopplungskreis (30) verbundene Basis und einen mit dem Emitter des dritten Transistors (Q10) und der ersten Stromquelle (Q9) verbundenen Emitter hat.

40 8. Audioausgangsverstärker nach Anspruch 6, dadurch gekennzeichnet, daß der Voransteuerabschnitt aufweist: einen Transistor (Q16), der eine mit dem Ausgangsanschluß des Differenzverstärkerabschnittes (28) verbundene Basis und einen mit dem zweiten Spannungsquellenanschluß (13) verbundenen Emitter hat; eine erste Diode (D5) mit einer mit dem Kollektor des Transistors (Q16) und dem ersten Eingangsanschluß des Ausgangsstufenverstärkerabschnittes (31) verbundenen Kathode und eine zweite Diode (D4) mit einer mit der Anode der ersten Diode (D5) verbundenen Kathode und einer mit dem zweiten Eingangsanschluß des Ausgangsstufenverstärkerabschnittes (31), dem Eingangsanschluß der Überstromdetektoreinrichtung (27) und der zweiten Stromquelle (Q12) verbundenen Anode.

50 9. Audioausgangsverstärker nach Anspruch 6, dadurch gekennzeichnet, daß der Ausgangsstufenverstärkerabschnitt aufweist: einen ersten Transistor (Q17) eines ersten Leittfähigkeitstyps, der einen mit dem ersten Spannungsquellenanschluß (12) verbundenen Kollektor, eine mit dem ersten Ausgangsanschluß des Voransteuerabschnittes (29) verbundene Basis und einen mit dem Signalausgangsanschluß (17) verbundenen Emitter hat, und einen zweiten Transistor (Q13) eines zweiten Leittfähigkeitstyps, der einen mit dem Signalausgangsanschluß (17) verbundenen Emitter, eine mit dem zweiten Ausgangsanschluß des Voransteuerabschnittes (29) verbundene Basis und einen mit dem zweiten Spannungsquellenanschluß (13) verbundenen Kollektor hat.

55 10. Audioausgangsverstärker nach Anspruch 6, dadurch gekennzeichnet, daß der Gegenkopplungskreis (30) aufweist: einen ersten Widerstand (R8), der zwischen dem Ausgangsanschluß (17) des Audioausgangsverstärkers und dem anderen Eingangsanschluß des Differenzverstärkerabschnittes (28) ange-



geschlossen ist, und einen zweiten Widerstand (R9), der zwischen dem anderen Eingangsanschluß des Differenzverstärkerabschnittes (28) und Masse angeschlossen ist.

- 5 11. Audioausgangsverstärker nach Anspruch 1, dadurch gekennzeichnet, daß die Überstromdetektoreinrichtung (27) aufweist: einen ersten Transistor (Q18) eines ersten Leitfähigkeitstyps, der eine mit der Verstärkereinrichtung (26) verbundene Basis hat; einen ersten Widerstand (R10), der mit dem Emitter des ersten Transistors (Q18) und dem Signalausgangsanschluß (17) verbunden ist, eine Diode (D6) mit einer mit dem Kollektor des ersten Transistors (Q18) verbundenen Kathode und einer mit dem ersten Spannungsquellenanschluß (12) verbundenen Anode, und einen zweiten Transistor (Q19) eines zweiten Leitfähigkeitstyps, der eine mit dem Kollektor des ersten Transistors (Q18) verbundene Basis, einen mit dem ersten Spannungsquellenanschluß (12) verbundenen Emitter und einen mit dem Steuereingangsanschluß der Schutzeinrichtung (25) verbundenen Kollektor hat.
- 10 12. Audioausgangsverstärker nach Anspruch 1, weiterhin mit einer Schutzverzögerungsschaltung (32) zum Verzögern eines Ausgangssignales der Bereitschaftseinrichtung (23) und zum Einspeisen des verzögerten Signales in die Schutzeinrichtung (25), wobei die Verzögerungszeit durch die Schutzverzögerungsschaltung (32) länger als diejenige der Verzögerungseinrichtung eingestellt ist.
- 15 13. Audioausgangsverstärker nach Anspruch 12, dadurch gekennzeichnet, daß die Schutzverzögerungseinrichtung (32) aufweist: einen Transistor (Q20) mit einer mit dem Ausgangsanschluß der Bereitschaftseinrichtung (23) verbundenen Basis und einem mit dem ersten Spannungsquellenanschluß (12) verbundenen Emitter, einen ersten und einen zweiten Widerstand (R11 und R12), die in Reihe zwischen dem Kollektor des Transistors (Q20) und dem zweiten Spannungsquellenanschluß (13) liegen, und einen Kondensator (C2), der an einem Ende mit dem Basisverbindungsknoten des ersten und des zweiten Widerstandes (R11 und R12) und dem Eingangsanschluß der Schutzeinrichtung (25) und am anderen Ende mit dem zweiten Spannungsquellenanschluß (13) verbunden ist.
- 20 14. Audioausgangsverstärker nach Anspruch 10, weiterhin mit einem ersten Kondensator (C4), der zwischen dem Signalausgangsanschluß (17) und dem Ausgangsanschluß der Verstärkereinrichtung (26) verbunden ist, einem zweiten Kondensator (C3), der zwischen einem Ende des Widerstandes (R9) des Gegenkopplungskreises (30) und Masse verbunden ist, und einem invertierenden Eingangsanschluß (15), der mit der Verstärkereinrichtung (26) verbunden ist, wobei der zweite Spannungsquellenanschluß (13) mit Masse verbunden ist und der invertierende Eingangsanschluß (15) an eine negative Spannungsquelle (-V) angeschlossen ist.
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Revendications

1. Amplificateur de sortie d'audiofréquences, comprenant :
 - 40 - une première borne (12) d'alimentation connectée afin qu'elle établisse un potentiel d'alimentation (V_{CC}),
 - une seconde borne d'alimentation (13) connectée afin qu'elle soit mise à un potentiel d'alimentation ($-V_{EE}$; GND) inférieur au potentiel d'alimentation (V_{CC}) de la première borne (12) d'alimentation,
 - 45 - une borne (16) d'entrée d'un signal de secours, connectée afin qu'elle reçoive un signal de secours,
 - un dispositif de secours (23) ayant une borne d'entrée connectée à la borne (16) d'entrée de signal de secours et destiné à commuter entre un mode normal de fonctionnement et un mode de secours,
 - un dispositif à retard (R2, R3, C1) destiné à retarder un signal de sortie du dispositif de secours (23),
 - 50 - un dispositif de polarisation (Q3, Q4, R4, D1-D3) commandé en fonction du signal de sortie du dispositif à retard (R2, R3, C1), et
 - un dispositif amplificateur (26) destiné à amplifier un signal d'audiofréquences qui lui est transmis, et dont le courant de fonctionnement est réglé par le dispositif de polarisation (Q3, Q4, R4, D1-D3),
 - 55 caractérisé par :
 - un dispositif (27) de détection d'une surintensité qui circule dans les éléments de sortie (Q17, Q13) du dispositif amplificateur (26), et



- un dispositif (25) de protection du dispositif amplificateur (26) par mise du dispositif de polarisation (Q3, Q4, R4, D1-D3) à l'état de non-fonctionnement lorsqu'une surintensité est détectée par le dispositif (27) de détection de surintensité, et dans lequel :
- l'amplificateur de sortie d'audiofréquences provoque la réduction progressive d'un signal de sortie du dispositif amplificateur (26) et réduit le bruit de commutation lors du passage d'un état de fonctionnement normal à un état de secours par commande du dispositif de polarisation (Q3, Q4, R4, D1-D3) avec un signal de sortie du dispositif à retard (R2, R3, C1), et
- la destruction des éléments de sortie (Q17, Q13) du dispositif amplificateur (26) est empêchée lors du passage d'un état normal de fonctionnement à un état de secours par commande du dispositif de protection (25) par le signal de sortie du dispositif à retard (R2, R3, C1).

2. Amplificateur de sortie d'audiofréquences selon la revendication 1, caractérisé en ce que le dispositif de secours (23) comporte un premier transistor (Q1) d'un premier type de conductivité qui a une base connectée à la borne (16) d'entrée de signal de secours et un émetteur connecté à la seconde borne (13) d'alimentation, une résistance (R1) connectée à une première extrémité à un collecteur du premier transistor (Q1), et un second transistor (Q2) d'un second type de conductivité qui possède une base connectée à l'autre extrémité de la résistance (R1), un émetteur connecté à la première borne (12) d'alimentation et un collecteur connecté à la borne d'entrée du dispositif à retard.

3. Amplificateur de sortie d'audiofréquences selon la revendication 1, caractérisé en ce que le dispositif à retard comprend une première et une seconde résistance (R2 et R3) connectées en série entre la borne de sortie du dispositif de secours (23) et la seconde borne d'alimentation (13), et un condensateur (C1) qui est connecté à une première extrémité au noeud de connexion de la première et de la seconde résistance (R2 et R3) et à la borne d'entrée du dispositif de protection (25) et qui est connecté à l'autre extrémité à la seconde borne d'alimentation (13).

4. Amplificateur de sortie d'audiofréquences selon la revendication 1, caractérisé en ce que le dispositif de polarisation comporte un premier transistor (Q3) d'un premier type de conductivité qui a une base connectée à la borne de sortie du dispositif à retard et un collecteur connecté à la première borne d'alimentation (12), une résistance (R4) connectée à une première extrémité à un émetteur du premier transistor (Q3), une première diode (D1) ayant une anode connectée à l'autre extrémité de la résistance (R4), une seconde diode (D2) ayant une anode connectée à la cathode de la première diode (D1) et une cathode connectée à la seconde borne d'alimentation (13), un second transistor (Q4) du premier type de conductivité qui a une base connectée à l'anode de la seconde diode (D2) et à la borne de sortie du dispositif de protection (25) et un émetteur connecté à la seconde borne d'alimentation (13), et une troisième diode (D3) ayant une anode connectée à la première borne d'alimentation (12) et une cathode connectée au collecteur du second transistor (Q4) et à la borne d'entrée de commande du dispositif amplificateur (26).

5. Amplificateur de sortie d'audiofréquences selon la revendication 1, caractérisé en ce que le dispositif de protection (25) comporte un premier transistor (Q5) du premier type de conductivité qui a une base connectée à une borne de sortie du dispositif à retard et un collecteur connecté à la première borne d'alimentation (12), une première résistance (R5) connectée à une première extrémité à un émetteur du premier transistor (Q5), un second transistor (Q8) d'un second type de conductivité qui a un émetteur connecté à l'autre extrémité de la première résistance (R5), une seconde résistance (R6) connectée entre la base et l'émetteur du second transistor (Q8), un troisième transistor (Q7) du premier type de conductivité, ayant une base connectée au collecteur du second transistor (Q8), un collecteur connecté à la base du second transistor (Q8) et un émetteur connecté à la seconde borne d'alimentation (13), un quatrième transistor (Q6) du premier type de conductivité qui a une base connectée à la base du troisième transistor (Q7) et à la borne de sortie du dispositif (27) de détection de surintensité, un collecteur connecté au dispositif de polarisation et un émetteur connecté à la seconde borne d'alimentation (13), et une troisième résistance (R7) connectée entre le noeud de connexion des bases du troisième et du quatrième transistor (Q7 et Q6) et la seconde borne d'alimentation (13).

6. Amplificateur de sortie d'audiofréquences selon la revendication 1, caractérisé en ce que le dispositif amplificateur (26) comporte une section (28) d'amplificateur différentiel ayant une première borne d'entrée connectée à la borne d'entrée (14) de signal d'audiofréquences, une première source de courant (Q9) commandée par une tension de polarisation créée par le dispositif de polarisation et



transmettant un courant de fonctionnement à la section (28) d'amplificateur différentiel, une section (29) de pilotage préalable connectée afin qu'elle reçoive un signal d'audiofréquences amplifié transmis par la section (28) d'amplificateur différentiel, une seconde source de courant (Q12) commandée par une tension de polarisation créée par le dispositif de polarisation et transmettant un courant de fonctionnement à la section (29) de pilotage préalable et au dispositif (27) de détection de surintensité, une section (31) d'amplificateur d'étage de sortie pilotée par un signal de sortie de la section (29) de pilotage préalable, et un circuit (30) à rétroaction négative destiné à renvoyer un signal d'audiofréquences de la borne (17) de sortie de signal à l'autre borne d'entrée de la section (28) d'amplificateur différentiel.

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7. Amplificateur de sortie d'audiofréquences selon la revendication 6, caractérisé en ce que la section (28) d'amplificateur différentiel comporte un premier transistor (Q14) d'un premier type de conductivité qui a un émetteur connecté à la seconde borne d'alimentation (13), un second transistor (Q15) du premier type de conductivité qui a un émetteur connecté à la seconde borne d'alimentation (13) et une base connectée à la base du premier transistor (Q14), un troisième transistor (Q10) d'un second type de conductivité qui a un collecteur connecté au collecteur du premier transistor (Q14) et à la borne d'entrée de la section (29) de pilotage préalable et une base connectée à la borne (14) d'entrée de signal d'audiofréquences, et un quatrième transistor (Q11) du second type de conductivité qui a un collecteur connecté au collecteur du second transistor (Q15) et au noeud de connexion des bases du premier et du second transistor (Q14 et Q15), une base connectée au circuit (30) de rétroaction négative et un émetteur connecté à l'émetteur du troisième transistor (Q10) et à la première source de courant (Q9).

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8. Amplificateur de sortie d'audiofréquences selon la revendication 6, caractérisé en ce que la section (29) de pilotage préalable comporte un transistor (Q16) qui a une base connectée à la borne de sortie de la section (28) d'amplificateur différentiel et un émetteur connecté à la seconde borne d'alimentation (13), une première diode (D5) ayant une cathode connectée au collecteur du transistor (Q16) et à la première borne d'entrée de la section (31) d'amplificateur d'étage de sortie, et une seconde diode (D4) ayant une cathode connectée à l'anode de la première diode (D5) et une anode connectée à la seconde borne d'entrée de la section (31) d'amplificateur d'étage de sortie, à la borne d'entrée du dispositif (27) de détection de surintensité et à la seconde source de courant (Q12).

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9. Amplificateur de sortie d'audiofréquences selon la revendication 6, caractérisé en ce que la section (31) d'amplificateur d'étage de sortie comporte un premier transistor (Q17) d'un premier type de conductivité qui a un collecteur connecté à la première borne d'alimentation (12), une base connectée à la première borne de sortie de la section (29) de pilotage préalable et un émetteur connecté à la borne (17) de sortie de signaux, et un second transistor (Q13) d'un second type de conductivité qui a un émetteur connecté à la borne (17) de sortie de signaux, une base connectée à la seconde borne de sortie de la section (29) de pilotage préalable, et un collecteur connecté à la seconde borne d'alimentation (13).

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10. Amplificateur de sortie d'audiofréquences selon la revendication 6, caractérisé en ce que le circuit de rétroaction négative (30) comporte une première résistance (R8) connectée entre la borne de sortie (17) de l'amplificateur de sortie d'audiofréquences et l'autre borne d'entrée de la section (28) d'amplificateur différentiel, et une seconde résistance (R9) connectée entre l'autre borne d'entrée de la section (28) d'amplificateur différentiel et la masse.

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11. Amplificateur de sortie d'audiofréquences selon la revendication 1, caractérisé en ce que le dispositif (27) de détection de surintensité comporte un premier transistor (Q18) d'un premier type de conductivité qui a une base connectée au dispositif amplificateur (26), une première résistance (R10) connectée entre l'émetteur du premier transistor (Q18) et la borne (17) de sortie de signal, une diode (D6) ayant une cathode connectée au collecteur du premier transistor (Q18) et une anode connectée à la première borne d'alimentation (12), et un second transistor (Q19) d'un second type de conductivité qui a une base connectée au collecteur du premier transistor (Q18), un émetteur connecté à la première borne d'alimentation (12) et un collecteur connecté à la borne d'entrée de commande du dispositif de protection (25).

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12. Amplificateur de sortie d'audiofréquences selon la revendication 1, comprenant en outre un circuit à



retard (32) de protection destiné à retarder un signal de sortie du dispositif de secours (23) et à transmettre le signal retardé au dispositif de protection (25), le temps de retard du circuit (32) à retard de protection étant réglé à une valeur supérieure à celle du dispositif à retard.

5 13. Amplificateur de sortie d'audiofréquences selon la revendication 12, caractérisé en ce que le dispositif (32) à retard de protection comporte un transistor (Q20) qui a une base connectée à la borne de sortie du dispositif de secours (23) et un émetteur connecté à la première borne d'alimentation (12), une première et une seconde résistance (R11 et R12) connectées en série entre le collecteur du transistor (Q20) et la seconde borne d'alimentation (13), et un condensateur (C2) connecté à une première
10 extrémité au noeud de connexion de base de la première et de la seconde résistance (R11 et R12) et à la borne d'entrée du dispositif de protection (25) et à l'autre extrémité à la seconde borne d'alimentation (13).

15 14. Amplificateur de sortie d'audiofréquences selon la revendication 10, comprenant en outre un premier condensateur (C4) connecté entre la borne (17) de sortie de signaux et la borne de sortie du dispositif amplificateur (26), un second condensateur (C3) connecté entre une première extrémité de la résistance (R9) du circuit de rétroaction négative (30) et la masse, et une borne (15) d'entrée d'inversion connectée au dispositif amplificateur (26), et dans lequel la seconde borne d'alimentation (13) est connectée à la masse (GND) et la borne d'entrée d'inversion (15) est connectée à une source de
20 tension négative (-V).