

LIQUID EJECTING PRINTING HEAD, PRODUCTION METHOD  
THEREOF AND PRODUCTION METHOD FOR BASE BODY  
EMPLOYED FOR LIQUID EJECTING PRINTING HEAD

BACKGROUND OF THE INVENTION



\*166166\*



\*G00002\*

Field of the Invention

5       The present invention relates to a production  
method for a base body for a liquid ejecting printing  
head (hereinafter simply referred to as "printing  
head"), in which an electrothermal transducer and  
printing functional elements are formed on a  
10   substrate, and a production method for a printing head  
employing the base body for the printing head, and  
more particularly to a production method for a  
printing head employing the base body for a printing  
head to be employed in an ink-jet printing apparatus  
15   adapted to be used in copy machine, facsimile,  
wordprocessor, printer as output device of host  
computer, video output printer and so forth.

Description of the Related Art

20

Conventionally, the printing head is constructed  
by forming an electrothermal transducer element on a  
monocrystalline substrate, arranging a functional  
element for driving the electrothermal transducer

- 2 -

element, a transistor array and so forth, outside of the silicon substrate, as a driver circuit for the electrothermal transducer element and connecting between the electrothermal transducer element and the transistor array by means of a flexible cable or wired bonding and so forth.

For the purpose of simplification of construction, reducing faulty product to be caused during production process and improvement for uniformity and reproductivity of characteristics of respective elements to be considered in head construction, there has been known an ink-jet printing apparatus having a printing head, in which the electrothermal transducer element and the functional element are formed on a common substrate, have been proposed in Japanese Patent Application Laid-open No. 72867/1982.

Fig. 1 is a section showing a part of the base body for the printing head constructed as set forth above. In Fig. 1, a reference numeral 1801 denotes a semiconductor substrate of monocrystalline silicon. 1804 denotes an N-type semiconductor epitaxial region, 1811 denotes an ohmic contact region of an N-type semiconductor with high impurity concentration. 1805 denotes a P-type semiconductor base region, and 1810 denotes an emitter region of a high impurity

concentration N-type semiconductor. These region  
forms a bipolar transistor. 1816 denotes a silicon  
oxide layer as a heat accumulation layer and an  
interlayer insulation layer. 1817 denotes a heat  
5 generating resistor layer, 1818 denotes a wiring  
electrode of aluminum (Al), 1819 denotes a silicon  
oxide layer as a protective layer, 1812 denotes a  
base-collector common electrode of Al and 1820 denotes  
a Ta layer as a protective layer. These form the base  
10 body for the printing head including the  
electrothermal transducer. Here, 1822 denotes a heat  
generating portion. The printing head is constructed  
by forming an upper plate and a liquid passage on the  
base body constructed set forth above.

15 On the other hand, while the construction set  
forth above is superior, there still exist a room for  
improvement in satisfying high speed driving, energy  
saving, high package density, low cost, high  
reliability strongly demanded for the recent printing  
20 apparatus.

At first, it is required to provide highly  
reliable printing head at low price. For achieving  
this, it becomes necessary to produce the printing  
head at satisfactorily high yield.

25 Namely, conventional interlayer insulation layer

1816 and the protective layer 1819 and so forth are formed by depositing BPSG, SiO, SiO<sub>2</sub>, SiON, SiN and so forth at 300 to 450 °C employing layer forming technology, such as normal pressure CVD, PE-CVD and so forth. However, in such temperature, wiring of Al or so forth or electrode or so forth causes a bunno shaped bulge (often in the extent of 2 μm in height and diameter) of Al or so forth called as hillock layer deposited (grown) by plasma CVD method and sputtering method, as shown in Fig. 2, for example, and grown. Then, by unevenness of the hillock 1101 and 1102, shorting is caused between wiring electrodes and between wiring and the protective layer of Ta (see protective layer 1820 shown in Fig. 1, for example) to result in operation failure to lower yield in production.

Therefore, it is a belief of the inventors that improvement of yield in production of the base body can be achieved by restricting growth of hillock in layer deposition by plasma CVD method and sputtering method.

#### SUMMARY OF THE INVENTION

Therefore, it is an object of the present

invention to solve the above-mentioned technical problem and thus to provide a production method of a base body for a highly reliable printing head and the printing head at low cost and high yield.

5       A protection method of a base body for a liquid ejecting printing head, according to the present invention, including an electrothermal transducer element for generating a thermal energy to be used in liquid ejection, a driving functional element driving  
10 the electrothermal transducer element, a plurality of wiring electrodes for connecting the driving functional element and the electrothermal transducer element, is characterized in that the protective layer is formed by depositing an insulative material over  
15 the electrothermal transducer element or the wiring electrode with elevating a temperature of the base body.

In such case, the base body temperature at a low temperature in the foregoing step is in a range of 200  
20 °C to 300 °C and at a high temperature is in a range of 350 °C to 400 °C. Further preferably, the base temperature at the low temperature is 300 °C and the base body temperature at high temperature is 350 °C.

On the other hand, the protective later is  
25 selected among SiN, SiO, SiO<sub>2</sub>, SiON, PSG, BSG, BPSG,

ZrO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, SiC, Si and Ta<sub>2</sub>O<sub>5</sub>. It should be noted that the materials of the protective layer formed at low temperature and the protective layer formed at high temperature are not necessarily the same. The protective layer formed at low temperature and the protective layer formed at high temperature are formed as two layer protective layer by switching the base body temperature. The two layer protective layer may be formed with various combinations of the insulative material listed above.

A production method of a liquid ejecting printing head having a base body for the liquid ejecting printing head, according to the present invention including electrothermal transducer element and a driving functional element for driving the electrothermal transducer element, is characterized by forming a P-type semiconductor layer by epitaxial growth on a P-type semiconductor substrate, and subsequently forming the driving functional element utilizing the P-type semiconductor.

A production method of a liquid ejecting printing head, according to the present invention, including a base body preparation process preparing a liquid ejecting printing head, in which an electrothermal transducer element, a driving functional element

driving the electrothermal transducer element, a wiring electrode connecting the driving functional element and the electrothermal transducer element, a protective layer provided on the wiring electrode are formed on a substrate, and an ink ejecting portion forming step for forming ejecting portion having ejection opening for ejecting an ink, is characterized in that the production method of a base body for the liquid ejecting printing head includes a deposition step for forming the protective layer by depositing an insulative material on the wiring electrode with elevating a base body temperature in stepwise fashion or sequentially.

When the electrothermal transducer element has a head generating resistor made of TaN, composition of TaN is to contain 1.9 to 1.0 of Ta relative to N in molecular weight ratio. The heat generating resistor may be made of HfB<sub>2</sub>, Poly-Si, Ta-Al, Ta-Ir, Au or Ag in place of TaN.

With the production method of the base body according to the present invention, the base body for the ink-jet printing head which is superior in durability, strong against repeatedly applied thermal impact, ink corrosion or cavitation, and can provide high quality printing image for a long period, can be

efficiently produced.

Also, with to the production method of the printing head according to the present invention, since the protective layer formed at low temperature is inserted, occurrence and growth of buno-shaped projection called as hillock during deposition (growth) of the layer by CVD method at high temperature, can be successfully prevented. Therefore, shorting between the wiring electrode or between the wiring and the protective layer of Ta due to unevenness due to hillocks 1101, 1102 as shown in Fig. 2, operation failure to cause lowering of production yield can be avoided. As a result, the printing head can be produced at high yield and thus highly reliable printing head can be provided at low price.

The above and the other effects, features and advantages of the present invention will become more apparent from the following descriptions of the embodiments thereof taken in conjunction with the accompanying drawings.

## BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a diagrammatic section showing one example of a base body for a printing head according to the present invention;

Fig. 2 is a diagrammatic section showing hillock and whisker on Al electrode produced by heating upon deposition of a protective layer;

Fig. 3 is a diagrammatic section showing a base body for an ink-jet printing head;

Fig. 4 is a diagrammatic section showing a layer depositing apparatus for forming respective layers of a base body used in the ink-jet printing head according to the invention;

Fig. 5 is a diagrammatic view showing a PE-CVD apparatus for forming a protective layer on a base body;

Fig. 6 is a graph illustrating a relationship between a substrate temperature and a breakdown voltage ratio;

Fig. 7 is a graph illustrating a relationship between an elapsed period from initiation of layer deposition in two stage layer deposition, layer thickness and a furnace temperature;

2 JUL 2002

Fig. 8 is a diagrammatic section showing a configuration of a wiring electrode;

Fig. 9 is a diagrammatic front elevation showing a configuration of the wiring electrode;

5 Fig. 10 is a diagrammatic section of the wiring electrode and the heat acting portion;

Fig. 11 is a diagrammatic front elevation showing a configuration of the wiring electrode;

10 Fig. 12 is a diagrammatic perspective view showing inside of an ink-jet printing head;

Fig. 13 is a diagrammatic illustration explaining driving method of a base body for an ink-jet printing head;

15 Fig. 14 is a diagrammatic perspective view showing the ink-jet printing head;

Fig. 15 is a diagrammatic section showing the ink-jet printing head;

20 Fig. 16 is a diagrammatic section longitudinally cutting a major element of a base body for an ink-jet printing head according to the invention;

Fig. 17 is a diagrammatic perspective view showing one example of an ink-jet printing apparatus employing a printing head according to the invention;

Fig. 18 is a graph illustrating a result of SST test;

Fig. 19 is a graph illustrating a result of CST test; and

5        Fig. 20 is a graph illustrating a result of printing durability test.

#### DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

10        The followings are experiments performed by the inventors.

##### [Experiment A]

Above a heating resistor body provided a heating resistor body shown in Fig. 3 and on an electrode  
15 provided below a region at least in the printing head, where ink flows or retained, a protective layer is normally provided. The protective layer serves for chemically and physically protecting a heating resistor body forming these electrode and head acting  
20 portion from the ink at the upper side for preventing shorting between the electrodes and leakage between the electrodes of the same kinds, particularly between selection electrodes and for further preventing contact between the ink and the electrode and

corrosion of the electrode which can be caused by applying power to the electrode contacting with the ink.

Required property of the protective layers are  
5 difference depending upon the position to be placed.  
For example, on the heat acting portion, for example,  
the protective layer is required high (I) heat  
resistance, (II) ink proofing property, (III) ink  
penetration resistance, (IV) heat conductivity, (V)  
10 anti-oxidation property, (VI) insulation ability and  
(VII) resistance to damage. In the region other than  
the heat acting portion, thermal condition is reduced,  
higher ink penetration resistance, ink proofing  
property, insulation ability and fracture resistance  
15 are required.

However, at the present, there have not been found  
a material for the protective layer which can satisfy  
all of the required properties of (I) to (VII) at  
respective desired level and can cover all of the heat  
20 acting portion and the electrode with a single layer.  
In this circumstance, in the practical printing heads,  
various materials which may mutually compensate  
properties required at respective portion to be  
placed, are selected to form the protective layer  
25 consisted of a plurality of layers. For such

protective layer of multi-layer structure, it is required to maintain sufficient bonding strength not only between the constituent layers but also with the adjacent layers, and not to cause failure due to lowering bonding force, such as abrasion or lift between the layers during production process of the printing head and over a practically use period.

Apart from this, in case of a multi-orifice type ink-jet printing head, a plurality of fine electrothermal transducer are formed simultaneously on the substrate, formation of respective layer and partial removal of the formed layer is repeated on the substrate in the production process. Thus, in the stage for forming the protective layer, the back surface of the portion where the protective layer is formed, fine unevenness with slapwedge portion (stepped portion), step coverage ability of the protective layer at the stepped portion becomes important. When step coverage is poor, penetration of the ink can be caused at this portion to be cause of stray current corrosion or electric breakdown. On the other hand, when possibility of causing defective portion in the formed protective layer is high in the production method, the ink may penetrate through the defective portion to frequently cause significant

shortening of the life of the electrothermal transducer.

In these reason, the protective layer is further required to have high step coverage, low possibility  
5 of occurrence of defective portion, such as pin hole, in the formed protective layer due to the production method thereof. Even if the defect ius caused, the defect has to be ignorable or lesser.

Particularly on the heat acting surface, severe  
10 temperature variation cycle between high temperature and low temperature is repeated for several thousands times per one second. Also, the ink on the heat acting surface is evaporated during high temperature period to generate bubble in the ink to elevate the  
15 pressure within an ink passage, and associating with lowering of temperature, the evaporated ink is condensed to eliminate the bubble to lower the pressure in the ink passage. Such pressure variation is repeated to constantly apply mechanical stress  
20 caused by repeated heat cycle. Therefore, on the protective layer provided for covering at least the upper surface of the heat acting portion, it is particularly required to have high impact resistance against mechanical stress and bonding strength between  
25 a plurality of layers consisting protective layer.

Therefore, experiment is performed with respect to breakage strength of the heat generating resistor body upon formation of the layer by varying layer formation temperature of SiN protective layer at the mid-way of  
5 layer formation by plasma CVD method.

The heat generating resistor was prepared by forming layer of  $\text{TaN}_{0.8\text{hex}}$  in reactive sputtering method according to the present invention. The layer forming condition is 24% in nitrogen gas pressure,  
10 total pressure of argon gas and nitrogen gas at 7.5 mTorr, sputtering power in 2 kW, and the substrate temperature of 200 °C. A layer formation apparatus is schematically illustrated in Fig. 4.

In Fig. 4, the reference numeral 301 denotes a  
15 tantalum target. The tantalum target 301 is provided on a flat plate form magnet 302. At a position opposing to the tantalum target 301, a substrate holder 303 holding a substrate 304 is arranged. The substrate 304 is constructed to heat at the  
20 predetermined temperature via the substrate holder 303 by a heater 305 mounted on the substrate holder 303. The substrate 304 side and the target 301 side are connected by a DC power source 306. BY application of the power source 306, a predetermined potential  
25 difference is established between the substrate 304

side and the target 301 side. The target 301, the substrate 304 and the power source 306 are housed within a chamber 309 and arranged therein. The interior space of the chamber 309 is situated in  
5 vacuum condition, and a predetermined mixture gas is fed into the chamber 309 from an introduction opening 310. As this mixture gas, a mixture gas of argon (Ar) and nitrogen (N<sub>2</sub>) can be considered, for example. On the other hand, within the chamber 309, a shutter 311  
10 for opening and closing in front of the target 301 is provided. The shutter 311 can be used effectively for controlling layer thickness of the layer on the substrate 304.

Lower heat accumulation layers 102 and 103 are  
15 respectively SiO<sub>2</sub> layers formed by way of thermal oxidation or layers, in which Ta layers 107 as cavitation resistant layers are formed above upper SiN protective layer 106. In formation of the protective layer, a plasma CVD apparatus as schematically shown  
20 in Fig. 5 was used.

In Fig. 5, a wafer 901 was mounted on an electrode 902 consisted of carbon. The entire electrode was arranged within a quartz cylinder. A heater 904 is designed for heating the overall quartz cylinder.  
25 Thus, the wafer and the electrode within the quartz

cylinder was heater to a given temperature. The interior of the quartz cylinder was ventilated by a pump. With introducing a material gas into the quartz cylinder, an RF voltage of 420 kHz was applied to an  
5 opposing carbon electrode tube to generate plasma between the wafer and the electrode tube to deposit the protective layer on the wafer 901 in the thickness of the range thicker greater than or equal to  $0.6\text{ }\mu\text{m}$  and less than or equal to  $1.0\text{ }\mu\text{m}$ .

10 In this experiments, other layer depositing conditions are set as follows depending upon the layer formation temperature. At the layer formation temperature lower than  $300\text{ }^{\circ}\text{C}$ ,  $\text{SiH}_2$  gas was 800 SCCM,  $\text{NH}_3$  gas was 7200 SCCM and pressure was 1.5 Torr. On  
15 the other hand, at the layer formation temperature higher than or equal to  $300\text{ }^{\circ}\text{C}$ ,  $\text{SiH}_4$  gas was 600 SCCM,  $\text{NH}_3$  gas was 4800 SCCM and pressure was 2.0 Torr.

Fig. 6 shows a breakdown voltage ratio  $K_b$  ( $K_b = V_b/V_{th}$ ) of a heat generating body in relation to the  
20 layer formation temperature of the protective layer  $\text{SiN}$  as a result of the experiments set forth above.

An actual drive voltage of the printing head is  $1.2 V_{th}$  (1.2 times of a threshold voltage for bubbling). In view of individual fluctuation, no  
25 problem will be arisen if  $K_b$  is greater than or equal

to 1.3, and the layer obtained at the layer formation temperature higher than or equal to 150 °C may be used as the printing head. Also, it was found that the layer formation temperature higher than or equal to  
5 200 °C is preferred in order to enhance reliability. Also, at the layer formation temperature higher than or equal to 300 °C, highly reliable heat generating body having Kb value greater than or equal to 1.8, could be obtained.

10. These layer formation temperature dependency is considered that, in the low temperature range, reaction of the material gas becomes insufficient to remain a large amount of non-reacted Si-H, N-H and so forth in the later to make the density of the layer  
15 low, and to make coupling force of the layer forming molecule insufficient.

At the layer formation temperature higher than or equal to 350 °C, TaN<sub>0.8hex</sub> layer was covered with dense and solid SiN layer for restricting change of property  
20 of the TaN<sub>0.8hex</sub> layer. Thus, the ink-jet printing head with high reliability could be obtained.

[Experiment B]

Next, study was made for influence for wiring portion on the base layer during formation of the  
25 protective layer 106 in the layer structure shown in

Fig. 3.

In the conventional layer structure shown in Fig. 3, after formation of wiring 105 of Al or Al alloy, the protective layer 108 having a thickness in the range greater than or equal to 0.6  $\mu\text{m}$  and less than or equal to 1.0  $\mu\text{m}$ . As the protective layer and the interlayer insulation layer, PSG, BPSG, SiO, SiO<sub>2</sub>, SiON and SiN layers are formed at a temperature in a range of higher than or equal to 300 °C and lower than or equal to 450 °C, by way of normal pressure CVD, plasma CVD or so forth.

In the conventional technology, a bulge in the order of greater than or equal to 1  $\mu\text{m}$  and less than or equal to 2  $\mu\text{m}$ , which is called as hillock 1101 by heating during formation of the protective layer, as is well known. Also, projection reaching several  $\mu\text{m}$  or more, called as whisker 1102 is also caused. If hillock 1101 and/or whisker 1102 are caused, failure of coverage is caused in the protective layer. Furthermore, the cavitation resistant layer Ta formed above and Al wiring may cause electrical shorting to result in operation failure. Size and density of the hillock 1101 and the whisker 1102 significantly affect for reliability and yield in production of the ink-jet printing apparatus.

In this experiments, with respect to the SiN protective layer in the former experiments set forth above, study was made for a relationship between the layer formation temperature and Al hillock, Al whisker and layer quality of the protective layer. The result is shown in the following table 1.

In the table 1, respective value of 100 °C to 450 °C in the column of the layer formation temperature represent that the layer is deposited at constant temperature and a given period. In the column of the hillock and whisker restriction, a mark "X" represents substantial growth of the hillock or whisker being observed, a mark "Δ" represents slight growth of the hillock or whisker being observed and a mark "O" represents little growth of hillock or whisker being observed. On the other hand, in the column of the layer quality, × represents particularly low density, Δ represents slightly low density and O represents high density.

TABLE 1

| SAMPLE NO. | LAYER<br>FORMATION<br>TEMP. (°C) | RESTRICTION<br>OF HILLOCK<br>OR WHISKER | LAYER<br>QUALITY |
|------------|----------------------------------|-----------------------------------------|------------------|
| 1          | 100                              | ○                                       | ×                |
| 2          | 150                              | ○                                       | Δ                |
| 3          | 200                              | ○                                       | Δ                |
| 4          | 250                              | ○                                       | Δ                |
| 5          | 300                              | ○                                       | Δ                |
| 6          | 350                              | Δ                                       | ○                |
| 7          | 400                              | ×                                       | ○                |
| 8          | 450                              | ×                                       | ○                |

From the foregoing table 1, it has been found that  
5 when layer deposition is performed at higher than or  
equal to 100 °C to lower than or equal to 300 °C, the  
hillock or whisker does not grow significantly.  
However, the layer deposited and formed at low  
temperature is relative "loose" in the layer quality  
10 to cause lowering of the Kb value and degradation of  
reliability of the base body and the printing head  
employing it. On the other hand, at the temperature

lower than or equal to 150 °C, difficulty should be arisen for controlling temperature in view of the construction of the CVD apparatus. Accordingly, the preferred layer formation temperature to obtain the  
5 SiN protective layer having relatively high density in the layer quality with restricting growth of hillock and whisker in the Al wiring is found in a range of higher than or equal to 200 °C to lower than or equal to 300 °C.

10 [Experiment C]

Next, layer deposition is performed by separating into two stages and varying layer formation temperature in deposition of the layer.

The first stage of layer deposition was performed  
15 at the layer formation temperature of 200 °C, 250 °C and 300 °C, at which effect of restriction of occurrence of hillock and whisker was found from the result of the table 1. The layer formation apparatus and layer forming condition other than layer formation  
20 temperature is the same as the experiment B. Evaluation was performed in the similar manner to the above. The results of the experiment C is shown in the following table 2.

In the following table 2, the indication of layer  
25 formation temperature 200 - 350 represents that layer

deposition in a layer thickness of approximately 1500 Å was performed at 200 °C, and thereafter layer deposition in a layer thickness greater than or equal to 4500 Å and less than or equal to 8500 Å was  
5 performed at 350 °C.

It should be noted that Fig. 7 is a graph illustrating a relationship between an elapsed time from initiation of layer deposition in two steps layer formation, and a layer thickness and a furnace  
10 temperature. In the example of Fig. 7, the initial growth temperature was set at 200 °C upon initiation of layer deposition, the deposition temperature was risen gradually, the temperature at the later stage of the growth of layer deposition was set at 350 °C and  
15 then the deposition temperature was maintained at constant to continue deposition. At this time, while the layer thickness is increased at substantially the constant rate from initiation of deposition, the protective layer at the initial stage of deposition  
20 has lower density in comparison with the protective layer formed at the later stage of deposition where the layer formation temperature is higher than that in the initial stage. The density is increased according to elevating of the deposition temperature.

TABLE 2

| SAMPLE NO. | LAYER FORMATION<br>TEMP. (°C) | RESTRICTION OF<br>HILLOCK OR<br>WHISKER |
|------------|-------------------------------|-----------------------------------------|
| 1          | 200-350                       | O                                       |
| 2          | 200-400                       | Δ                                       |
| 3          | 200-450                       | ×                                       |
| 4          | 200-350                       | O                                       |
| 5          | 250-400                       | Δ                                       |
| 6          | 250-450                       | ×                                       |
| 7          | 300-350                       | O                                       |
| 8          | 300-400                       | Δ                                       |
| 9          | 300-450                       | ×                                       |

In the two steps layer deposition set forth above,  
5 remarkable restriction of occurrence of hillock and/or  
whisker could be achieved in the layer formation  
temperature of higher than or equal to 200 °C to lower  
than or equal to 300 °C in the first stage and in the  
layer formation temperature of higher than or equal to  
10 350 °C to lower than or equal to 400 °C in the first

stage. The layer quality was high density and solid. Thus, highly reliable protective layer can be obtained.

This is because that upon layer formation of the  
5 high density layer at higher layer formation  
temperature at the second stage, the layer of the  
first stage formed at lower layer formation  
temperature than that in the second stage may depress  
the Al wiring against local stress caused in the Al  
10 wiring. Thus, with the process as set forth above,  
growth of the hillock and/or whisker can be  
successfully restricted.

In the shown experiments, a hot wall type plasma  
CVD apparatus in which overall reaction chamber can be  
15 heated, was employed for multi-number batch type and  
whereby superior in applicability for mass-production.  
However, a batch process type having parallel flat  
electrodes or cold wall type individual piece  
processing type, in which a substrate support  
20 (susceptor) mounting the substrate is heated, may also  
be employed.

The protective layer is not limited to SiN layer  
but can be SiO<sub>2</sub> layer, SiON layer, SiO layer, SiC  
layer, Si layer, PSG layer, PSG layer, BPSG layer, ZrO<sub>2</sub>  
25 layer, Al<sub>2</sub>O<sub>3</sub> layer, Ta<sub>2</sub>O<sub>5</sub> layer or layer formed by way

of normal pressure CVD method or sputtering method. Also, it is further possible to be two stage layer deposition with the combination of the above.

5 The base body for the ink-jet printing head in the shown embodiment is preferred to be formed by performing process at step of forming the layer at relatively low substrate temperature and a step of forming the layer at relatively high substrate temperature.

10 At this time, it is preferred that the substrate temperature in the former step is set in the range of 200 °C to 300 °C, and the substrate temperature in the later step is set in the range of 350 °C to 400 °C. The base body for the ink-jet printing head thus  
15 obtained can restrict hillock phenomenon to be caused in the electrode layer set forth above. The ink-jet printing head employing such base body has quite excellent ink-jet head printing head characteristics.

20 The embodiments of the base body for the ink-jet printing head according to the present invention will be discussed hereinafter.

The base body 100 for the ink-jet printing head generally has head accumulating layers 102 and 103 on the substrate 101. These heat accumulation layers are  
25 provided for efficiently transmitting the energy

caused by application of voltage to the heat generating body. The heat accumulation layer is constructed with a material having low heat conductivity. The heat accumulation layer 103 also  
5 serves as an insulation layer.

Above the heat accumulation layer 103, a resistor layer 104 forming the heat generating body set forth above, the wiring layer 105 formed of a material having high electric conductivity is stacked. The  
10 portion where the wiring layer 105 is not provided, serves as the heat generating resistor.

In the construction set forth above, when an electrical signal is applied to the heat generating resistor via the wiring 105, the heat generating  
15 resistor generates a heat. Also, in the base body for the ink-jet printing head, the protective layer 106 can be provided for the purpose of covering of the wiring 105 and/or the heat generating body. This protective layer 106 contributes for preventing the  
20 heat generating resistor or the wiring 105 from contacting with the ink or stray current corrosion or electrical insulation breakdown due to penetration of the ink. On the protective layer, a cavitation resistant layer 107 is typically provided. The  
25 cavitation resistant layer is provided for the purpose

of protection of the protective layer 106 and the heat  
generating resistor from cavitation caused by  
collapsing of bubble after ink ejection by heating of  
the heat generating resistor, i.e. upon ejection of  
5 the ink.

Concerning heat generating resistor and the base  
body for the ink-jet printing head having layer  
construction, discussion will be given for formation  
of a bipolar type NPN transistor 1821 as driving  
10 function element in the base body on a P-type silicon  
substrate 1801.

Hereinafter, discussion will be given for the  
present invention will reference to the drawings.  
However, the present invention should not be limited  
15 to the shown embodiments and can be any one which can  
achieve the task of the present invention.

Fig. 1 is a diagrammatic section of one embodiment  
of a base body for the printing head to be produced  
according to the present invention.

20 The base body 1800 as the base body for the  
printing head is formed a heat acting portion 1810 as  
electrothermal transducer element and bipolar type NPN  
transistor 1821 as driving function element on the P-  
type silicon substrate 1801.

25 In Fig. 1, 1801 denotes the P-type silicon

2 JUL 2002

substrate, 1802 denotes an N-type collector buried region forming a functional element, 1803 denotes a P-type isolation buried region for functional element isolation, 1804 denotes an N-type epitaxial region, 5 1805 denotes a P-type base region, 1806 denotes a P-type isolation buried region for element isolation, 1807 denotes an N-type collector buried region for forming the functional element, 1808 denotes a high concentration P-type base region for forming the 10 element, 1809 denotes a high concentration P-type isolation region for element isolation, 1810 denotes an N-type emitter for forming element, 1811 denotes a high concentration N-type collector for forming the element, 1812 denotes a collector and base common 15 electrode, 1813 denotes an emitter electrode, and 1814 denotes an isolation electrode. Here, NPN transistor is formed. The collector regions 1802, 1804, 1807 and 1811 completely surround emitter region 1810 and the base regions 1805 and 1808. On the other hand, as the 20 element isolation region, respective cells are surrounded by P-type isolation buried region 1806, P-type isolation region 1807 and high concentration P-type isolation region 1809 for electrical isolation.

Here, NPN transistor 1821 has an NPN transistor 25 structure with two high concentration N-type collector

region 1811 formed on the P-type silicon substrate 1801 via an N-type collector buried region 1802 and N-type collector buried region 1802, two high concentration P-type base region 1808 formed inside of  
5 the high concentration N-type collector region 1811 via the N-type collector buried region 1802 and the P-type base region 1805, and a high concentration N-type emitter region 1810 formed between the high concentration P-type base region 1808 via the N-type  
10 collector buried region 1802 and the P-type base region 1805. Then, the NPN transistor 1821 acts as a diode by connecting the high concentration N-type collector region 1811 and the high concentration base region 12801 via the collector and base common  
15 electrode 1812. Also, adjacent the NPN transistor 1821, the P-type isolation buried region 1803, the P-type isolation region 1806 and high concentration P-type isolation region 1804 as element isolation regions are formed in order. On the other hand, the  
20 resistor layer 1817 is formed on the P-type silicon substrate 1801 via the N-type epitaxial region 1804, the heat accumulation layer 1815 and the interlayer insulation layer 1816 which also serves as the heat accumulation layer integrally provided with the head  
25 accumulation layer 1815. By respectively forming two edges 1818' as connecting end faces by cutting the

wiring electrode 1818 formed on the resistor layer 1817, heat acting portion 1822 is constructed.

The entire surface of the base body 1800 for the printing head is covered with the heat accumulation layer 1815 formed with thermal oxidation layer or so forth. From functional elements, respective electrodes 1812, 1813, 1814 are formed with Al so forth. It should be noted that respective electrodes 1812, 1813 and 1814 have side surfaces (end portions) inclined at an angle  $\theta$  (greater than or equal to  $30^\circ$  and less than or equal to  $75^\circ$ ) relative to the normal are shown in enlarged manner in Figs. 8 and 9 (electrode 1814, emitter, collector and base and so forth are neglected).

The base body 1800 is constructed by covering the P-type silicon substrate 1801 for the printing head having driving portion (functional element) set forth above with the heat accumulation layer 1815 including the collector and base common electrode 1812, the emitter electrode and the isolation electrode 1814. In the upper layer, the interlayer insulation layer 1816 of silicon compound, such as SiO, SiO<sub>2</sub>, SiN, SiON and so forth is formed by normal pressure CVD method, plasma CVD method, sputtering method and so forth. Since Al or so forth forming respective electrodes

1812, 1813, 1814 have inclined end surfaces, step coverage of the interlayer insulation layer is superior to permit to form the interlayer insulation layer 1816 thinner in comparison with the conventional one without degrading heat accumulation effect. By partially opening the interlayer insulation layer 1816, the collector and base common electrode 1812, the emitter electrode 1813 and the isolation electrode 1814 are electrically connected, and on the interlayer insulation layer 1816, the wiring electrode 1818 of Al or so forth for forming the electorial wiring is provided. namely, after partially opening the interlayer insulation layer, the electrothermal transducer element constructed with the resistor layer 1817 constructed with fine polycrystal of  $\text{TaN}_{0.8\text{hex}}$  by reactive sputtering and the wiring electrode 1818 of Al or so forth formed by deposition method or sputtering method, is provided.

Fig. 10 is an enlarged section of the electrothermal transducer, and Fig. 11 is an enlarged plan view of the electrothermal transducer.

The wiring electrode 1818 of Al or so forth has edge portion (and side surface portion) 1818' as connecting end face inclined greater than or equal to 30K relative to the normal. Furthermore, on the heat

acting portion 1822 of the electrothermal transducer element shown in Fig. 1, the protective layer 1820 of SiO, SiO<sub>2</sub>, SiN, SiON, SiC, Si, PSG, BSG, BPSG, ZrO<sub>2</sub> Al<sub>2</sub>O<sub>3</sub>, Ta<sub>2</sub>O<sub>5</sub> and the protective layer 1816 of Ta and so forth are provided integrally with the interlayer insulation layer 1819.

Furthermore, the base body 1800 is formed into a linear tapered shaped configuration of edge portion (or side portion) 1818' (see Fig. 11) of the wiring electrode 1818. The configurations of the edge portion and both sides of the collector and base common electrode 1812, the emitter electrode 1813 and the isolation electrode 1814 are also in linear tapered configuration as shown in Figs. 8 and 12, respectively.

On the other hand, since quite high step coverage can be obtained in the first protective layer 1819, the thickness of the first protective layer 1819 can be made thinner (e.g., greater than or equal to 0.6  $\mu$ m and less than or equal to 1.0  $\mu$ m) than that in the configuration where the edge portion 1818' is right angle. As a result, the thermal energy generated at the heat acting portion 1822 can be effectively and quickly transmitted to the ink. In conjunction therewith, throughput of the apparatus for forming the

first protective layer can be improved to be about double in comparison with the prior art.

Furthermore, upon forming the interlayer insulation layer 1816, the protective layer 1819 and  
5 so forth with SiO, SiON, SiN, SiO<sub>2</sub>, SiC, Si, PSG, BSG, BPSG, ZrO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, TaO<sub>5</sub> and so forth by way of plasma CVD method and sputtering method, the deposition method that the lower layer of the layer is deposited at low temperature in the range higher than or equal  
10 to 200 °C and lower than or equal to 300 °C, and subsequently the upper layer of the layer is deposited at a temperature range higher than or equal to 350 °C and lower than or equal to 400 °C. Namely, growth of the hillock and/or whisker which can be grown during  
15 layer deposition at high temperature, can be effectively restricted by the layer formed at low temperature. In comparison with the case where the layer is deposited at one depositing operation at the constant temperature without varying the layer forming  
20 temperature in several steps during layer formation within the temperature range high than or equal to 250 °C and lower than or equal to 450 °C, shorting due to growth of hillock or whisker can be reduced to significantly improve yield in production. It should  
25 be noted that in the following discussion, for the

electrodes other than wiring electrodes, the edge portion (connecting end surface) will also be referred to as side surface.

Next, discussion will be given for basic operation of the functional element (drive portion) constructed as set forth above.

Fig. 13 is a diagrammatic illustration for explaining the driving method of the base body 1800 shown in Fig. 1.

Here, as shown in Figs. 1 and 13, the collector and base common electrode 1812 correspond to an anode electrode of the diode, the emitter electrode 1813 corresponds to a cathode electrode of the diode. Namely, by applying the positive potential bias (VH1) on the collector and base common electrode 1812, the NPN transistor in a cell (SH1, SH2) is turned ON so that the bias current flows through the emitter electrode 1813 as the collector current and the base current. On the other hand, as a result of construction shorting the base and collector, rising and falling characteristics of the electrothermal transducer element (RH1, RH2) becomes better to improve controllability of causing of film boiling and growth and shrinking of bubble associated therewith to permit stable ink ejection. The reason is considered

2 JUL 2002

that, in the ink-jet printing head utilizing the thermal energy, the transistor characteristics and the film boiling characteristics are closely associated, and small amount of accumulation of minority carrier  
5 in the transistor contribute for quick switching characteristics for improving rising characteristics provides unexpectedly significant effect. On the other hand, parasitic effect is relatively small to eliminate fluctuation between the elements so that  
10 stable drive current can be obtained.

Here, by grounding the isolation electrode 1814, flowing of the charge into the cell can be prevented to avoid a problem of malfunction of other elements.

In such semiconductor device, it is desired that  
15 the concentration of the N-type collector buried region is set to be greater than or equal to  $1 \times 10^{18} \text{ cm}^{-3}$ , the concentration of the P-type base region is set to be greater than or equal to  $5 \times 10^{14} \text{ cm}^{-3}$  and smaller than or equal to  $5 \times 10^{17} \text{ cm}^{-3}$ , the area of the  
20 junction between the high concentration base region 1808 and the electrode is set to be as small as possible. Thus, a leak current flowing from the NPN transistor via the P-type silicon substrate 1801 and the isolation region can be prevented.

25 Further detailed discussion will be given for the

driving method of the base body set forth above,

While only two semiconductor functional elements (cells) are shown in Fig. 13, such functional elements are arranged corresponding to 128 in number of  
5 electrothermal transducer elements, for example, in a given interval, in practical construction and electrical matrix connection is established for permitting block driving. Here, for simplification of disclosure, discussion will be given for driving the  
10 electrothermal transducer elements RH1 and RH2 as two segments in the same group.

In order to drive the electrothermal transducer element RH1, the group is selected by a switching signal G1. In conjunction therewith, the  
15 electrothermal transducer element RH1 is selected by the switching signal S1. Then, the diode cell SH1 in the transistor construction is supplied a positively biased current to cause heating in the electrothermal transducer element RH1. The thermal energy causes  
20 variation of the state in the ink to generate bubble for ejecting ink through ejection opening.

Similarly, when the electrothermal transducer element RH2 is to be driven, the electrothermal transducer element RH2 is selected by the switching  
25 signal G1 and the switching signal S2 to drive the

2 JUL 2002

diode cell SH2 to supply a current to the electrothermal transducer element.

At this time, the P-type silicon substrate 1801 is grounded via the isolation regions 1803 and 1809.

5 Thus, by arranging the isolation regions 1803, 1806 and 1809 in each semiconductor element (cell), malfunction due to electrical interference between respective semiconductor elements can be successfully eliminated.

10 The base body 1800 thus constructed is assembled with an ink passage wall member of photosensitive resin for forming the ink passage 206 communicated with a plurality of ejection openings 207, an upper plate 205 having the ink supply opening 211 to form  
15 the ink-jet printing type printing head 208, as shown in Figs. 14 and 15.

In this case, the ink supplied from the ink supply opening 211 is accumulated in a common liquid chamber 210 therein and supplied to respective ink passages  
20 . 206. At this condition, by driving the heat acting portion of the base body 1800, the ink is ejected through the ink ejecting openings 207.

Next, an example, in which a drive element of a logic circuit or so forth, for example, in place of  
25 the diode array, is provided on the common substrate

to the printing head, will be discussed.

For higher density, higher printed image quality and higher printing speed of the printing apparatus, it is inherently required to increase number of the  
5 ejection openings. An example for eliminating increasing of the wiring connection between the printing head and the printing apparatus and eliminating electrical energy loss to permit efficient driving will be discussed hereinafter.

10 On the substrate which is the same substrate on which the heat generating resistor is formed, a shift transistor having MOS transistor construction and adapted to perform drive signal processing and a power transistor of high voltage bipolar transistor for  
15 heating the heat generating element are included.

These drive elements are formed on the Si substrate in semiconductor technology generally called as Bi-CMOS technology. On the same substrate to the Si substrate, the heat acting portion is formed.

20 Fig. 16 is a diagrammatic section as cut to longitudinally cut the major elements.

To Si substrate 240 as P-type conductor, dopant, such as As or so forth is implanted by ion implantation and diffusion means to form N-type buried  
25 layer 2402. Then, an N-type epitaxial layer 2403 is

formed in a thickness greater than or equal to 5  $\mu\text{m}$  and less than or equal to 10  $\mu\text{m}$  thereover.

On the other hand, by introducing impurity, such as B or so forth in the epitaxial layer 2403, P-type well region 2404 is formed. Subsequently, by photolithography, oxidation diffusion and ion implantation and so forth, doping of impurity is repeated to form P-MOS 2450 in the N-type epitaxial region and N-MOS 2451 is formed in the P-type well region. The P-MOS 2450 and N-MOS 2451 are formed with gate wiring 2415 if polycrystalline silicon deposited in a thickness greater than or equal to 4000 Å and less than or equal to 5000 Å via a gate insulation layer 2415 of several hundreds Å of thickness, source region 2405 and drain region 2406 formed by doping N-type or P-type impurity.

On the other hand, the NPN type transistor 2453 to be the power transistor is formed by forming a collector region 2411; a base region 2412 and an emitter region 2413 within the N-type epitaxial layer through impurity doping, diffusion process and so forth.

Also, between respective elements, isolative oxide layer 2453 formed by field oxidation in the thickness greater than or equal to 5000 Å and less than or equal

to 10000 Å are formed. The field oxide layer serves as a first heat accumulation layer 2414 below the heat acting portion 2455.

After formation of respective elements, an  
5 interlayer insulation layer 2416 of PSG, BPSG or so forth is deposited by CVD method in a thickness about 7000 Å. Then, by heat treatment of flattening process, wiring with a first layer Al electrode 2417 is performed through contact holes.

10        Thereafter, the interlayer insulation layer 2418 of SiO or so forth is deposited in the thickness greater than or equal to 5000 Å and less than or equal to 10000 Å by way of plasma CVD method. Then, through contact holes, TaN<sub>0.8hex</sub> layer according to the present  
15 invention is deposited in the thickness of about 1000 Å as the resistor later 2419 by way of sputtering method.

Next, as set out with respect to experiments B and C, a protective layer 2421 of SiN layer is formed by  
20 two stage layer deposition into about 10000 Å of thickness by initially depositing at a temperature higher than or equal to 200 °C and lower than or equal to 300 °C, and subsequently at a temperature higher than or equal to 350 °C and lower than or equal to 400  
25 °C.

In the upper most layer, a cavitation resistant layer 2422 of Ta or so forth is deposited in the thickness about 2000 Å with opening a pad portion 2454.

5        Finally, annealing process is performed under H<sub>2</sub> atmosphere at about 400 °C to complete the base body of the printing head.

10       In the final annealing process, improvement of contacting ability between Al and Si substrate and recovery of damage caused in the elements by various heat treatment and plasma process or so forth.

15       After completion of the base body of the printing head, the ink ejection openings for ejection of ink and so forth are formed in the similar manner to the former embodiment and thus formed into the ink-jet printing head.

      Here, while the power transistor is constructed with the bipolar transistor, it can be formed with MOS transistor.

20       As a liquid (ink) for printing applicable for the ink-jet printing head according to the present invention, various liquid or ink can be selected. Amongst, generally, it is preferred to have an ink composition containing 0.5 wt% to 20 wt% of dye, 10  
25    wt% to 90 wt% of (polyhydric) alcohol, water soluble

organic solvent, such as polyalkyl glycol and so forth. As one example, the preferred ink composition contains 3 wt% of C.I. food black 2, 25 wt% of dimethyl glycol, 20 wt% of N-methyl-2-pyrrolidone and  
5 52 wt% of water.

Next, one example of an ink-jet printing apparatus employing the printing head according to the present invention will be discussed with reference to Fig. 17. Fig. 17 is a schematic perspective view showing one  
10 example of the ink-jet printing apparatus, to which the present invention is applied.

The printing head 2200 is mounted on a carriage 2120 engaging with engaging with spiral groove 2121 of a lead screw 2104 driven to rotate via driving force  
15 transmission gears 2102 and 2103 according to forward and reverse revolution of a driving motor 2101. The printing head 2200 is thus driven to reciprocate in the directions of arrows a and b along a guide 2119 together with the carriage 2120 by the driving force  
20 of the driving motor 2101. A paper holding plate 2105 for a printing paper P transported over a platen 2106 by not shown printing medium feeding apparatus fixes the printing paper P on the platen 2106 over the carriage shifting direction.

25 The reference numerals 2107 and 2108 are photo-

coupler serving as a home position detecting means for detecting a lever 2109 of the carriage 2120 for switching direction of revolution of the driving motor 2101, 2110 is a support member supporting a capping member 2111 for capping the entire surface of the printing head 2110 set forth above, 2112 is a suction means for sucking the interior space of the capping member 2111 for performing suction recovery of the printing head 2200 via an opening 2113 in the cap, 2114 denotes a cleaning blade, 2115 is a shifting member for shifting the blade in the back and forth direction. These components are supported on a main body support plate 2116. The cleaning blade 2114 is not necessarily the shown configuration but can be of any known configuration.

On the other hand, the reference numeral 2117 is a lever for initiating sucking for suction recovery, which is shifted according to movement of a cam 2118 engaging with the carriage so that the driving force of the driving motor 2101 is controlled by a known transmission means, such as switching of clutch or so forth. A printing control portion for providing a signal for the heating portion 2110 provided in the printing head 2200 and for controlling driving of respective mechanism is provided on the main body side

of the printing apparatus (not shown).

The ink-jet printing apparatus 2100 constructed as set forth above is adapted to perform printing with reciprocally shifting the printing head 2200 over the entire width of the printing paper P with respect to the printing paper P transported across the platen 2106 by the printing medium feeding apparatus. Since the printing head produced in the method set forth above is employed, high precision and high speed printing becomes possible.

Also, in the ink-jet printing apparatus, an electrical signal providing means for providing electrical signal for making the printing head to eject the ink, is provided. Also, as the ink-jet printing apparatus, only in the form for performing typical printing medium, such as printing paper, a textile printing apparatus for performing printing of pattern on a cloth or so forth can be included. In the textile printing apparatus, in order to perform continuous printing for elongated yard good, the ink-jet printing head employing the heat generating resistor of the present invention which is difficult to cause degradation of printing quality due to significant fluctuation due to breakage of wiring or variation of resistance during printing, is

particularly preferred.

The present invention achieves distinct effect when applied to a recording head or a recording apparatus which has means for generating thermal  
5 energy such as electrothermal transducers or laser light, and which causes changes in ink by the thermal energy so as to eject ink. This is because such a system can achieve a high density and high resolution recording.

10 A typical structure and operational principle thereof is disclosed in U.S. patent Nos. 4,723,129 and 4,740,796, and it is preferable to use this basic principle to implement such a system. Although this system can be applied either to on-demand type or  
15 continuous type ink jet recording systems, it is particularly suitable for the on-demand type apparatus. This is because the on-demand type apparatus has electrothermal transducers, each disposed on a sheet or liquid passage that retains  
20 liquid (ink), and operates as follows: first, one or more drive signals are applied to the electrothermal transducers to cause thermal energy corresponding to recording information; second, the thermal energy induces sudden temperature rise that exceeds the  
25 nucleate boiling so as to cause the film boiling on

2 JUL 2002

heating portions of the recording head; and third, bubbles are grown in the liquid (ink) corresponding to the drive signals. By using the growth and collapse of the bubbles, the ink is expelled from at least one  
5 of the ink ejection orifices of the head to form one or more ink drops. The drive signal in the form of a pulse is preferable because the growth and collapse of the bubbles can be achieved instantaneously and suitably by this form of drive signal. As a drive  
10 signal in the form of a pulse, those described in U.S. patent Nos. 4,463,359 and 4,345,262 are preferable. In addition, it is preferable that the rate of temperature rise of the heating portions described in U.S. patent No. 4,313,124 be adopted to achieve better  
15 recording.

U.S. patent Nos. 4,558,333 and 4,459,600 disclose the following structure of a recording head, which is incorporated to the present invention: this structure includes heating portions disposed on bent portions in  
20 addition to a combination of the ejection orifices, liquid passages and the electrothermal transducers disclosed in the above patents. Moreover, the present invention can be applied to structures disclosed in Japanese Patent Application Laying-open Nos.  
25 123670/1984 and 138461/1984 in order to achieve similar effects. The former discloses a structure in

which a slit common to all the electrothermal transducers is used as ejection orifices of the electrothermal transducers, and the latter discloses a structure in which openings for absorbing pressure waves caused by thermal energy are formed corresponding to the ejection orifices. Thus, irrespective of the type of the recording head, the present invention can achieve recording positively and effectively.

10       The present invention can be also applied to a so-called full-line type recording head whose length equals the maximum length across a recording medium. Such a recording head may consists of a plurality of recording heads combined together, or one integrally arranged recording head.

15       In addition, the present invention can be applied to various serial type recording heads: a recording head fixed to the main assembly of a recording apparatus; a conveniently replaceable chip type recording head which, when loaded on the main assembly of a recording apparatus, is electrically connected to the main assembly, and is supplied with ink therefrom; and a cartridge type recording head integrally including an ink reservoir.

25       It is further preferable to add a recovery system, or a preliminary auxiliary system for a recording head

as a constituent of the recording apparatus because they serve to make the effect of the present invention more reliable. As examples of the recovery system, are a capping means and a cleaning means for the recording head, and a pressure or suction means for the recording head. As examples of the preliminary auxiliary system, are a preliminary heating means utilizing electrothermal transducers or a combination of other heater elements and the electrothermal transducers, and a means for carrying out preliminary ejection of ink independently of the ejection for recording. These systems are effective for reliable recording.

The number and type of recording heads to be mounted on a recording apparatus can be also changed. For example, only one recording head corresponding to a single color ink, or a plurality of recording heads corresponding to a plurality of inks different in color or concentration can be used. In other words, the present invention can be effectively applied to an apparatus having at least one of the monochromatic, multi-color and full-color modes. Here, the monochromatic mode performs recording by using only one major color such as black. The multi-color mode carries out recording by using different color inks, and the full-color mode performs recording by color

mixing.

Furthermore, although the above-described  
embodiments use liquid ink, inks that are liquid when  
the recording signal is applied can be used: for  
5 example, inks can be employed that solidify at a  
temperature lower than the room temperature and are  
softened or liquefied in the room temperature. This  
is because in the ink jet system, the ink is generally  
temperature adjusted in a range of 30°C - 70°C so that  
10 the viscosity of the ink is maintained at such a value  
that the ink can be ejected reliably.

In addition, the present invention can be applied  
to such apparatus where the ink is liquefied just  
before the ejection by the thermal energy as follows  
15 so that the ink is expelled from the orifices in the  
liquid state, and then begins to solidify on hitting  
the recording medium, thereby preventing the ink  
evaporation: the ink is transformed from solid to  
liquid state by positively utilizing the thermal  
20 energy which would otherwise cause the temperature  
rise; or the ink, which is dry when left in air, is  
liquefied in response to the thermal energy of the  
recording signal. In such cases, the ink may be  
retained in recesses or through holes formed in a  
25 porous sheet as liquid or solid substances so that the  
ink faces the electrothermal transducers as described

2 JUL 2002

in Japanese Patent Application Laying-open Nos.  
56847/1979 or 71260/1985. The present invention is  
most effective when it uses the film boiling  
phenomenon to expel the ink.

5        Furthermore, the ink jet recording apparatus of  
the present invention can be employed not only as an  
image output terminal of an information processing  
device such as a computer, but also as an output  
device of a copying machine including a reader, and as  
10    an output device of a facsimile apparatus having a  
transmission and receiving function.

Hereinafter, concrete embodiments of the present  
invention will be discussed in further detail.

[First Embodiment]

15        In the substrate for the ink-jet printing head of  
Fig. 3, the surface of the substrate was cleaned by  
plasma cleaning within the same apparatus immediately  
before layer deposition. The heat accumulating layer  
was formed by forming  $\text{SiO}_2$  in a thickness of  $1.2 \mu\text{m}$  by  
20    thermal oxidation method. Also, the heat accumulation  
layer 104 which also serves as the interlayer  
insulation layer was formed by depositing  $\text{SiON}$  in a  
thickness of  $1.2 \mu\text{m}$  by the plasma CVD method.

Here, as the resistor layer 104, polycrystalline  
25     $\text{TaN}_{0.8\text{hex}}$  having fine X-ray defraction pattern (II) was

deposited in a thickness of 1000 Å by way of reactive sputtering method. In the shown embodiment, the TaN<sub>0.8hex</sub> layer was deposited as the resistor layer under the following condition by the reactive  
5 sputtering method. Namely, the reactive sputtering was performed under the condition of 24% of nitrogen gas partial pressure ratio, 7.5 mTorr of total pressure of a mixture gas of argon gas and nitrogen gas, 2.0 kW of sputtering DC power, 200 °C of  
10 environmental temperature, and 200 °C of substrate temperature. Since orientation of (100) plane of TaN<sub>0.8hex</sub> is strong for the peak of X-ray defraction, the plane distance was  $d = 2.55 \text{ Å}$ . Also, at  $2\theta =$  about 31°, weak defraction peak of TaN<sub>0.8hex</sub>(001) was  
15 observed.

On the fine polycrystalline TaN<sub>0.8hex</sub> layer, Al as a conductor for supplying thermal energy for ejecting ink was deposited in the thickness of 5500 Å by sputtering. The Al layer is deposited continuously by  
20 sputtering within the same apparatus before taking out to expose to the atmosphere. By this continuous deposition, penetration of impurity and moisture into the resistor layer and Al wiring can be successfully prevented. Furthermore, tight contact between both  
25 layers can be ensured to make it possible to form

highly reliable base body for the printing head.

Subsequently, the Al layer and  $\text{TaN}_{0.8\text{hex}}$  layer are patterned into predetermined configurations. The heat acting portion 108 is the region where the Al layer  
5 above the  $\text{TaN}_{0.8\text{hex}}$  layer was removed.

As the protective layer 106, the first layer protective layer SiN was deposited by plasma CVD method in the thickness of about 1500 Å at 300 °C, and subsequently second layer protective layer was  
10 deposited by the plasma CVD method in the thickness of about 8500 Å at 350 °C. Thus, approximately 1 µm of SiN was deposited as the protective layer 106. Thereafter, by way of DC sputtering, Ta layer was deposited in the thickness of 2000 Å to form the  
15 cavitation resistant layer 107. Thus, the base body is completed.

Here, the layer 103 and the layer 106 are formed by the same plasma CVD apparatus and the layer depositing conditions are controlled at respective of  
20 predetermined conditions. Also, the layer 104 and the layer 107 are also formed by the same reactive sputtering layer depositing apparatus with the same Ta target with controlling the layer forming conditions to respective of predetermined conditions to form two  
25 kinds of layers. In this way, since the layer

deposition apparatus to be used becomes lesser,  
contamination in the apparatus becomes smaller.  
Furthermore, since batch opening can be reduced as  
least as possible, the production process with high  
5 yield and high operation efficiency can be  
established.

Fig. 18 shows a result of SST test. This SST test  
was performed by preparing the ink-jet printing head  
having the resistor layer forming the heat generating  
10 resistor to measure the breakdown voltage in the  
manner set forth above, by providing 7 sec. of  
rectangular voltage to the electrothermal transducer  
element as  $1 \times 10^5$  pulses of 2 kHz to measure  
resistance value with elevating the charged voltage  
15 per every 0.05 Vth for measuring variation of  
resistance until breakage is caused in the  
electrothermal transducer element. It should be noted  
that the SST test was performed by applying pulse to  
the heat generating resistor without performing ink  
20 ejection.

The step coverage of the Al electrode by the two  
layer protective layer in the embodiment 1 is quite  
good. When fine polycrystalline  $\text{TaN}_{0.8\text{hex}}$  is employed  
as the heat generating resistor, variation of  
25 resistance value the electrothermal transducer element

2 JUL 2002

becomes quite small. Also, it is appreciated that the breakdown voltage ratio  $K_b$  ( $K_b = \text{charged voltage/bubbling voltage}$ ) is a value of about  $1.6 V_{th}$ .

Charging of drive voltage to the heat generating resistor at the time where  $HfB_2$  becomes to be employed in the base body of the ink-jet printing head as the heat generating body is mainly a single pulse drive only by a main pulse for ejecting ink. However, in the recent years, pulse drive system is changing to so-called double pulse driving by controlling ink ejection amount and applying a subsidiary pulse for the purpose of heating for adjustment of the head temperature.

Conventionally, driving voltage of the single pulse is set between  $1.1 V_{th}$  to  $1.2 V_{th}$  in view of durability of the heat generating resistor.

On the other hand, the double pulse driving consisted of the main pulse, subsidiary pulse and resting period therebetween. For example, when the ejection amount is reduced under low temperature, the ejection amount is increased for stable image quality by performing adjustment for setting the subsidiary pulse width longer or so forth. As a result, converting charge energy into the charge voltage upon single pulse, the drive voltage of  $1.3 V_{th}$  at the

maximum is present. Namely, by establishing double pulse, the charge energy to the heat generating resistor is getting higher.

Thus, result of heat pulse endurance test (CST  
5 test) at 1.3 Vth as the maximum drive voltage is shown in Fig. 19. The CST test is performed only by charging pulse to the heat generating resistor and ink is not contained in the printing head.

From the result of experiment, the electrothermal  
10 transducer element employing the protective layer in two layers in the present invention, is found to have substantially 0% of resistance variation.

A head having the heat generating resistor of the first embodiment is prepared, and printing endurance  
15 test is performed by installing the head to an apparatus which is constructed by modifying BJ10V (Canon Kabushiki Kaisha; tradename) as the ink-jet printing apparatus. The result of printing endurance test is shown in Fig. 20. The test is performed by  
20 printing a test printing pattern built-in the BJ10V on a paper of A4. As the ink, an ink in the ink cartridge employed in the BJ10V is used as is. In this case, the drive voltage was 1.3Vth.

The head employing two layer protective layer in  
25 the first embodiment has 0% of resistance variation

similar to the CST test and shows good durability.

[Second Embodiment]

As the protective layer 106 of the ink-jet printing head, the first protective layer SiN was deposited in the thickness of about 1500 Å at 300 °C, and then second protective layer SiN was deposited in the thickness of about 8500 Å at 350 °C to form the base body having the protective layer in the thickness of 1 µm in total. With employing this base body, the ink-jet printing head was prepared. Other layer construction and layer deposition method are similar to that of the first embodiment.

In Fig. 18, the result of SST test performed with employing the second embodiment of the ink-jet printing head. The condition of the SST test is similar to that in the first embodiment.

It is found that the second embodiment shows good value of the breakdown voltage  $K_b$  of 1.8 Vth.

The result of CST test is shown in Fig. 19. The condition of the CST test is also similar to that of the first embodiment.

Similarly to the first embodiment, the result shows that variation of the resistance value is little in the second embodiment.

Fig. 20 shows a result of printing endurance test employing modified BJ10V similarly to the first embodiment, but employing the second embodiment of the ink-jet printing head.

5       The second embodiment demonstrates good result having substantially 0% variation of the resistance value of the resistor later, similarly to the first embodiment.

[Comparative Example]

10       The ink-jet printing head prepared (1) by forming the base body with depositing the protective layer SiN of the second embodiment in the thickness about 1  $\mu$ m at 200 °C by way of plasma CVD method, as a comparative example 1-1, and (2) by forming the base  
15       body with depositing the protective layer SiN of the second embodiment in the thickness about 1  $\mu$ m at 350 °C by plasma CVD method, as a comparative example 1-2.

Results of the SST test was performed by using the electrothermal transducer element employing the  
20       resistor layers of respective of the comparative examples 1-1 and 1-2. The test was performed in the same manner to that for the first and second embodiments.

In the comparative example 1-1, the protective  
25       layer SiN is loose to cause corrosion of the Al wiring

by alkaline ink through pin hole to cause increasing of the resistance value and lower the breakdown voltage to 1.3 Vth.

5 In the comparative example 1-2, since hillock is grown on the Al during layer formation of the protective layer SiN at high temperature, shorting is caused with the cavitation resistant layer Ta to reduce resistance value, and lower the breakdown voltage to 1.3 Vth.

10 Fig. 19 shows the results of CST test. The test was performed in the same manner to the foregoing first and second embodiments.

15 In the comparative example 1-1, the resistance value is increased and in the comparative example, the resistance value is decreased. In both case, breakage was caused at the pulse in the order of  $1 \times 10^6$ .

20 Fig. 20 shows the results of printing endurance test by employing the ink-jet printing heads of the comparative examples 1-1 in the modified BJ10V as used for the first and second embodiments. Other conditions are the same as those for the first and second embodiments.

25 The comparative example 1-1 causes ejection failure due to breakage of the Al electrode by corrosion by the ink during the printing endurance

test.

The comparative example 1-2 causes ejection failure due to breakage of the Al electrode by shorting between the hillock in the Al electrode and  
5 the Ta layer during the printing endurance test.

From the results set forth above, the first and second embodiments of the ink-jet printing heads are found to be suitable for expansion of lift and for higher image quality for superior printing image  
10 quality and durability.

On the other hand, the ink-jet printing heads of the comparative examples causes variation of the resistance value to cause clear lowering of the printing image quality. Also, in the light of the durability  
15 of the printing head, the first and second embodiments are found superior.

As set forth above, the present invention achieves the effects summarized as follows.

In the ink-jet printing head according to the  
20 present invention, the heat generating resistor has little fluctuation of the resistance even after use for a long period and thus achieved long life and high reliability. The ink-jet printing head employing the base body for the ink-jet printing head having such  
25 heat generating resistor can be perform high quality

printing with stable ink ejection even when repeated printing in the printing system where a preparatory pulse is applied before the main pulse for ejecting ink, as the drive signal for the head, is performed  
5 for a long period.

The ink-jet printing head according to the present invention has the stacked structure of the base body for the ink-jet printing head to certainly provide tight fitting ability between the layers and has  
10 sufficient durability against repeatedly acting thermal pulse and impact force and can constantly provide desired ink ejection even in repeated use for a long period.

The base body for the ink-jet printing head in the  
15 ink-jet printing head according to the present invention is constantly supplied the component material stably. Also, in production of the heat generating resistor, harmful influence, such as contamination by impurity will never be caused. On  
20 the other hand, the heat generating resistor has high reliability, and even in the driving method controlling ink ejecting condition by the double pulse including the main pulse and the subsidiary pulse, which will become major, sufficient durability can be  
25 achieved.

The heat generating resistor of the base body for the ink-jet printing head in the ink-jet printing head according to the present invention can provide high quality printed image for a long period for  
5 maintaining desired durability even driven at high frequency.

The heat generating resistor according to the present invention can certainly maintain sufficient durability and high quality image even in the driving  
10 method controlling the ejecting condition with a plurality of pulses in high speed driving. On the other hand, corresponding to speeding of the printing speed, increasing of number of nozzles to be employed in the head can be easily achieved to ensure  
15 constantly stable and desired ink ejection to constantly and stable form high quality image.

In the production method of the base body for the ink-jet printing head according to the present invention, the base body for the ink-jet printing head  
20 having high durability, high strength against repeatedly applied thermal impact, small fluctuation of resistance value and resistive against ink corrosion or cavitation, and certainly provide high quality printed image for a long period.

25 Although the invention has been illustrated and

described with respect to exemplary embodiment  
thereof, it should be understood by those skilled in  
the art that the foregoing and various other changes,  
omissions and additions may be made therein and  
5 thereto, without departing from the spirit and scope  
of the present invention. Therefore, the present  
invention should not be understood as limited to the  
specific embodiment set out above but to include all  
possible embodiments which can be embodied within a  
10 scope encompassed and equivalents thereof with respect  
to the feature set out in the appended claims.

The present invention has been described in detail  
with respect to various embodiments, and it will now  
be apparent from the foregoing to those skilled in the  
15 art that changes and modifications may be made without  
departing from the invention in its broader aspects,  
and it is the intention, therefore, in the appended  
claims to cover all such changes and modifications as  
fall within the true spirit of the invention.

## WHAT IS CLAIMED IS:

1. A liquid ejecting printing head including a base body, in which an electrothermal transducer element  
5 generating a thermal energy to be used for ejection of a liquid, a driving functional element for driving said electrothermal transducer element, a wiring electrode connecting said driving functional element and said electrothermal transducer element, an  
10 insulative protective layer provided on said wiring electrode are formed on a substrate, wherein said protective layer on said electrothermal transducer element or said wiring electrode is formed of an insulative compound deposited to gradually  
15 increase density from a side close to said substrate to a side remote from said substrate.
2. A liquid ejecting printing head as claimed in claim 1, wherein when said electrothermal transducer  
20 element includes a head generating resistor made of TaN, composition of TaN is to contain 1.9 to 1.0 of Ta relative to N in molecular weight ratio.
3. A liquid ejecting printing head as claimed in

claim 1, wherein said electrothermal transducer element includes a heat generating resistor made of  $\text{HfB}_2$ , Poly-Si, Ta-Al, Ta-Ir Au or Ag.