

Fitting

Description

5 The invention relates to a fitting, in particular for
installations comprising pressure exchangers with
tubular chambers through which flow takes place
alternately, a rotatable closing element being arranged
inside a housing, the housing having a plurality of
10 connections for connecting lines, the housing being
connected to a first pipeline system and in each case
one end of at least one pressure exchanger, a
respective other end of a pressure exchanger being
connected to a second pipeline system with the
15 interposition of further fittings, and the closing
element being provided with a motor-operated drive
shaft.

For the purpose of treating water, the reverse osmosis
20 process is often used. In this case, a fluid stream to
be purified is forced at high pressure through a
membrane system which, in the case of large quantities
of fluid, comprises a plurality of membrane modules.
In such membrane modules, separation into pure water
) 25 and an enriched concentrate is carried out through a
membrane, since only some of a fluid to be purified can
flow through a membrane. The proportion flowing
through emerges as a usable proportion, as pure water
or else permeate, on the other side of the membrane.
30 The part which does not flow through leaves a membrane
module as brine, a concentrate of the fluid enriched
with salts and minerals, as a proportion which cannot
be used and is under high pressure. This pressure is
around 2 bar with a module inlet pressure of about 65
35 bar.

US 5 306 428 discloses a reverse osmosis installation
in which pressure exchangers in the form of tubular

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chambers are used to recover energy. By using these, the still high pressure of the high energy brine flowing out of the membrane module is transferred to a fluid still to be purified. Thus, a pump drive output
5 which is lower by the amount of this pressure increase is required for the fluid to be fed in in order to generate the high pressure needed for the reverse osmosis process.

10 For the purpose of controlling and/or changing over the fluid paths of the brine into and out of the pressure exchangers, a fitting with a rotating closing element is used, in addition to other fittings. With the aid of said fitting, the tubular chambers of the pressure
15 exchangers have brine emerging from the membrane modules applied to them alternately. The rotating closing element is constructed as a roll, in which connecting ducts are arranged in the manner of a 3-way valve. During the changeover operations, all the flow
20 paths are shut off completely. In order to avoid pressure surges during such changeover operations, pressure equalizing ducts are arranged within the roll.

Depending on the operating period of a membrane, its
25 separation capability decreases and a fluid to be purified has to remain for a correspondingly longer time within a membrane module. For this reason, in the prior art, the changeover times of the roll are influenced with the aid of an actuating motor.
30 However, this fitting is suitable only for small reverse osmosis installations, since the flow cross sections within the fitting are approximately the same size as the flow cross sections of the ducts to be filled. In the case of large installations and the
35 fluid columns to be displaced therein, and as a result of the forces necessitated thereby, a considerable problem of dimensioning the fitting arises.

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The invention is based on the problem of developing a changeover device, in particular for large reverse osmosis and similar installations, with the aid of which large flows of fluid can be distributed between
5 different pressure exchangers in a straightforward and fault-free manner.

The solution to this program provides for a flow splitter provided with a plurality of transfer paths to
10 be arranged within the housing, for openings of the transfer paths to be arranged at two axial ends and on the circumference of the flow splitter, and for a rotating, disk-like control element to be arranged in a sealing manner at each end of the flow splitter. Thus,
15 in the case of such fluid flows which are to be controlled and which change direction periodically, a changeover with few pressure surges can be achieved.

Refinements of the invention provide for the end
20 regions of the flow splitter inside the housing to be connected to the tubular chambers in which a pressure exchange is carried out with the aid of the changing fluid flows. In each case a connection for a supply of high pressure fluid and a discharge of low pressure
25 fluid are arranged on the housing of the fitting, in the circumferential region of the flow splitter and on the housing. What is known as brine under high pressure, HPB, for example, flows to the fitting through the connection for a high pressure fluid.
30 Following pressure transmission, the brine then flows in depressurized form, as what is known as LPB, out of the housing through the discharge for low pressure fluid.

35 In the flow splitter there are arranged flow paths with the aid of which the flows having different pressures are distributed. In this case, within the flow splitter, two outer flow paths are connected to a high pressure side and a central flow path, arranged between

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the former, is connected to a low pressure side. In order to ensure long-term operating reliability under the continuously changing pressure loadings, one or more reinforcing elements can additionally be arranged
5 in one or more of the flow paths. This depends on the physical configuration of the flow splitter and the materials used.

The flow splitter can be an integral constituent part
10 of the housing; it has been shown to be advantageous if the flow splitter is constructed as a housing insert. In this way, housing fabrication is simplified and the number of sealing points located on the housing can be reduced. It has likewise proven to be advantageous with
15 regard to the closing behavior if the flow splitter is constructed as a ceramic or a (ceramic-) coated component.

The control elements are advantageously constructed in
20 the manner of rotating rotary slide, which means that secure management of the sealing functions is possible, in addition to simple production. Therefore, a previously known closing element is replaced by control elements which act as temporary closing elements only
25 during their rotational movement. The control elements alternately control the flow through the overflow paths of the flow splitter, which means that secure and efficient flow changeover is ensured. Furthermore, the control elements are provided with control openings
30 located opposite one another in pairs, which means that a flow of a large amount is achieved in a small space.

With the aid of the refinement in which the control openings of a control element are arranged to be offset
35 by at most 90° from one another in each case in relation to the control openings of the other control element, alternating changeover of the flow direction to the tubular chambers connected to the housing is

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carried out in an extremely simple way during a rotational movement of the control elements.

Since the control elements are subjected to alternating
5 loading in operation, they are provided with
reinforcements on the side facing away from the flow
splitter. It is likewise possible to provide the
control elements with reinforcements on their
circumference. These may be additional material
10 masses, built-in components, supporting elements,
tensioning elements and the like. This depends on the
materials used.

In order to reduce the forces between flow splitter and
15 control element, one or more depressions are arranged
on the ends of the flow splitter in order to form
narrow bearing surfaces. This measure avoids contact
over the entire area, by which higher frictional forces
are caused. Instead, the formation of narrow contact
20 surfaces is thus possible, which also permit improved
sealing at the same time.

In order to separate different pressure regions in the
chambers located in the housing, seals bear on the
25 control elements on the side facing away from the flow
splitter. These can be of a sliding ring seal design.
Apart from the ability to be produced easily, the
advantage of the known secure sealing action is
therefore provided. In addition, the shaft is arranged
30 in a region of the housing which is shielded by the
seals and is connected to the low pressure side LPB.
As a result, a passage of the shaft through the housing
wall to the outside advantageously only has to be
sealed by a conventional shaft seal designed for low
35 pressure. This entails less effort than sealing off
such a shaft leadthrough with respect to the high
pressure side HPB. And, within the fitting, as a
result no additional seals are required for the passage
of a shaft.

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Further refinements provide for a shaft driving the control elements to pass through the flow splitter and for the control elements to be connected in a force-transmitting manner to the shaft. This simplifies the mounting and the driving of the control elements. The control elements are constructed as ceramic or coated components, which provide high resistance to wear and attack by the fluid flows to be controlled.

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Mounting and maintenance are made considerably easier if flow splitter, shaft and control elements are all constructed as a housing insert. Thus, serviceability can be ensured in an extremely short time. And, as a result of the arrangement of sealing zones arranged on the circumference of the flow splitter between inlet and outlet, overflow between these two zones is avoided.

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For a gentle changeover, provision is made for the tubular chambers of the pressure converter to be connected to one another briefly by the position and the size of the control openings during a movement of the rotary slide. The position and the size of the control openings on the control elements constructed as rotary slides permits a flow changeover which is free of pressure surges, since a simultaneous connection to a supply of high pressure fluid is thereby always ensured. Closing a control opening of a connected tubular chamber is at the same time connected with opening of another previously closed control opening of a further tubular chamber and vice versa. Because of the enlarged control openings and because of their position on the control element, an overlap with the flow openings arranged fixedly in the flow splitter is achieved. Such an overlap in this case has a beneficial effect on the changeover and the behavior of the flowing fluid columns affected thereby.

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Depending on the flow rate of the pressure converter, the position of the control openings is changed at a continuous and/or discontinuous speed. The degree to which the tubular chambers are filled can therefore be
5 influenced. The use of a discontinuous speed permits a longer residence time of the flow openings over the control openings, utilizing the full opening cross section. The discontinuous movement achieves greater channel filling in a shorter time and thus a maximum
10 possible flow rate. This can be done with the aid of an appropriately designed drive motor. When a conventional rotary drive with continuous movement of the control elements is used, the same device can also be used for small installations, since a smaller flow
15 rate is switched therewith. Conversely, with a discontinuous movement of the control elements, at a given flow rate the overall volume of the device can be reduced. With the aid of adjustable switching times of the control elements, the volume throughput can be
20 influenced as a function of the pressure differences present.

Refinements of the invention are illustrated in the drawings and will be described in more detail in the
25 following text. In the drawings:

figs. 1a & 1b show two sectional views of the fitting, offset through 90°, in a first operating state, in each case in the plane of the
30 inlets and outlets,

figs. 2a & 2b show two sectional views of the fitting, offset through 90°, in a second operating state, the control elements in each case being illustrated rotated
35 through 90° with respect to figs. 1a & 1b,

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- fig. 3a shows a perspective view of the flow splitter,
- 5 fig. 3b shows a perspective view of the flow splitter, in which one quarter of the flow splitter has been cut away in order to make the flow paths visible,
- 10 fig. 4a shows a perspective view of the flow splitter in the assembly with the two control elements in a first operating state, the upper part having been cut away in order to clarify the flow direction,
- 15 fig. 4b shows a perspective view of the flow splitter in the assembly with the two control elements in a second operating state, the control elements being
- 20 illustrated rotated through 90° in each case with respect to fig. 4a.

A fitting 1 is shown in section in fig. 1a. The housing 2 has two connections 3, 4 with the aid of which a connection to the tube chambers, not illustrated, from a pressure exchanger system is made. By means of the connections 3, 4, an exchange of a fluid which flows through under high pressure and flows back at lower pressure is made alternately. Arrows 5, 6 show the respectively prevailing flow directions. The distance between the connections 3, 4 is chosen in accordance with the distance between tubular chambers to be connected thereto. This integration of the connections 3, 4 into the housing 2 avoids unnecessary additional sealing points.

Arranged inside the housing 2 is a flow splitter 7 which, in the exemplary embodiment shown, is configured as a separate insert. It can equally well be

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configured as a single-piece component with the housing 2. The flow splitter 7, formed as an insert here, is sealed off with respect to the housing 2 with the aid of seals 8. In the region of the circumference of the flow splitter 7 there is arranged a chamber 9, which is used to discharge a depressurized fluid. In each case a control element 12, 13 bears in a sealing manner on the ends 10, 11 and is set rotating with the aid of a shaft 14 driven by a motor, not illustrated. The force is transmitted between shaft 14 and the control elements 12, 13 by means of bearing elements 15. These can be configured as polygons or force-fitting and form-fitting in another way. The shaft 14 is mounted in the interior of the housing 2 at one end and, on the opposite side, is mounted and sealed off in a cover 16 which closes the housing 2.

The rotating control elements 12, 13, which are configured in the manner of rotary slides here, have reinforcements 12.1 to 13.2. These reinforcements improve the alternating bending loading of the control elements 12, 13 during the changeover operation. Depending on the materials used, that is to say metal or ceramic or combinations thereof, these reinforcements can be formed as accumulations of material, plates, rings, struts or the like.

In the illustration of fig. 1, a fluid under high pressure, for example a high pressure brine HPB, flows from two T-shaped flow paths 17, 18 through control openings 19, 20 arranged opposite one another in pairs and belonging to the control element 13 into an end region 21 of the housing 2 and from there, via the connection 4, to a tubular chamber. At the same instant, a fluid under a low pressure, for example a low pressure brine LPB, flows through the connection 3 from a tubular chamber into the end region 22 of the housing 2.

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Seals 23 bearing on each control element 12, 13 prevent fluid exchange with other housing regions. The seals 23 are constructed in the manner of a sliding ring seal, held in the housing 2 so as to be secured against rotation, and bear in a sealing manner on the control elements 12, 13 under the pressure of springs 24.

Fig. 1b corresponds to the exemplary embodiment of fig. 1a in terms of the instantaneous position of the control elements in relation to the flow splitter. However, a section rotated through 90° is shown in fig. 1b. It reveals that, of the control element 12, the control openings 25, 26 arranged in pairs are connected in a fluid-carrying manner to a flow path 27 which is arranged in the center of the flow splitter 7. The central flow path 27, designed for an outward flow of a low pressure fluid identified by LPB, is arranged between the two flow paths 17, 18 designed for a high pressure fluid HPB. In order to manage the alternatingly occurring forces securely, a reinforcing element 29 of a transverse rib type is arranged in the flow path 27. This ensures a beneficial flow of force within the flow splitter 7.

A low pressure fluid led through the connection 3 into the housing 2 flows via the control opening 25, 26 into the flow path 27 and from there flows out of the housing as low pressure fluid via an opening 28 in the flow splitter 7 and an outlet 30. Arranged opposite the outlet 30 on the housing 2 is a connection 31 for the supply of high pressure fluid HPB to the housing 2. With the aid of the chamber 32 arranged on the circumference of the flow splitter 7, the high pressure fluid is led to the two T-shaped flow paths 17 and 18. With the aid of the low pressure chamber 9 arranged opposite, the low pressure fluid is discharged from the housing 2 via the outlet 30.

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Figs. 2a and 2b show the same sections through the fitting as figs. 1a and 1b but in a second operating state. In this case, the control elements 12 and 13 have been rotated onward through 90° in each case via the shaft 14 and the bearing elements 15. The fluid HPB flowing into the flow paths 17, 18 through the high pressure connection 31 and the chamber 32 is now deflected via the control openings 25, 26 into the chamber 22, from where it passes via the connection 3 to a tubular chamber (not illustrated). At the same time, low pressure fluid LPB flows via the connection 4 from a second tubular chamber into the chamber 21, through the control openings 19, 20 into the central flow path 27 in the flow splitter 7 and from there out of the fitting via the opening 28, the chamber 9 and the connection 30. By means of further rotation of the parts 12, 13, 14 and 15 through 90° , the first operating state, illustrated in figs. 1a and 1b, is then reached again.

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Fig. 3a shows a perspective view of the flow splitter 7 with a central flow path 27, and fig. 3b shows, by means of a partial section in the flow splitter 7, the position of the outer flow paths 17 and 18 still located therein. In the central flow path 27 there is a reinforcing element 29, in which there is an opening for the shaft 14 to be led through. Furthermore, a plurality of depressions 33 is made in the end 11 of the flow splitter 7, which means that narrow bearing surfaces 34 are formed on the end face 11. This reduces the frictional forces between the parts sliding on one another and at the same time improves the sealing action. The T-shaped course of the flow paths 17, 18 ensures in the simplest way that an alternating outflow of a high pressure fluid into the respectively connected tubular chamber becomes possible as a result of the control openings 19, 20; 25, 26 sliding alternately past. A fluid flows out of the central

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flow path 27 to the outside via an opening 28 and via the outlet 30 from the housing 2.

Figs. 4a and 4b show a perspective arrangement of the functional parts in the form of the flow splitter 7, the control elements 12, 13, the shaft 14 and the bearing elements 15 of the fitting 1, in each case in partial section. Here, fig. 4a shows the first operating state and fig. 4b the second operating state with the parts 12, 13, 14 and 15 rotated through 90° in each case with respect to the flow splitter 7. In fig. 4a it becomes clear how, in a first operating state, the high pressure fluid HPB flows through the flow paths 17, 18 and the control openings 19, 20 to the side at the front in this view. At the same time, on the other side or, here, the rear side, the path via the central flow path 27 to the opening 28 is free via the flow openings 25, 26 arranged in pairs, the latter being hidden.

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In the second operating state, shown in fig. 4b, the relationships in the converse state are illustrated. For this purpose, the control elements 12, 13 are shown as having been rotated through 90° with respect to the flow splitter 7 with the aid of the shaft 14 and the bearing elements 15. In this view of the drawing, a high pressure fluid HPB flows rearward via the flow openings 25, 26 of the control element 12. At the same time, via the flow openings 19, 20 likewise arranged in pairs (19 has been cut away by the partial sectional illustration), a depressurized low pressure fluid LPB passes from the front side of the view of the drawing into the central flow path 27 and flows out of the fitting from there via the opening 28.

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By means of this solution having the control elements 12, 13 arranged on both sides of a flow splitter 7, an extremely compact changeover fitting with high operational reliability is provided. At the same time,

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the number of sealing points and pipeline connections needed for such a fitting could be reduced to a minimum.

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Patent claims

- 5 1. A fitting (1) for changing fluid paths, in particular for installations comprising pressure exchangers with tubular chambers through which flow takes place alternately, a rotatable closing and distributing element being arranged inside a
10 housing (2), the housing (2) having a plurality of connections (3, 4) for connecting lines of pipeline systems, and the closing and distributing element being provided with a motor-operated drive shaft (14), characterized in that a flow splitter
15 (7) provided with a plurality of transfer paths (17, 18, 27) is arranged within the housing (2), in that openings of the transfer paths (17, 18, 27) are arranged at two axial ends (10, 11) and on the circumference of the flow splitter (7), and in
20 that a rotating, disk-like control element (12, 13) is arranged in a sealing manner at each end of the flow splitter (7) as a closing element.
- 25 2. The fitting as claimed in claim 1, characterized in that the end regions (10, 11) of the flow splitter (7) are connected to the tubular chambers.
- 30 3. The fitting as claimed in claim 1 or 2, characterized in that in each case a connection for a supply (31) of high pressure fluid (HPB) and a discharge (30) of low pressure fluid (LPB) are
35 arranged on the housing (2), in the circumferential region of the flow splitter (7).

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4. The fitting as claimed in claim 1, 2 or 3, characterized in that at least three flow paths (17, 18, 27) are arranged in the flow splitter (7).
5. The fitting as claimed in claim 4, characterized in that, within the flow splitter (7), at least two outer flow paths (17, 18) are connected to a high pressure side (HPB) and at least one central flow path (27), arranged between the former, is connected to a low pressure side (LPB).
6. The fitting as claimed in claim 4 or 5, characterized in that one or more reinforcing elements (29) are arranged in one or more of the flow paths (17, 18, 27).
7. The fitting as claimed in claim 4, 5 or 6, characterized in that outer flow paths (17, 18) have a T-shaped course.
8. The fitting as claimed in one of claims 1 to 7, characterized in that the flow splitter (7) is constructed as a housing insert.
9. The fitting as claimed in claim 8, characterized in that the flow splitter (7) is constructed as an interchangeable insert arranged in a sealing manner.
10. The fitting as claimed in one of claims 1 to 9, characterized in that the flow splitter (7) is constructed as a ceramic or a coated component.
11. The fitting as claimed in one of claims 1 to 10, characterized in that the control elements (12, 13) are constructed as rotary slides.

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12. The fitting as claimed in one of claims 1 to 11, characterized in that the control elements (12, 13) are provided with control openings (19, 20; 25, 26) located opposite one another in pairs.
- 5 13. The fitting as claimed in claim 12, characterized in that the control openings (19, 20) of a control element (13) are arranged to be offset by at most 90° from one another in each case in relation to
- 10 the control openings (25, 26) of the other control element (12).
14. The fitting as claimed in one of claims 11, 12 or 13, characterized in that the control elements
- 15 (12, 13) are provided with reinforcements (12.1, 12.2, 13.1, 13.2) on the side facing away from the flow splitter (7).
15. The fitting as claimed in one of claims 11 to 14,
- 20 characterized in that the control elements (12, 13) are provided with reinforcements on the circumference.
16. The fitting as claimed in one of claims 1 to 15,
- 25 characterized in that one or more depressions (33) are arranged on the ends (10, 11) of the flow splitter (7) in order to form narrow bearing surfaces (34).
- 30 17. The fitting as claimed in one of claims 1 to 17, characterized in that the control elements (12, 13) bear on seals (23) on the side facing away from the flow splitter (7).
- 35 18. The fitting as claimed in claim 17, characterized in that the seals (23) are of a sliding ring seal design.

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19. The fitting as claimed in claim 17 or 18, characterized in that the shaft (14) is arranged in a region of the housing which is shielded by the seals (23) and is connected to the low pressure side (LPB).
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20. The fitting as claimed in claim 17, 18 or 19, characterized in that the seals (23) bear in a sealing manner on the control elements (12, 13) under the pressure of springs (24).
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21. The fitting as claimed in one of claims 1 to 20, characterized in that a shaft (14) driving the control elements (12, 13) passes through the flow splitter (7).
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22. The fitting as claimed in one of claims 1 to 21, characterized in that the control elements (12, 13) are connected to the shaft (14) in a force-transmitting manner.
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23. The fitting as claimed in one of claims 1 to 22, characterized in that the control elements (12, 13) are constructed as ceramic or coated components.
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24. The fitting as claimed in one of claims 1 to 23, characterized in that flow splitter (7), shaft (14) and control elements (12, 13) are constructed as a housing insert.
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25. The fitting as claimed in claims 3, 8 or 24, characterized in that sealing zones are arranged on the circumference of the flow splitter (7), between inlet (31) and outlet (30).
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26. The fitting as claimed in one or more of claims 1 to 25, characterized in that the tubular chambers of the pressure converter are connected to one

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another briefly via the flow splitter (7) by the position and the size of the control openings (19, 20; 25, 26) during a movement of the control element (12, 13).

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27. The fitting as claimed in claim 26, characterized in that the position and size of the control openings (19, 20; 25, 26) permit a flow changeover which is free of pressure surges.

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28. The fitting as claimed in claim 26 or 27, characterized in that closing control openings (19, 20; 25, 26) of a tubular chamber is at the same time connected with opening previously closed control openings (19, 20; 25, 26) of another tubular chamber and vice versa.

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29. The fitting as claimed in one of claims 1 to 28, characterized in that, depending on the flow rate of the pressure converter, the position of the control openings (19, 20; 25, 26) is changed at a continuous and/or discontinuous speed.