

SPECIFICATION

TITLE OF THE INVENTION

PROCESS FOR PRODUCING POLYMER COMPOSITION

5 BACKGROUND OF THE INVENTION

Field of the Invention

The present invention relates to a process for producing a polymer composition, more specifically, relates to a process for producing a polymer composition by
10 continuous polymerization.

Description of Related Art

Resin compositions such as methacrylic ester polymers are produced by continuous polymerization in which a raw
15 material polymer, a polymerization initiator and the like are continuously supplied to a reactor to be polymerized. As such continuous polymerization processes, there are known a continuous solution polymerization process using a solvent (or a dispersion medium, which also applies
20 hereinafter) to conduct continuous polymerization, and a continuous bulk polymerization process using no solvent to conduct continuous polymerization.

In general, a continuous solution polymerization process is not efficient since use of a solvent causes a
25 low productivity. In contrast, a continuous bulk

polymerization process has an advantage of being able to produce a polymer composition efficiently since the polymerization is conducted without using a solvent. Practically, the continuous bulk polymerization, however, has various problems compared with the continuous solution polymerization, such as that reaction control is difficult due to high viscosity of a reaction mixture, and when an inner surface of a reactor is cooled to remove heat from a reaction system, this degrades quality of a polymer composition and thus of a resin composition obtained therefrom. Then, a process is proposed which uses a reactor of a complete mixing type, fully fills the reactor with liquid to exclude a gas phase part therefrom, and conducts continuous bulk polymerization under an adiabatic condition with no heat transfer to or from the outside (JP 07-126308 A). Further, in order to assure such adiabatic condition, a continuous bulk polymerization apparatus is proposed which controls a supply amount of a raw material monomer and a supply amount of a polymerization initiator so as to make a temperature in the reactor equal to a setting temperature of an outer surface of the reactor (JP 2006-104282 A).

SUMMARY OF THE INVENTION

Technical Problem

In recent years, applications of resin compositions such as methacrylic ester polymers has been expanded furthermore, a demand is increasing for more efficiently producing a polymer composition of high quality (for example, a polymer composition having superior properties such as heat resistance and heat stability, and less immixed with impurities). However, it has been proved that the conventional process for producing a polymer composition (JP 07-126308 A and JP 2006-104282 A) are not always sufficient to meet the demand.

The purpose of the present invention is to provide a process for producing a polymer composition, which process is able to more efficiently produce the polymer composition with high quality.

Solution to Problem

The inventors considered using at least two reactors of a complete mixing type in combination to conduct continuous polymerization. As to a continuous solution polymerization process, apparatuses having two stages of reactors are known, such as that the most part of polymerization is conducted in the former reactor and the polymerization is completed in the latter reactor while removing a polymerization initiator therefrom (JP 01-172401 A); and that polymerization is conducted to some extent in

the former reactor and a solvent is added to the latter reactor to conduct polymerization (JP 05-331212 A). In processes using such apparatuses, however, removal of heat from a reaction system is conducted by reflux cooling (a raw material monomer or the like in the reactor is evaporated to be taken out of the reactor, and it is returned to the reactor again after subjected to cold condensation), this brings about local or rapid cooling of the reaction system, which causes gel to adhere to and grow on the inner surface of the reactor. Especially in a case of conducting the polymerization in a less amount of solvent or with a high polymerization ratio in order to increasing a productivity, a viscosity of a mixture in the reaction system becomes high, this makes the local or rapid cooling of the reaction system arise more easily, which makes the adhering and growing of the gel on the inner surface of the reactor prominent. As a result, there is a problem such as that gelled substance is immixed into a resultant polymer composition as impurities. The inventors have considered earnestly on a novel process for producing a polymer composition which is able to more efficiently produce the polymer composition with high quality, and finally completed the present invention.

The present invention provides the following [1] to [4].

[1] A process for producing a polymer composition, which comprises

a first polymerization step of supplying a raw material monomer and a polymerization initiator to a first reactor of a complete mixing type through its supply port to be subjected to continuous polymerization under an adiabatic condition in the first reactor of the complete mixing type, and taking a resultant intermediate composition from an effluent port located at a top of the first reactor of the complete mixing type; and

a second polymerization step of supplying the intermediate composition to a second reactor of a complete mixing type through its supply port to be further subjected to continuous polymerization under an adiabatic condition in the second reactor of the complete mixing type, and taking a resultant polymer composition from an effluent port located at a top of the second reactor of the complete mixing type;

wherein the first polymerization step is conducted at a temperature from 125 to 170°C, and the second polymerization step is conducted at a temperature from 130 to 180°C.

[2] The process for producing the polymer composition according to the above [1], wherein a ratio of an average residence time in the second reactor of the complete mixing

type to an average residence time in the first reactor of the complete mixing type is from $9/1$ to $1/9$.

[3] The process for producing the polymer composition according to the above [1], wherein the continuous polymerization in the first polymerization step and the second polymerization step is continuous bulk polymerization.

[4] A molded article prepared from the polymer composition produced by the process according to any of the above [1] to [3].

Advantageous Effects of Invention

According to the present invention, there is provided a novel process for producing a polymer composition which is able to more efficiently produce the polymer composition with high quality, more specifically, a polymer composition having high heat stability.

Brief Description of Drawings

Fig. 1 shows a schematic view for explaining a process for producing a polymer composition in one embodiment of the present invention.

Following reference signs denote the following elements:

1 ... raw material monomer tank (supply source of raw

material monomer)

3 ... polymerization initiator tank (supply source of polymerization initiator and, if necessary, of raw material monomer)

5 5 ... pump

7 ... pump

9 ... raw material supply line

10 ... first reactor

11a ... supply port

10 11b ... effluent port

11c ... another supply port

13 ... jacket (temperature regulating means)

14 ... stirrer

15 ... connection line

15 17 ... polymerization initiator tank (supply source of additional polymerization initiator and, if necessary, of raw material monomer)

19 ... pump

20 ... second reactor

20 21a ... supply port

21b ... effluent port

21c ... another supply port

23 ... jacket (temperature regulating means)

24 ... stirrer

25 25 ... effluent line

31 ... preheater

33 ... devolatilizing extruder

35 ... discharge line

37 ... recovery tank

5 T ... temperature sensor (temperature detecting means)

DETAILED DESCRIPTION OF THE EMBODIMENTS

A process for producing a polymer composition of the present invention is conducted by using at least two
10 reactors of a complete mixing type, and continuous polymerization such as any of continuous bulk polymerization and continuous solution polymerization is conducted in each of the reactors. A process for producing a polymer composition of the present invention will be
15 understood as a process for conducting continuous bulk polymerization when continuous bulk polymerization is conducted in all of the reactors, and understood as a process for conducting continuous solution polymerization when continuous solution polymerization is conducted in all
20 of the reactors. However, a process for producing a polymer composition of the present invention is not limited thereto, but may be those wherein continuous bulk polymerization is conducted in one reactor (e.g. at least one former reactor) and continuous solution polymerization
25 is conducted in another reactor (e.g. at least one latter

reactor).

Hereinafter, one embodiment of the present invention will be described in detail with reference to Fig. 1.

First of all, a continuous polymerization apparatus
5 used to conduct a process for producing a polymer
composition in this embodiment is explained. The process
for producing a polymer composition in this embodiment is
conducted by using at least the first reactor 10 and the
second reactor 20. These reactors 10 and 20 are both a
10 reactor of a complete mixing type, and used to conduct
continuous bulk polymerization as continuous polymerization
at the first polymerization step and the second
polymerization step in this embodiment.

More specifically, the first reactor 10 is provided
15 with a supply port 11a and an effluent port 11b, and
preferably further provided with a jacket 13 as a
temperature regulating means for regulating a temperature
of an outer surface of the reactor and a stirrer 14 for
stirring a content therein. Similarly, the second reactor
20 20 is provided with a supply port 21a and an effluent port
21b, and preferably further provided with a jacket 23
surrounding an outer surface of the reactor as a
temperature regulating means for regulating a temperature
of the outer surface of the reactor and a stirrer 24 for
25 stirring a content therein. The effluent ports 11b and 21b

are located at a top of each of the reactors. On the other hand, the supply ports 11a and 21a may be generally located at an appropriate position of a lower part of each of the reactors, although this embodiment is not limited thereto.

5 Each of these reactors 10 and 20 may be provided with a temperature sensor T as a temperature detecting means for detecting a temperature in the reactor.

The first reactor 10 and the second reactor 20 may have the same or different inner volume from each other.
10 Making the inner volume of the first reactor and the inner volume of the second reactor different from each other, it is possible to effectively differentiate between the first reactor 10 and the second reactor 20 in an average residence time.

15 The stirrers 14 and 24 are a member for substantially attaining a complete mixing condition in the reactors. These stirrers may have any appropriate stirring blade(s), for example, may have blades of MIG impeller, MAXBLEND impeller (registered trademark, manufactured by Sumitomo
20 Heavy Industries, Ltd.), paddle impeller, double helical ribbon impeller, FULLZONE impeller (registered trademark, manufactured by Kobelco Eco-Solutions Co., Ltd.) and so on. In order to increase stirring effect in the reactor, it is preferable to provide the reactor with a baffle(s).
25 However, this embodiment is not limited thereto, but may

have any appropriate configuration in place of the stirrers 14 and 24 as long as a complete mixing condition can be substantially attained in the reactors.

In general, the reactors 10 and 20 are more preferable when they have a higher stirring efficiency. However, in view of avoiding the reactors from being added with an unnecessary amount of heat by the stirring operation, it is preferable that a power of stirring is not more than necessary. The power of stirring is not specifically limited, but preferably 0.5 to 20 kW/m^3 , and more preferably 1 to 15 kW/m^3 . As a viscosity of the reaction system becomes higher (or a content ratio of a polymer in the reaction system becomes higher), it is preferable to set the power of stirring at a larger level.

As shown in the drawings, the supply port 11a of the first reactor 10 is connected through a raw material supply line 9 to a raw material monomer tank (a supply source of a raw material monomer) 1 and a polymerization initiator tank (a supply source of a polymerization initiator and, if necessary, of a raw material monomer) 3 via pumps 5 and 7, respectively. In this embodiment, the supply source of the raw material monomer and the polymerization initiator is the raw material monomer tank 1 and the polymerization initiator tank 3, but the number of the supply source of the raw material monomer and the polymerization initiator,

the forms of the raw material monomer and the polymerization initiator (in a case of a mixture, for example, a composition thereof) and so on are not particularly limited as long as the raw material monomer and the polymerization initiator can be supplied to the first reactor 10, appropriately. Although it is not necessary for this embodiment, but another supply port 11c may be provided to the first reactor 10 and this supply port 11c may be connected to the polymerization initiator tank 3 via the pump 7 as shown by a dotted line in Fig. 1. The effluent port 11b of the first reactor 10 is connected to the supply port 21a of the second reactor 20 through a connection line 15. The effluent port 21b of the second reactor 20 is linked up to an effluent line 25. Thus, the first reactor 10 and the second reactor 20 are connected in series. There is preferably no pump on the connection line 15 between the effluent port 11b of the first reactor 10 and the supply port 21a of the second reactor 20.

It is not necessary for this embodiment, but the second reactor 20 may be connected to a polymerization initiator tank (a supply source of an additional polymerization initiator and, if necessary, of a raw material monomer) 17 via a pump 19. In this embodiment, the supply source of the additional polymerization initiator is the polymerization initiator tank 17, but the

number of the supply source of the additional polymerization initiator, the form of the polymerization initiator (in a case of a mixture, for example, a composition thereof) and so on are not particularly limited as long as the additional polymerization initiator can be supplied to the second reactor 20, appropriately. In a case where the polymerization initiator tank 17 and the pump 19 are present, the supply port 21a of the second reactor 20 may be connected to the polymerization initiator tank 17 via the pump 19 through the connection line 15 as shown by a solid line in Fig. 1, or the second reactor 20 may be provided with another supply port 21c so that this supply port 21c is connected to the polymerization initiator tank 17 via the pump 19 as shown by, for example, a dotted line in Fig. 1.

The pumps 5 and 7 and, if present, the pump 19 are not particularly limited, but preferably pumps being able to set flow rates from the raw material monomer tank 1 and the polymerization initiator tank 3 and a flow rate from the polymerization initiator tank 17, if present, at constant values. More specifically, multiple reciprocating pumps are preferred, and more preferred are pulsation-free controlled-volume pumps such as a duplicate pulsation-free controlled-volume pump and a triplex pulsation-free controlled-volume pump. By using these, it is possible to

control a supply amount (or a supply flow rate, which also applies hereinafter) of the raw material monomer and the polymerization initiator to the first reactor 10 and, if necessary, an additional supply amount of the
5 polymerization initiator (or the raw material monomer and the polymerization initiator) to the second reactor 20.

Further, it is not necessary for this embodiment, but the connection line 15 for connecting the effluent port 11b of the first reactor 10 to the supply port 21a of the
10 second reactor 20 is preferably provided with a jacket or the like (not shown in the drawings) surrounding an outer surface of the connection line 15, as a temperature regulating means for controlling a temperature of the connection line 15. Thereby, it is possible to control the
15 temperature of the connection line 15 (more specifically, a temperature of the outer surface of the connection line, and thus a temperature in the connection line) so that this temperature is a substantially same temperature as the temperature in the first reactor 10. In a case where the
20 first reactor 10 is provided with the temperature sensor T as a temperature detecting means for detecting the temperature in the first reactor 10 as in this embodiment, the temperature regulating means of the connection line 15 can be controlled so that the temperature of the connection
25 line 15 is at a substantially same temperature as the

temperature in the first reactor 10 detected by this temperature sensor T.

It is preferable that each of the members described in the above with reference to Fig. 1 is appropriately
5 connected to a control unit (not shown in the drawings) so as to enable the control unit to control their operations. Thereby, in order to make the temperature of the outer surface of the reactor set for each of the jackets (temperature regulating means) 13 and 23 correspond to the
10 temperature in the reactor detected by the temperature sensor (temperature detecting means) T with respect to each of the first reactor 10 and the second reactor 20, the apparatus is controllable by adjusting the supply amounts of the raw material monomer and the polymerization
15 initiator to the first reactor 10 with the operation of the pumps 5 and 7 or by regulating the temperature of the outer surface of the reactor set for the jackets 13 and 23; and also, in a case where the polymerization initiator tank 17 and the pump 19 are present, the apparatus is controllable
20 by adjusting the additional supply amount of the polymerization initiator (or the raw material monomer and the polymerization initiator) to the second reactor 20 with the operation of the pump 19. Further, in order to make the temperature in the connection line 15 substantially
25 equal to the temperature in the first reactor 10 detected

by the temperature sensor (temperature detecting means) T, the apparatus is controllable by adjusting the temperature of the outer surface of the connection line 15 set for the jacket (temperature regulating means, not shown in the drawings) surrounding the connection line 15. It is preferable that the temperature in the connection line 15 is actually measured by the temperature detecting means for detecting the connection line 15. However, in some cases depending on the polymerization reaction conditions in the first reactor 10, due to some causes such as that all of the supplied polymerization initiator is spent, an intermediate composition (hereinafter described) taken from the effluent port 11b does not let the polymerization reaction proceed in the connection line 15, that is, no heat of the polymerization reaction is generated in the connection line 15. In such case, the temperature of the jacket surrounding the connection line 15 is set at the substantially same temperature as the temperature in the first reactor 10, or the connection line 15 is covered with a lagging in place of the jacket, so that the temperature in the connection line 15 can become the substantially same temperature as the temperature in the first reactor 10, and considering the temperature in the connection line 15 as a substantially same temperature as the temperature of the jacket surrounding the connection line 15 is allowable.

The jackets 13 and 23 surround almost the whole of the reactors 10 and 20, respectively to appropriately heat or retain the heat of the reactors 10 and 20 by introducing steam, hot water, organic heat medium or the like from a heat medium supply route (not shown in the drawings). The temperature of the jackets 13 and 23 is able to be appropriately regulated with a temperature or pressure of the heat medium to be introduced. The heat medium introduced into the jackets 13 and 23 is removed from a heat medium discharge route (not shown in the drawings). The temperature and/or pressure of the jackets 13 and 23 are detected by a sensor such as a temperature sensor (not shown in the drawings) located on the heat medium discharge route. The point of location of a sensor such as the temperature sensor is not particularly limited, but it may be located, for example, on the heat medium supply route, or in the jackets 13 and 23. When the connection line 15 is provided with the jacket, the jacket of the connection line 15 may have a similar structure to these jackets 13 and 23.

For the polymerization reaction in the reactors 10 and 20, it is required to proceed at a generally constant temperature in each of the reactors 10 and 20 in view of obtaining a polymer with a constant quality. Therefore, the above described temperature regulating means (jackets

13 and 23) is controlled at a constant temperature which has been set beforehand, so that the temperature inside the reactors 10 and 20 can be maintained respectively at a generally constant temperature.

5 The setting temperature of the above described temperature regulating means (jackets 13 and 23) is transmitted to a supply flow rate control means, which hereinafter described, to be used as data for determining whether control of the supply flow rate with the monomer
10 supply means (pump 5) and/or the initiator supply means (pump 7 and, if present, pump 19) is necessary or not. The setting temperature of the above described temperature regulating means (jackets 13 and 23) can be regulated by controlling the temperature or pressure of the above
15 described heat medium.

As to the supply flow rate control means, an example thereof is a control unit (not shown in the drawings) provided with CPU, ROM, RAM and so on.

20 The ROM of the control unit is a device for storing a program which controls the pumps 5 and 7 and, if present, the pump 19 and so on. The RAM of the control unit is a device for temporary storing data of the temperatures in the reactors 10 and 20 detected by the temperature sensor T, data of the setting temperatures of the jackets 13 and 23,
25 data of, if present, the setting temperature of the jacket

of the connection line 15, and so on in order to execute the above program.

The CPU of the control unit executes the program stored in the ROM based on data such as the data of the temperatures in the reactors 10 and 20 and the data of the setting temperatures of the jackets 13 and 23 stored in the above RAM so that the supply flow rates of the raw material monomer and/or the polymerization initiator to the reactors 10 and 20 is controlled by the monomer supply means (pump 5) and/or the initiator supply means (pump 7 and, if present, pump 19). In a case where the connection line 15 is provided with the jacket as the temperature regulating means, the CPU of the control unit executes the program stored in the ROM (which may be either a part of the above program or other program than the above program) based on data such as the data of the temperatures in the reactors 10 and 20 and the data of the setting temperature of the jacket (not shown in the drawings) of the connection line 15 stored in the above RAM so that the setting temperature of the jacket of the connection line 15 can be controlled.

An example of the control by the supply flow rate control means (control unit) will be described below.

When the temperature in the reactor 10 detected by the temperature sensor T exceeds the setting temperature of the jacket 13 as the temperature regulating means, the CPU

executes the program in the ROM to control, for example, the pump 7 so as to decrease the supply flow rate of the polymerization initiator into the reactor 10. In a case where the polymerization initiator tank 17 and the pump 19 are present, when the temperature in the reactor 20 detected by the temperature sensor T exceeds the setting temperature of the jacket 23 as the temperature regulating means during the pump 19 supplies the polymerization initiator to the reactor 20 to conduct the polymerization, the CPU executes the program in the ROM to control, for example, the pump 19 so as to decrease the supply flow rate of the polymerization initiator into the reactor 20. By conducting such control, polymerization heat generated in the reactors 10 and/or 20 can be decreased, and thereby the temperatures in the reactors 10 and/or 20 can be lowered.

On the other hand, when the temperature in the reactor 10 is below the setting temperature of the jacket 13, the CPU executes the program in the ROM to control, for example, the pump 7 so as to increase the supply flow rate of the polymerization initiator into the reactor 10. In a case where the polymerization initiator tank 17 and the pump 19 are present, when the temperature in the reactor 20 is below the setting temperature of the jacket 23 during the pump 19 supplies the polymerization initiator to the reactor 20 to conduct the polymerization, the CPU executes

the program in the ROM to control, for example, the pump 19 so as to increase the supply flow rate of the polymerization initiator into the reactor 20. By conducting such control, polymerization heat generated in the reactors 10 and/or 20 can be increased, and thereby the temperatures in the reactors 10 and/or 20 can be raised.

For example, when the control over the pump 7 and, if present, the pump 19 for the polymerization reaction in the reactors 10 and 20 results in remarkable decrease in the total supply flow rate into the reactors 10 and 20, it is preferable to not only control the pump 7 and, if present, the pump 19 so as to decrease the supply flow rate of the polymerization initiator, but also to control the pump 5 so as to increase the supply flow rate of the raw material monomer at the same time.

Further, as another example of the control, the following control is noted. That is, when the temperature in the reactor 10 detected by the temperature sensor T exceeds the setting temperature of the jacket 13 as the temperature regulating means, the pump 5 is controlled to increase the supply flow rate of the raw material monomer, so that the relative supply flow rate of the polymerization initiator into the reactor 10 is decreased. By conducting such control, the temperature in the reactor 10 can also be lowered.

A ratio of the supply flow rate of the raw material monomer and the supply flow rate of the polymerization initiator can be appropriately set depending on the kind of the polymer generated, the kind of the polymerization initiator used, and so on.

Also, degree of increase or decrease in the supply flow rate of the raw material monomer and/or the supply flow rate of the polymerization initiator can be appropriately set depending on the kind of the polymer generated, the kind of the polymerization initiator used, and so on. However, in a case what is supplied to the reactors 10 and 20 by the initiator supply means is not the polymerization initiator only, but the raw material monomer comprising the polymerization initiator, it is necessary to consider a content ratio of the polymerization initiator in the raw material monomer comprising polymerization initiator to control the supply flow rate of the polymerization initiator.

Further, as still another example of the control, the following control is noted for a case where the connection line 15 is provided with the jacket as the temperature regulating means. That is, when the temperature in the reactor 10 detected by the temperature sensor T is different from the temperature in the connection line 15 (conveniently, the setting temperature of the jacket of the

connection line 15) by a degree more than, for example, $\pm 5^{\circ}\text{C}$, the setting temperature of the jacket of the connection line 15 is regulated so that the temperature in the connection line 15 (conveniently, the setting
5 temperature of the jacket of the connection line 15) becomes a substantially same temperature as the temperature of the reactor 10.

Additionally, it is not necessary for this embodiment, but a preheater 31 and a devolatilizing extruder 33 may be
10 located downstream of the effluent line 25. There may be a pressure adjusting valve (not shown in the drawings) provided between the preheater 31 and the devolatilizing extruder 33. An extruded object after devolatilization is discharged from a discharge line 35.

15 As the preheater 31, any appropriate heater can be used as long as it is able to heat a viscous fluid. As the devolatilizing extruder 33, a single or multi screw devolatilizing extruder can be used.

Further, there may be a recovery tank 37 for storing
20 the raw material monomer which is separated and recovered from a volatile component (comprising unreacted raw material, mainly) having separated with the devolatilizing extruder 33.

25 Next, a process for producing a polymer composition

conducted by using such apparatus will be described. In this embodiment, a case of conducting continuous polymerization of a methacrylic ester monomer, in the other words, a case of producing a methacrylic ester polymer will
5 be described as an example, although the present invention is not limited thereto.

- Preparation

At first, the raw material monomer, the polymerization
10 initiator and so on are prepared.

As the raw material monomer, a methacrylic ester monomer is used in this embodiment.

Examples of the methacrylic ester monomer are

- alkyl methacrylate (of which alkyl group has 1 to 4
15 carbons) alone, or

- a mixture of not less than 80% by weight of alkyl methacrylate (of which alkyl group has 1 to 4 carbons) and not more than 20% by weight of other vinyl monomer copolymerizable therewith.

20 Examples of alkyl methacrylate (of which alkyl group has 1 to 4 carbons) include methyl methacrylate, ethyl methacrylate, n-propyl methacrylate, isopropyl methacrylate, n-butyl methacrylate, t-butyl methacrylate, sec-butyl methacrylate, isobutyl methacrylate, and so on. Among them,
25 methyl methacrylate is preferred. The above described

examples of alkyl methacrylate may be used alone or in combination of at least two of them.

Examples of copolymerizable vinyl monomer include monofunctional monomers having one double bond which is radical-polymerizable and multifunctional monomers having two or more double bonds which are radical-polymerizable. More specifically, the monofunctional monomers having one double bond which is radical-polymerizable include, for example, methacrylic esters such as benzyl methacrylate and 2-ethylhexyl methacrylate (except for the above described alkyl methacrylate (of which alkyl group has 1 to 4 carbons)); acrylic esters such as methyl acrylate, ethyl acrylate, propyl acrylate, butyl acrylate, and 2-ethylhexyl acrylate; unsaturated carboxylic acids or acid anhydrides thereof such as acrylic acid, methacrylic acid, maleic acid, itaconic acid, maleic acid anhydride, and itaconic acid anhydride; hydroxy group-containing monomers such as 2-hydroxyethyl acrylate, 2-hydroxypropyl acrylate, monoglycerol acrylate, 2-hydroxyethyl methacrylate, 2-hydroxypropyl methacrylate, and monoglycerol methacrylate; nitrogen-containing monomers such as acrylamide, methacrylamide, acrylonitrile, methacrylonitrile, diacetoneacrylamide, and dimethylaminoethyl methacrylate; epoxy group-containing monomers such as allyl glycidyl ether, glycidyl acrylate, and glycidyl methacrylate;

styrene based monomers such as styrene and α -methylstyrene. The multifunctional monomers having two or more double bonds which are radical-polymerizable include, for example, diesters of unsaturated carboxylic acids and glycols such as ethylene glycol dimethacrylate, and butane diol dimethacrylate; unsaturated carboxylic acid alkenyl esters such as allyl acrylate, allyl methacrylate, and allyl cinnamate; polybasic acid polyalkenyl esters such as diallyl phthalate, diallyl maleate, triallyl cyanurate, and triallyl isocyanurate; esters of unsaturated carboxylic acid and polyalcohol such as trimethylolpropane triacrylate; and divinylbenzene. The above described examples of copolymerizable vinyl monomer may be used alone or in combination of at least two of them.

As the polymerization initiator, for example, a radical initiator is used in this embodiment.

Examples of a radical initiator include azo compounds such as azobisisobutyronitrile, azobisdimethylvaleronitrile, azobiscyclohexanenitrile, 1,1'-azobis(1-acetoxy-1-phenylethane), dimethyl 2,2'-azobisisobutylate, and 4,4'-azobis-4-cyanovaleric acid; organic peroxides such as benzoyl peroxide, lauroyl peroxide, acetyl peroxide, caprylyl peroxide, 2,4-dichlorobenzoyl peroxide, isobutyl peroxide, acetyl cyclohexylsulfonyl peroxide, t-butyl peroxy-pivalate, t-butyl peroxyneodecanoate, t-butyl

peroxyneohexanoate, t-butyl peroxy-2-ethylhexanoate, 1,1-di(t-butylperoxy)cyclohexane, 1,1-di(t-butylperoxy)-3,3,5-trimethylcyclohexane, 1,1-di(t-hexylperoxy)-3,3,5-trimethylcyclohexane, isopropyl peroxydicarbonate, isobutyl peroxydicarbonate, s-butyl peroxydicarbonate, n-butyl peroxydicarbonate, 2-ethylhexyl peroxydicarbonate, bis(4-t-butylcyclohexyl) peroxydicarbonate, t-amyl peroxy-2-ethylhexanoate, 1,1,3,3-tetramethyl butyl peroxy-ethylhexanoate, 1,1,2-trimethyl propyl peroxy-2-ethylhexanoate, t-butyl peroxy isopropyl monocarbonate, t-amyl peroxy isopropyl monocarbonate, t-butyl peroxy-2-ethylhexyl carbonate, t-butyl peroxy allyl carbonate, t-butyl peroxy isopropyl carbonate, 1,1,3,3-tetramethyl butyl peroxy isopropyl monocarbonate, 1,1,2-trimethyl propyl peroxy isopropyl monocarbonate, 1,1,3,3-tetramethyl butyl peroxy isononate, 1,1,2-trimethyl propyl peroxy-isononate, and t-butyl peroxybenzoate.

These polymerization initiators may be used alone or in combination of at least two of them.

The polymerization initiator is selected according to the kinds of the polymer generated and the raw material monomer used. For example, while the present invention is not particularly limited, those of radical polymerization initiator having a half-life not more than one minute at the polymerization temperature are preferable. When the

half-life at the polymerization temperature is at most one minute, the reaction rate is suitable, thus the initiator is suitable for the polymerization reaction in the continuous polymerization apparatus.

5 The supply amount of the polymerization initiator (radical initiator) is not particularly limited, but generally 0.001 to 1% by weight with respect to the raw material monomer (the raw material monomer eventually supplied to the reactor 10). In a case where the
10 polymerization initiator tank 17 and the pump 19 are present in addition to the polymerization initiator tank 3 and the pump 7, the polymerization initiator can be supplied separately into the first reactor 10 and the second reactor 20. When the polymerization initiator tank
15 17 supplies the mixture of the raw material monomer and the polymerization initiator to the second reactor 20 by the pump 19, the total supply amount of the polymerization initiator supplied to the reactor 10 and the reactor 20 is made within the above range with respect to the sum of the
20 raw material monomer eventually supplied to the reactor 10 and the raw material monomer additionally supplied to the reactor 20.

 In addition to the raw material monomer and the polymerization initiator described above, any appropriate
25 other component(s), for example, a chain transfer agent, a

mold release agent, a rubbery polymer such as butadiene and styrene-butadiene rubber (SBR), a heat stabilizing agent, an ultraviolet absorbing agent, and so on may be used. The chain transfer agent is used for adjusting a molecular weight of the polymer generated. The mold release agent is used for improving moldability (or processability) of a resin composition obtained from the polymer composition. The heat stabilizing agent is used for preventing a produced polymer from thermal degradation. The ultraviolet absorbing agent is used for preventing a produced polymer from being degraded by ultraviolet rays.

As to the chain transfer agent, either monofunctional or polyfunctional chain transfer agent can be used. More specifically, examples thereof include alkyl mercaptans such as n-propyl mercaptan, isopropyl mercaptan, n-butyl mercaptan, t-butyl mercaptan, n-hexyl mercaptan, n-octyl mercaptan, 2-ethylhexyl mercaptan, n-dodecyl mercaptan, and t-dodecyl mercaptan; aromatic mercaptans such as phenyl mercaptan and thiocresol; mercaptans having 18 or less carbons such as ethylene thioglycol; polyalcohols such as ethylene glycol, neopentyl glycol, trimethylolpropane, pentaerythritol, dipentaerythritol, tripentaerythritol, and sorbitol; those of which hydroxyl group is esterified with thioglycolic acid or 3-mercaptopropionic acid, 1,4-dihydronaphthalene, 1,4,5,8-tetrahydronaphthalene, β -

terpinene, terpinolene, 1,4-cyclohexadiene, hydrogen sulfide and so on. These may be used alone or in combination of at least two of them.

The supply amount of the chain transfer agent is not particularly limited since it varies depending on the kind of the chain transfer agent used and so on. For example, in a case of using mercaptans, it is preferably 0.01 to 3% by weight, and more preferably 0.05 to 1% by weight with respect to the raw material monomer (the raw material monomer eventually supplied to the reactor 10).

The mold release agent is not particularly limited. Specifically, esters of higher fatty acids, higher fatty alcohols, higher fatty acids, higher fatty acid amides, metal salts of higher fatty acids and so on are exemplified. As the mold release agent, one or more kinds thereof may be used.

As to the esters of higher fatty acids, more specifically, examples thereof include saturated fatty acid alkyl esters such as methyl laurate, ethyl laurate, propyl laurate, butyl laurate, octyl laurate, methyl palmitate, ethyl palmitate, propyl palmitate, butyl palmitate, octyl palmitate, methyl stearate, ethyl stearate, propyl stearate, butyl stearate, octyl stearate, stearyl stearate, myristyl myristate, methyl behenate, ethyl behenate, propyl behenate, butyl behenate, octyl behenate; unsaturated fatty acid

alkyl esters such as methyl oleate, ethyl oleate, propyl oleate, butyl oleate, octyl oleate, methyl linoleate, ethyl linoleate, propyl linoleate, butyl linoleate, octyl linoleate; saturated fatty acid glycerides such as lauric monoglyceride, lauric diglyceride, lauric triglyceride, 5 palmitic monoglyceride, palmitic diglyceride, palmitic triglyceride, stearic monoglyceride, stearic diglyceride, stearic triglyceride, behenic monoglyceride, behenic diglyceride, behenic triglyceride; unsaturated fatty acid glycerides such as oleic monoglyceride, oleic diglyceride, 10 oleic triglyceride, linolic monoglyceride, linolic diglyceride, linolic triglyceride. Among them, methyl stearate, ethyl stearate, butyl stearate, octyl stearate, stearic monoglyceride, stearic diglyceride, stearic 15 triglyceride, and the like are preferred.

As to the higher fatty alcohols, more specifically, examples thereof include saturated fatty (or aliphatic) alcohols such as lauryl alcohol, palmityl alcohol, stearyl alcohol, isostearyl alcohol, behenyl alcohol, myristyl 20 alcohol, cetyl alcohol; unsaturated fatty (or aliphatic) alcohols such as oleyl alcohol, linolyl alcohol. Among them, stearyl alcohol is preferred.

As to the higher fatty acids, more specifically, examples thereof include saturated fatty acids such as 25 caproic acid, caprylic acid, capric acid, lauric acid,

myristic acid, palmitic acid, stearic acid, arachidic acid, behenic acid, lignoceric acid, 12-hydroxyoctadecanoic acid; unsaturated fatty acids such as palmitoleic acid, oleic acid, linoleic acid, linolenic acid, cetoleic acid, erucic acid, ricinoleic acid.

As to the higher fatty acid amides, more specifically, examples thereof include saturated fatty acid amides such as lauric acid amide, palmitic acid amide, stearic acid amide, behenic acid amide; unsaturated fatty acid amides such as oleic acid amide, linoleic acid amide, erucic acid amide; amides such as ethylene-bis-lauric acid amide, ethylene-bis-palmitic acid amide, ethylene-bis-stearic acid amide, N-oleyl stearamide. Among them, stearic acid amide and ethylene-bis-stearic acid amide are preferred.

As to the metal salts of higher fatty acids, examples thereof include sodium salts, potassium salts, calcium salts and barium salts of the above-described higher fatty acids, and so on.

A used amount of the mold release agent is preferably adjusted in a range from 0.01 to 1.0 part by weight, and more preferably adjusted in a range from 0.01 to 0.50 part by weight, with respect to 100 parts by weight of a polymer contained in a polymer composition to be obtained.

The heat stabilizing agent is not particularly limited. A phosphorous-based heat stabilizing agent and organic

disulfide compounds are exemplified as the heat stabilizing agent. Among them, the organic disulfide compounds are preferable. As the heat stabilizing agent, one or more kinds thereof may be used.

5 As to the phosphorus-based heat stabilizing agent, examples thereof include tris(2,4-di-tert-butylphenyl)phosphite, 2-[[2,4,8,10-tetrakis(1,1-dimethylethyl)dibenzo [d,f][1,3,2]dioxaphosphine-6-yl]oxy]-N,N-bis[2-[[2,4,8,10-tetrakis(1,1-

10 dimethylethyl)dibenzo [d,f][1,3,2]dioxaphosphine-6-yl]oxy]-ethyl]ethanamine, diphenyl tridecyl phosphite, triphenyl phosphite, 2,2-methylenebis(4,6-di-tert-butylphenyl)octylphosphite, bis(2,6-di-tert-butyl-4-methylphenyl)pentaerythritol diphosphite, and so on. Among

15 them, 2,2-methylenebis(4,6-di-tert-butylphenyl)octylphosphite is preferred.

As to the organic disulfide compounds, examples thereof include dimethyl disulfide, diethyl disulfide, di-n-propyl disulfide, di-n-butyl disulfide, di-sec-butyl

20 disulfide, di-tert-butyl disulfide, di-tert-amyl disulfide, dicyclohexyl disulfide, di-tert-octyl disulfide, di-n-dodecyl disulfide, di-tert-dodecyl disulfide, and so on. Among them, di-tert-alkyl disulfide is preferred, and di-tert-dodecyl disulfide is more preferred.

25 A used amount of the heat stabilizing agent is

preferably 1 to 2,000 ppm by weight with respect to a polymer contained in a polymer composition to be obtained. On molding a polymer composition (more specifically, a resin composition after devolatilization) to prepare a molded article from the polymer composition of the present invention, a molding temperature is set at a higher temperature for the purpose of improving its molding processability in some cases. Use of the heat stabilizing agent is effective for such case.

As the kinds of the ultraviolet absorbing agent, a benzophenone-based ultraviolet absorbing agent, a cyanoacrylate-based ultraviolet absorbing agent, a benzotriazole-based ultraviolet absorbing agent, a malonic ester-based ultraviolet absorbing agent, an oxalic anilide-based ultraviolet absorbing agent and so on are exemplified. These ultraviolet absorbing agents may be used alone or in combination of at least two of them. Among them, the benzotriazole-based ultraviolet absorbing agent, the malonic ester-based ultraviolet absorbing agent, and the oxalic anilide-based ultraviolet absorbing agent are preferable.

As to the benzophenone-based ultraviolet absorbing agent, examples thereof include 2,4-dihydroxybenzophenone, 2-hydroxy-4-methoxybenzophenone, 2-hydroxy-4-methoxybenzophenone-5-sulfonic acid, 2-hydroxy-4-

octyloxybenzophenone, 4-dodecyloxy-2-hydroxybenzophenone, 4-benzyloxy-2-hydroxybenzophenone, 2,2'-dihydroxy-4,4'-dimethoxybenzophenone, and so on.

As to the cyanoacrylate-based ultraviolet absorbing agent, examples thereof include ethyl 2-cyano-3,3-diphenylacrylate, 2-ethylhexyl 2-cyano-3,3-diphenylacrylate, and so on.

As to the benzotriazole-based ultraviolet absorbing agent, examples thereof include 2-(2-hydroxy-5-methylphenyl)-2H-benzotriazole, 5-chloro-2-(3,5-di-tert-butyl-2-hydroxyphenyl)-2H-benzotriazole, 2-(3-tert-butyl-2-hydroxy-5-methylphenyl)-5-chloro-2H-benzotriazole, 2-(3,5-di-tert-pentyl-2-hydroxyphenyl)-2H-benzotriazole, 2-(3,5-di-tert-butyl-2-hydroxyphenyl)-2H-benzotriazole, 2-(2H-benzotriazole-2-yl)-4-methyl-6-(3,4,5,6-tetrahydrophthalimidylmethyl)phenol, 2-(2-hydroxy-5-tert-octylphenyl)-2H-benzotriazole, and so on.

As to the malonic ester-based ultraviolet absorbing agent, 2-(1-aryl alkylidene)malonates are generally used, and examples thereof include dimethyl 2-(p-methoxybenzylidene)malonate and so on.

As to the oxalic anilide-based ultraviolet absorbing agent, 2-alkoxy-2'-alkyloxalic anilides are generally used, and examples thereof include 2-ethoxy-2'-ethyloxalic anilide and so on.

A used amount of the ultraviolet absorbing agent is preferably 5 to 1,000 ppm by weight with respect to a polymer contained in a polymer composition to be obtained.

In the raw material monomer tank 1, the raw material
5 monomer (one kind or a mixture of two or more kinds) as described above is appropriately prepared (together with other component(s) such as the chain transfer agent as the case may be). In the polymerization initiator tank 3, the polymerization initiator as described above is
10 appropriately prepared with the raw material monomer if necessary (together with other component(s) such as the chain transfer agent as the case may be). The polymerization initiator tank 3 may store the polymerization initiator alone or in the form of the
15 mixture of the raw material monomer and the polymerization initiator (may further comprising other component(s) such as the chain transfer agent as the case may be). In a case of using the polymerization initiator tank 17, in the polymerization initiator tank 17, the polymerization
20 initiator as described above is appropriately prepared with the raw material monomer if necessary (together with other component(s) such as the chain transfer agent as the case may be). The polymerization initiator tank 17 may store the polymerization initiator alone or in the form of the
25 mixture of the raw material monomer and the polymerization

initiator (may further comprising other component(s) such as the chain transfer agent as the case may be). However, in a case where the polymerization initiator tank 17 is connected to the supply port 21c via the pump 19, storing
5 of the polymerization initiator alone raises a concern of local proceeding of the polymerization reaction in the reactor 20 since the polymerization initiator is solely supplied to the reactor 20. On the contrary, storing in the form of the mixture of the raw material monomer and the
10 polymerization initiator is able to solve such concern since the polymerization initiator is mixed with a part of the raw material monomer beforehand.

- First polymerization Step

15 The raw material monomer and the polymerization initiator are supplied to the first reactor 10 through the supply port 11a from the raw material monomer tank 1 and the polymerization initiator tank 3 as the supply source of the raw material monomer and the polymerization initiator.
20 More specifically, the raw material monomer is supplied from the raw material monomer tank 1 by the pump 5, and the polymerization initiator (preferably, the mixture of the raw material monomer and the polymerization initiator, which is also simply referred to as the polymerization
25 initiator herein) is supplied from the polymerization

initiator tank 3 by the pump 7, and they merge together through the raw material supply line 9 into the first reactor 10 via the supply port 11a. Also, the polymerization initiator may be supplied from the
5 polymerization initiator tank 3 by the pump 7 to the first reactor 10 via the supply port 11c as shown by the dotted line in Fig. 1.

For supplying the polymerization initiator to the first reactor 10, when the mixture of the raw material
10 monomer and the polymerization initiator is prepared in the polymerization initiator tank 3 and supplied therefrom, it is preferable to adjust a ratio A : B in a range from 80:20 to 98:2 wherein A represents the supply flow rate (kg/h) of the raw material monomer from the raw material monomer tank
15 1, and B represents the supply flow rate (kg/h) of the mixture of the raw material monomer and the polymerization initiator (of which content ratio of the polymerization initiator is 0.002 to 10% by weight) from the polymerization initiator tank 3.

20 The temperature of the raw material monomer and the polymerization initiator supplied to the first reactor 10 is not particularly limited. However, this is one of factors which may change the polymerization temperature by losing a heat balance in the reactor, and therefore it is
25 preferable to adjust that temperature appropriately by a

heater/cooler (not shown in the drawings) before the supply to the reactor 10.

The raw material monomer and the polymerization initiator supplied to the first reactor 10 as described in the above are subjected to continuous polymerization, continuous bulk polymerization in this embodiment (in other words, polymerization with no solvent), under an adiabatic condition (condition with substantially no heat transfer to or from outside of the reactor) in the first reactor 10. This first polymerization step has only to proceed the polymerization reaction partway, and an intermediate composition is taken from the effluent port 11b of the first reactor 10.

In the first polymerization step, the continuous polymerization can be conducted under a condition in which the reactor is filled with the reaction mixture while substantially no gas phase is present (hereinafter referred to as a fully filled condition). This is especially suitable to the continuous bulk polymerization. The fully filled condition can prevent beforehand the problems such as that gel adheres to and grows on the inner surface of the reactor, and that this gel is immixed into the reaction mixture to degrade quality of a polymer composition obtained in the end. Further, the fully filled condition enables all of the inner volume of the reactor to be used

as a reaction space, and thereby a high productivity can be attained.

Since the effluent port 11b of the first reactor 10 is located at the reactor's top, the fully filled condition is conveniently realized simply by conducting the supply to
5 and the taking from the first reactor 10, continuously.

Further in the first polymerization step, the continuous polymerization is conducted under the adiabatic condition. This is especially suitable to the continuous
10 bulk polymerization. The adiabatic condition can prevent beforehand the problems such as that gel adheres to and grows on the inner surface of the reactor, and that this gel is immixed into the reaction mixture to degrade quality of a polymer composition obtained in the end. Further, the
15 adiabatic condition enables the polymerization reaction to become stable, and self regulating characteristics for suppressing a runaway reaction can be brought about.

The adiabatic condition can be realized by making the temperature of the inside of the first reactor 10 and the
20 temperature of the outer surface thereof generally equal to each other. More specifically, this can be realized, with the use of the above described control unit (not shown in the drawings), by adjusting the supply amounts of the raw material monomer and the polymerization initiator to the
25 first reactor 10 with operating the pumps 5 and 7 such that

the temperature of the outer surface of the first reactor 10 set for the jacket (temperature regulating means) 13 and the temperature in the first reactor 10 detected by the temperature sensor (temperature detecting means) T correspond to each other. It is not preferable to set the temperature of the outer surface of the reactor much higher than the temperature in the reactor since it adds extra amount of heat into the reactor. The smaller the difference between the temperature in the reactor and the temperature of the outer surface of the reactor is, the better it is. More specifically, it is preferable to adjust the temperature difference within the range of $\pm 5^{\circ}\text{C}$.

The heat generated in the first reactor 10 such as polymerization heat and stirring heat is generally carried away on taking the intermediate composition from the first reactor 10. The amount of the heat carried away by the intermediate composition is determined by the flow rate and the specific heat of the intermediate composition, and the temperature of the polymerization reaction.

The temperature of the continuous polymerization in the first polymerization step is understood as the temperature in the first reactor 10 (detected by the temperature sensor T). The first polymerization step is conducted at a temperature from 125 to 170°C , more

preferably at a temperature from 125 to 160°C. It is noted, however, that the temperature in the reactor may change according to various conditions until it reaches a static state.

5 The pressure of the continuous polymerization in the first polymerization step is understood as the pressure in the first reactor 10. This pressure is a pressure not less than a vapor pressure of the raw material monomer at the temperature in the reactor to prevent gas of the raw material monomer from generating in the reactor, and is
10 generally about 1.0 to 2.0 MPa in gauge pressure.

 A time period subjected to the continuous polymerization in the first polymerization step is understood as an average residence time in the first
15 reactor 10. The average residence time in the first reactor 10 can be set according to the productivity of the polymer in the intermediate composition and so on, and is not particularly limited, but, for example, from 15 minutes to 6 hours. The average residence time in the first
20 reactor 10 can be adjusted by using the pumps 5 and 7 to change the supply amount (supply flow rate) of the raw material monomer or the like to the first reactor 10. However, since the average residence time depends in a large part on the inner volume of the first reactor 10, how
25 the inner volume of the first reactor 10 and the inner

volume of the second reactor 20 are designed is important as hereinafter described.

As described in the above, the intermediate composition is taken from the effluent port 11b of the first reactor 10. The obtained intermediate composition comprises the generated polymer and the unreacted raw material monomer, and may further comprise the unreacted polymerization initiator, decomposed substance of the polymerization initiator, and so on.

Although this embodiment is not limited thereto, the polymerization rate in the intermediate composition is, for example, 5 to 80% by weight. The polymerization rate in the intermediate composition generally corresponds to the content ratio of the polymer in the intermediate composition.

- Second polymerization Step

The second polymerization step is conducted in series with and following to the first polymerization step.

After the intermediate composition obtained as described in the above is taken from the effluent port 11b of the first reactor, it is supplied to the second reactor 20 from the supply port 21a through the connection line 15. Then, the intermediate composition is further subjected to continuous polymerization, continuous bulk polymerization

in this embodiment, under an adiabatic condition in the first reactor 20. This second polymerization step is to let the polymerization reaction proceed to the desired polymerization rate, and a polymer composition (or
5 polymerization syrup) is taken from the effluent port 21b of the second reactor 20.

Hereinafter, the second polymerization step will be described mainly with respect to different points from the first polymerization step, and explanations similar to
10 those for the first polymerization step apply unless otherwise explained.

Although it is not necessary to this embodiment, the polymerization initiator tank 17 and the pump 19 may be used, if necessary. In a case of using the polymerization
15 initiator tank 17 and the pump 19, the additional (or fresh) polymerization initiator (preferably, the mixture of the raw material monomer and the polymerization initiator) is supplied from the polymerization initiator tank 17 by the pump 19 through the connection line 15 to the second
20 reactor 20 via the supply port 21a or the another supply port 21c, and thereby the intermediate composition is added with the additional polymerization initiator. The temperature of the polymerization initiator supplied to the second reactor 20 from the polymerization initiator tank 17
25 is not particularly limited. However, this is one of

factors which may change in the polymerization temperature by losing a heat balance in the reactor, and therefore it is preferable to adjust that temperature appropriately by a heater/cooler (not shown in the drawings) before the supply
5 to the reactor 20.

Also it is preferable to conduct the continuous polymerization so that the temperature of the connection line 15 is a substantially same temperature as the temperature in the first reactor 10. Avoiding the
10 temperature of the connection line 15 from being too low with respect to the temperature in the first reactor 10, a viscosity of the intermediate composition in the connection line 15 is prevented from being increased, so that the intermediate composition can be supplied to the second
15 reactor 20, stably. Avoiding the temperature of the connection line 15 from being too high with respect to the temperature in the first reactor 10, the temperature in the second reactor is prevented from being increased, so that qualities such as heat stability of a resin composition to
20 be obtained can be maintained. In order to make the temperature of the connection line 15 at a substantially same temperature as the temperature in the first reactor 10, the connection line 15 can be provided with the jacket as the temperature regulating means to adjust the setting
25 temperature of the jacket. When polymerization heat is not

generated in the connection line, the temperature of the connection line 15 is made at a substantially same temperature as the temperature in the first reactor 10 by providing the connection line 15 with a lagging, in place
5 of the jacket, to retain its heat (or to thermally insulate it from the outside).

For supplying the polymerization initiator to the second reactor 20, when the mixture of the raw material monomer and the polymerization initiator is prepared in the
10 polymerization initiator tanks 3 and 17 and supplied therefrom, it is preferable to adjust a ratio $A : (B_1 + B_2)$ in a range from 80:20 to 98:2 and a ratio $B_1 : B_2$ in a range from 10:90 to 90:10 wherein A represents the supply flow rate (kg/h) of the raw material monomer from the raw
15 material monomer tank 1, B_1 represents the supply flow rate (kg/h) of the mixture of the raw material monomer and the polymerization initiator (of which content ratio of the polymerization initiator is 0.002 to 10% by weight) from the polymerization initiator tank 3, and B_2 represents a
20 supply flow rate (kg/h) of the mixture of the raw material monomer and the polymerization initiator (of which content ratio of the polymerization initiator is 0.002 to 10% by weight) from the polymerization initiator tank 17.

Also in the second polymerization step, the continuous
25 polymerization can be conducted under a fully filled

condition. This is especially suitable to the continuous bulk polymerization. The fully filled condition can prevent beforehand the problems such as that gel adheres to and grows on the inner surface of the reactor, and that
5 this gel is immixed into the reaction mixture to degrade quality of the polymer composition obtained in the end. Further, the fully filled condition enables all of the inner volume of the reactor to be used as a reaction space, and thereby a high productivity can be attained.

10 Since the effluent port 21b of the second reactor 20 is located at the reactor's top, the fully filled condition is conveniently realized simply by conducting the supply to and the taking from the second reactor 20, continuously.

Also, further in the second polymerization step, the
15 continuous polymerization is conducted under the adiabatic condition. This is especially suitable to the continuous bulk polymerization. The adiabatic condition can prevent beforehand the problems such as that gel adheres to and grows on the inner surface of the reactor, and that this
20 gel is immixed into the reaction mixture to degrade quality of the polymer composition obtained in the end. Further, the adiabatic condition enables the polymerization reaction to become stable, and self regulating characteristics for suppressing a runaway reaction can be brought about.

25 The adiabatic condition can be realized by making the

temperature of the inside of the second reactor 20 and the temperature of the outer surface thereof generally equal to each other. More specifically, this can be realized, with the use of the above described control unit (not shown in the drawings), by adjusting the supply amounts of the raw material monomer and the polymerization initiator to the second reactor 20 with operating the pumps 5 and 7 and, if present, the pump 19 such that the temperature of the outer surface of the second reactor 20 set for the jacket (temperature regulating means) 23 and the temperature in the second reactor 20 detected by the temperature sensor (temperature detecting means) T correspond to each other. It is not preferable to set the temperature of the outer surface of the reactor much higher than the temperature in the reactor since it adds extra amount of heat into the reactor. The smaller the difference between the temperature in the reactor and the temperature of the outer surface of the reactor is, the better it is. More specifically, it is preferable to adjust the temperature difference within the range of $\pm 5^{\circ}\text{C}$.

The heat generated in the second reactor 20 such as polymerization heat and stirring heat is generally carried away on taking the polymer composition from the second reactor 20. The amount of the heat carried away by the polymer composition is determined by the flow rate and the

specific heat of the polymer composition, and the temperature of the polymerization reaction.

The temperature of the continuous polymerization in the second polymerization step is understood as the temperature in the second reactor 20. The second polymerization step is conducted at a temperature from 130 to 180°C, more preferably at a temperature from 140 to 180°C. Since the continuous polymerization is conducted under the adiabatic condition in the second polymerization step, the polymerization heat generated by the polymerization reaction makes the temperature at the second polymerization step higher than the temperature at the first polymerization step. Avoiding the temperature of the second polymerization step from being too low, a polymerization rate in the second polymerization step and therefore a productivity is prevented from being significantly decreased, so that the polymer composition can be efficiently produced, without requiring a larger reactor and installation for recovering the monomer. Avoiding the temperature of the second polymerization step from being too high, the syndiotacticity of the obtained polymer is prevented from being lowered, and therefore heat resistance of a resin composition obtained in the end is prevented from being lowered. Also, avoiding the temperature of the second polymerization step from being

too high, the polymerization initiator is prevented from being readily decomposed, and this eliminates necessity of a more amount of the polymerization initiator, which was used to compensate for drop in the polymerization efficiency, and therefore the heat stability of the resin composition obtained in the end is prevented from being lowered.

The pressure of the continuous polymerization in the second polymerization step is understood as the pressure in the second reactor 20. This pressure is generally about 1.0 to 2.0 MPa in gauge pressure, and may be equal to the pressure in the first polymerization step.

A time period subjected to the continuous polymerization in the second polymerization step is understood as an average residence time in the second reactor 20. The average residence time in the second reactor 20 can be set according to the productivity of the polymer in the polymer composition and so on, and is not particularly limited, but, for example, from 15 minutes to 6 hours. A ratio of the average residence time in the second reactor 20 to the average residence time in the first reactor 10 is preferably from 9/1 to 1/9, and more preferably from 8/2 to 2/8. The average residence time in the second polymerization step may be equal to the average residence time in the first polymerization step, but

preferably different from it. The average residence time in the second reactor 20 can be adjusted by using the pumps 5 and 7 and, if present, the pump 19 to change the supply amount (supply flow rate) of the raw material monomer or the like to the second reactor 20. However, since the average residence time depends in a large part on the inner volume of the second reactor 20, how the inner volume of the first reactor 10 and the inner volume of the second reactor 20 are designed is important as hereinafter described.

As described in the above, the polymer composition is taken from the effluent port 21b of the second reactor 20. The obtained polymer composition comprises the generated polymer, and may further comprise the unreacted raw material monomer, the unreacted polymerization initiator, decomposed substance of the polymerization initiator, and so on.

Although this embodiment is not limited thereto, the polymerization rate in the polymer composition is, for example, 30 to 90% by weight. The polymerization rate in the polymer composition generally corresponds to the content ratio of the polymer in the polymer composition. The higher the polymerization rate, the higher the productivity of the polymer, but also the higher the viscosity of the composition from intermediate composition

to the polymer composition, resulting in the larger the necessary power for stirring. The lower the polymerization rate, the lower the productivity of the polymer, resulting in the larger the load for recovering the unreacted raw material monomer. Therefore, it is preferable to set an appropriate polymerization rate as a target or a guide.

According to this embodiment, the first polymerization step is conducted at the temperature from 125 to 170°C, and the second polymerization step is conducted at the temperature from 130 to 180°C, and thereby it becomes possible to produce the polymer composition having high heat stability, with high productivity.

Furthermore, according to this embodiment, the ratio of an average residence time in the second reactor 20 to the average residence time in the first reactor 10 is preferably from 9/1 to 1/9, and thereby it becomes possible to produce the polymer composition having high heat stability, with high productivity.

In general, the following tendency is observed: the higher the polymerization temperature, the lower the syndiotacticity of the obtained polymer, the lower the heat resistance of a resin composition obtained in the end. Also, the following tendency is observed: the more amount of the polymerization initiator decomposed, the lower the polymerization efficiency, the more amount of the

polymerization initiator necessarily used to compensate for the polymerization efficiency, and as a result, the lower the heat stability of the resin composition obtained in the end. If the residence time becomes longer, the necessary amount of the polymerization initiator becomes small, so that the heat stability can be prevented from being lowered. However, this is not effective since it requires a larger reactor. Thus, it is more preferable to conduct the polymerization at a lower temperature in view of obtaining a resin composition having higher heat resistance and heat stability. However, if continuous polymerization is conducted in one stage only at a lower temperature with the use of the conventional continuous polymerization apparatus (JP 07-126308 A and JP 2006-104282 A), it brings about the polymerization rate lowered and the productivity significantly lowered for retaining the adiabatic condition, and therefore in order to assure the high productivity it requires a larger reactor and installation for recovering the monomer, so that it is not efficient.

In contrast, by conducting the continuous polymerization in two stages as in this embodiment, the polymerization reaction conditions, more specifically, the temperature, the time period (average residence time), the amount of the polymerization initiator (a ratio of the polymerization initiator to the raw material monomer) and

so on can be set for the first polymerization step and the second polymerization step, independently.

For example, it is possible in this embodiment to conduct the continuous polymerization in the first polymerization step at a relatively lower temperature and then to further conduct the continuous polymerization in the second polymerization step at a relatively higher temperature. More specifically, the first polymerization step is conducted at the temperature from 125 to 170°C, and the second polymerization step is conducted at the temperature from 130 to 180°C, and thereby it becomes possible to obtain a higher polymerization rate in the second polymerization step and a higher productivity compared with a case for conducting continuous polymerization in only one stage at a lower temperature, and to obtain a resin composition having higher heat stability and heat resistance compared with a case for conducting continuous polymerization in only one stage at a higher temperature. Furthermore, compared with a case for conducting the first polymerization step of the two stage continuous polymerization at a temperature less than 125°C, it becomes possible to reduce a used amount of the polymerization initiator in total for accomplishing a desired polymerization rate and thus to obtain a resin composition having higher heat stability.

How the polymerization reaction conditions are set for each of the first polymerization step and the second polymerization step may vary according to the polymer generated, the raw material monomer and the polymerization initiator used, the heat resistance, heat stability and productivity desired, and so on.

- Devolatilization Step

As described in the above, the polymer composition (polymerization syrup) taken from the effluent port 21b of the second reactor 20 may comprise the unreacted raw material monomer and polymerization initiator and so on, in addition to the generated polymer. Although this embodiment is not limited thereto, such polymer composition is preferably subjected to, for example, devolatilization to separate and recover the raw material monomer.

More specifically, the polymer composition is transferred to the preheater 31 through the effluent line 25. The polymer composition in the preheater 31 is added with a part or all of an amount of heat necessary to volatilize the volatile component which is mainly composed of the unreacted raw material monomer. Then, the polymer composition is transferred to the devolatilizing extruder 33 via the pressure adjusting valve (not shown in the drawings), and the volatile component is at least partially

removed in the devolatilizing extruder, and a residual extruded object is formed into pellets and discharged from the discharge line 35. Thereby, the resin composition comprising a methacrylic ester polymer is produced in the
5 form of the pellets.

As a method for transferring the above polymer composition, a method described in JP 4-48802 B is preferable. As a method of using a devolatilizing extruder, methods described in, for example, JP 3-49925 A, JP 51-
10 29914 B, JP 52-17555 B, JP 1-53682 B, JP 62-89710 A and so on are preferable.

Further, during or after devolatilization of the polymer composition in the devolatilizing extruder described above, the polymer composition or the extruded
15 object can be added with a mold release agent such as higher alcohols and higher fatty acid esters, an ultraviolet absorbing agent, a heat stabilizing agent, a colorant, an antistatic agent and so on, in order to incorporate them into the resin composition, if necessary.

20 The volatile component removed in the devolatilizing extruder 33 consists primarily of the unreacted raw material monomer and includes impurities; e.g. impurities originally contained in the raw material monomer, additives used if necessary, volatile by-product(s) generated in the
25 process of polymerization, oligomer such as dimer and

trimer, decomposed substance of the polymerization initiator, and so on. In general, a larger amount of the impurities make the obtained resin composition colored, which is not preferable. Then, the volatile component removed in the devolatilizing extruder 33 (which consists primarily of the unreacted raw material monomer and includes impurities as described above) may be passed through a monomer recovery column (not shown in the drawings), and treated by means of distillation, adsorption and so on in the monomer recovery column to remove the impurities from the above described volatile component. Thereby, the unreacted raw material monomer can be recovered with high purity, so that it can be suitably reused as the raw material monomer for polymerization. For example, continuous distillation is conducted in the monomer recovery column to recover the unreacted raw material monomer with high purity as a distillate liquid from the top of the monomer recovery column, and it may be transferred and recycled to the raw material monomer tank 1 after it is reserved in the recovery tank 37 once, or it may be transferred and recycled to the raw material monomer tank 1 without being reserved in the recovery tank 37. On the other hand, the impurities removed in the monomer recovery column may be disposed as a waste.

In order to prevent the recovered raw material monomer

from causing the polymerization reaction in the recovery tank 37 and/or the raw material monomer tank 1, it is preferable that a polymerization inhibitor exists in the recovery tank 37 or the raw material monomer tank 1 at a ratio of, for example, 2 to 8 ppm by weight with respect to the raw material monomer, and more preferably, in addition to this, an oxygen concentration in a gas phase in the recovery tank 37 or the raw material monomer tank 1 is set at 2 to 8% by volume. If the recovered raw material monomer is wanted to be preserved in the recovery tank 37 for a long time, it is preferable to reserve it at a low temperature of, for example, 0 to 5°C.

In this embodiment, the continuous bulk polymerization apparatus wherein the first reactor and the second reactor are both used to conduct the continuous bulk polymerization is described. However, the continuous polymerization apparatus of the present invention is not limited thereto, one or both of the first reactor and the second reactor may be used to conduct continuous solution polymerization. In such embodiment, since a solvent is used for the solution polymerization, the continuous polymerization apparatus is provided, in addition to a similar configuration to the continuous polymerization apparatus described in the above with reference to Fig. 1, with a solvent tank and a supply

line and a pump (supply means) associated with the solvent tank to supply the solvent to a certain reactor for conducting the solution polymerization. The solvent tank and the supply line and the pump (supply means) associated
5 with the solvent tank are not particularly limited, those similar to conventionally used ones can be used. The solvent can be supplied to the certain reactor for conducting the solution polymerization after being mixed with raw material monomer and/or the polymerization
10 initiator, or can be supplied to the certain reactor for conducting the solution polymerization, directly. In the above certain reactor, the polymerization step is conducted similarly (under an adiabatic condition) to the polymerization step described in the above with reference
15 to Fig. 1, except that the solvent is used in the polymerization reaction. As to the solvent, it is appropriately selected according to the raw material monomer of the solution polymerization reaction and so on, and not particularly limited, but examples thereof include
20 toluene, xylene, ethyl benzene, methyl isobutyl ketone, methyl alcohol, ethyl alcohol, octane, decane, cyclohexane, decalin, butyl acetate, pentyl acetate, and so on. A ratio C : D is, for example, 70:30 to 95:5, and preferably 80:20 to 90:10, but not limited thereto, wherein C represents a
25 supply flow rate (kg/h) of the raw material monomer to the

certain reactor for conducting the solution polymerization, and D represents a supply flow rate (kg/h) of the solvent to this certain reactor.

5 The process for producing the polymer composition of the present invention is hereinbefore described through the embodiment of the present invention in detail. According to the present invention, the polymerization can be conducted in at least two stages in series by using at
10 least the first reactor and the second reactor, so that the polymerization reaction conditions, more specifically, the temperature, the time period (average residence time), the amount of the polymerization initiator (a ratio of the polymerization initiator to the raw material monomer) and
15 so on can be set for the first polymerization step and the second polymerization step, independently, and the first polymerization step is conducted at the temperature from 125 to 170°C ,and the second polymerization step is conducted at the temperature from 130 to 180°. Thereby, it
20 becomes possible to control syndiotacticity of the polymer contained in the resin composition obtained in the end, and to produce more efficiently the polymer composition which is suitable for obtaining the resin composition having high heat resistance and heat stability.

However, the present invention is not limited to the above embodiment, and various modifications can be made. For example, three or more reactors can be used to conduct the polymerization in three or more stages in series. 5 Further, the process for producing the polymer composition of the present invention is conducted continuously, but it may be conducted in a batch method.

The polymer composition produced by the process of the present invention is preferably used as a material for a 10 molded article, and the molded article obtained therefrom has an advantage of showing high heat resistance and heat stability. For example, the polymer composition produced by the process of the present invention (more specifically, 15 the resin composition after devolatilization) is molded alone or together with any suitable other component(s) according to any molding process such as injection molding and extrusion molding to prepare a molded article. The polymer composition produced by the process of the present 20 invention is preferably used for preparing a molded article by injection molding, and it is possible to prepare a molded article with good moldability and prevent silver streaks from occurring. Especially, since the resin composition comprising a methacrylic ester based polymer 25 has a superior transparency, the molded article prepared

from it by injection molding has high transparency and less occurrence of silver streaks and good moldability, and therefore it is preferably utilized as a material for a light guide plate, which is used as a member of a backlight unit for various types of liquid crystal displays, or for vehicle members such as a rear lamp cover, a head lamp cover, a visor, a meter panel, and so on.

Injection molding can be conducted by filling (injecting into) a mold having a certain thickness with at least the polymer composition produced by the process of the present invention in a molten state, followed by cooling, and then thus molded article is released from the mold. More specifically, the molded article can be prepared by, for example, supplying a molding machine from a hopper with the polymer composition produced by the process of the present invention (more specifically, the resin composition after devolatilization) alone or in combination with any other suitable components, retracting and rotating a screw to measure the resin composition in a cylinder of the molding machine, melting the resin composition in the cylinder, filling a mold (e.g. metal mold) with the molten resin composition under pressure, holding the pressure for a certain time period until the mold is sufficiently cooled, opening the mold to eject the molded article therefrom.

Thus, according to another aspect of the present invention, there is also provided a molded article prepared from the polymer composition produced by the process of the present invention. It is noted that conditions for preparing the molded article of the present invention from the polymer composition (for example, in a case of injection molding, a temperature for melting a molding material, a temperature of a mold to which the molding material is injected, a pressure to be held after the mold is filled with the molding material, and so on) can be appropriately set and do not specifically limited.

Examples

Examples of the process for producing polymer composition of the present invention are shown below, though the present invention is not limited to these examples.

(Example 1)

In this example, generally, continuous polymerization was conducted in two stages according to the embodiment described above with reference to Fig. 1 to produce a polymer composition in the form of pellets (resin composition). More specifically, this was as explained below.

A raw material monomer mixed liquid 1 was prepared by mixing 98.606 parts by mass of methyl methacrylate and 0.987 part by mass of methyl acrylate together, and adding thereto 0.284 part by mass of n-octyl mercaptan as a chain transfer agent, and 0.123 part by mass of stearyl alcohol as a mold release agent.

A polymerization initiator mixed liquid 1 was prepared by mixing 99.820 parts by mass of methyl methacrylate, and 0.180 part by mass of t-amyl peroxy-2-ethylhexanoate as a polymerization initiator.

A polymerization initiator mixed liquid 2 was prepared by mixing 99.840 parts by mass of methyl methacrylate, and 0.160 part by mass of 1,1-di(t-butylperoxy)cyclohexane as a polymerization initiator.

For producing a polymer composition in this example, the apparatus shown in Fig. 1 was used. A reactor of a complete mixing type having a capacity of 13 liters was used as the first reactor 10, and a reactor of a complete mixing type having a capacity of 6 liters was used as the second reactor 20. The raw material monomer mixed liquid 1, the polymerization initiator mixed liquid 1, and the polymerization initiator mixed liquid 2 as prepared above were charged to the raw material monomer tank 1, the polymerization initiator tank 3, and the polymerization initiator tank 17, respectively.

The raw material monomer mixed liquid 1 and the polymerization initiator mixed liquid 1 flowed through the raw material supply line 9 respectively from the raw material monomer tank 1 and the polymerization initiator tank 3, and were supplied continuously to the first reactor 10 through the supply port 11a located at its lower part.

The supply of the raw material monomer mixed liquid 1 and the polymerization initiator mixed liquid 1 to the first reactor 10 was conducted so that a ratio of flow rates of them was 19.2:1 and an average residence time in the first reactor 10 was 64 minutes. A temperature in the first reactor 10 was 130°C, and a temperature of the jacket 13 surrounding the outer surface of the first reactor 10 was 130°C, so that the continuous polymerization was conducted under an adiabatic condition with substantially no heat transfer. This continuous polymerization was conducted under a condition in which the first reactor 10 was filled with a reaction mixture (mixed liquid) and substantially no gas phase was present (fully filled condition).

The reaction mixture in the first reactor 10 was continuously taken out as an intermediate composition from the effluent port 11b located on the top of the first reactor 10. The intermediate composition thus taken was continuously flowed the connection line 15 and supplied to

the second reactor 20 through the supply port 21a located at its lower part. The connection line 15 was provided with the jacket surrounding its outer surface. This jacket was used to be controlled so that the intermediate composition flowing through the inside of the connection line 15 was maintained at a temperature equal to the temperature in the first reactor (130°C in this example). In addition, the polymerization initiator mixed liquid 2 was continuously supplied from the polymerization initiator tank 17 to the second reactor 20 through the another supply port 21c.

The supply of the intermediate composition and the polymerization initiator mixed liquid 2 to the second reactor 20 was conducted so that a ratio of flow rates of them was 24.7:1. An average residence time in the second reactor 20 was 26 minutes. A temperature in the second reactor 20 was 175°C, and a temperature of the jacket 23 surrounding the outer surface of the second reactor 20 was 175°C, so that the continuous polymerization was conducted under an adiabatic condition with substantially no heat transfer. This continuous polymerization was conducted under a condition in which the second reactor 20 was filled with a reaction mixture (mixed liquid) and substantially no gas phase was present (fully filled condition).

The reaction mixture in the second reactor 20 was

continuously taken out as a polymer composition from the effluent port 21b located on the top of the second reactor 20. The polymer composition thus obtained was continuously flowed the effluent line 25 and heated in the preheater 31 to 200°C, and a volatile component such as the unreacted raw material monomer was separated therefrom at 240°C by the devolatilizing extruder 33 equipped with a vent. A resin composition obtained after devolatilization was extruded in a molten state, cooled with water, and then cut into pellets which were discharged from the discharge line 35. Thus, the resin composition was produced in the form of pellets.

A polymerization rate (wt%) was determined from the supply weights per hour of the raw material monomer mixed liquid 1, the polymerization initiator mixed liquid 1, and the polymerization initiator mixed liquid 2, and the production (discharge) weight per hour of the pellets. Further, with respect to the produced pellets, heat stability (wt%) and heat resistance (°C) were evaluated, and reduced viscosity (cm³/g) was measured as explained below. Results of them are shown in Table 1.

<Heat stability>

Using a TG-DTA apparatus ("TG/DTA 6300" produced by Seiko Instruments Inc.), the pellets produced in the above

were subjected to temperature rising from 50°C to 500°C with a rising temperature rate of 2°C/min under nitrogen flow of 200 mL/min, and change in its weight was measured.

On the basis of the weight of the pellets at the point
5 of 50°C, a weight loss therefrom was determined. Assuming that a rate of the weight loss was 100 wt% at the point of 500°C, a rate of the weight loss (wt%) from 260 to 300°C was calculated.

The rate of the weight loss (wt%) from 260 to 300°C
10 represents heat stability, showing that the smaller its value, the lesser occurrence of thermal degradation starting from an unsaturated end, i.e. the better the heat stability.

15 <Heat resistance>

Using a DSC apparatus ("DSC6200" produced by Seiko Instruments Inc.), according to the differential scanning calorimetry method provided in JIS K 7121, the pellets produced in the above were subjected to temperature rising
20 to 150°C with a rising temperature rate of 20°C/min under nitrogen flow of 100 mL/min and held for 5 minutes, and then subjected to temperature reduction to -50°C with a falling temperature rate of 20°C/min and held for one minute. Then, they were subjected to temperature rising
25 from -50°C to 215°C with a rising temperature rate of

10°C/min, and a mid-point glass transition temperature (T_{mg}) was determined. It shows that the larger its value, the higher the heat resistance.

5 <Reduced viscosity>

In conformity with ISO 1628-6, 0.5g of the pellets produced in the above was dissolved in chloroform to prepare a solution of 50 cm³, its viscosity was determined by Cannon-Fenske viscometer at 25°C.

10

(Example 2)

In this example, a polymer composition was produced in the form of pellets similarly to Example 1, except for the followings.

15 A polymerization initiator mixed liquid 1 was prepared by mixing 99.790 parts by mass of methyl methacrylate, and 0.210 part by mass of t-amyl peroxy-2-ethylhexanoate as a polymerization initiator.

20 A polymerization initiator mixed liquid 2 was prepared by mixing 99.860 parts by mass of methyl methacrylate, and 0.140 part by mass of 1,1-di(t-butylperoxy)cyclohexane as a polymerization initiator.

25 A temperature in the first reactor 10 was 140°C, and a temperature of the jacket 13 surrounding the outer surface of the first reactor 10 was 140°C, so that the continuous

polymerization was conducted under an adiabatic condition with substantially no heat transfer. Further, the jacket formed on the connection line 15 was used to be controlled so that the intermediate composition flowing through the inside of the connection line 15 was maintained at a temperature of 140°C.

As with Example 1, a polymerization rate (wt%) was determined from the supply weights per hour of the raw material monomer mixed liquid 1, the polymerization initiator mixed liquid 1, and the polymerization initiator mixed liquid 2, and the production (discharge) weight per hour of the pellets. Also as with Example 1, with respect to the produced pellets, heat stability (wt%) and heat resistance (°C) were evaluated, and reduced viscosity (cm³/g) was measured. Results of them are shown in Table 1.

(Example 3)

In this example, a polymer composition was produced in the form of pellets similarly to Example 1, except for the followings.

A polymerization initiator mixed liquid 1 was prepared by mixing 99.807 parts by mass of methyl methacrylate, and 0.193 part by mass of t-amyl peroxy-2-ethylhexanoate as a polymerization initiator.

A polymerization initiator mixed liquid 2 was prepared

by mixing 99.920 parts by mass of methyl methacrylate, and 0.080 part by mass of 1,1-di(t-butylperoxy)cyclohexane as a polymerization initiator.

5 A temperature in the first reactor 10 was 150°C, and a temperature of the jacket 13 surrounding the outer surface of the first reactor 10 was 150°C, so that the continuous polymerization was conducted under an adiabatic condition with substantially no heat transfer. Further, the jacket formed on the connection line 15 was used to be controlled
10 so that the intermediate composition flowing through the inside of the connection line 15 was maintained at a temperature of 150°C.

As with Example 1, a polymerization rate (wt%) was determined from the supply weights per hour of the raw
15 material monomer mixed liquid 1, the polymerization initiator mixed liquid 1, and the polymerization initiator mixed liquid 2, and the production (discharge) weight per hour of the pellets. Also as with Example 1, with respect to the produced pellets, heat stability (wt%) and heat
20 resistance (°C) were evaluated, and reduced viscosity (cm³/g) was measured. Results of them are shown in Table 1.

(Comparative Example 1)

In this comparative example, generally, continuous
25 polymerization was conducted in one stage without using the

polymerization initiator mixed liquid 2, differently from Example 1, to produce a polymer composition in the form of pellets. More specifically, this was as explained below.

Similarly to Example 1, a raw material monomer mixed liquid 1 was prepared by mixing 98.606 parts by mass of methyl methacrylate and 0.987 part by mass of methyl acrylate together, and adding thereto 0.284 part by mass of n-octyl mercaptan as a chain transfer agent, and 0.123 part by mass of stearyl alcohol as a mold release agent.

Differently from Example 1, a polymerization initiator mixed liquid 1 was prepared by mixing 99.779 parts by mass of methyl methacrylate, and 0.221 part by mass of 1,1-di(t-butylperoxy)cyclohexane as a polymerization initiator.

For producing a polymer composition in this comparative example, the apparatus shown in Fig. 1 was used while being modified by omitting the second reactor 20 and the polymerization initiator tank 17 (and members related to them). A reactor of a complete mixing type having a capacity of 13 liters was used as the first reactor 10. The raw material monomer mixed liquid 1 and the polymerization initiator mixed liquid 1 as prepared above were charged to the raw material monomer tank 1 and the polymerization initiator tank 3, respectively.

The raw material monomer mixed liquid 1 and the polymerization initiator mixed liquid 1 flowed through the

raw material supply line 9 respectively from the raw material monomer tank 1 and the polymerization initiator tank 3, and were supplied continuously to the first reactor 10 through the supply port 11a located at its lower part.

5 The supply of the raw material monomer mixed liquid 1 and the polymerization initiator mixed liquid 1 to the first reactor 10 was conducted so that a ratio of flow rates of them was 16.2:1 and an average residence time in the first reactor 10 was 64 minutes. A temperature in the first reactor 10 was 175°C, and a temperature of the jacket 10 13 surrounding the outer surface of the first reactor 10 was 175°C, so that the continuous polymerization was conducted under an adiabatic condition with substantially no heat transfer. This continuous polymerization was 15 conducted under a condition in which the first reactor 10 was filled with a reaction mixture (mixed liquid) and substantially no gas phase was present (fully filled condition).

 The reaction mixture in the first reactor 10 was 20 continuously taken out as a polymer composition from the effluent port 11b located on the top of the first reactor 10. The polymer composition thus obtained was continuously flowed the effluent line 25 (without supplied to the second reactor 20) and heated in the preheater 31 to 200°C, and a 25 volatile component such as the unreacted raw material

monomer was separated therefrom at 240°C by the devolatilizing extruder 33 equipped with a vent. A polymer composition obtained after devolatilization was extruded in a molten state, cooled with water, and then cut into pellets which were discharged from the discharge line 35. Thus, the polymer composition was produced in the form of pellets.

A polymerization rate (wt%) was determined from the supply weights per hour of the raw material monomer mixed liquid 1 and the polymerization initiator mixed liquid 1, and the production (discharge) weight per hour of the pellets. Further, as with Example 1, with respect to the produced pellets, heat stability (wt%) and heat resistance (°C) were evaluated, and reduced viscosity (cm³/g) was measured. Results of them are shown in Table 1.

(Comparative Example 2)

In this comparative example, a polymer composition was produced in the form of pellets similarly to Example 1, except for the followings.

A polymerization initiator mixed liquid 1 was prepared by mixing 99.799 parts by mass of methyl methacrylate, and 0.201 part by mass of t-amyl peroxy-2-ethylhexanoate as a polymerization initiator.

A polymerization initiator mixed liquid 2 was prepared

by mixing 99.780 parts by mass of methyl methacrylate, and 0.220 part by mass of 1,1-di(t-butylperoxy)cyclohexane as a polymerization initiator.

5 A temperature in the first reactor 10 was 120°C, and a temperature of the jacket 13 surrounding the outer surface of the first reactor 10 was 120°C, so that the continuous polymerization was conducted under an adiabatic condition with substantially no heat transfer. Further, the jacket formed on the connection line 15 was used to be controlled
10 so that the intermediate composition flowing through the inside of the connection line 15 was maintained at a temperature of 120°C.

As with Example 1, a polymerization rate (wt%) was determined from the supply weights per hour of the raw
15 material monomer mixed liquid 1, the polymerization initiator mixed liquid 1, and the polymerization initiator mixed liquid 2, and the production (discharge) weight per hour of the pellets. Also as with Example 1, with respect to the produced pellets, heat stability (wt%) and heat
20 resistance (°C) were evaluated, and reduced viscosity (cm³/g) was measured. Results of them are shown in Table 1.

Table 1

	First reactor		Second reactor		Polymeriza tion rate (wt%)	Reduced viscosity (cm ³ /g)	Heat stability (wt%)	Heat resistance T _{mg} (°C)
	Polymeriza tion temp. (°C)	Residence time (min)	Polymeriza tion temp. (°C)	Residence time (min)				
Example 1	130	64	175	26	58	55.4	2.9	115
Example 2	140	64	175	26	56	56.1	2.9	115
Example 3	150	64	175	26	57	55.1	2.7	115
Comparative example 1	175	64	-	-	61	53.7	3.1	113
Comparative example 2	120	64	175	26	56	54.8	3.1	115

As understood from Table 1, Examples 1 to 3 produced the polymer composition (resin composition) showing the heat stability and the heat resistance better than those of Comparative example 1, while the polymerization rate was retained at an equal level and the reduced viscosity, which gives an indication of a molecular weight of the polymer, was retained at an equal level to those of Comparative example 1. Further, Examples 1 to 3 produced the polymer composition (resin composition) showing the heat stability better than that of Comparative example 2, though the polymerization rate, the reduced viscosity and the heat resistance were at an equal level to those of Comparative example 2.

(Example 4)

In this example, generally, continuous polymerization was conducted in two stages according to the embodiment described above with reference to Fig. 1 to produce a polymer composition in the form of pellets (resin composition). Further, in order to evaluate its moldability, the produced pellets were molded into a molded article. More specifically, this was as explained below.

A raw material monomer mixed liquid 1 was prepared by mixing 93.0835 parts by mass of methyl methacrylate, 6.375 parts by mass of methyl acrylate and 0.076 part by mass of

ethylene glycol dimethacrylate together, and adding thereto 0.322 part by mass of n-octyl mercaptan as a chain transfer agent, 0.121 part by mass of stearic monoglyceride and 0.013 part by mass of methyl stearate as mold release agents, 0.0005 part by mass of di-tert-dodecyl disulfide as a heat stabilizing agent, and 0.009 part by mass of dimethyl 2-(p-methoxybenzylidene)malonate as an ultraviolet absorbing agent.

A polymerization initiator mixed liquid 1 was prepared by mixing 99.752 parts by mass of methyl methacrylate, and 0.248 part by mass of t-amyl peroxy-2-ethylhexanoate as a polymerization initiator.

A polymerization initiator mixed liquid 2 was prepared by mixing 99.280 parts by mass of methyl methacrylate and 9.6 parts by mass of methyl acrylate, and 0.120 part by mass of 1,1-di(t-butylperoxy)cyclohexane as a polymerization initiator.

For producing a polymer composition in this example, the apparatus shown in Fig. 1 was used. A reactor of a complete mixing type having a capacity of 13 liters was used as the first reactor 10, and a reactor of a complete mixing type having a capacity of 6 liters was used as the second reactor 20. The raw material monomer mixed liquid 1, the polymerization initiator mixed liquid 1, and the polymerization initiator mixed liquid 2 as prepared above

were charged to the raw material monomer tank 1, the polymerization initiator tank 3, and the polymerization initiator tank 17, respectively.

The raw material monomer mixed liquid 1 and the polymerization initiator mixed liquid 1 flowed through the raw material supply line 9 respectively from the raw material monomer tank 1 and the polymerization initiator tank 3, and were supplied continuously to the first reactor 10 through the supply port 11a located at its lower part.

The supply of the raw material monomer mixed liquid 1 and the polymerization initiator mixed liquid 1 to the first reactor 10 was conducted so that a ratio of flow rates of them was 16.7:1 and an average residence time in the first reactor 10 was 46 minutes. A temperature in the first reactor 10 was 140°C, and a temperature of the jacket 13 surrounding the outer surface of the first reactor 10 was 140°C, so that the continuous polymerization was conducted under an adiabatic condition with substantially no heat transfer. This continuous polymerization was conducted under a condition in which the first reactor 10 was filled with a reaction mixture (mixed liquid) and substantially no gas phase was present (fully filled condition).

The reaction mixture in the first reactor 10 was continuously taken out as an intermediate composition from

the effluent port 11b located on the top of the first reactor 10. The intermediate composition thus taken was continuously flowed the connection line 15 and supplied to the second reactor 20 through the supply port 21a located at its lower part. The connection line 15 was provided with the jacket surrounding its outer surface. This jacket was used to be controlled so that the intermediate composition flowing through the inside of the connection line 15 was maintained at a temperature equal to the temperature in the first reactor (140°C in this example). In addition, the polymerization initiator mixed liquid 2 was continuously supplied from the polymerization initiator tank 17 to the second reactor 20 through the another supply port 21c.

The supply of the intermediate composition and the polymerization initiator mixed liquid 2 to the second reactor 20 was conducted so that a ratio of flow rates of them was 18.3:1. An average residence time in the second reactor 20 was 19 minutes. A temperature in the second reactor 20 was 175°C, and a temperature of the jacket 23 surrounding the outer surface of the second reactor 20 was 175°C, so that the continuous polymerization was conducted under an adiabatic condition with substantially no heat transfer. This continuous polymerization was conducted under a condition in which the second reactor 20 was filled

with a reaction mixture (mixed liquid) and substantially no gas phase was present (fully filled condition).

The reaction mixture in the second reactor 20 was continuously taken out as a polymer composition from the effluent port 21b located on the top of the second reactor 20. The polymer composition thus obtained was continuously flowed the effluent line 25 and heated in the preheater 31 to 200°C, and a volatile component such as the unreacted raw material monomer was separated therefrom at 240°C by the devolatilizing extruder 33 equipped with a vent. A resin composition obtained after devolatilization was extruded in a molten state, cooled with water, and then cut into pellets which were discharged from the discharge line 35. Thus, the resin composition was produced in the form of pellets.

A polymerization rate (wt%) was determined from the supply weights per hour of the raw material monomer mixed liquid 1, the polymerization initiator mixed liquid 1, and the polymerization initiator mixed liquid 2, and the production (discharge) weight per hour of the pellets. Further, with respect to the produced pellets, MFR (melt mass flow rate) and moldability were evaluated as explained below. Results of them are shown in Table 2.

In conformity with JIS K 7210, with respect to the produced pellets, MFR was measured at 230°C under a load of 37.3 N.

5 <Moldability>

The pellets produced in the above were supplied from a hopper to a molding machine set at a certain cylinder temperature, and injection molding was repeatedly conducted through the cylinder in this molding machine, thereby
10 molded articles were prepared in sequence. Conditions for the injection molding are shown in below. After the cylinder temperature became stable, ten molded articles in sequence obtained by sequential ten shots (cycles) of injection molding were taken as samples, and a silver
15 streaks occurrence ratio was determined by counting samples showing occurrence of silver streaks among these ten samples. More specifically, the molded articles were subjected to visual observation, and occurrence of silver streaks was recognized when silver streaks was observed in
20 the molded article. The silver streaks occurrence ratio were determined for three different cylinder temperatures according to the similar procedures.

Metal mold:

Rectangle of 23 cm × 30.5 cm (plane view),
25 thickness of 0.8 mm

One fan gate (located on a longitudinal side of the rectangle in the plane)

Gate width 304 mm

Molding machine:

5 Electric servo drive injection molding machine ("J450ELIII-890H" produced by The Japan Steel Works, LTD.)

Cylinder temperature:

300°C, 305°C, 310°C at a nozzle head temperature (molding temperature)

10 Hopper side temperature:

220°C

Molding conditions:

	Injection pressure	179 MPa
	Injection speed	160 mm/sec
15	Metal mold temperature	80°C
	Injection time period	0.4 sec
	Back pressure	15 MPa
	Screw rotation speed	45 rpm
	Holding pressure	45 MPa
20	Holding pressure time	11 sec

Molding cycle:

100 sec (including cooling time of 70 sec)

Residence time in cylinder:

12 min

(Comparative Example 3)

In this comparative example, generally, continuous polymerization was conducted in one stage without using the polymerization initiator mixed liquid 2, differently from Example 4, to produce a polymer composition in the form of pellets. Further, in order to evaluate its moldability, the produced pellets were molded into a molded article similarly to Example 4. More specifically, this was as explained below.

A raw material monomer mixed liquid 1 was prepared by mixing 95.0955 parts by mass of methyl methacrylate, 4.387 parts by mass of methyl acrylate and 0.076 part by mass of ethylene glycol dimethacrylate together, and adding thereto 0.298 part by mass of n-octyl mercaptan as a chain transfer agent, 0.121 part by mass of stearic monoglyceride and 0.013 part by mass of methyl stearate as mold release agents, 0.0005 part by mass of di-tert-dodecyl disulfide as a heat stabilizing agent, and 0.009 part by mass of dimethyl 2-(p-methoxybenzylidene)malonate as an ultraviolet absorbing agent.

A polymerization initiator mixed liquid 1 was prepared by mixing 99.767 parts by mass of methyl methacrylate, and 0.233 part by mass of 1,1-di(t-butylperoxy)cyclohexane as a polymerization initiator.

For producing a polymer composition in this

comparative example, the apparatus shown in Fig. 1 was used while being modified by omitting the second reactor 20 and the polymerization initiator tank 17 (and members related to them). A reactor of a complete mixing type having a capacity of 13 litters was used as the first reactor 10. The raw material monomer mixed liquid 1 and the polymerization initiator mixed liquid 1 as prepared above were charged to the raw material monomer tank 1 and the polymerization initiator tank 3, respectively.

The raw material monomer mixed liquid 1 and the polymerization initiator mixed liquid 1 flowed through the raw material supply line 9 respectively from the raw material monomer tank 1 and the polymerization initiator tank 3, and were supplied continuously to the first reactor 10 through the supply port 11a located at its lower part.

The supply of the raw material monomer mixed liquid 1 and the polymerization initiator mixed liquid 1 to the first reactor 10 was conducted so that a ratio of flow rates of them was 16.7:1 and an average residence time in the first reactor 10 was 46 minutes. A temperature in the first reactor 10 was 175°C, and a temperature of the jacket 13 surrounding the outer surface of the first reactor 10 was 175°C, so that the continuous polymerization was conducted under an adiabatic condition with substantially no heat transfer. This continuous polymerization was

conducted under a condition in which the first reactor 10 was filled with a reaction mixture (mixed liquid) and substantially no gas phase was present (fully filled condition).

5 The reaction mixture in the first reactor 10 was continuously taken out as a polymer composition from the effluent port 11b located on the top of the first reactor 10. The polymer composition thus obtained was continuously flowed the effluent line 25 (without supplied to the second
10 reactor 20) and heated in the preheater 31 to 200°C, and a volatile component such as the unreacted raw material monomer was separated therefrom at 240°C by the devolatilizing extruder 33 equipped with a vent. A polymer composition obtained after devolatilization was extruded in
15 a molten state, cooled with water, and then cut into pellets which were discharged from the discharge line 35. Thus, the polymer composition was produced in the form of pellets.

 A polymerization rate (wt%) was determined from the
20 supply weights per hour of the raw material monomer mixed liquid 1 and the polymerization initiator mixed liquid 1, and the production (discharge) weight per hour of the pellets. Further, as with Example 4, with respect to the produced pellets, MFR (melt mass flow rate) and moldability
25 were evaluated. Results of them are shown in Table 2.

Table 2

	First reactor		Second reactor		Polymeriza tion rate (wt%)	MFR (g/ 10min)	Moldability (Silver streaks occurrence ratio) (%)		
	Polymeriza tion temp. (°C)	Residence time (min)	Polymeriza tion temp. (°C)	Residence time (min)			300°C	305°C	310°C
Example 4	140	46	175	19	57.5	11	0	0	30
Comparative example 3	175	46	-	-	55.9	11	0	30	100

As understood from Table 2, Example 4 produced the polymer composition showing the better moldability (lower silver streaks occurrence ratio in the molded article) than that of Comparative example 3 even when molded at a higher temperature (molding temperature higher than 300°C, e.g. at 305°C or more), while the polymerization rate was retained at an equal level and the MFR, which may give an indication for determining the molding conditions, was retained at an equal level to those of Comparative Example 3.

Industrial Applicability

The present invention can be used for producing a polymer composition which is suitable for obtaining a resin composition comprising a methacrylic ester polymer(s).

The present application claims priority to Japanese Patent Application No. 2011-59480 filed on March 17, 2011, entitled "PROCESS FOR PRODUCING POLYMER COMPOSITION." The contents of that application are incorporated herein by the reference thereto in their entirety.

WHAT IS CLAIMED IS:

1. A process for producing a polymer composition, which comprises

5 a first polymerization step of supplying a raw material monomer and a polymerization initiator to a first reactor of a complete mixing type through its supply port to be subjected to continuous polymerization under an adiabatic condition in the first reactor of the complete mixing type, and taking a resultant intermediate
10 composition from an effluent port located at a top of the first reactor of the complete mixing type; and

a second polymerization step of supplying the intermediate composition to a second reactor of a complete mixing type through its supply port to be further subjected
15 to continuous polymerization under an adiabatic condition in the second reactor of the complete mixing type, and taking a resultant polymer composition from an effluent port located at a top of the second reactor of the complete mixing type;

20 wherein the first polymerization step is conducted at a temperature from 125 to 170°C, and the second polymerization step is conducted at a temperature from 130 to 180°C.

25 2. The process for producing the polymer composition

according to claim 1, wherein a ratio of an average residence time in the second reactor of the complete mixing type to an average residence time in the first reactor of the complete mixing type is from 9/1 to 1/9.

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3. The process for producing the polymer composition according to claim 1, wherein the continuous polymerization in the first polymerization step and the second polymerization step is continuous bulk polymerization.

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4. A molded article prepared from the polymer composition produced by the process according to any of claims 1 to 3.