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IR-1209

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FAST SWITCHING SMARTFET

FIELD OF THE INVENTION

5 This invention relates to power integrated circuits, and more specifically relates to a very fast power MOSFET with an integrated thermal shutdown circuit which operates at high speed.

BACKGROUND OF THE INVENTION

10 MOSgated power devices, such as IGBTs and power MOSFETs having integrated current and thermal monitoring circuits to turn off the power device under certain fault conditions are well known. The power supply for such power integrated devices is derived from the input signal pulse. When the device speed is increased, the power supply or V_{cc} pulse lasts, for example, for only 100
15 nanoseconds for a 25 kHz application. However, the temperature monitoring circuit, for example, requires about 5 microseconds to complete its calculation. Since V_{cc} power is available only for 100 nanoseconds, the temperature sensing circuit would lose its power supply
20 and would malfunction if the system is operated at about 25 kHz or higher.

BRIEF DESCRIPTION OF THE INVENTION

25 In accordance with the invention, the temperature monitoring circuit of a power integrated MOSgated device, for example, the temperature monitor circuit in the IR6012 device made by the International Rectifier Corporation of El Segundo, California, is modified to store or memorize the last temperature



calculation when V_{CC} disappears. Thus, the overtemperature signal is memorized in a small capacitor to guarantee that the overtemperature signal will not be lost between two pulses at a frequency greater than about 16 kHz (a period of about 60 microseconds). A charge storage capacitor is also added to store the input voltage V_{CC} after the pulse terminates. For example, a 100 picofarad capacitor is integrated into the silicon chip, and takes only about 0.15 mm² in area.

The capacitor used to store the overtemperature signal may be about 30 picofarads. The 100 picofarad capacitor is sufficiently large to supply the power to the overtemperature circuit, and is also large enough to charge the 30 picofarad capacitor.

The values given above can be varied as desired but the capacitor charged from V_{CC} is preferably larger than the capacitor which stores the overtemperature signal and must be large enough to "refresh" the overtemperature signal at each V_{CC} cycle.

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 shows a partial block and partial circuit diagram of the present invention.

DETAILED DESCRIPTION OF THE INVENTION

Figure 1 shows the novel circuit of the invention when applied to a power MOSFET having circuits integrated with the power chip to provide overtemperature and overcurrent protection. The prior art circuit is described in more detail in copending U.S. application Serial No. 08/298,383, filed August 30, 1994, entitled POWER MOSFET WITH OVERCURRENT AND OVER-TEMPERATURE PROTECTION AND CONTROL CIRCUIT DECOUPLED FROM BODY DIODE,



and in the names of Bruno C. Nadd and Talbott M. Houk (IR-1070), the subject of which is incorporated herein by reference.

Thus in the prior power integrated circuit, there is provided a power MOSFET 10 conventionally formed in a silicon chip. Other MOSgated power devices could be used. Power MOSFET 10 comprises a die having a drain electrode 11, a source electrode 12, a gate electrode 12a and a conventional current sense electrode 14. The die may be housed in a housing having connection pins extending therefrom. The input pin 13 of the device is connected to a logic level source which, for example, swings between 0 and 5 volts at the desired frequency of operation of the power MOSFET 10. The input pin 13 is connected to the gate 12a through an on/off switching circuit 20. Circuit 20 is turned off to turn off MOSFET 10 in the presence of predetermined conditions, such as an overcurrent, as measured by overcurrent monitor circuit 22 or overtemperature, as measured by temperature monitor circuit 23. The monitor circuits are preferably integrated into the same die or chip which contains the junctions of MOSFET 10.

The overcurrent circuit 22 receives a current measurement input from current sense terminal 14 and delivers an output to logic circuit 21 which opens switching circuit 20 if a current fault is monitored.

Overtemperature circuit 23 is powered from the V_{CC} pulses which may be derived from input pin 13. A suitable circuit produces an overtemperature output which, in the prior art, was connected to an input in logic circuit 21 so that the switching circuit can be turned off in the presence of the predetermined overtemperature condition.



The prior art circuit was also provided with zener diode 30 and diode 31 connected between the gate and drain electrodes of MOSFET 10 and a diode 32 connected as shown.

5 In accordance with the invention, the prior art thermal shutdown circuit 23 is modified by adding a MOSFET 50, diode 51, capacitor 52 and resistor 53. The V_{CC} input, derived from input pin 13 and which powers the overtemperature circuit, has added thereto the diode 60
10 and capacitor 61. Both diodes 51 and 60 are preferably polysilicon diodes integrated on the same silicon chip as contains the junctions of power MOSFET 10.

The "settle time" for the overtemperature circuit 23 is about 0.5 microseconds. However, the
15 overtemperature output signal can be lost between two pulses of operating power (V_{CC}) at frequencies greater than about 16 kHz. The addition of diode 51, capacitor 52 and resistor 53 ensures that the overtemperature calculation is not lost by virtue of a sufficiently long
20 R-C time constant. Thus, if capacitor 52 is 30 picofarads (0.05 mm^2 in area on the chip) and resistor 53 is 10 megohms, the time constant will be about 300 microseconds. Other time constants can be used.

It will be observed that the circuit will now
25 operate properly only if V_{IN} or V_{CC} is present for at least one microsecond each cycle. To protect the device for low duty cycles, the filter capacitor 61 and diode 60 are added to the V_{CC} input circuit to the overtemperature monitor 23. Capacitor 61 is preferably 100 picofarads to
30 be able to supply the overtemperature circuit 23 for several microseconds and to charge the 30 picofarad capacitor 52.

Thus, in a circuit configuration in which the V_{CC} is only a 100 nanosecond pulse at, for example, 20 kHz, the filtered V_{CC} is on long enough to refresh the overtemperature signal each cycle.

5 Although the present invention has been
described in relation to particular embodiments thereof,
many other variations and modifications and other uses
will become apparent to those skilled in the art. It is
preferred, therefore, that the present invention be
10 limited not by the specific disclosure herein, but only
by the appended claims.

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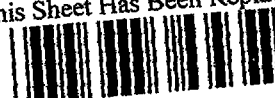


WHAT IS CLAIMED IS:

1. A MOSgated power integrated circuit device comprising: a MOSgated power device having output electrodes and an input gate electrode; an input signal circuit for supplying a high frequency signal to said gate electrode to turn said power device on and off at high frequency; an overtemperature monitor circuit for monitoring the temperature of said power device and for producing an output signal operable to disconnect said input signal circuit from said input gate electrode when the temperature monitored exceeds a predetermined value; said overtemperature monitor circuit having terminal means being connectable to a source of voltage V_{CC} for powering said overtemperature monitor circuit; said source of voltage V_{CC} being derived from said input signal circuit; and at least a first capacitor circuit means coupled to said temperature monitor circuit for storing the output signal of said temperature monitor circuit between pulses of the voltage V_{CC} to prevent loss of said output signal between said V_{CC} pulses.

2. The device of claim 1 which further includes second capacitor circuit means coupled to terminal means which is connectable to said voltage source V_{CC} to ensure that the overtemperature monitor circuit will be powered on for a time longer than its settle time.

3. The device of claim 1 wherein said high frequency signal at said input signal circuit has a frequency in excess of about 16 kHz.





4. The device of claim 2 wherein said high frequency signal at said input signal circuit has a frequency in excess of about 16 kHz.

5. The device of claim 1 wherein said MOSgated device is a power MOSFET.

6. The device of claim 1 wherein said at least first capacitor circuit means includes a diode means and control MOSFET means in series with a first capacitor and in series with said terminal means for said input voltage V_{CC} .

7. The device of claim 2 wherein said second capacitor circuit means includes a diode means and a second capacitor in series with said terminal means for said input voltage V_{CC} .

8. The device of claim 6 wherein said second capacitor means comprises said diode means and a second capacitor in series with said terminal means for said input voltage V_{CC} .

9. The device of claim 3 wherein said first capacitor circuit means includes a diode means and control MOSFET means in series with a first capacitor and in series with said terminal means for said input voltage V_{CC} .

10. The device of claim 4 wherein said second capacitor circuit means includes a diode means and a second capacitor in series with said terminal means for said input voltage V_{CC} .





11. The device of claim 4 wherein said second capacitor means comprises said diode means and a second capacitor in series with said terminal means for said input voltage V_{cc} .

12. The device of claim 9 wherein said first capacitor has a value of about 30 picofarads.

13. The device of claim 10 wherein said second capacitor has a value of about 100 picofarads.

14. The device of claim 11 wherein said first capacitor has a value of about 30 picofarads and said second capacitor has a value of about 100 picofarads.

