

Description**TECHNICAL FIELD**

5 This invention relates to coatings applied by fusion coating processes and more particularly to coating powders that yield wrinkle finishes upon curing. It relates still more particularly to such powders made from thermosettable hydroxy-functional resins.

BACKGROUND OF THE INVENTION

10 The coating compositions of this invention are dry, free flowing powders that may be used in fusion coating processes. "Fusion coating processes" are herein defined as those coating processes in which a coating powder is distributed over a substrate (which may be hot or cold) and heat, supplied from the substrate or an external source, fuses the powder into a continuous film. Examples of fusion coating
15 processes include fluidized bed, electrostatic spraying, hot flocking, and cloud chambers. When the coating powder is based upon heat curing resins, as is the case of the hydroxy-functional resins of this invention, sufficient heat in excess of that required to fuse the powder must be available to cure the coating and fully develop its physical and chemical properties.

20 Wrinkle finishes are desired in many applications and are commonly applied to office equipment such as typewriters, staplers, dictating equipment, file cabinets, and the like. In addition to being aesthetically pleasing, these finishes have certain utilitarian functions: they hide surface defects of a substrate even when applied in thin films and, having a low gloss, they do not show scratches. Wrinkle finishes, as contemplated for the purposes of this invention, are reticulated, i.e., made up of a pattern of raised veins across the surface and are exemplified by interconnected star-burst patterns, mosaics, and by patterns similar to that
25 of an alligator hide.

Wrinkle finish coatings conventionally are applied from solvent-based paints, usually using two coats, to establish a compound system in which the surface sets up first. When the rest of the coating cures, the resulting shrinkages deform the previously set surface and cause a fine wrinkle pattern to develop on the surface of the coating.

30 Epoxy resin-based powder coatings having wrinkle finishes are taught in U. S. Patent No. 4,341,819. The wrinkle pattern is achieved by means of a special curing agent, methylene disalicylic acid, acting upon the epoxy groups of the resin. Because of the rather poor weatherability of epoxy resin coatings, these wrinkle-finish coatings are used almost exclusively on surfaces protected from the weather and are very popular for interior uses.

SUMMARY OF THE INVENTION

Accordingly, it is the object of this invention to provide a coating powder which will yield a coating having a low gloss and a randomly developed wrinkle pattern on its surface.

40 It is another object of this invention to provide a coating powder adapted to give a weatherable wrinkle finish.

It is another object of this invention to provide a method for generating a wrinkle finish on a powder coating made from a hydroxy-functional resin.

45 It is yet another object of this invention to provide a wrinkle finish on an article having a powder coating based on a hydroxy-functional resin.

These and other objects of this invention are achieved through the use of an amine salt of trifluoromethanesulfonic acid as the catalyst for curing a hydroxy-functional resin, the essence of the coating powder.

DETAILED DESCRIPTION OF THE INVENTION

50 Trifluoromethanesulfonic acid, also known as triflic acid, is one of the strongest of all known monoprotic acids. It is about 427 times as strong as nitric acid but it is not an oxidizing agent and is extremely stable to high temperatures. It is available as FC-28 from the 3M Company. By itself or in an aqueous glycol ether solution, the acid does not act as a wrinkle-producing catalyst in the curing of the powder coating
55 composition on a bare metal surface. However, an amine salt of the acid, called an amine triflate, does cause a remarkably abrupt dulling of the surface of the molten powder and the formation of a skin within seconds of fusion, followed by a slumping of the skin as the resinous mass is cured beneath it. For the

purposes of this invention, the meaning of the term amine shall include ammonia as well as amines having the formula R_xN wherein R is an alkyl group, preferably one having from 1 to 4 carbon atoms, and x is from 1 to 3. Examples include methyl-, dimethyl-, and trimethylamine, ethylamine, propylamine, dipropylamine, butylamine, and dibutylamine. The diethylamine salt is a preferred catalyst for the wrinkle-forming curing process of this invention. The amine salts are suitably used as solutions in a mixture of water and a polar organic solvent such as a glycol ether. The diethylamine triflate is available from 3M as FC-520 Resin Catalyst, a 60% solution in a 50/50 mixture of water and diethyleneglycol monoethyl ether. A starburst type wrinkle is achieved with the hydroxy-functional polyester even though the amine triflate has a pH on the order of about 4.5. For an attractive alligator finish on such polyester-based coatings, it is preferred that the pH is from 6.5 to 10; an excess of the amine over the stoichiometric amount being used in making the salt alkaline. Nevertheless, the alligator finish is achieved on the epoxy resin-based coatings even when the catalyst does not contain excess amine. When four different lots of FC-520 salt which were effective catalysts for the epoxy alligator finish were diluted with equal amounts of water, the resulting solutions had pH values of 4.7-4.9. In general, then, the pH may be from 4.5 to 10 or even higher although a large excess of amine may be harmful to other desirable properties of the coating.

The amount of active catalyst is from 0.05 to 1 part per hundred parts by weight of the resin (phr); the term resin herein means the combination of the hydroxy-functional resin and the curing agent. Preferably, the active catalyst is used in an amount ranging from 0.2 to 0.8 phr. The types and amounts of filler and pigment used are to be taken into account when determining the level of catalyst for a particular formulation of the coating powder of this invention, as will be seen below.

The curing agent in the coating composition of this invention is preferably one that splits out a volatile by-product of the curing reaction. Aminoplasts, particularly the melamine/formaldehyde resins, urea/glyoxal condensation products, and the alkoxyated derivatives of each are examples of such a curing agent. Hexamethoxymethyl melamine and tetramethoxymethyl glycouril exemplify the preferred curing agents. A curing agent in solid form is preferred for convenience in formulation. The tetramethoxymethyl glycouril, available from American Cyanamid under its trademark and number POWDERLINK 1174, is a solid. The amount of curing agent may be from 4% to 20% by weight of the resin, but preferably it is from 5 to 7%.

The wrinkle finish powder coatings are derived from hydroxy-functional resins exemplified by hydroxy-functional polyesters, epoxy resins (through the secondary hydroxyl group in each unit), hydroxy-functional acrylate and methacrylate resins, cellulose esters such as cellulose acetate/butyrate, and polyvinylbutyral.

The polyester resin is predominantly hydroxyl in functionality; its acid number is preferably about 12 or less and, even more preferably, not more than about 5. The hydroxyl number, on the other hand, is preferably from 25 to 50, as conventionally reported. The amount of curing agent used depends on the hydroxyl number; as the number goes up, so does the amount of curing agent.

The epoxy resins are exemplified by the diglycidyl ether condensation polymers resulting from the reaction of epichlorohydrin with a bisphenol in the presence of an alkaline catalyst. Bisphenol A is most commonly used but the bisphenols B, F, G and H are also suitable. By controlling the operating conditions and varying the ratio of the reactants, products of various equivalent weights can be made. For the purposes of this invention, the epoxide equivalent weight (EEW) may be from 600 to 2000 and the hydroxyl equivalent weight may be from 300 to 400. These are available from a wide variety of commercial sources. The GT-series of bisphenol A epoxies from Ciba-Geigy, including 7004, 7013, 7014, 7074, and 7097 are examples of useful epoxy resins in this invention. Shell Chemical Co. also supplies suitable epoxy resins under its Epon trademark.

Epoxy/polyester hybrids are also contemplated for use in this invention. The hydroxyl function is contributed by the epoxy resin. Acid functional polyester resins specifically designed for curing with bisphenol A epoxy resins have an acid number of from 35 to 75 (equivalent weight about 750-1600) and are generally used at a stoichiometric ratio $\pm 10\%$ with the epoxy. The weight ratio of epoxy to polyester is typically from 50:50 to 30:70.

Hydroxy-functional acrylate and methacrylate polymers are exemplified by the homopolymers and copolymers of hydroxyethyl and hydroxypropyl acrylate and methacrylate. Comonomers include alkyl esters of acrylic and methacrylic acid wherein the alkyl group contains from 1 to 8 carbon atoms, styrene, ethylene, propylene, and vinyl monomers. The hydroxyl equivalent weight is from about 600 to about 1400. They are available from the Polymer Division of S. C. Johnson & Son, Inc.

Mixtures of the hydroxy-functional resins are also useful in the practice of this invention. An essential property that must be considered when formulating a coating powder is the ability of the powder to fuse into a continuous and void free film. As a guide to formulation chemists, two relatively simple test procedures have been established to measure the ability of a coating powder to fuse over a substrate. One of these is gel time which provides a measure of the reactivity of a given system; the other

is the hot plate melt flow (HPMF) test which is a combined measure of both the reactivity and melt viscosity of the coating powder. It is generally true that the gel time and the HPMF are a function of the molecular weight and functionality of the resin, the nature of the curing agent, and the activity of the catalyst. The HPMF and melt viscosity are also influenced by fillers which generally increase the viscosity depending on the amount used, the particle size, the surface area and the surface chemistry of the fillers.

For each 100 parts by weight of the resin, from 0 to 100 parts by weight of fillers and pigments may be added to the formulation. Silica, mica, talc, and diatomaceous earth are examples of the fillers. Alkaline fillers, however, such as the sodium potassium aluminum silicate sold under the MINEX trademark seem to interfere with the catalytic action of the amine triflates. The presence of even a substantially neutral salt like barium sulfate requires an additional amount of the catalyst. Even so, the following pigments exemplify those contemplated in this invention: carbon black, titanium dioxide, nickel-titanium oxide, nickel-antimony-titanium oxide, ferrite yellow oxide, ferric oxides, raw sienna, phthalocyanine blue, phthalocyanine green, ultramarine blue, toluidine red, parachlor red, and organic maroons. Titanium dioxide also interferes to some extent with the catalyst and that is taken into account in formulating the coating composition. The various grades of titanium oxide have varying effects on the appearance of the finish. A very pronounced alligator finish may be obtained on a white coating when an alkaline-reacting titanium oxide having an alumina/silica coating such as that designated R-902 by Dupont is used. Also, titanium oxides by SCM Pigments called Zopaque RCL-2 and RCL-9 permit an alligator finish. An organic-coated titania designated R-101 by Dupont also permits a very desirable finish. On the other hand, an alumina-coated titanium oxide designated R-900 by Dupont greatly slows the cure and an organically treated, silica-encapsulated titanium oxide designated Zopaque RCL-6 by SCM can prevent the formation of a wrinkle finish almost entirely. The effect of R-960 titania (Dupont), which has a silica/alumina coating, on the wrinkle may be minimized by using lesser amounts of the pigment.

Other ingredients may be useful for particular compositions. Flow or leveling agents are useful to promote the formation of a continuous coating. These are exemplified by polyacrylic esters, non-ionic fluorinated alkyl ester surfactants, non-ionic alkylaryl polyether alcohols, and silicones. Benzoin is useful as a bubble release agent.

Melt mixing is the preferred method for making the coating powders. The dry ingredients are weighed into a batch mixer and are mixed with a a medium intensity horizontal plow mixer or a lesser intensity tumble mixer; in the latter case care must be taken that all ingredients are thoroughly distributed. When liquids are to be mixed into the powder, a high intensity impeller mixer such as a Henschel or Wellex mixer is advantageous. Mixing times range from 1 to 3 minutes for the high intensity mixers to 30-60 minutes for the tumble mixers. The premix is then further mixed and compounded as the resin is melted in either a single screw or a twin screw extruder for 0.5 to 1 minute. The extrudate is cooled quickly and broken into small chips suitable for grinding.

The coating powder is applied to substrates by conventional means, including the electrostatic fluidized beds, electrostatic spray guns, and triboelectric guns. Hot flocking may also be used.

ASTM Specification D-3451 defines a procedure for measuring gel time in which a small quantity of powder is dropped onto a hot plate at a given temperature, e.g. 205 °C (400 °F) and stroked with a tongue depressor until continuous and readily breakable filaments are formed when the depressor is lifted from the sample. The elapsed time for this to occur is measured in seconds and is the gel time. Although gel time, by itself, is not an indicator of whether a certain resin composition of this invention will provide a wrinkled finish to the coating made therefrom, the minimum gel time for compositions of this invention is preferably about 30 seconds.

To obtain the desired wrinkle finish, the HPMF of the hydroxy-functional polyester powder coating composition should be at least about 50 but if it is more than 150 mm when measured at 375 °F (190 °C), the gel time must not be greater than about 280 seconds. If these two properties do not fall within these limits, the desired wrinkle finish of this invention is not obtained. In this test a pellet of powder having a diameter of 12.7mm and 6mm thick is placed on a hot plate set at 375 °F (190 ± 2 °C) at an inclination angle of 35°. The pellet melts and runs down the plate. The length of the flow is measured in millimeters. The distance the coating flows is dependent on the initial melt viscosity, the rate of reaction, the temperature at which the test is conducted, and the type and amount of catalyst.

As will be seen in the following examples, the gel times for the bisphenol A epoxy resins are on the order of about twice those of the hydroxy-functional polyesters whereas the HPMF is about the same order of magnitude.

In the examples of hydroxy-functional polyester coating powders that follow, the correlation between the HPMF, the gel time, and the production of a wrinkle finish is apparent.

EXAMPLES 1-7

Coating powders were prepared in accordance with this invention by initially blending at high speed the POWDERLINK 1174 curing agent and the polyester resin identified in Table I in weight ratios of 6:94 in Examples 1-4; 8:92 in Example 5; and 10:90 in Examples 6 and 7; along with the following ingredients:

	phr
RESIFLOW P-67 flow agent	1.4
Benzoin	0.8
Bartex 65 barium sulfate	30
Titanium dioxide (R-960)	0.4
Black pigment	0.76
Red pigment	1.5
Yellow pigment	3.6
Diethylamine triflate (FC-520)	0.6

The blend was then melt-mixed in a Buss extruder whose front zone was maintained at 180°F and whose rear zone was unheated. The extrudate was then chipped and ground with 0.2 % by weight of colloidal alumina (Degussa) to a fine powder that passed through a 60 mesh screen (U.S. Standard).

Precleaned steel test panels (from "Q" Panel Co.) measuring 3" X 6" X 0.032" (7.6 X 15.2 X 0.08 cm) were coated using standard electrostatic spray techniques and baked in an oven at about 400°F (205°C) for 15 minutes to give a coating having a thickness of from about 2.5 to about 4.0 mils. The 60° gloss for each panel was 8.2 % or less. Other properties are given in Table I.

TABLE I

Ex. No.	Polyester Resin*	OH #	Acid #	Visc mPa	Gel time secs	HPMF mm	Wrinkle
1	Arakote 3109	30	--	4500	55	87	Yes
2	AN 745	30	5	7100	41	77	Yes
3	Ruco 112	30	--	4500	35	72	Yes
4	Crylcoat 2392	30	--	6500	38	54	Yes
5	Ruco 121	41	5	4000	40	74	Yes
6	Morton ***	47	12	2200	39	81	Yes
7**	Morton ***	47	12	2200	65	126	Yes

* Arakote 3109 is sold by Ciba-Geigy

AN 745 is sold by Hoechst Celanese

Ruco 112 and 121 are sold by Ruco Polymer Corporation

Crylcoat 2392 is sold by UCB

** Catalyst level reduced to 0.2 phr

*** Captive product of assignee; not commercially available

COMPARATIVE EXAMPLES A-D

The general procedures of Example 1 were repeated except for the substitution of the polyester resins shown in Table II for that of Example 1. As is shown in the table, none of these powder coating compositions produced a wrinkle finish. The weight ratios of curing agent to resin were 6:94 for Examples

A,B, and E; and 8:92 for Examples C & D.

TABLE II

C. Ex .	Polyester Resin	OH #	Acid #	Visc mPa	Gel time secs	HPMF mm	Wrinkle
A	Ruco 111	23	4	6500	24	49	No
B	Crylcoat 3493	30	--	---	29	46	No
C	Ruco 118	41	13	7500	25	28	No
D	XP 3932	40	13	4000	29	46	No
E*	Arakote 3109	30	--	4500	298	150+	No

* Formulation contained only 0.1 phr of the FC-520 catalyst and 50 phr of barium sulfate

COMPARATIVE EXAMPLES F-Q

Here, the general procedures of Example 1 were followed except for the substitution of the catalysts shown in Table III. As shown, none of these other catalysts, including cyclamic acid, provided a fused coating having a wrinkle finish.

TABLE III

C.Ex.	Catalyst*	Type	Gel time secs.	HPMF mm	Wrinkle
F	Nacure 4167	phosphate	300+	150+	No
G	Nacure 5225	dodecyl- benzene sulfonic acid salt	79	88	No
H	Nacure 3525	dinonyl- naphthalene disulfonic acid salt	66	77	No
J	Nacure 2500	p-toluene sulfonic acid salt	54	79	No
K	Nacure XP330	zinc salt of dinonyl- naphthalene sulfonic acid	31	39	No
L	Nacure XP350	sulfonic acid ester	69	61	No
M	Cycat 4045	amine blocked aromatic sulfonic acid	54	79	No
N	Cycat 4040	strong acid	25	26	No
O	Cycat 600	organic acid	22	18	No
P	Cycat 296-9	acid	300+	54	No
Q	Cyclamic acid	---	40	57	No

* Nacure is a trademark of King Industries
 Cycat is a trademark of American Cyanamid
 Cyclamic acid is a product of Abbott Laboratories

EXAMPLES 8-14

The general procedure of Examples 1-7 was repeated except that benzoin was not used, 40 parts of the Bartex 65 filler was used, only 0.5 part of the amine triflate was used, and the epoxy resin identified in Table V was used. The weight ratio of the resin to the Powderlink 1174 curing agent is also given in the table.

TABLE V

Ex. No.	Epoxy Resin	Ratio	eq wt (OH)	epoxy eq wt	Gel time secs	HPMF mm	Wrinkle
8	GT-7013 *	6:94	-400	650-725	300+	67	yes
9	GT-7074 *	7:93	323	950-	130	56	alligator
4							
10	GT-7074 *	8:92	323	950-1175	134	55	alligator
11	GT-7097 *	8:92	303	1667-2000	104	56	alligator
12	GT-7097 *	9:91	303	same	82	59	alligator
13	GT-7097 *	10:90	303	same	88	61	alligator
14	Epon 2004 **	6:94	-325	875-975	300+	63	yes †

* Ciba-Geigy

** Epon is a trademark of Shell Chemical Co.

† poor cure

EXAMPLE 15

Ruco 112 polyester (94 parts), Powderlink 1174 curing agent (6 parts), Resiflow P-67 and Uraflow B flow agents (1.4 and 0.8 parts, respectively), Bartex 65 filler (40 parts), Raven #22 carbon black (3 parts), and the dibutylamine salt of triflic acid (0.4 part, pH=9.3) were blended in a Henschel blender at 2200 rpm for 1 minute. The blend was then melt mixed in an extruder having a front zone at 180 °F and an unheated rear zone. The extrudate was then mixed with 0.2% by weight of alumina "C" and ground in a high speed, 12 pin grinder to a 60 mesh size. The gel time of the resulting coating powder was 99 seconds and the HPMF was 92 mm. A Q-panel electrostatically coated with about 2.5 to 4.0 mils of the powder was heated at 400 °F for 15 minutes. A wrinkle finish was achieved.

EXAMPLE 16

The general procedure of Example 15 was repeated except that the pH of the dibutylamine salt was 8.3. A wrinkle pattern substantially identical to that of Example 15 was achieved.

Claims

1. A powder coating composition comprising a hydroxy-functional resin, a curing agent, and an amine salt of trifluoromethane-sulfonic acid as a catalyst.
2. A powder coating composition according to claim 1 wherein the curing agent is an aminoplast condensation product.
3. A powder coating composition according to claim 2 wherein the curing agent is an alkoxyated aminoplast.

TABLE V

Ex. No.	Epoxy Resin	Ratio	eq wt (OH)	epoxy eq wt	Gel time secs	HPMF mm	Wrinkle
8	GT-7013 *	6:94	-400	650-725	300+	67	yes
9	GT-7074 *	7:93	323	950-	130	56	alligator
4							
10	GT-7074 *	8:92	323	950-1175	134	55	alligator
11	GT-7097 *	8:92	303	1667-2000	104	56	alligator
12	GT-7097 *	9:91	303	same	82	59	alligator
13	GT-7097 *	10:90	303	same	88	61	alligator
14	Epon 2004 **	6:94	-325	875-975	300+	63	yes †

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EXAMPLE 16

The general procedure of Example 15 was repeated except that the pH of the dibutylamine salt was 8.3. A wrinkle pattern substantially identical to that of Example 15 was achieved.

Claims

1. A powder coating composition comprising a hydroxy-functional resin, a curing agent, and an amine salt of trifluoromethane-sulfonic acid as a catalyst.
2. A powder coating composition according to claim 1 wherein the curing agent is an aminoplast condensation product.
3. A powder coating composition according to claim 2 wherein the curing agent is an alkoxyated aminoplast.



4. A powder coating composition according to any preceding claim wherein the amine of the catalyst is diethylamine.
5. A powder coating composition according to any preceding claim wherein the catalyst has a pH of from 4.5 to 10.
6. A powder coating composition according to any preceding claim wherein the resin is a polyester.
7. A powder coating composition according to claim 6 wherein the hot plate melt flow value is at least 50 mm.
8. A powder coating composition according to claim 7 wherein the hot plate melt flow value is more than 150 mm and the gel time of the composition is less than 280 seconds.
9. A powder coating composition according to any one of claims 6 to 8 wherein the catalyst has a pH of at least 6.5.
10. A powder coating composition according to any one of claims 1 to 5 wherein the resin is an epoxy resin.
11. A composition according to any one of claims 1 to 5 wherein the resin is a hydroxy-functional acrylate or methacrylate resin.
12. A composition according to any preceding claim wherein the amount of catalyst is from 0.05 to 1 part per hundred parts by weight of the combined weight of the resin and the curing agent.
13. A composition according to any preceding claim wherein the amount of catalyst is from 0.2 to 0.8 phr.
14. A method for imparting a wrinkle finish to a coating on a substrate, comprising applying a powder coating composition according to any preceding claim to a surface of the substrate and fusing the powder.
15. An article having a wrinkle finish coating comprising a fused powder composition according to any one of claims 1 to 13.

Patentansprüche

1. Pulverlackzusammensetzung, die ein hydroxyfunktionelles Harz, ein Härtungsmittel und ein Aminsalt von Trifluormethansulfonsäure als Katalysator umfaßt.
2. Pulverlackzusammensetzung nach Anspruch 1, bei der das Härtungsmittel ein Aminoplast-Kondensationsprodukt ist.
3. Pulverlackzusammensetzung nach Anspruch 2, bei der das Härtungsmittel ein alkoxylierter Aminoplast ist.
4. Pulverlackzusammensetzung nach einem der vorausgehenden Ansprüche, bei der das Amin des Katalysators Diethylamin ist.
5. Pulverlackzusammensetzung nach einem der vorausgehenden Ansprüche, bei der der Katalysator einen pH-Wert von 4,5 bis 10 hat.
6. Pulverlackzusammensetzung nach einem der vorausgehenden Ansprüche, bei dem das Harz ein Polyester ist.
7. Pulverlackzusammensetzung nach Anspruch 6, bei der der Heizplatten-Schmelzflußwert wenigstens 5 mm ist.



8. Pulverlackzusammensetzung nach Anspruch 7, bei der der Heizplatten-Schmelzflußwert größer als 150 mm ist und die Gelzeit der Zusammensetzung geringer als 280 sec ist.
- 5 9. Pulverlackzusammensetzung nach einem der Ansprüche 6 bis 8, bei der der Katalysator einen pH-Wert von wenigstens 6,5 hat.
- 10 10. Pulverlackzusammensetzung nach einem der Ansprüche 1 bis 5, bei der das Harz ein Epoxharz ist.
11. Zusammensetzung nach einem der Ansprüche 1 bis 5, bei der das Harz ein hydroxyfunktionelles Acrylat- oder Methacrylatharz ist.
12. Zusammensetzung nach einem der vorausgehenden Ansprüche, bei der die Katalysatormenge 0,05 bis 1 Teil je 100 Gewichtsteile des vereinigten Gewichtes des Harzes und des Härtungsmittels beträgt.
- 15 13. Zusammensetzung nach einem der vorausgehenden Ansprüche, bei der die Katalysatormenge 0,2 bis 0,8 phr beträgt.
14. Verfahren zur Erzeugung eines Runzeleffektes eines Überzuges auf einem Substrat, bei dem man eine Pulverlackzusammensetzung nach einem der vorausgehenden Ansprüche auf einer Oberfläche des Substrates aufbringt und das Pulver schmilzt.
- 20 15. Gegenstand mit einem Überzug mit Runzeleffekt, der eine aufgeschmolzene Pulverzusammensetzung nach einem der Ansprüche 1 bis 13 umfaßt.

25 Revendications

1. Composition de revêtement pulvérulente comprenant une résine hydroxy-fonctionnelle, un agent de traitement et un sel d'amine de l'acide trifluorométhanesulfonique comme catalyseur.
- 30 2. Composition de revêtement pulvérulente selon la revendication 1, dans laquelle l'agent de traitement est un produit de condensation aminoplaste.
3. Composition de revêtement pulvérulente selon la revendication 2, dans laquelle l'agent de traitement est un aminoplaste alcoylé.
- 35 4. Composition de revêtement pulvérulente selon l'une quelconque des revendications précédentes, dans laquelle l'amine du catalyseur est la diéthylamine.
5. Composition de revêtement pulvérulente selon l'une quelconque des revendications précédentes, dans laquelle le catalyseur a un pH de 4,5 à 10.
- 40 6. Composition de revêtement pulvérulente selon l'une quelconque des revendications précédentes, dans laquelle la résine est un polyester.
- 45 7. Composition de revêtement pulvérulente selon la revendication 6, dans laquelle la valeur d'écoulement à l'état fondu à plaque chaude est d'au moins 50 mm.
8. Composition de revêtement pulvérulente selon la revendication 7, dans laquelle la valeur d'écoulement à l'état fondu à plaque chaude est supérieure à 150 mm et le temps de gélification de la composition est inférieur à 280 s.
- 50 9. Composition de revêtement pulvérulente selon l'une quelconque des revendications 6 à 8, dans laquelle le catalyseur a un pH d'au moins 6,5.
- 55 10. Composition de revêtement pulvérulente selon l'une quelconque des revendications 1 à 5, dans laquelle la résine est une résine époxy.



11. Composition selon l'une quelconque des revendications 1 à 5, dans laquelle la résine est une résine d'acrylate ou de méthacrylate hydroxyfonctionnelle.
- 5 12. Composition selon l'une quelconque des revendications précédentes, dans laquelle la quantité de catalyseur est de 0,05 à 1 partie pour 100 parties en masse de la masse combinée de résine et d'agent de traitement.
13. Composition selon l'une quelconque des revendications précédentes, dans laquelle la quantité de catalyseur est de 0,2 à 0,8 partie pour 100 parties en masse de résine.
- 10 14. Procédé pour conférer une finition ridée à un revêtement sur un substrat, comprenant l'application d'une composition de revêtement pulvérulente selon l'une quelconque des revendications précédentes à une surface du substrat et la fusion de la poudre.
- 15 15. Article ayant un revêtement à finition ridée comprenant une composition pulvérulente fondue selon l'une quelconque des revendications 1 à 13.

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