

## PREPARATION OF FILLER-METAL WELD ROD BY INJECTION MOLDING OF POWDER

This invention relates to the preparation of filler-metal weld rod and, more particularly, to the preparation of weld rod of difficult-to-deform alloys.

### BACKGROUND

In a form of welding, a metallic article to be welded is locally melted, and the melted metal is mixed with a second metal. The temperature is thereafter reduced so that the melted mixture solidifies. In one approach, the second metal is another article, so that the two articles are joined together. In another approach, the second metal is an overlay deposit that is also melted during the welding process, with the result that the first article is overlaid with the second metal.

A filler metal may be used in either of these approaches. In the joining of two articles by welding, the filler metal may be added into the melted zone to fill the space between the two articles. In the overlay process, the filler metal may form substantially the entire overlay. The filler metal may be the same as one or both of the articles being joined in the first approach. In the second approach, the filler metal may be the same as the article being overlaid, such as when the dimensions of the article are being restored during a repair process, or of a different composition to provide particular properties to the surface of the overlaid article.

The filler metal is often supplied as a weld rod that is used in automated welding apparatus and other welding procedures such as manual welding. (As used herein, "rod" and "weld rod" include physical forms that are considered rods and also physical forms that are considered wires, avoiding the need for any arbitrarily selected distinction as to whether the physical form is a rod or a wire.) A heat source, such as an electrical welding power supply or a beam source such as a laser or electron beam, heats the region of the article to be melted, forming a molten pool. The filler-metal weld rod is gradually fed into the molten pool to supply the desired volume of the filler metal.

The filler metal may be produced in rod form in various ways. In one approach, it is cast as a billet and then extruded or wire drawn to smaller transverse size. In another approach, it is consolidated as a powder into a billet, and then extruded or wire drawn to smaller transverse size. In either of these fabrication techniques, the extruded article is centerless ground to achieve the desired shape and size, and to remove the remnants of the extrusion operation. In other approaches, the rod may be cast to shape from powder or produced from a tube filled with a powder mixture.

Some alloys of interest as filler metals in welding applications, notably titanium aluminides and nickel-base superalloys with a high volume fraction of gamma prime phase when heat treated, cannot be wire drawn due to their work hardening properties and limited ductilities. The welding filler metal weld rod is therefore conventionally produced by a specialized extrusion process, followed by acid etching and centerless grinding of the extruded material. As a result, the manufacturing yields of usable weld rod are low, typically about 25 percent of the weight of the starting material. The process is also relatively expensive. The cost of the weld rod is therefore high, relative to the material cost. More recently, techniques have been developed to make the weld rod from powder by specialized casting or wire drawing of a powder-filled tube.

Although the recently developed processes for manufacturing titanium aluminide and high-gamma prime nickel-base superalloys are operable, there continues to be a need for a further-improved approach to the fabrication of weld rod and related types of products. The present invention fulfills this need, and further provides related advantages.

## BRIEF SUMMARY OF THE INVENTION

One aspect of the present invention provides a method for preparing a filler-metal weld rod of a filler-metal composition; avoiding the use of water comprising the steps of providing a mass of metallic powders, wherein the mass of metallic powders together have the filler-metal composition; mixing the metallic powders with a temporary thermoplastic binder to form an injection-moldable mixture; thereafter injection molding the injection-moldable mixture at an injection-molding temperature above the thermoplastic temperature of the thermoplastic binder to form an injection-molded rod;

thereafter removing excess thermoplastic binder from an external surface of the injection-molded rod; and thereafter sintering the injection-molded rod to form the filler-metal weld rod, wherein the temporary thermoplastic binder is removed in the step of sintering and the sintered filler-metal weld rod has a relative density of not greater than 90 percent.

Other features and advantages of the present invention will be apparent from the following more detailed description of the preferred embodiment, taken in conjunction with the accompanying drawings, which illustrate, by way of example, the principles of the invention. The scope of the invention is not, however, limited to this preferred embodiment.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a block flow diagram of an approach for practicing the invention;

Figure 2 is a schematic illustration of an injection-molding apparatus; and

Figure 3 is an elevational view of a filler-metal weld rod produced by the approach of Figure 1.

#### DETAILED DESCRIPTION OF THE INVENTION

Figure 1 depicts the steps in a method for preparing a filler-metal weld rod of a filler-metal composition. A mass of metallic powders is provided, step 20. The mass of metallic powders taken together have the filler-metal composition. The metallic powders are preferably prealloyed. That is, each powder particle has the net filler-metal composition as to metallic elements. Prealloyed metallic powders for compositions of interest are available commercially, or can be prepared specially by known techniques. The metallic powder particles may instead be of different compositions, but selected so

that the net composition of all of the metallic powder particles taken together is the filler-metal composition of interest.

The present approach is operable to produce any of a wide range of filler-metal compositions. As long as prealloyed powders or powders whose compositions can be combined to define a composition of interest are available, the present approach may be utilized. However, some filler-metal weld-rod compositions are of particular interest, because they are difficult or impossible to produce by conventional techniques. One preferred filler metal is a nickel-base superalloy that is heat treatable to produce more than about 30 volume percent gamma prime phase. Members of this class of materials work harden so rapidly and are of such limited ductility that it is difficult to produce them by wire drawing or other technique requiring gross deformation of the material to form the weld rod of this filler metal. Examples of such high-gamma prime nickel-base superalloys include Rene<sup>TM</sup> 142 alloy having a nominal filler-metal composition in weight percent of about 12.0 percent cobalt, about 6.8 percent chromium, about 1.5 percent molybdenum, about 4.9 percent tungsten, about 2.8 percent rhenium, about 6.35 percent tantalum, about 6.15 percent aluminum, about 1.5 percent hafnium, about 0.12 percent carbon, about 0.015 percent boron, balance nickel and minor elements; and Rene<sup>TM</sup> 195 alloy having a nominal filler-metal composition in weight percent of from about 7.4 to about 7.8 percent chromium, from about 5.3 to about 5.6 percent tantalum, from about 2.9 to about 3.3 percent cobalt, from about 7.6 to about 8.0 percent aluminum, from about 0.12 to about 0.18 percent hafnium, from about 0.5 to about 0.6 percent silicon, from about 3.7 to about 4.0 percent tungsten, from about 1.5 to about 1.8 percent rhenium, from about 0.01 to about 0.03 percent carbon, from about 0.01 to about 0.02 percent boron, balance nickel and incidental impurities.

Another preferred filler metal is an intermetallic alloy such as a titanium-base intermetallic alloy, which also has a high rate of work hardening and limited ductility, and therefore is difficult or impossible to form into weld rods by gross deformation processes. Titanium aluminide is an example. One such class of titanium aluminide filler-metal weld rods have a composition in atomic percent of from about 45.5 to about 48.0 percent aluminum and from about 48 to about 50.5 percent titanium, with the

balance other elements. Examples of other intermetallic alloys of interest include nickel aluminide, niobium silicide, and molybdenum silicide.

Some other alloys of interest are difficult to manufacture as weld rod because of their high work hardening rates that make them difficult to draw at room temperature. The conventional approach to weld-rod fabrication for these materials requires multiple steps of cold drawing and annealing, so that the production cost is high. The present approach allows the production of such materials much more economically. Examples include Waspalloy, having a nominal composition in weight percent of 13.0 percent cobalt, 0.04 percent carbon, 1.5 percent aluminum, 3.0 percent titanium, 19.0 percent chromium, 4.3 percent molybdenum, balance nickel; Ti-64, having a nominal composition in weight percent of 6 percent aluminum, 4 percent vanadium, balance titanium; A286, having a nominal composition in weight percent of 24-27 percent nickel, 13.5-16 percent chromium, 1.9-2.35 percent titanium, 1.0-1.5 percent molybdenum, 0.1-0.5 percent vanadium, 0.08 percent maximum carbon, 2.0 percent maximum manganese, 1.0 percent maximum silicon, 0.35 percent maximum aluminum, 0.030 percent maximum sulfur, 0.001-0.01 percent boron, balance iron; and Alloy 718, having a nominal composition in weight percent of from about 50 to about 55 percent nickel, from about 17 to about 21 percent chromium, from about 4.75 to about 5.50 percent columbium plus tantalum, from about 2.8 to about 3.3 percent molybdenum, from about 0.65 to about 1.15 percent titanium, from about 0.20 to about 0.80 percent aluminum, 1.0 percent maximum cobalt, and balance iron totaling 100 percent by weight.

Optionally, nonmetallic powders may be mixed with the metallic powders. The nonmetallic powders are typically hard intermetallic compounds such as carbides, borides, or the like that are not melted during welding but are incorporated into the weldment when the weld rod is later used in a welding procedure.

The metallic powders (and nonmetallic powders, if any) are mixed with a thermoplastic binder to form an injection-moldable mixture, step 22. The thermoplastic binder is temporary in the sense that it is removed in a later step and is not present in the final weld rod. The thermoplastic binder may be any operable thermoplastic binder suitable for

sintering operations, preferably an organic or hydrocarbon thermoplastic binder. Examples include polyethylene, polypropylene, wax such as paraffin wax or carnauba wax, and polystyrene. A sufficient amount of the thermoplastic binder is used to render the mixture cohesive and pliable at temperatures above the thermoplastic temperature of the thermoplastic binder. The mixing of the powders and the binder is preferably performed at a mixing temperature that is above the thermoplastic temperature of the thermoplastic binder, which is typically 200°F (about 93 °F) or greater but depends upon the specific thermoplastic binder material that is used. The thermoplastic binder material becomes flowable or "molten" at and above the thermoplastic temperature, which aids in the mixing. The mixing at this mixing temperature achieves a mixture that is flowable and injection moldable at or above the thermoplastic temperature, but which is relatively inflexible and hard below the thermoplastic temperature.

The injection-moldable mixture preferably does not contain any added water, although there may be a minor amount of water present as an impurity. A substantial amount of water, if present, would chemically react with the constituents of typical alloys of interest. The presence of a significant amount of water may also lead to centerline porosity after injection molding and sintering. Centerline porosity, if present, may be removed by swaging or a similar mechanical deformation process where the alloy is malleable. However, the removal of the centerline porosity adds to the cost of the product, a cost that is avoided in the present approach. Additionally, such gross mechanical deformation processes cannot be readily used with many alloys that may be made into filler-metal weld rods by the present approach due to their limited ductilities, such as intermetallic alloys and high-gamma-prime nickel-base superalloys. Hot isostatic pressing cannot generally be used to close internal porosity. Consequently, approaches that produce centerline porosity cannot be used to produce weld rods of many of the materials of most interest. The combination of little or no water, use of thermoplastic binder, and elevated-temperature injection molding of the present approach aids in avoiding the centerline porosity, and none has been observed in prototype specimens of weld rod produced by the present approach. Accordingly, it is preferred that the thermoplastic binder is non-

aqueous, water is not mixed with the injection-moldable mixture, and no water is used in the subsequent step of removal of excess thermoplastic binder.

The injection-moldable mixture of metallic powders and thermoplastic binder is thereafter injection molded to form an injection-molded rod, step 24. The injection molding step 24 is performed with the injection-moldable mixture at an injection-molding temperature above the thermoplastic temperature of the thermoplastic binder.

The thermoplastic binder is therefore flowable, reducing the friction with the injection nozzle during the injection molding. Any type of operable injection-molding apparatus may be used to accomplish step 24. A preferred injection-molding apparatus 40 is illustrated in Figure 2. The injection-molding apparatus 40 includes an injection head 42 in the form of a chamber, with an injection nozzle 44 as the outlet of the chamber. A movable piston 46 forces the injection-moldable mixture 48 contained within the injection head 42 through the injection nozzle 44. The injection head 42 includes a controllable heater 49 that heats the injection-moldable mixture to the injection-molding temperature. The injection nozzle 44 preferably has a circular cross section, although it could have other shapes.

Preferably, no closed mold is used to receive and shape the injection-moldable mixture 48 as it flows from the injection nozzle 44. Because of the rod shape of the weld rod that is being made, such a closed mold would have to be elongated. It would be difficult to injection mold into such an elongated hollow mold due to friction. Instead, a movable receiver 50 is positioned to receive the injection-moldable mixture 48 that flows from the injection nozzle 44. A receiving surface 52 of the movable receiver 48 moves away from the injection nozzle 44 at a linear rate that is adjusted to be the same as the linear rate at which the injection-moldable mixture 48 flows from the injection nozzle 44. This movement allows the injection-moldable mixture 48 to be smoothly and continuously deposited onto the moving receiving surface 52. The shape of the injection-moldable mixture 48 is maintained by the combination of this movement and the consistency of the mixture of the metal powders and the thermoplastic binder. In Figure 2, the movable receiver 50 is depicted as a continuous conveyer, but it could be any other operable structure such as a movable plate-like surface.

To perform the injection molding step 24 using this preferred injection-molding apparatus 40, the injection-moldable mixture 48 is loaded into the injection head 42. The piston 46 is moved to force the injection-moldable 48 mixture out of the injection nozzle 44 and onto the movable receiver 50. The receiving surface 52 of the movable receiver 50 moves away from the injection nozzle 44 at the same linear rate as the injection-moldable mixture 48 is forced from the injection nozzle 44, so that the injection-molded mixture is deposited upon the receiving surface 52 to form an injection molded rod 54. The injection-moldable mixture 48 is above the thermoplastic temperature of the thermoplastic binder as it emerges from the injection nozzle 44. The injection-moldable mixture quickly cools so that by a point about 2 inches or so from the injection nozzle 44 the injection-moldable mixture 48 is below the thermoplastic temperature of the thermoplastic material and is therefore relatively rigid and hard. It may therefore be picked up and handled with care.

Any excess thermoplastic binder is thereafter removed from an external surface 56 of the injection-molded rod 54, step 26. The excess thermoplastic binder is readily removed with a solvent for the excess thermoplastic binder. The solvent is contacted to the external surface 56 to dissolve the excess thermoplastic binder at the surface of the injection-molded rod 54 and below the surface as well. The solvent is selected according to the specific thermoplastic binder that is used. The solvent is preferably not aqueous in nature.

The injection-molded rod 54 is thereafter sintered, step 28, at a sintering temperature to form a filler-metal weld rod 58, illustrated in Figure 3. The sintering is preferably performed in a vacuum oven. As the temperature of the injection-molded rod 54 is increased, the remaining temporary thermoplastic binder is evaporated and removed, preferably leaving no trace chemicals that might later contaminate the weld. The sintering is preferably solid-state sintering and thus below the melting point of the metal. After sintering, the filler-metal weld rod 58 preferably has a cylindrical diameter of from 0.010 inch to 0.250 inch (about 0.025 cm to about 0.64 cm), preferably 0.035 to 0.070 inch (about 0.089 cm to about 0.18 cm). The diameter of the injection-molded rod 54 is therefore somewhat greater than this sintered cylindrical diameter of the filler-metal weld

rod 58, to account for shrinkage during sintering. The filler-metal weld rod 58 may be of a selected short length or of a much longer length for use in automated welding apparatus.

The sintering step 28 preferably sinters the filler-metal weld rod 58 to a relative density of not greater than 90 percent. The "relative density" is the percentage of the full density that is reached. For example, the weight of a weld rod 58 of 90 percent relative density is 90 percent of the weight of a weld rod of the same volume and same material, but of full density. Preliminary studies have demonstrated that a relative density of 90 percent or slightly lower is sufficient for the weld rod 58 to perform as required in subsequent welding operations.

On the other hand, for some other welding operations the filler-metal weld rod 58 must have a higher relative density in order to perform successfully. The higher relative density is preferably not achieved with further sintering, because the sintering times and temperatures become prohibitively large. Instead, to achieve a higher relative density the filler-metal weld rod is preferably optionally further densified by a process such as hot isostatic pressing, step 30. Hot isostatic pressing at a temperature of greater than about 2100°F (about 1150°C) for nickel-base superalloys or greater than about 2150°F (about 1180°C) for titanium aluminides, at a pressure of from about 15,000 to about 25,000 pounds per square inch (about 1050 to about 1760 kilogram per square cm), and for a time of about 1-5 hours increases the relative density of the weld rod 58 to about 98-99 percent.

Initial studies indicate that the as-fabricated weld rod 58 is sufficiently straight, of round cross section, and of the desired diameter to be used for most applications. Centerless grinding, step 32, may optionally be used to improve the quality of the surface finish of the weld rod 58, if desired.

The final filler-metal weld rod 58 is used in a welding procedure, step 34. The welding may be surface welding of a single article. Such welding is used, for example, to repair a damaged region at the surface of the article, and for this application the composition of the filler metal is typically the same as that of the substrate being repaired. Surface

welding may also be used to apply a coating, such as a hard facing, to the surface of the article. The filler-metal weld rod 58 may also be used to join two or more pieces together by welding.

The present approach has been reduced to practice to make 0.050 inch (about 0.13 cm) diameter weld rod of Rene<sup>TM</sup> 142 alloy, in pieces about 24 inches (about 61 cm) in length, both with and without steps 30 and 32 of Figure 1. There were no centerline defects.

Although a particular embodiment of the invention has been described in detail for purposes of illustration, various modifications and enhancements may be made without departing from the spirit and scope of the invention. Accordingly, the invention is not to be limited except as by the appended claims.

## CLAIMS

1. A method for preparing a filler-metal weld rod of a filler-metal composition, avoiding the use of water comprising the steps of  
  
providing a mass of metallic powders, wherein the mass of metallic powders together have the filler-metal composition;  
  
mixing the metallic powders with a temporary thermoplastic binder to form an injection-moldable mixture; thereafter  
  
injection molding the injection-moldable mixture at an injection-molding temperature above the thermoplastic temperature of the thermoplastic binder to form an injection-molded rod; thereafter  
  
removing excess thermoplastic binder from an external surface of the injection-molded rod; and thereafter  
  
sintering the injection-molded rod to form the filler-metal weld rod, wherein the temporary thermoplastic binder is removed in the step of sintering and the sintered filler-metal weld rod has a relative density of not greater than 90 percent.
2. The method of claim 1, wherein the step of providing the mass of metallic powders includes the step of  
  
providing the net metallic composition as a nickel-base superalloy that is heat treatable to produce more than about 30 volume percent gamma prime phase.
3. The method of claim 1, wherein the step of providing the mass of metallic powders includes the step of  
  
providing the net metallic composition as an intermetallic alloy.
4. The method of claim 1, wherein the step of providing the mass of metallic powders includes the step of

providing the net metallic composition as a titanium aluminide intermetallic alloy.

5. The method of claim 1, wherein the step of providing includes the step of providing the mass of metallic powders having a nominal filler-metal composition in atomic percent of from about 45.5 to about 48.0 percent aluminum and from about 48 to about 50.5 percent titanium, with the balance other elements.

6. The method of claim 1, wherein the step of providing includes the step of providing nonmetallic particles mixed with the metallic powders.

7. The method of claim 1, wherein the step of mixing includes the step of mixing the metallic powders and the temporary thermoplastic binder at a mixing temperature above the thermoplastic temperature of the thermoplastic binder.

8. The method of claim 1, wherein the step of sintering includes the step of sintering the filler-metal weld rod to a relative density of not greater than 90 percent.

9. The method of claim 1, including an additional step, after the step of sintering, of hot isostatic pressing the filler-metal weld rod.

10. The method of claim 1, wherein the step of injection molding includes the steps of providing an injection-molding apparatus including an injection head with an injection nozzle, and a movable receiver positioned to receive the injection-moldable mixture flowing from the injection nozzle, loading the injection-moldable mixture into the injection head, and

forcing the injection-moldable mixture out of the injection nozzle onto the movable receiver, while moving the movable receiver away from the injection nozzle at the same linear rate as the injection-moldable mixture is forced from the injection nozzle.