



\*G00002\*

1

## DEFLECTION YOKE WITH RINGING SUPPRESSION MEANS

This invention relates to a deflection arrangement for a video display.

To provide deflection of the electron beams in a cathode ray tube (CRT) of a television receiver, a deflection yoke comprising vertical and horizontal windings is mounted over the neck of the CRT. For a saddle-toroid (ST) or hybrid yoke, the horizontal winding comprises two saddle shaped coils that are placed  
5 into a nonmagnetic saddle shaped housing with the coils being symmetrically disposed about the horizontal axis and plane. The vertical winding typically comprises two coils, each coil toroidally wound around an upper or a lower half, respectively, of a toroidal core. After the winding is completed, each core  
10 piece is placed against the outside of the saddle shaped housing, with each of the vertical coils being symmetrically disposed about the vertical axis and plane.

The vertical deflection coil is situated in the horizontal deflection field that is produced by the horizontal deflection coil. Therefore, during horizontal retrace, a fast transition in the horizontal deflection field may induce, by  
15 magnetic coupling, a corresponding voltage pulse in each of the vertical deflection coils. Each vertical deflection coil includes a capacitance between its winding turns and a self-inductance. The capacitance forms with the self-inductance of the vertical deflection coil a resonant circuit that is excited by the induced pulse during horizontal retrace and that may produce current ringings  
20 in the vertical deflection coil following horizontal retrace. The ringings have an amplitude that, typically, decays during the following horizontal trace. Such ringings are undesirable because they may produce visual artifacts in the left side of the picture displayed on the faceplate of the CRT.

Each vertical deflection coil may be formed by wire turns being toroidally  
25 wound on the magnetically permeable ferrite core with the wire being carried by a flyer of a winding machine. In some prior art deflection yokes, in which the horizontal deflection current is at a frequency  $f_H$ , that is 15.7 KHZ in the NTSC standard, the winding turns of each of the vertical deflection coils are wound in a progressive manner.

30 In the progressive manner winding technique, all the wire turns in the vicinity of each angular position on the toroidal core are wound consecutively. After all the wire turns in a given angular position are wound, wire turns in an



\*166166\*

In the progressive manner winding technique, all the wire turns in the vicinity of each angular position on the toroidal core are wound consecutively. After all the wire turns in a given angular position are wound, wire turns in an adjacent angular position are wound. A change in the angular position from each angular position to its corresponding adjacent angular position occurs progressively and substantially only in one angular direction around the circular perimeter of the core, from the beginning to the end of each coil. Thus, in the progressive manner winding technique, the wire that forms the wire turns is not returned backward, for example, to its starting point throughout the winding process of the coil.

In one prior art vertical deflection yoke having a vertical deflection coil, that is believed to be wound in the above-mentioned progressive manner winding technique, an R-C network is coupled between first and second intermediate terminals or taps, of the first and second vertical deflection coils, respectively. The first and second vertical deflection coils are wound on the upper and lower halves, respectively, of the core. The first intermediate terminal is coupled between end terminals of the first vertical deflection coil such that a first portion of the first vertical deflection coil is coupled between the first intermediate terminal and one of the end terminals and a second portion of the first vertical deflection coil is coupled between the first intermediate terminal and the other one of the end terminals. Similarly, the second intermediate terminal is coupled between end terminals of the second vertical deflection coil. It is believed that the R-C network is used there for suppressing the ringings. However, such arrangement may not be sufficient to suppress ringings produced in a vertical deflection coil wound in the progressive manner winding technique and in which the frequency of the horizontal deflection current is at, for example,  $2 \times f_H$ .

It is well known that in a vertical deflection coil wound with a multiple layer winding technique, the ringings induced in each vertical deflection coil during horizontal retrace are substantially less objectionable than those induced in each vertical deflection coil having the same number of winding turns but wound in the progressive manner winding technique. In the multiple layer winding technique, each of the vertical deflection coils is formed as a plurality of layers, such as 5 layers. In contrast to the progressive manner winding technique, in the multiple layer winding technique, after a given layer of wire

turns is completely wound around the core, the wire is returned backward, for example, to or close to its starting point and a subsequent layer of wire turns is wound over the preceding one. After each layer is wound, the wire may be returned to its starting point by, for example, a shootback method in which the return wire follows a generally direct path along the outside of the core. This winding process continues until all the layers of the coil are wound.

Typically, the direction of the vertical deflection field is angularly rotated at an electron beam exit portion of a typical deflection yoke relative to at an electron beam entrance portion of the yoke. This rotation is referred to as a spiral winding effect. The spiral winding effect occurs because, in order to simplify the winding process, the winding turns in the vertical deflection coil are wound in a nonradial manner. Assume a first deflection yoke having a horizontal deflection coil driven by a horizontal deflection current at the frequency  $f_H$ . The first deflection yoke is adapted to provide horizontal and vertical deflection in a CRT. Also assume that the number of winding layers in each vertical deflection coil of such deflection yoke, for example, five winding layers, is selected to provide ringings at an acceptable magnitude. Assume a second deflection yoke that can provide deflection in a similar type of CRT but that has a horizontal deflection coil driven at the frequency  $2 \times f_H$ .

Should the number of winding layers selected for forming the vertical deflection coil of the aforementioned second deflection yoke so as to suppress the ringings be substantially larger than in the first vertical deflection yoke, the spiral winding effect will be substantially different in the two yokes. This is so because the different number of winding turns in each layer requires a different winding "pitch". Because of the different spiral winding effects, should the number of winding layers be different in the vertical deflection coils of the first and second deflection yokes, a CRT that is adapted by a lensing process to operate with the first deflection yoke may not be suitable for operation with the second deflection yoke. It may be desirable to reduce a difference between the CRT lensing required for operation with the first and second deflection yokes. This is so in order, for example, to utilize the same type CRT with any of the first and second deflection yokes. By utilizing the same type of CRT with each of the deflection yokes, a cost reduction is obtained. Therefore, it may be desirable to maintain the number of winding layers in a given vertical deflection coil of the first deflection yoke, for example, the same as in that of the second deflection

yoke. It follows that it may be desirable to reduce the ringings in the second deflection yoke without resorting to using a larger number of winding layers in the vertical deflection coil of the second deflection yoke than in that of the first deflection yoke.

5 A deflection yoke embodying an aspect of the invention for producing electron beam scanning in a cathode ray tube of a video display includes a core made of a permeable magnetic material. A first vertical deflection coil cooperates with the core for producing a vertical deflection field. The first vertical deflection coil has a plurality of winding layers wound around the core in  
10 a multiple layer winding technique. A horizontal deflection coil produces a horizontal deflection field. A ringing suppressing impedance is coupled to an intermediate terminal between end terminals of the first vertical deflection coil for suppressing ringings that are produced in the first vertical deflection coil by the horizontal deflection field.

15 FIGURE 1 illustrates a cross section of a deflection yoke arrangement, embodying an aspect of the invention that is mounted on a cathode ray tube;

FIGURE 2 illustrates a cross section of the vertical deflection coils of FIGURE 1, in more detail, and a ringing suppression network, embodying an aspect of the invention; and

20 FIGURE 3 illustrates the way the ringings suppressing network and the winding layers of the vertical deflection coils of FIGURE 2 are coupled.

Referring to FIGURE 1, there is shown a deflection yoke 10 mounted on a neck 66 of, for example, a 31V, 110° CRT 67 such as, for example, Thomson's A79ECU13X. Yoke 10 includes a pair of vertical deflection coils 11a and 11b  
25 toroidally wound on a magnetically permeable core 12, and a pair of, for example, conventional saddle type horizontal deflection coils 13. Coils 13 are energized with a deflection current  $I_H$  at 14A p-p having the horizontal deflection frequency of  $2 \times f_H$  that is approximately 32 KHZ. A plastic insulator 14 electrically and physically, but not magnetically, separates the vertical and  
30 horizontal deflection coils and may provide support and alignment structure not generally illustrated for the coils and the core. Toroidal core 12 is split into two symmetrical upper and lower halves core pieces 102a and 102b, respectively.

FIGURE 2 illustrates a cross section in the X-Y plane of vertical deflection coils 11a and 11b that are wound in the multiple layer winding technique. A  
35 network 100 suppresses the ringings, in accordance with an inventive feature.

Similar numeral and symbols in FIGURES 1 and 2 indicate similar items or functions. Coils 11a and 11b are mounted symmetrically with respect to the plane X-Z that is defined between core pieces 102a and 102b. The interconnection of the layers in coil 11b is similar to that in coil 11a, hence, not shown in detail.

Each vertical deflection coil assembly is wound separately on a winding machine, for example, in the same manner. The machine rigidly clamps, for example, core piece 102a of FIGURE 2, with the longitudinal axis of the core oriented in a vertical direction. The flyer of the winding machine, to which one end of a spool of a conductor wire is attached, is indexed in a horizontal direction until the starting position of a first layer 44a of conductor turns is reached. To reduce the skin effect at the higher horizontal deflection frequency, the conductor wire of the spool includes seven wire strands. Each winding turn of the vertical deflection coil may be formed simultaneously from the seven wire strands.

The flyer begins to wind around the core piece and continues winding in the same angular direction around the core piece, as shown by the arrow, until first layer 44a is completely wound. The wire is then returned backward, by a wire portion shown in a schematic manner in FIGURE 2 and referred to by reference numeral 144a, for example, close to the same starting point of the first layer 44a, for winding the next winding layer, 45a. Each of the last three winding layers, 46a-48a, of coil 11a is wound in a similar way. The result is that each of the toroidally wound vertical deflection coils on each core piece, 102a and 102b, of magnetically permeable core 12 comprises five winding layers. The individual winding layers, 44a-48a, for example, of coil 11a may occupy or subtend different winding angles or arcuate regions on the core in order that the vertical deflection field produced by the deflection coils provides the desired degree of field nonuniformity that may be necessary to, for example, converge the electron beams.

As indicated before, the coil on each core piece is wound in a continuous fashion with a given layer being completely wound before a subsequent layer is begun. As explained in U.S. Patent No. 4,511,871, in the names of Schler, Jr. et al., entitled MODIFIED DEFLECTION YOKE COILS HAVING SHOOTBACK WINDINGS, that is incorporated by reference herein, after a given layer is completely wound, the wire may be returned to the starting point for

winding the next winding layer in, for example, the well known shootback method.

In accordance with an aspect of the invention, R-C, ringing suppression or damping network 100 is coupled between a pair of winding turns 443a and 443b. Winding turn 443a is located between end winding turns 441a and 442a, such as, for example, half way through, or in the middle of winding layer 44a. Winding layer 44a is wound closer to core piece 102a than any of the other winding layers, 45a-48a. Winding turn 443b is analogous to winding turn 443a. Winding turn 443b is located in the first winding layer, 44b, wound closer to core piece 102b than any of winding layers 45b-48b.

Each winding layer of coils 11a and 11b includes, for example, 80 winding turns, with a total winding turns of 400 in each of coils 11a and 11b. The winding turns in each winding layer are concentrated mainly in four bundles 500-503 such that between the bundles the winding concentration density is substantially smaller than within the bundle. Each bundle in a given layer contains approximately 20 winding turns to form the total of 80 winding turns in the layer. The winding turn density of each of, for example, layers 45a-48a may be made, for example, smaller in the vicinity of winding turn 443a, so as to expose winding turn 443a to the outside of yoke 10. By so exposing winding turn 443a, an access is provided to attach a lead 100c of network 100, for example, by soldering lead 100c to winding turn 443a, after coil 11a has been already wound.

Network 100 includes a capacitor 100a coupled in series with a ringing attenuating resistor 100b. Capacitor 100a forms a low impedance to the ringings that are at a high frequency of, for example, 1 MHz. The value of resistor 100b is selected to provide, for example, critical damping of the ringings.

FIGURE 3 illustrates a schematic interconnection between the layers of coils 11a and 11b and network 100. Similar symbols and numerals in FIGURES 1-3 indicate similar items or functions. As shown in FIGURE 3, network 100 is coupled between winding turns 443a and 443b of winding layers 44a and 44b, respectively.

Advantageously, by providing ringing attenuating network 100 that is coupled to coils 11a and 11b, wound in the multiple layer winding technique, ringings in coils 11a and 11b are significantly reduced. Such arrangement is particularly effective for reducing the ringings when frequency of the horizontal deflection current is at a frequency substantially higher than  $f_H$ , such as  $2 \times f_H$ .

## CLAIMS

1. A deflection yoke (10) for producing electron beam scanning in a cathode ray tube (67) of a video display, having a core (12) made of a permeable magnetic material;

toroidal first and second symmetrically arranged vertical deflection coils (11a, 11b) cooperating with said core, for producing a vertical deflection field, said vertical deflection coils each having a plurality of winding layers (44a-48a, 44b-48b) wound around said core in a multiple layer winding technique;

a horizontal deflection coil (13) for producing a horizontal deflection field; characterized by

a ringing suppressing impedance (100) coupled between intermediate terminals (443a, 443b) located between end winding turns of respective winding layers of said first and second vertical deflection coils (11a, 11b) closest to said core, for suppressing ringings that are produced in said vertical deflection coils by said horizontal deflection field.

2. A deflection yoke (10) according to Claim 1, characterized in that said impedance (100) comprises a resistor (100b) coupled in series with a capacitor (100a) that form a series arrangement coupled between said first (11a) and second (11b) vertical deflection coils.