

Description

The present invention relates to resin compositions for gears. More particularly, it pertains to resin compositions for gears excellent in terms of mass production, accuracy and mechanical strengths, containing resins called thermotropic liquid crystal polymers which show anisotropy when molten.

Statement of Prior Arts

Gears made of resins, as compared with gears made of metals, being light in weight and excellent in self-lubrication, corrosion resistance, noise suppression, workability, mass productivity, etc., are finding applications in various industries. However, these resins have their own drawbacks which include low heat resistance, large thermal deformation and large shrinkage in working, etc., and for this reason, their miniaturization and uses in high temperature atmosphere are limited. In answer to the social demands of resin gears for miniaturization, strengthening and widening of usable temperature range, responsive arrangements for thermosetting resins, mixing of fibers, raising of melting points of thermoplastic resins and other improvements have been attempted.

However, the thermosetting resins are not adaptable for mass production and show low workability. The mixing of fibers and raising of melting points respectively provide recognizable effects in increase in mechanical strengths and improvement in heat resistance, but at the cost of lowered workability and mass productivity because of marked increase in viscosity at the time of melting.

Attempts have been being made assiduously for strengthening, miniaturization and expansion of usable temperature range without losing these resins' advantageous features, but are still insufficient.

Summary of the Invention

The present inventors, in an effort to solve such problems, engaged in studies and found out that if the basic resins are thermotropic liquid crystal polymers which give anisotropy when molten, a remarkable reduction in their molten viscosity is realizable and increases in strength by way of mixing of fibers are achievable without lowering workability and mass productivity, which finding has led to completion of this invention.

According to the invention there is provided a method for molding a gear wheel by introducing a resin composition into a mold, characterized in that the composition comprises (a) 30 to 98% by weight of a melt-processable polymer which is capable of forming an anisotropic phase in the molten state and (b) 2 to 70% by weight of a fibrous material, and in that the composition is introduced into the mold through a gate located at or near to the axial center thereof.

As described in greater detail hereinafter, the composition employed for the molding may contain as desired, lubricants, antistatic agents and conductive fillers.

The method of the present invention enables the production of gear wheels having a degree of miniaturization and strength which were hitherto scarcely available with resin gears. The product gear wheels are suitable for use under exposure to high temperatures and chemical substances.

The polymers used according to the invention which achieve a marked reduction in viscosity when molten are polymer compositions which display optical anisotropy when molten and which are thermoplastic and workable by fusion (melt-processable), such compositions being generally classified as thermotropic liquid crystal polymers.

Such polymers which form the anisotropic melt phase have a property that under their molten state, the polymer molecule chains are regularly aligned in parallel arrangement. The state in which molecules are arranged in this way is often called liquid crystal state or nematic phase of liquid crystalline material. Such polymers are manufactured from monomers which are generally slender, and flat, which have appreciably high rigidity along the long axis of molecule and which have a plurality of chain-extending bonds which are normally in coaxial or parallel relation to each other.

The property of the anisotropic fused phase may be confirmed by the accustomed polarization inspection method based on use of crossed polarizers. More particularly, confirmation of the anisotropic fused phase may be made by observation of the sample mounted on the Leitz hot stage in a nitrogen atmosphere at a magnification of 40 powers, using a polarizing microscope. The aforementioned polymers are optically anisotropic. That is, they permit transmission of light beam, when put between crossed polarizers. If the sample is optically anisotropic, the polarized light will be transmitted, even when it is in stationary state.

Components of the polymers which form the anisotropic fused phase as above-mentioned include:

- ① One or more of aromatic dicarboxylic acids and alicyclic dicarboxylic acids;
- ② One or more of aromatic diols, alicyclic diols and aliphatic diols;
- ③ One or more of aromatic hydrocarboxylic acids;
- ④ One or more of aromatic thiol-carboxylic acids;
- ⑤ One or more of aromatic dithiols and aromatic thiol phenols; and
- ⑥ One or more of hydroxylamines and aromatic diamines.

And the polymers which form the anisotropic fused phase are composed of combinations such as:

- I) Polyesters formed of ① and ②;
- II) Polyesters formed of ③ only;

- III) Polyesters formed of ①, ② and ③;
- IV) Polythiol esters formed of ④ only;
- V) Polythiol esters formed of ① and ⑤;
- VI) Polythiol esters formed of ①, ④ and ⑤;
- 5 VII) Polyester amides formed of ①, ③ and ⑥; and
- VIII) Polyester amides formed of ①, ②, ③ and ④.

Although not included in the category of combinations of components hereabove mentioned, organic polyazomethines are included in polymers which form the anisotropic fused phase. Particular examples mentioned as such polymers are poly (nitrilo-2-methyl-1,4-phenylenenitriloethylidyne-1,4-phenylene-ethylidyne), poly (nitrilo-2-methyl-1,4-phenylenenitrilomethylidyne-1,4-phenylenemethylidyne), and poly (nitrilo-2-chloro-1,4-phenylenenitrilomethylidyne-1,4-phenylenemethylidyne).

Further, polymers which are not included in the category of combinations of components above-mentioned, but form the anisotropic fused phase, include polyester carbonates. They substantially comprise 4-oxybenzoyl units, dioxyphenyl units, dioxycarbonyl units and terephthaloyl units.

15 In the following, compounds which provide components of the aforementioned combinations I) VIII) are listed:

Mentioned as aromatic dicarboxylic acids are: aromatic dicarboxylic acids such as terephthalic acid, 4,4'-diphenyldicarboxylic acid, 4,4'-triphenyldicarboxylic acid, 2,6-naphthalenedicarboxylic acid, diphenylether-4,4'-dicarboxylic acid, diphenoxyethane-4,4'-dicarboxylic acid, diphenoxybutane-4,4'-dicarboxylic acid, diphenylethane-4,4'-dicarboxylic acid, isophthalic acid, diphenyl ether-3,3'-dicarboxylic acid, diphenoxyethane-3,3'-dicarboxylic acid, diphenylethane-3,3'-dicarboxylic acid and naphthalene-1,6-dicarboxylic acid, and derivatives of the aforementioned aromatic dicarboxylic acids substituted with alkyls, alkoxyis or halogens such as chloroterephthalic acid, dichloroterephthalic acid, bromoterephthalic acid, methylterephthalic acid, dimethylterephthalic acid, ethylterephthalic acid, methoxyterephthalic acid and ethoxyterephthalic acid.

Mentioned as alicyclic dicarboxylic acids are: alicyclic dicarboxylic acids such as trans-1,4-cyclohexanedicarboxylic acid, cis-1,4-cyclohexanedicarboxylic acid and 1,3-cyclohexanedicarboxylic acid, and derivatives of the aforementioned alicyclic dicarboxylic acids substituted with alkyls, alkoxyis or halogens such as trans-1,4-(1-methyl)cyclohexanedicarboxylic acid and trans-1,4-(1-chloro)cyclohexanedicarboxylic acid.

Mentioned as aromatic diols are: aromatic diols such as hydroquinone, resorcinol, 4,4'-dihydroxydiphenyl, 4,4'-dihydroxytriphenyl, 2,6-naphthalenediol, 4,4'-dihydroxydiphenyl ether, bis(4-hydroxyphenoxy) ethane, 3,3'-dihydroxydiphenyl, 3,3'-dihydroxydiphenyl ether, 1,6-naphthalenediol, 2,2-bis(4-hydroxyphenyl) propane and 2,2-bis(4-hydroxyphenyl)methane; and alkyl, alkoxy or halogen derivatives of the aforementioned aromatic diols, such as chlorohydroquinone, methylhydroquinone, 1-butylhydroquinone, phenylhydroquinone, methoxyhydroquinone, phenoxyhydroquinone, 4-chlororesorcinol and 4-methylresorcinol.

Mentioned as alicyclic diols are: alicyclic diols such as trans-1,4-cyclohexanediol, cis-1,4-cyclohexanediol, trans-1,4-cyclohexanedimethanol, cis-1,4-cyclohexanedimethanol, trans-1,3-cyclohexanediol, cis-1,2-cyclohexanediol, trans-1,3-cyclohexanedimethanol, and alkyl, alkoxy or halogen derivatives of the aforementioned alicyclic diols such as trans-1,4-(1-methyl)cyclohexanediol and trans-1,4-(1-chloro)cyclohexanediol.

Mentioned as aliphatic diols are: straight-chain or branched aliphatic diols such as ethylene glycol, 1,3-propanediol, 1,4-butanediol and neopentyl glycol.

45 Mentioned as aromatic hydroxycarboxylic acids are: aromatic hydroxycarboxylic acids such as 4-hydroxybenzoic acid, 3-hydroxybenzoic acid, 6-hydroxy-2-naphthoic acid and 6-hydroxy-1-naphthoic acid, and alkyl, alkoxy or halogen derivatives of the aromatic hydroxycarboxylic acids such as 3-methyl-4-hydroxybenzoic acid, 3,5-dimethyl-4-hydroxybenzoic acid, 2,6-dimethyl-4-hydroxybenzoic acid, 3-methoxy-4-hydroxybenzoic acid, 3,5-dimethoxy-4-hydroxybenzoic acid, 6-hydroxy-5-methyl-2-naphthoic acid, 6-hydroxy-5-methoxy-2-naphthoic acid, 3-chloro-4-hydroxybenzoic acid, 2-chloro-4-hydroxybenzoic acid, 2,3-dichloro-4-hydroxybenzoic acid, 3,5-dichloro-4-hydroxybenzoic acid, 2,5-dichloro-4-hydroxybenzoic acid, 3-bromo-4-hydroxybenzoic acid, 6-hydroxy-5-chloro-2-naphthoic acid, 6-hydroxy-7-chloro-2-naphthoic acid and 6-hydroxy-5,7-dichloro-2-naphthoic acid.

55 Mentioned as aromatic mercaptocarboxylic acids are: 4-mercaptobenzoic acid, 3-mercaptobenzoic acid, 6-mercapto-2-naphthoic acid and 7-mercapto-2-naphthoic acid.

Mentioned as aromatic dithiols are: benzene-1,4-dithiol, benzene-1,3-dithiol, 2,6-naphthalenedithiol and 2,7-naphthalenedithiol.

Mentioned as aromatic mercaptophenols are: 4-mercaptophenol, 3-mercaptophenol, 6-mercaptophenol and 7-mercaptophenol.

60 Mentioned as aromatic hydroxyamine and aromatic diamine are: 4-aminophenol, N-methyl-4-aminophenol, 1,4-phenylenediamine, N-methyl-1,4-phenylenediamine, N,N'-dimethyl-1,4-phenylenediamine, 3-aminophenol, 3-methyl-4-aminophenol, 2-chloro-4-aminophenol, 4-amino-1-naphthol, 4-amino-4'-hydroxydiphenyl, 4-amino-4'-hydroxydiphenyl ether, 4-amino-4'-hydroxydiphenylmethane, 4-amino-4'-hydroxydiphenyl sulfide, 4,4'-diaminophenyl sulfide(thiodianiline), 4,4'-diaminophenyl sulfone, 2,5-diaminotoluene, 4,4'-ethylenedianiline, 4,4'-diaminodiphenylethane, 4,4'-diaminodiphenyl-

methane(methylenedianiline) and 4,4'-diaminodiphenyl ether(oxydianiline).

There are polymers, of the aforementioned polymers I(~VIII) consisting of respective components above-mentioned, which either form the anisotropic fused phase or not, depending on the components, composition ratio in the polymer and the sequence distribution, but the polymers employed according to this invention are restricted to those of the aforementioned polymers which form the anisotropic fused phase.

The polyesters of the aforementioned I), II) and III) and the polyester amides of VIII) abovementioned being polymers which form the anisotropic fused phase appropriate for use according to this invention may be formed by a wide variety of ester forming processes which permit reactions between organic monomer compounds having functional groups capable of forming the required repetitive units by condensation. Such functional groups of these organic monomers compounds may include carboxyl group, hydroxyl group, ester group, acyloxy group, acid halides and amine group. The aforementioned organic monomer compounds may be subjected to the reaction by way of fusion acidolysis in the absence of heat exchange fluid. According to this method, a fused solution of reaction materials is formed first by heating the monomers together. As the reaction proceeds, solid polymer particles become suspended in the solution. Vacuum may be applied for facility in removal of volatile matters (e.g., acetic acid or water) which have been produced as by-products at the final stage of the condensation.

Besides, the slurry condensation method may be adopted for forming wholly aromatic polyesters, which are preferred according to this invention. By this method, the solid product is obtained in the state of being suspended in heat exchange medium.

Whether the aforementioned fusion acidolysis process or slurry polymerization process is employed, the organic monomer reaction substances from which the wholly aromatic polyesters are derived may be supplied for the reaction in a modified state (i.e., as lower acyl esters) in which the hydroxyl groups of such monomers at the normal temperature are esterified. The lower acyl groups should desirably have 2~4 carbon atoms. Preferably, acetic acid esters of the reaction products from such organic monomers are subjected to the reaction.

Further, mentioned as representative examples of the catalyzer arbitrarily usable either in the fusion acidolysis or slurry process are: dialkyltin oxides (e.g., dibutyltin oxide), diaryltin oxides, titanium dioxide, antimony trioxide, alkoxytitanium silicate, titanium alkoxide, alkali and alkaline earth metal salts of carboxylic acids (e.g., zinc acetate), and such gaseous catalyzers as Lewis acids (e.g., BF_3) and hydrogen halides (e.g. HCl), etc. The amount of the catalyzers used should be in general 0.001~1% by weight, preferably, 0.01~0.2% by weight, based on the total weight of the monomers.

The wholly aromatic polymers suitable for use with the method of this invention show a tendency of generally being substantially insoluble in solvents and accordingly they are unfit for solution processing. However, these polymers may be readily processed by the ordinary fusion method, as already described. Especially preferably wholly aromatic polymers should be soluble in pentafluorophenol to some degree.

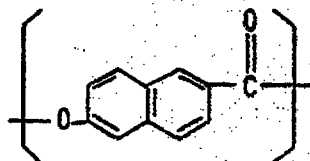
The wholly aromatic polyester preferable used according to this invention generally should have weight-average molecular weights of 2,000~200,000, preferably, 10,000~50,000 and especially preferably, 20,000~25,000. On the other hand, the preferred wholly aromatic polyester amide should generally have molecular weights of 5,000~50,000, preferably, 10,000~30,000, or 15,000~17,000, for example. Measurement of such molecular weight may be made by gel permeation chromatography and other standard measuring methods which do not involve solution formation of polymers, for example, by determining the terminal groups by way of infrared spectroscopy on compression-molded film. Alternatively, the molecular weight of the polymer may be measured, by applying the light scattering method in its pentafluorophenol solution.

The aforementioned wholly polyesters and polyester amides, when dissolved at 60°C in pentafluorophenol at a concentration of 0.1% by weight, will give intrinsic viscosities (I.V.) of at least 2.0 dl/g, e.g., 2.0~10.0 dl/g.

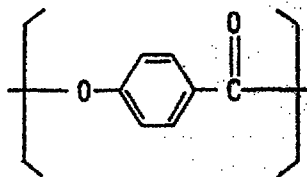
Polyesters which form the anisotropic melt phase especially preferred for use with the method of this invention should contain approx. 10 mol% or more of repetitive units containing naphthalene part such as 6-hydroxy-2-naphthoic acid, 2,6-dihydroxynaphthalene and 2,6-dicarboxynaphthalene. The preferable polyester amides contain repetitive units having the aforementioned naphthalene part and a part consisting of 4-aminophenol or 1,4-phenylenediamine. Particular examples are given hereunder:

(1) Polyesters substantially comprising the following repetitive units I and II:

I



II



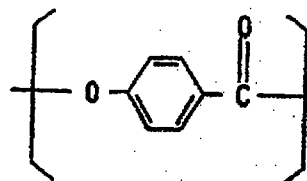
5

These polyesters contain 10~90 mol% of unit I and 10~90 mol% of unit II. Under a mode, the unit I exists up to the amount of 65~85 mol%, preferably 70~80 mol% (e.g., approx, 75 mol%). Under another mode, the unit II exists in such far small amounts in concentration as 20~30 mol%. And at least part of the hydrogen atoms bonded to the rings may be substituted, as the case may be, by substituents selected from the group consisting of alkyl groups having 1~4 carbon atoms, alkoxy groups having 1~4 carbon atoms, halogens, phenyl, substituted phenyls and their combinations.

15

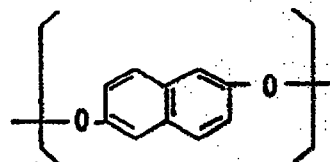
(2) Polyesters substantially comprising the following repetitive units I, II and III:

I



20

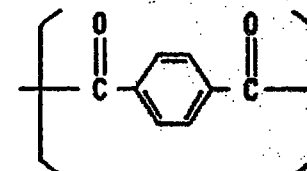
II



25

30

III



35

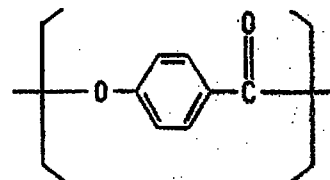
40

45

These polyesters contain 30~70 mol% of unit I. They should preferably contain 40~60 mol% of unit I, 20~30 mol% of unit II and 20~30 mol% of unit III. Further, at least part of the hydrogen atoms bonded to the rings may, as the case may be, be substituted by any substituents selected from the group consisting of alkyl groups having 1~4 carbon atoms, alkoxy groups having 1~4 carbon atoms, halogens, phenyl, substituted phenyls and their combinations.

(3) Polyesters substantially comprising the following repetitive units I, II, III and IV:

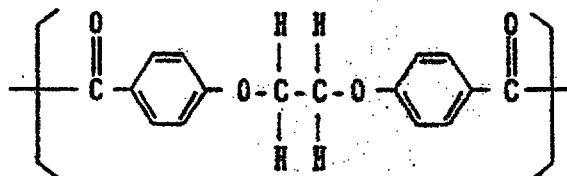
I



50

55

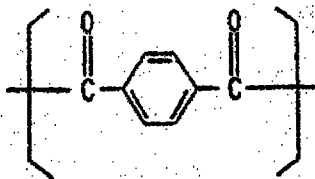
II



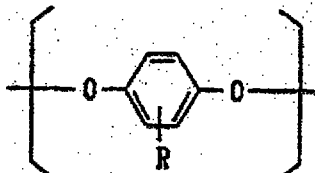
60

65

III



IV

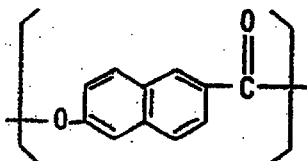


(where R represents methyl-, chloro-, bromo-group or their combinations, which are substituents for the hydrogen atoms on the benzene ring.)

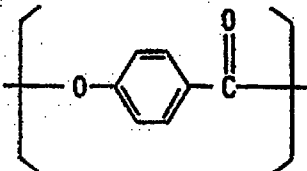
They contain 20~60 mol% of unit I, 5~18 mol% of unit II, 5~35 mol% of unit III and 20~40 mol% of unit IV. These polyesters should preferably contain, 35~45 mol% of unit I, 10~15 mol% of unit II, 15~25 mol% of unit III and 25~35 mol% of unit IV. Provided that the sum total molar concentration of units II and III is substantially equivalent to the mol concentration of unit IV. Besides, at least part of the hydrogen atoms bonded to the ring may, as the case may be, be substituted by any substituents selected from the group consisting of alkyl groups having 1~4 carbon atoms, halogens, phenyl, substituted phenyls and their combinations. These wholly aromatic polyesters, when dissolved at 60°C in pentafluorophenol at a concentration of 0.3 w/v% will generally give their intrinsic viscosities at least 2.0 dl/g, e.g., 2.0~10.0 dl/g.

(4) Polyesters substantially comprising the following repetitive units I, II, III and IV:

I



II



III Dioxyaryl unit represented by a general formula of $-(\text{O}-\text{Ar}-\text{O})-$ (where Ar represents divalent groups having at least one benzene ring).

IV Dicarboxyaryl units represented by a general formula



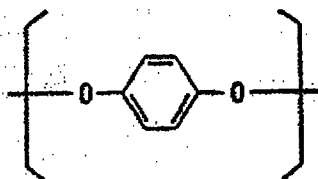
(where Ar' signifies divalent groups having at least one benzene ring).

These polyesters contain approx. 20~40 mol% of unit I, more than 10 mol% but less than 50 mol% of unit II, more than 5 mol% but less than 30 mol% of unit III and more than 5 mol% but less than 30 mol% of unit IV. They should preferably contain 20~30 mol% (e.g., approx. 25 mol%) of unit I, 25~40 mol% (e.g., approx. 35 mol%) of unit II, 15~25 mol% (e.g., approx. 20 mol%) of unit III and 15~25 mol% (e.g., approx. 20 mol%) of unit IV. Besides, at least part of the hydrogen atoms bonded to the ring may, as the case be, be substituted by substituents selected from the group consisting of alkyl groups having 1~4 carbon atoms, alkoxy groups having 1~4 carbon atoms, halogens, phenyl, substituted phenyls and their combinations.

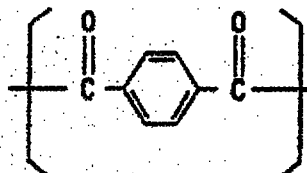
In units III and IV, the divalent bonds which connect one unit to other units on both sides thereof within the main chain of the polymer are in symmetrical arrangement on one or more benzene rings (for example, they are arranged at mutually para positions or at diagonal positions on the rings, when they exist on a

naphthalene ring). However, such symmetrical units as may be derived from resorcinol and isophthalic acid are also usable.

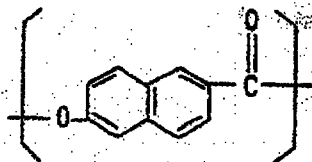
Preferably dioxyaryl unit III is:



and desirable dicarboxyaryl unit IV is:

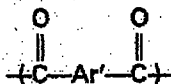


(5) Polyesters substantially comprising the following repetitive units I, II and III:



II Dioxyaryl unit represented by a general formula --O--Ar--O-- (where Ar signifies a divalent group having at least one benzene ring).

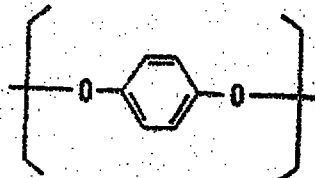
III Dicarboxyaryl unit represented by a general formula



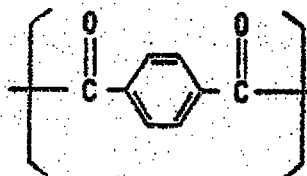
(where Ar' signifies a divalent group having at least one benzene ring).

These polyesters contain 10~90 mol% of unit I, 5~45% of unit II, and 5~45 mol% of unit III. They should preferably contain 10~40 mol% of unit I, 10~40 mol% of unit I, 10~40 mol% of unit II and 10~40 mol% of unit III. Further preferably, such polyesters should contain 60~80 mol% of unit I, 10~20 mol% of unit II and 10~20 mol% of unit III. Besides, at least part of hydrogen atoms bonded to the ring(s) may be substituted, as appropriate, by substituents selected from alkyl groups having 1~4 carbon atoms, alkoxy groups having 1~4 carbon atoms, halogens, phenyl, substituted phenyls and their combinations.

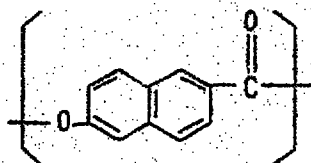
Preferably dioxyaryl unit II is:



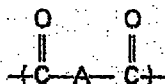
and desirable decarboxyaryl unit III is:



(6) Polyester amides substantially comprising following repetitive units I, II, III and IV:



II General formula



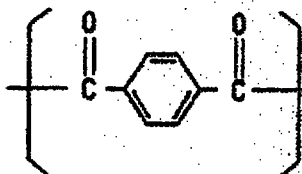
(where Ar' signifies a divalent group having at least one benzene ring or divalent trans-cyclohexane group).

II General formula $\left[\text{Y} - \text{Ar} - \text{Z} \right]$ (where Ar indicates a divalent group having at least 1 benzene ring, Y gives O, NH or NR, and Z stands for NH or Nr, respectively; and R designates an alkyl group having 1~6 carbon atoms or aryl group).

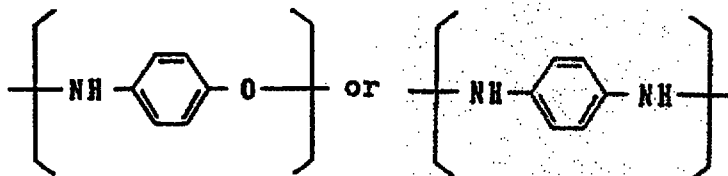
IV General formula $\left[\text{O} - \text{Ar}' - \text{S} \right]$ (where Ar' denotes a divalent group having at least 1 benzene ring).

These polyesters contain 10~90 mol% of unit I, 5~45 mol% of unit II, 5~45 mol% of unit III, and 0~40 mol% of unit IV. Besides, at least part of the hydrogen atoms bonded to the rings may be substituted by substituents selected from among a group consisting of alkyl groups having 1~4 carbon atoms, alkoxyl groups, halogens, phenyl, substituted phenyls and their combinations.

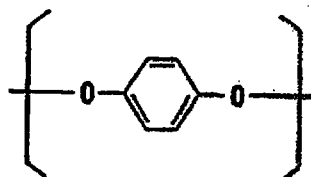
Preferable dicarboxyaryl II unit is:



and preferable unit III should be:



and further, desirable dioxyaryl unit IV should be:



Furthermore, polymers forming the anisotropic melt phase of this invention may include polymers in which part of one high molecular chain is composed of polymer segments forming the anisotropic melt phase, while the remaining part is composed of segments of thermoplastic resins which do not form the anisotropic melt phase.

Mentioned as the fibers used according to this invention are the following:

Metal fibers used include fibers of mild steel, stainless steel, copper and its alloys, bronze, aluminum and its alloys and lead, while carbon fibers used are PAN base fibers made from polyacrylonitrile as the material and pitch base fibers.

Available as usable glass fibers are, besides normal glass fiber, glass fibers coated with such metals as nickel and copper, silane fiber, aluminosilicate glass fiber, hollow glass fiber and non-hollow fiber; inorganic fibers include various fibers such as of rockwool, zirconia, alumina silica, potassium titanate,

barium titanate, silicon carbide, alumina, silica and blast furnace slag; and whiskers used are silicon nitride whisker, silicon oxide nitride whisker, basic magnesium sulfate whisker, barium titanate whisker, silicon carbide whisker and boron whisker.

Available as synthetic fibers are Aramid which is a fully aromatic polyamide and Kynol which is a phenolic resin fiber.

Ore fibers used include asbestos, wollastonite, etc., while natural fibers available are cellulose fibers and flax yarns.

Preferable fibers are carbon fibers, glass fibers, inorganic fibers and synthetic fibers, particularly favorable being PAN and pitch base carbon fibers and in addition and potassium titanate.

The fibers abovementioned may be used singly or in combination of more than two types and the surface treatment of fibers normally used for their mixing with thermoplastic resins will provide preferable results. For the surface treatment, such approaches may be taken as used of coupling agents of silanes, titanates, etc., coating with low and high molecular weight organic compounds and oxidation treatment, etc.

These fibers are utilized in amounts of from 2 to 70% by weight of the total weight including the weight of the resin, values of 10 to 50 percent by weight being preferred.

The fiber length in the fibrous material is desirably less than 12 mm, so as to facilitate kneading.

As desired, the lubricants will include solid lubricant like molybdenum disulfide and graphite, which are available as plate crystal, polymer lubricants including fluoropolymers such as polytetrafluoroethylene, tetrafluoroethylene-hexafluoropropylene copolymer, polytrichlorofluoroethylene and tetrafluoroethylene-perfluoroalkyl vinyl ether copolymer, mineral oils and silicones, and oil lubricants which are low molecular organic compounds, of which particularly preferred are molybdenum disulfide, graphite and polytetrafluoroethylene.

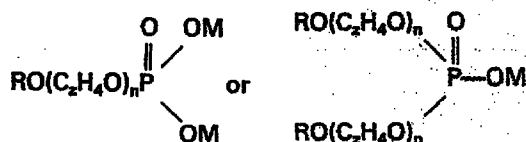
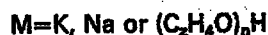
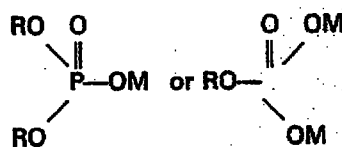
These lubricants are used in 1~50% by weight of the total weight of the product including the weight of the resin, from 2 to 30% by weight being preferable.

The antistatic agent which is used as desired is effective for protection against fine injury on gears from dust deposited from air. This end may be served either by applying it on the surface or by incorporating into the resin composition, the latter being preferred, taking account of workability.

The antistatic agents may be classified into cationic, anionic, nonionic and amphoteric types.

Mentioned as antistatic agents of anionic type are:

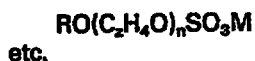
Phosphoric acid ester type:



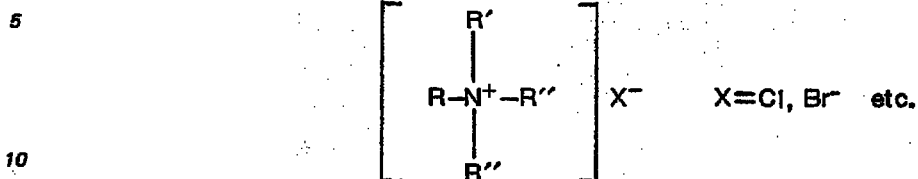
Sulfuric acid type:



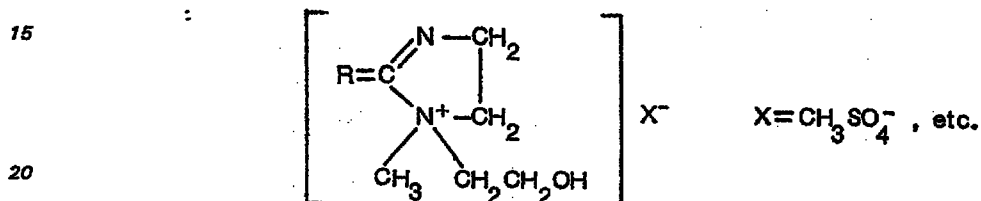
Sulfuric acid ester type:



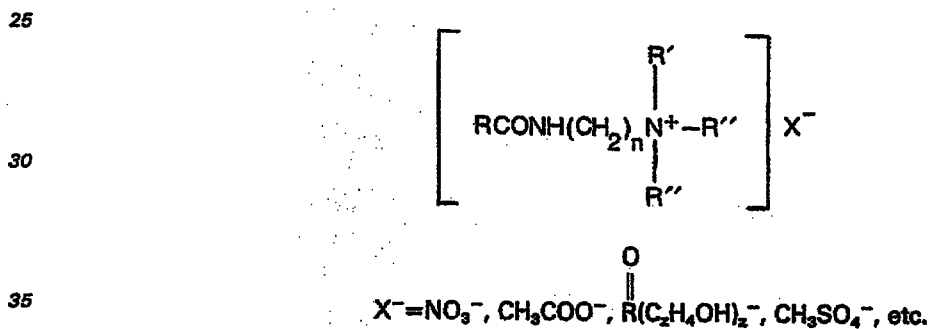
Mentioned as cationic type are:
Quaternary ammonium salts:



Imidazoline type:



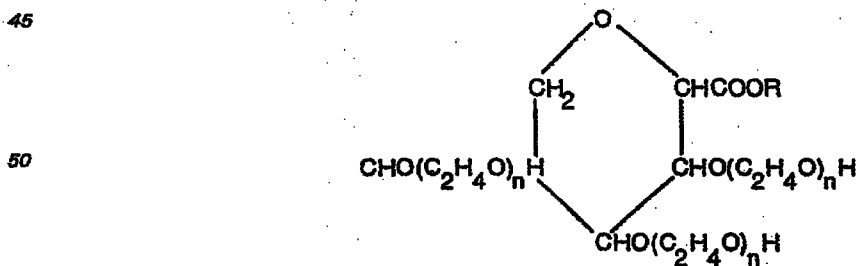
Amidoamine type:



Mentioned as nonionic type are:
Alkyl-ether, -ester type:



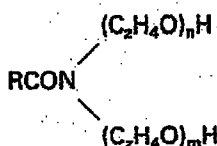
Polyoxyethylene sorbitan ester type:



Alkyl-amine type:



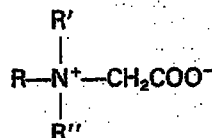
Alkyl-amide type:



etc.

Mentioned as amphoteric type are:

Betain type:



Alanine type:



These antistatic agents are used in the similar manner as ordinary thermoplastic resins, but in view of thermal stability, etc., the anionic, nonionic and amphoteric are desirable, of which the nonionic is especially preferred.

The antistatic agent is used in 0.1 to 5% by weight of the total weight of the gear including the weight of the resin.

Ordinary methods for prevention of troubles resulting from static, besides the use of antistatic agents, may be used. They include application of conductive coating and mixing-in of conductive fillers, the latter being preferable. Usable as the conductive fillers are such metal powders as powder of iron, bronze, copper, aluminum and nickel, and their flakes; carbon powder like powder of carbon black and acetylene black and carbon microballoon; glass flakes coated with such metals as nickel, silver and copper, and such metal oxides of iron or tin, of which carbon powder is especially desirable.

These conductive fillers are used in 0.5 to 50% by weight of the total weight of the product including the weight of the resin, etc., or preferably 2 to 30% by weight.

The polymer compositions used according to this invention which form the anisotropic melt phase may contain one or more of ① polymers which form other anisotropic melt phase, ② thermoplastic resins which do not form the anisotropic melt phase, ③ thermosetting resins, ④ lower molecular organic compounds and ⑤ inorganic materials. In these compositions, the polymers which form the anisotropic melt phase and the remaining part are allowed to be either thermodynamically compatible or not.

The aforementioned ② thermoplastic resins include: e.g., polyethylene, polypropylene, polybutylene, polybutadiene, polyisoprene, polyvinyl acetate, polyvinyl chloride, polyvinylidene chloride, polystyrene, acrylic resins, ABS resin, AS resin, Bs resin, polyurethane, silicone resins, polyacetal, polycarbonate, polyethylene terephthalate, polybutylene terephthalate, aromatic polyesters, polyamides, polyacrylonitrile, polyvinyl alcohol, polyvinyl ether, polyether imide, polyamide imide, polyether ether imide, polyether ether ketones, polyether sulfones, polysulfones, polyphenylene sulfides and polyphenylene oxides.

And the aforementioned ③ thermosetting resins include: e.g., phenol resins, epoxy resins, melamine resins, urea resins, unsaturated polyester resins and alkyl resins.

Then the aforementioned ④ low molecular weight organic compounds include: e.g., materials which are added to common thermoplastic resins and thermosetting resins, that is, molecular weight organic compounds for use as plasticizers, stabilizers such as antioxidants and ultraviolet ray absorbers; flame retardants, coloring agents such as dyes, pigments, etc., foaming agents, further, bridging agents such as divinyl base compounds, peroxides, vulcanizers; and lubricants for improvement in fluidity and mold release properties.

Further the aforementioned ⑤ inorganic compounds include materials which are added to common thermoplastic resins and thermosetting resins, such as kaolin, baked clay, talc, Canada mica, mica, vermiculite, calcium silicate, feldspar powder, acid clay, pagodite clay, sericite, sillimanite, bentonite, glass flake, glass powder, glass beads, slate powder and silicates like silane; carbonates such as calcium carbonates, white lead, barium carbonate, magnesium carbonate and dolomite; sulfates such as baryta powder, blank fixe, precipitate calcium sulfate and calcined plaster; hydroxides like hydrated alumina; oxides like alumina, antimony oxide, magnesia, titanium oxide, zinc white, amorphous silica, flint quartz, silica sand, white carbon and diatomaceous earth.

Besides organic compounds, woody powders like wood flour, coconut flour, nut flour and pulp powder, may be added.

Suitable methods, of molding gears according to this invention include the molding methods used with ordinary thermoplastic resins for example injection molding or extrusion molding press-forming, stamping or cutting.

The characteristics of the gears obtained are very much influenced by the position of the gate at the time of molding. Thus when molding a gear using a resin which shows anisotropy when molten, a product having high strength at the root of the teeth and small coefficient of linear expansion is obtained, if the gate is positioned at the axial center. This is a notable characteristic peculiar only to resins which show anisotropy when molten; this property avails these resin compositions in achieving the out-standing improvement in the characteristics of gears. The word axial center implies that the gate should be located as near to the axial center as its design permits at the time of setting up the mold. Thus it may be placed in the neighborhood, if, in fact, the gate can not be positioned at the axial center.

10 [Effect of the Invention]

As hereinabove described, the resin compositions of this invention are most suitable as compounds for gears having high mechanical strengths, high resistance to heat and thermal deformation and showing very small shrinkage when being molded, and the molded gears permit miniaturization and expansion of their usable temperature range. And the gears obtained with these resin compounds for gears have high teeth root strength to provide high load bearing capacity and give very small molding shrinkage, so that only small errors are involved with these gears in single pitch, neighboring pitch, accumulating pitch, normal pitch, etc., and therefore, their use is effective not merely as ordinary spur gears or cylindrical gears but as such gears as helical gears, double helical gears, straight bevel gears, spiral bevel gears, zero bevel gears, crossed helical gears, hypoid gears, worm gears and multithread worm gears, etc., in which their intermeshing pitch circle is not on the same plane as the direction in which the force is transmitted or their pitch helix is not parallel to the axial direction of the cylinder.

These gears are usable in such varied fields as electronic, electric parts, automobile parts and sundries, etc. Especially, they are suitable for uses in electronic and electric fields such as electronic copying machines, etc., which are subjected to strict environmental using conditions, or in automobile field like wiper gears.

[Preferred Embodiments]

The present invention will become more apparent from the following description taken in connection with its preferred embodiments:

30

Example 1

After extrusion and kneading of 80 parts of resin A and 20 parts of PAN base carbon fiber, a test piece was formed, using Nissei injection molder FS-75N II. The molding conditions were such that the temperature of the cylinder part was held at 290°C, the nozzle at 300°C, and the mold 80°C, and the injection pressure was set at 29.4 MPa (300 kg/cm²), with the test piece being in the shape of a spur gear having a pitch circle diameter of 60 mm and a module of 1.0 mm. The test piece thus molded was left standing for 24 hours in a thermostatic chamber held at 23°C with 50% humidity and measurements were taken respectively of teeth root strength, coefficient of linear expansion, specific wear rate and thermal deformation temperature. The teeth root strength was measured on a torsion tester manufactured by Shimazu by applying torque on the spur gear side, with the worm of the worm gear fixed. The coefficient of linear expansion was calculated from the readings taken of the teeth tip diameter as the temperature was varied between 80°C and 150°C. The specific wear was measured, using the Suzuki's wear tester. The measurement of the thermal deformation temperature was taken as usual 1.82 MPa or (18.6 kgf/cm²) with a test piece prepared under the similar conditions.

50

55

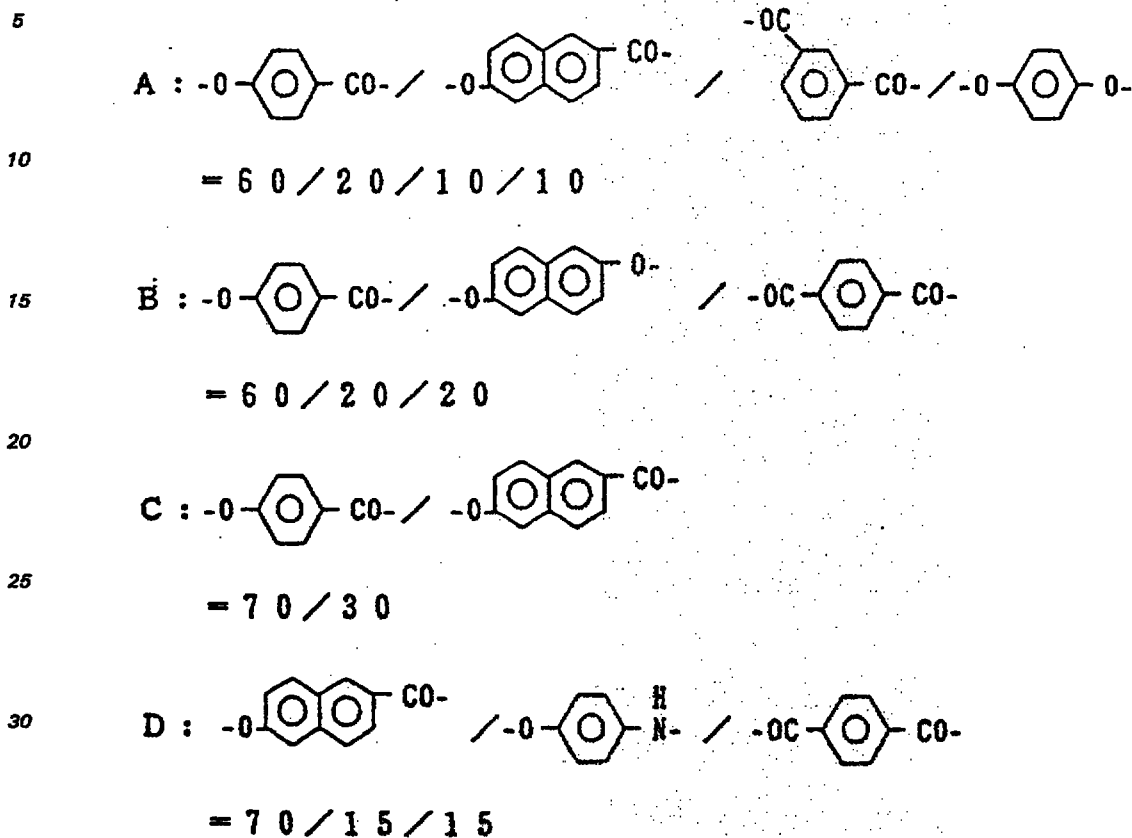
60

65

EP 0 206 600 B1

Subsequently various measurements of Examples from 2 to 12 and Comparative Examples from 1 through 13 were similarly made with test pieces respectively prepared.

The polymers A, B, C and D which form the anisotropic fused phase have the following structural units:



Definite manufacturing methods of the afore-mentioned resins A, B, C and D are described hereunder:

[Resin A]

1081 parts by weight of 4-acetoxybenzoic acid, 460 parts by weight of 6-acetoxy-2-naphthoic acid, 166 parts by weight of isophthalic acid and 194 parts by weight of 1,4-diacetoxybenzene were charged in a reaction vessel equipped with a stirrer, nitrogen inlet tube and a discharge tube and this mixture was heated to 260°C in a nitrogen current. The content of the reaction vessel was, then, vigorously stirred for a time period of 2.5 hours at 260°C and, then, 3 hours at 280°C while letting acetic acid flow out of the reaction vessel. Then the temperature was further raised to 320°C and after stopping the introduction of nitrogen, the pressure inside the reaction vessel was reduced, the pressure being dropped to 13.3 Pa (0.1 mmHg) 15 minutes later, and its content was stirred at this temperature and pressure for 1 hour.

The polymer thus obtained was found to be at a concentration of 0.1% by weight and have an intrinsic viscosity of 5.0, as measured in pentafluorophenol at 60°C.

50 [Resin B]

1081 parts by weight of 4-acetoxybenzoic acid, 489 parts by weight of 2,6-diacetoxynaphthalene and 332 parts by weight of terephthalic acid were charged in a reaction vessel equipped with a stirrer, nitrogen inlet tube and discharge tube and this mixture was heated to 250°C in a nitrogen current. It was vigorously stirred for 2 hours at 250°C and, then, for 2.5 hours at 280°C, while letting acetic acid flow out of the reaction chamber. Then the temperature was further raised to 320°C and after stopping the introduction of nitrogen, the pressure inside the reaction vessel was gradually reduced, the pressure being dropped to 26.6 Pa (0.2 mmHg) 30 minutes later and its content was stirred for 1.5 hours at this temperature and pressure.

The polymer thus obtained was found to be at a concentration of 0.1% by weight and had an intrinsic viscosity of 2.5, as measured in pentafluorophenol at 60°C.

60 [Resin C]

1261 parts by weight of 4-acetoxybenzoic acid and 691 parts by weight of 6-acetoxy-2-naphthoic acid were charged into a reaction vessel equipped with a stirrer, nitrogen inlet tube and discharge tube and this mixture was heated to 250°C under a nitrogen current. It was vigorously stirred for 3 hours at 250°C and, then, for 2 hours at 280°C, while letting acetic acid flow out of the reaction vessel. Then its temperature was

raised to 320°C and after stopping the introduction of nitrogen, the pressure inside the reaction vessel was gradually reduced, thus the pressure being dropped to 13.3 Pa (0.1 mmHg) 20 minutes later. It was, then, stirred for 1 hour at this temperature and pressure.

The polymer thus obtained was found to be at a concentration of 0.1% by weight and have an intrinsic viscosity of 5.4, as measured in pentafluorophenol.

[Resin D]

1612 parts by weight of 6-acetoxy-2-naphthoic acid, 290 parts by weight of 4-acetoxyacetanilide, 249 parts by weight of terephthalic acid and 0.4 parts by weight of sodium acetate were charged into a reaction vessel equipped with a stirrer, nitrogen inlet tube and discharge tube and this mixture was heated to 250°C in a nitrogen current. Its content was vigorously stirred for 1 hour at 250°C and, then, for 3 hours at 300°C. Then its temperature was further raised to 340°C and after stopping the introduction of nitrogen, the pressure inside the reaction vessel was reduced, thus the temperature being dropped to 26.6 Pa (0.2 mmHg) 30 minutes later. It was, then, stirred for 30 minutes at this temperature and pressure.

The polymer thus obtained was found to be at a concentration of 0.1% by weight and have an intrinsic viscosity of 3.9, as measured in pentafluorophenol.

It should be noted that the fibers, lubricants and antistatic agents, etc used are as follows:

Carbon fibers;	
20 PAN base:	made by Toho Besuron K. K. C6—N
Pitch base:	made by Kureha Kagaku K. K., C—106S
Glass fiber;	made by Asahi Fiber Glass K. K., 847
Tismo;	made by Otsuka Kagaku Yakuhin K. K., Potassium titanate
Molybdenum disulfide;	made by Nihon Moribuden K. K., Powder
25 Wollastonite;	made by Interpace Corp.
Graphite;	made by Superior Graphite Co.
PTFE;	made by Daikin Kogyo K. K., Fluon L169
Antistatic agent;	made by Kao Sekken K. K., Electrostripper EA
POM;	made by Polyplastics, Duracon M90
30 PBT;	made by Polyplastics, Duraneck 2000
Nylon;	made by Polyplastics, 66 Nylon

In Comparative Example 7, the product was bone-dried by annealing at 190°C for 1 hour and after being immersed in hot water at 95°C for 5 hours, showed a water absorbing capacity of 1.3% by weight. This was used as the test piece.

The results of Tables 1 through 4 clearly indicate that the gear compositions of this invention are significantly superior to other compositions in teeth root strength, coefficient of linear expansions, specific wear as well as in thermal deformation temperature.

40 Brief Description of the Drawings:

Fig. 1 is a sketch showing the position of the center gate, and

Fig. 2 is a sketch showing the positions of the 4 point gates.

Table 5 shows the effect on the composition of the use of antistatic agent. The test piece was continuously moved by a work gear for 8 hours in a room having only small dust which was controlled to constant temperature and humidity and, then, after leaving it for 2 hours, its teeth root strength was measured in the similar manner.

Tables 6 and 7 indicate the effect of gate position. In these tables also, "center gate" identifies the gate being positioned at the center g, as shown in Fig. 1, and "4 point gates" signifies gates being positioned at the four points a, b, c and d.

TABLE 1
Reinforcing Effects of Fibers

Example No.	Resin	Fiber	Teeth root strength kg·cm	Coefficient of linear expansion cm/cm/°C	Specific wear mm ³ /kg·km	Thermal deformation temperature °C
Example 1	A(80)	CF(20)	(kg·mm ÷ 10)	(mm/mm/°C)		
Comp. Example 1	A(100)		680	2.2×10^{-5}	0.9×10^{-2}	220
Example 1	C(80)	CF(20)	410	2.7×10^{-5}	62.4×10^{-2}	175
Comp. Example 2	C(100)		714	1.8×10^{-5}	0.3×10^{-2}	230
			423	2.5×10^{-5}	50.5×10^{-2}	180

Notes: The numbers in () designates parts by weight.

GF: Glass fiber

CF: Carbon fiber (PAN base)

CpF: Carbon fiber (pitch base)

The same designations apply in the following tables.

TABLE 2
Comparisons with Other Resins

Example No.	Resin	Fiber	State	Teeth root strength kg·cm (kg·mm ÷ 10)	Coefficient of linear expansion cm/cm/°C (mm/mm/°C)	Specific wear mm ³ /kg·km	Thermal deformation temperature °C
Example 1	A(80)	CF(20)		680	2.2×10^{-5}	0.9×10^{-2}	220
Example 2	B(80)	"		705	2.1×10^{-5}	0.5×10^{-2}	230
Example 3	C(80)	"		714	1.8×10^{-5}	0.3×10^{-2}	230
Example 4	D(80)	"		729	0.7×10^{-5}	0.3×10^{-2}	235
Comp. Example 5	POM(80)	"		456	8.5×10^{-5}	3.6×10^{-2}	160
Comp. Example 6	PBT(80)	"		374	7.2×10^{-5}	15.2×10^{-2}	210
Comp. Example 7	Nylon(80)	"	Bone dried state	533	4.8×10^{-5}	4.1×10^{-2}	220
Comp. Example 8	Nylon(80)	"	Wet state	285	17×10^{-5}	8.9×10^{-2}	190

TABLE 3
Comparisons in Terms of Fiber and Resin

Example No.	Resin	Fiber	Teeth root strength kg·cm (kg·mm ÷ 10)	Coefficient of linear expansion cm/cm°C (mm/mm°C)	Specific wear mm ³ /kg·km	Thermal deformation temperature °C
Example 2	C(80)	CF(20)	714	1.8×10^{-5}	0.3×10^{-2}	230
Example 5	C(80)	CpF(20)	672	1.9×10^{-5}	0.4×10^{-2}	230
Comp. Example 9	POM(80)	CpF(20)	424	8.9×10^{-5}	3.8×10^{-2}	160
Example 6	C(80)	CG(20)	682	1.9×10^{-5}	62.5×10^{-2}	230
Comp. Example 10	POM(80)	GF(20)	433	9.2×10^{-5}	79.1×10^{-2}	160
Example 7	C(80)	Tismo(20)	529	2.1×10^{-5}	10.0×10^{-2}	210
Comp. Example 11	POM(80)	Tismo(20)	411	9.4×10^{-5}	12.5×10^{-2}	160
Example 8	C(80)	Wollastonite(20)	452	2.5×10^{-5}	10.2×10^{-2}	190
Comp. Example 12	POM(80)	Wollastonite(20)	324	9.4×10^{-5}	12.5×10^{-2}	115

TABLE 4
Comparisons in Terms of Lubricant

Example No.	Resin	Fiber	Lubricant	Teeth root strength kg·cm	Coefficient of linear expansion cm/cm/°C	Specific wear mm ³ /kg·km
Example 5	C(80)	CpF(20)		672	1.9×10^{-5}	0.4×10^{-2}
Example 9	C(80)	"	Graphite(5)	670	2.0×10^{-5}	0.2×10^{-2}
Comp. Example 13	POM(80)	"		421	9.0×10^{-5}	10×10^{-2}
Example 10	C(80)	"	MoS ₂ (5)	671	2.0×10^{-5}	0.3×10^{-2}
Example 11	C(80)	"	PTFE(5)	670	2.1×10^{-5}	0.1×10^{-2}

TABLE 5
Effect of Antistatic Agent

Example No.	Resin	Fiber	Antistatic agent	Teeth root strength kg·cm	
				Initial value	After 8 hr operation
Example 2	C(80)	CF(20)	none	714	699
Example 2	C(80)	CF(20)	added (0.4)	714	710

TABLE 6
Gate Position at the Time of Molding

Example No.	Resin	Fiber	Gate position	Teeth root strength kg·cm	Coefficient of linear expansion cm/cm/°C
Example 2	C(80)	CF(20)	Center gate	714	1.8×10^{-5}
Comp. Example 14	C(80)	"	4 Point gates	549	3.7×10^{-5}
Comp. Example 15	C(80)	"	1 Point gate Only one at a	487	4.9×10^{-5}
Comp. Example 16	C(80)	"	2 Point gates Two points at a and c	525	4.2×10^{-5}
Comp. Example 17	POM(80)	"	4 Point gates	452	8.5×10^{-5}
Comp. Example 5	POM(80)	"	Center gate	456	8.5×10^{-5}
Comp. Example 18	PBT(80)	"	4 Point gates	373	7.2×10^{-5}
Comp. Example 6	PBT(80)	"	Center gate	374	7.2×10^{-5}

TABLE 7
Effect of the Type of Resin used in Gate Position

Example No.	Resin	Gate position	Teeth root strength kg · cm	Coefficient of linear expansion cm/cm/°C
			(kg · mm ÷ 10)	(mm/mm/°C)
Example 13	A(100)	Center gate	410	2.3×10^{-5}
Comp. Example 19	A(100)	4 Point gates	302	3.9×10^{-5}
Example 14	B(100)	Center gate	418	2.0×10^{-5}
Comp. Example 20	B(100)	4 Point gates	307	3.9×10^{-5}
Example 15	C(100)	Center gate	423	0.9×10^{-5}
Comp. Example 21	C(100)	4 Point gates	300	4.1×10^{-5}
Example 16	D(100)	Center gate	457	0.6×10^{-5}
Comp. Example 22	D(100)	4 Point gates	319	4.4×10^{-5}
Comp. Example 23	POM(100)	Center gate	276	10×10^{-5}
Comp. Example 24	POM(100)	4 Point gates	276	10×10^{-5}
Comp. Example 25	PBT(100)	Center gate	243	10×10^{-5}
Comp. Example 26	PBT(100)	4 Point gates	242	10×10^{-5}

Claims

1. A method for molding a gear wheel by introducing a resin composition into a mold, characterized in that the composition comprises (a) 30 to 98% by weight of a melt-processable polymer which is capable of forming an anisotropic phase in the molten state and (b) 2 to 70% by weight of a fibrous material, and in that the composition is introduced into the mold through a gate located at or near to the axial center thereof.

2. A method as claimed in claim 1, characterized in that the polymer is a thermotropic liquid crystal polymer.

3. A method as claimed in any preceding claim, characterized in that the fibrous material is selected from one or more of metal fibers, carbon fibers, glass fibers, inorganic fibers, synthetic fibers and mineral fibers.

4. A method as claimed in any preceding claim, characterized in that the fibrous material is surface-treated prior to its addition into the composition.

5. A method as claimed in any preceding claim, characterized in that the proportion of fibrous material in the composition is 10 to 50% by weight.

6. A method as claimed in any preceding claim, characterized in that the fibrous material has a fibre length of less than 12 mm.

7. A method as claimed in any preceding claim, characterized in that the composition additionally contains 1 to 50% by weight of a lubricant.

8. A method as claimed in claim 7, characterized in that the lubricant content in the composition is 2 to 30% by weight.

**EP 0 206 600 B1**

TABLE 7
Effect of the Type of Resin used in Gate Position

Example No.	Resin	Gate position	Teeth root strength kg · cm	Coefficient of linear expansion cm/cm/°C
			(kg · mm ÷ 10)	(mm/mm/°C)
Example 13	A(100)	Center gate	410	2.3×10^{-5}
Comp. Example 19	A(100)	4 Point gates	302	3.9×10^{-5}
Example 14	B(100)	Center gate	418	2.0×10^{-5}
Comp. Example 20	B(100)	4 Point gates	307	3.9×10^{-5}
Example 15	C(100)	Center gate	423	0.9×10^{-5}
Comp. Example 21	C(100)	4 Point gates	300	4.1×10^{-5}
Example 16	D(100)	Center gate	457	0.6×10^{-5}
Comp. Example 22	D(100)	4 Point gates	319	4.4×10^{-5}
Comp. Example 23	POM(100)	Center gate	276	10×10^{-5}
Comp. Example 24	POM(100)	4 Point gates	276	10×10^{-5}
Comp. Example 25	PBT(100)	Center gate	243	10×10^{-5}
Comp. Example 26	PBT(100)	4 Point gates	242	10×10^{-5}

Claims

1. A method for molding a gear wheel by introducing a resin composition into a mold, characterized in that the composition comprises (a) 30 to 98% by weight of a melt-processable polymer which is capable of forming an anisotropic phase in the molten state and (b) 2 to 70% by weight of a fibrous material, and in that the composition is introduced into the mold through a gate located at or near to the axial center thereof.

2. A method as claimed in claim 1, characterized in that the polymer is a thermotropic liquid crystal polymer.

3. A method as claimed in any preceding claim, characterized in that the fibrous material is selected from one or more of metal fibers, carbon fibers, glass fibers, inorganic fibers, synthetic fibers and mineral fibers.

4. A method as claimed in any preceding claim, characterized in that the fibrous material is surface-treated prior to its addition into the composition.

5. A method as claimed in any preceding claim, characterized in that the proportion of fibrous material in the composition is 10 to 50% by weight.

6. A method as claimed in any preceding claim, characterized in that the fibrous material has a fibre length of less than 12 mm.

7. A method as claimed in any preceding claim, characterized in that the composition additionally contains 1 to 50% by weight of a lubricant.

8. A method as claimed in claim 7, characterized in that the lubricant content in the composition is 2 to 30% by weight.



9. A method as claimed in any preceding claim, characterized in that the composition additionally contains 0.1 to 5% by weight of an antistatic agent.

10. A method as claimed in any preceding claim, characterized in that the composition additionally contains 0.5 to 50% by weight of a conductive filler.

Patentansprüche

1. Verfahren zum Formpressen eines Zahnrads durch Einführen einer Harz-Zusammensetzung in eine Form, dadurch gekennzeichnet, daß die Zusammensetzung

(a) 30 bis 98 Gew.-% eines in der Schmelze verarbeitbaren Polymers, das zur Bildung einer anisotropen Phase im geschmolzenen Zustand befähigt ist, und

(b) 2 bis 70 Gew.-% eines faserförmigen Materials umfaßt und daß die Zusammensetzung in die Form durch eine Anschnittöffnung eingeführt wird, die im axialen Zentrum oder in der Nähe des axialen Zentrums der Form angeordnet ist.

2. Verfahren nach Anspruch 1, dadurch gekennzeichnet, daß das Polymer ein thermotropes Flüssigkristall-Polymer ist.

3. Verfahren nach irgendeinem vorhergehenden Anspruch, dadurch gekennzeichnet, daß das faserförmige Material aus einem oder mehreren der Materialien Metallfasern, Kohlenstofffasern, Glasfasern, anorganischen Fasern, synthetischen Fasern und Mineralfasern ausgewählt ist.

4. Verfahren nach irgendeinem vorhergehenden Anspruch, dadurch gekennzeichnet, daß das faserförmige Material vor seinem Hinzufügen in die Zusammensetzung oberflächenbehandelt wird.

5. Verfahren nach irgendeinem vorhergehenden Anspruch, dadurch gekennzeichnet, daß der Anteil des faserförmigen Materials in der Zusammensetzung 10 bis 50 Gew.-% beträgt.

6. Verfahren nach irgendeinem vorhergehenden Anspruch, dadurch gekennzeichnet, daß das faserförmige Material eine Faser-Länge von weniger als 12 mm hat.

7. Verfahren nach irgendeinem vorhergehenden Anspruch, dadurch gekennzeichnet, daß die Zusammensetzung zusätzlich 1 bis 50 Gew.-% eines Gleitmittels enthält.

8. Verfahren nach Anspruch 7, dadurch gekennzeichnet, daß der Gleitmittel-Gehalt in der Zusammensetzung 2 bis 30 Gew.-% beträgt.

9. Verfahren nach irgendeinem vorhergehenden Anspruch, dadurch gekennzeichnet, daß die Zusammensetzung zusätzlich 0,1 bis 5 Gew.-% eines antistatischen Mittels enthält.

10. Verfahren nach irgendeinem vorhergehenden Anspruch, dadurch gekennzeichnet, daß die Zusammensetzung zusätzlich 0,5 bis 50 Gew.-% eines leitfähigen Füllstoffs enthält.

Revendications

1. Un procédé pour mouler une roue d'engrenage en introduisant une composition de résine dans un moule, caractérisé en ce que la composition comprend (a) 30 à 98% en poids d'un polymère façonnable à l'état fondu qui est capable de former une phase anisotrope à l'état fondu et (b) 2 à 70% en poids d'une matière fibreuse, et en ce que la composition est introduite dans le moule par une entrée située au niveau ou près de son centre axial.

2. Un procédé tel que revendiqué dans la revendication 1, caractérisé en ce que le polymère est un polymère thermotrope à cristaux liquides.

3. Un procédé tel que revendiqué dans l'une quelconque des revendications précédentes, caractérisé en ce que la matière fibreuse est choisie parmi une ou plusieurs de fibres métalliques, fibres de carbone, fibres de verre, fibres inorganiques, fibres synthétiques et fibres minérales.

4. Un procédé tel que revendiqué dans l'une quelconque des revendications précédentes, caractérisé en ce que la matière fibreuse est traitée en surface avant son addition à la composition.

5. Un procédé tel que revendiqué dans l'une quelconque des revendications précédentes, caractérisé en ce que la proportion de matière fibreuse dans la composition est de 10 à 50% en poids.

6. Un procédé tel que revendiqué dans l'une quelconque des revendications précédentes, caractérisé en ce que la longueur des fibres de la matière fibreuse est inférieure à 12 mm.

7. Un procédé tel que revendiqué dans l'une quelconque des revendications précédentes, caractérisé en ce que la composition contient, de plus, 1 à 50% en poids d'un lubrifiant.

8. Un procédé tel que revendiqué dans la revendication 7, caractérisé en ce que la proportion de lubrifiant dans la composition est de 2 à 30% en poids.

9. Un procédé tel que revendiqué dans l'une quelconque des revendications précédentes, caractérisé en ce que la composition contient, de plus, 0,1 à 5% en poids d'un agent antistatique.

10. Un procédé tel que revendiqué dans l'une quelconque des revendications précédentes, caractérisé en ce que la composition contient, de plus, 0,5 à 50% en poids d'une charge conductrice.