

PUMP ✓

The invention concerns a centrifugal-or half axial pump for pumping of fluids, mainly sewage water.

In literature there are lot of types of pumps and pump impellers for this purpose described, all however having certain disadvantages. Above all this concerns problems with clogging and low efficiency.

Sewage water contains a lot of different types of pollutants, the amount and structure of which depend on the season and type of area from which the water emanates. In cities plastic material, hygiene articles, textile etc are common, while industrial areas may produce wearing particles. Experience shows that the worst problems are rags and the like which stick to the leading edges of the vanes and become wound around the impeller hub. Such incidents cause frequent service intervals and a reduced efficiency.

In agriculture and pulp industry different kinds of special pumps are used, which should manage straw, grass, leaves and other types of organic material. For this purpose the leading edges of the vanes are swept backwards in order to cause the pollutants to be fed outwards to the periphery instead of getting stuck to the edges. Different types of disintegration means are often used for cutting the material and making the flow more easy. Examples are shown in SE-435 952, SE-375 831 and US- 4 347 035.

As pollutants in sewage water are of other types more difficult to master and as the operation times for sewage water pumps normally are much longer, the above mentioned special pumps do not fullfil the requirements when pumping sewage water, neither from a reliability nor from an efficiency point of view.

A sewage water pump quite often operates up to 12 hours a day which means that the energy consumption depends a lot on the total efficiency of the pump.

Tests have proven that it is possible to improve efficiency by up to 50 % for a sewage pump according to the invention as compared with known sewage pumps. As the life cycle cost for an electrically driven pump normally is totally dominated by the energy cost (c:a 80 %), it is evident that such a dramatic increase will be extremely important.

In literature the designs of the pump impellers are described very generally, especially as regards the sweep of the leading edges. An unambiguous definition of said sweep does not exist.

Tests have shown that the design of the sweep angle distribution on the leading edges is very important in order to obtain the necessary self cleaning ability of the pump impeller. The nature of the pollutants also calls for different sweep angles in order to provide a good function.

Literature does not give any information about what is needed in order to obtain a gliding, transport, of pollutants outwards in a radial direction along the leading edges of the vanes. What is mentioned is in general that the edges shall be obtuse-angled, swept backwards etc. See SE-435 952.

When smaller pollutantans such as grass and other organic material are pumped, relatively small angles may be sufficient in order to obtain the radial transport and also to disintegrate the pollutants in the slot between pump impeller and the surrounding housing. In practice disintigration is obtained by the particles being cut through contact with the impeller and the housing when the former rotates having a periphery velocity of 10 to 25 m/s. This cutting process is improved by the surfaces being provided with cutting devices, slots or the like.

Different sorts of notches and cutting means are described in SE-435 952 and SE-375 831. They have all in common that the vane is located behind a shoulder. This means a considerable loss of efficiency as compared with an even contour which is used in high efficiency pumps for clean water.

In SE-435 952 an embodiment is shown where an axial aperture is located behind a shoulder. The theory is that pollutants shall be fed outwards to said aperture by the vanes having leading edges strongly swept backwards. This embodiment described very generally, is however not suitable to pump heavy pollutants contained in sewage water.

In SE- 375 831 a solution is described using the opposite principle that pollutants are transported towards the centre, away from the slot. This fact, in combination with the previously mentioned shoulder, makes feeding into the slot impossible.

As previously mentioned, it is a condition that the leading edges of the vanes are swept strongly backwards in order to make a transport of the pollutants outwards and into the slot at the periphery possible. If this is not obtained, serious shut downs will occur very soon. Pump impellers of this type are described in SE-9704222-0 and SE-9704223-8. When the pollutants slide outwards and reach the slot between the vane and the pump housing wall, there is however a risk that they stick to the periphery of the leading edge and clog within the slot.

In DE-614 426 there is shown a device meant to solve such problems, without the need for the previously mentioned shoulder. The pump is a centrifugal pump having a very sharp linking from the axial inlet to the radial part of the flow channel. The periphery of the leading edge is here located downstream of said linking in the radial part of the channel.

A device is further mentioned which has a solid notch in front of the leading edge with a decreasing height up to a cutting knife, followed by a spiral formed groove with a

triangular cross section and sharp corners and which widens towards the periphery. In addition it is stated that the basic principle for this type of solution is that the replacable cutting means shall disintegrate the pollutants. If this should fail, for instance if the cutting means is blunt, the consequence will be that the decreasing height of the notch will compress the pollutants to clogg where the area has its minimum, i.e. within the area of said cutting means.

The above mentioned patent thus describes a solution which, under certain conditions, may obtain a self cleaning ability, but which has got important disadvantages concerning efficiency, wear resistance and life. In addition there are no details given about the very important conditions regarding the leading edges of the vanes and thus it has no meaning to try to apply this described device when pumping sewage water.

The invention concerns a device for pumping sewage water and which eliminates the disadvantages combined with previously known solutions.

The invention is described more closely below with reference to the enclosed drawings.

Fig 1 shows a three dimensional view of a pump housing, Fig 2 a radial cut through a schematic view of a pump according to the invention, Fig 3 a a schematic axial view towards the pump housing surface and Fig 4 a cylindric cut through a groove in the pump housing surface.

In the drawings 1 stands for a centrifugal pump housing having a cylindric inlet 2. 3 stands for a pump impeller with a cylindric hub 4 and a vane 5. 6 stands for the leading edge of the vane , 7 the pump housing wall, 8 a groove in the wall, 9 the direction of rotation and z the rotation axis. 10 and 11 stand for the edges of the groove 8, 12 a surface in the groove, 13 the bottom of the groove and h its depth.

An important principle with the invention is that the pollutants in the pumped liquid are not disintegrated by cutting means. To the contrary, a much more robust construction is used which feeds the pollutants outwards to the periphery. This means that the life of the machine is increased considerably, especially when pumping wearing particles. The design is also stable, meaning that a decrease of the wear on the pump housing wall will occur.

The invention concerns a pump having a special type of pump impeller 3 where the leading edges 6 of the vane or vanes 5 are located upstream of the pump housing, i. e. within the cylindric inlet 2 and where the leading edges lie in a plane perpendicular to the rotation axis z of said impeller.

According to the invention one or several notches, grooves 8, are provided in the wall of the pump housing and which extend over a surface 7 opposing the impeller, i. e. from the essentially cylindric inlet 2 to the essentially axial pump housing surface and having a form specified below. The groove or grooves 8 cooperate with the leading edges 6 of the vane or vanes in such a way that pollutants are fed in the direction of the pump outlet.

In order to secure the feeding through the pump and to make sure of other advantages as compared with known technique, the groove 8 is given a special route and geometry .

In Fig 4 the form of a cylindric cut through the groove is shown characterized in a smooth connection 10 to the pump housing surface 7 at the side from which the impeller passes. The opposing side 11 of the groove in the mentioned cylinder cut, is a, with relation to the pump housing wall, mainly orthogonal surface 12, which continuously transforms into a mainly elliptic bottom 13, which has a characterizing transverse axis, the length of which being at least twice the depth of the groove. This

THIS SHEET HAS BEEN
REPLACED

rounding of the bottom is important as wearing particles will be transported from the surface 7 by secondary currents and thus the wear on said surface will be considerably reduced.

Between the smooth connection 10 to the surface 7 and the bottom 13 of the groove there is a mainly linear transition 14. The angle Υ between said transition and the surface 7 shall lie within the interval 2 to 25 degrees, where Υ is defined as:

$$\Upsilon = \arctan (\Delta z / (r \cdot \Delta \theta))$$

where Δz is the axial displacement and $r \cdot \Delta \theta$ is the tangential extension.

Fig 3 shows the sweep angle β of the groove 8 where

$$\beta = \arctan (\sqrt{ (dr \cdot dr + dz \cdot dz) / (r \cdot d\theta) })$$

and where dr , $d\theta$ and dz are infinitesimal displacements along the edge of the groove.

According to the invention, the sweep angle β shall have a value between 10 and 45 degrees along its entire route in order to obtain the best result.

By help of the invention several advantages are obtained when compared with the solutions known up to now. The following could be mentioned:

The need for a specific and permanent or replaceable cutting means is eliminated as the feeding function takes care of the pollutants and bring them away.

The swept groove 8 acts as a slot seal which brings about a direct efficiency increase as the leakage through the slot is reduced.

This Sheet Has Been Replaced



A reduction of the wear of the surface adjacent the groove is obtained as the wearing particles are brought away from this area after having passed through the groove. In this way a good efficiency is kept also when the sewage water contains wearing particles.

A long life is obtained as wearing particles in the pumped medium cause a wear which preserves the original forms of the details. This means that a good function is kept, also after a certain wear,

The device is adapted to a pump impeller having an optimal form from a performance point of view, as the route of the groove 8 transforms from an axial to a radial direction.



This Sheet Has Been Replaced



Claims

1. A pump of a centrifugal- or half axial type for pumping of sewage water, comprising a pump housing (1) having a cylindric inlet (2) and an impeller (3) consisting of a central hub (3) and one or several vanes (5) with leading edges (6) being swept backwards, characterized in, that the leading edges (6) of the vanes (5) are located in a plane mainly perpendicular to the impeller shaft (z) and that one or several feeding grooves (8) are arranged in the wall of the pump housing (1) on a surface (7) opposite said vanes (5), the grooves being located upstream of the area of said leading edges, routing from inlet towards outlet and swept in the rotation direction of the impeller.

2. A pump according to claim 1, characterized in, that the sweep angle (β), i. e. the angle between the edge of the groove (8) and an arc having the impeller axis as its centre, in each point on that edge and defined as :

$$\beta = \arctan \left(\sqrt{dr \cdot dr + dz \cdot dz} / (r \cdot d\theta) \right),$$

has a value between 10 and 45 degrees along its entire route, where dr , $d\theta$ and dz are infinitesimal displacements along the edge of the groove.

3. A pump according to claim 1, characterized in, that a cylindric cut B-B through the groove (8) shows a smooth connection to the pump housing surface (7) at the side from which the impeller (3) passes, with an angle (γ) between the sloping part (14) of the groove and the pump housing surface (7) and defined as:

$$\gamma = \arctan \left(\Delta z / (r \cdot \Delta \theta) \right),$$

having a value between 2 and 25 degrees.

THIS SHEET HAS BEEN
REPLACED



4. A pump according to claim 3, characterized in, that as seen in an arbitrary cylinder cut B-B through the groove (8), the opposing side of said groove being described as a mainly orthogonally directed side (12), which continuously transforms into a mainly elliptic bottom (13).

5. A pump according to claim 4, characterized in, that the transverse axis in the ellipse that characterizes said bottom (13) of the groove (8) has a length of at least twice the depth (h) of said groove.



This Sheet Has Been Replaced

