

**Product for a welded construction made of AlMgMn alloy
having improved mechanical strength**

Technical sphere

The invention relates to the sphere of rolled or extruded products such as sheets, profiles, wires or tubes made of AlMgMn-type aluminium alloy containing more than 3% by weight of Mg, intended for welded constructions having a high yield stress, good resistance to fatigue and good toughness for structural applications such as ships, industrial vehicles or welded bicycle frames.

State of the art

The optimum dimensioning of welded structures made of aluminium alloy leads to the use of 5,000 series AlMg alloys according to the Aluminium Association nomenclature, in the cold-worked state (state H1 according to the standard NF-A-02006) or partially softened state (state H2), or stabilized state (state H3), while maintaining high resistance to corrosion (state H116) rather than the annealed state (state O). However, the improvement in the mechanical characteristics relative to the state O does not usually remain after welding, and certifying and monitoring organizations generally recommend that only the characteristics in state O be taken into consideration for welded structures. The resistance to fatigue and the fissure propagation rate should also be taken into consideration for dimensioning.

In this sphere, research has concentrated mainly on the implementation of the welding operation itself. There have also been attempts to improve the corrosion resistance of the article by appropriate thermomechanical treatments.

Japanese patent application JP 06-212373 proposes the use of an

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alloy containing 1.0 to 2.0% of Mn, 3.0 to 6.0% of Mg and less than 0.15% of iron to minimize the reduction in the mechanical strength due to welding. However, the use of an alloy having such a high manganese content leads to a reduction in the resistance to fatigue and in the toughness.

Object of the invention

The object of the invention is significantly to improve the mechanical strength and fatigue resistance of welded structures made of AlMgMn alloy, under predetermined welding conditions, without unfavourable consequences for other parameters such as toughness, corrosion resistance and cutting deformation, due to internal stresses.

The invention relates to products for welded constructions made of AlMgMn aluminium alloy composed of (% by weight):

$$3.0 < \text{Mg} < 5.0$$

$$0.5 < \text{Mn} < 1.0$$

$$\text{Fe} < 0.25$$

$$\text{Si} < 0.25$$

$$\text{Zn} < 0.40$$

optionally one or more of the elements Cr, Cu, Ti, Zr such that:

$$\text{Cr} < 0.25$$

$$\text{Cu} < 0.20$$

$$\text{Ti} < 0.20$$

$$\text{Zr} < 0.20$$

other elements < 0.05 each and < 0.15 in total, wherein $\text{Mn} + 2\text{Zn} > 0.75$.

Description of the invention

Contrary to earlier research which concentrated on the welding process and the thermomechanical treatments, the inventors have found a particular range of composition for minor alloying elements, in particular iron, manganese and zinc, leading to an interesting set of properties combining static mechanical



characteristics, toughness, resistance to fatigue, resistance to corrosion and cutting deformation, this set of properties being particularly well adapted to the use of these alloys for naval construction, utility vehicles or the welded frames of bicycles.

This set of properties is obtained by combining a low iron content, $< 0.25\%$, preferably $< 0.20\%$, and even 0.15% , and a manganese and zinc content such that $Mn + 2Zn > 0.75\%$, preferably $> 0.8\%$. The Mn content should be $> 0.5\%$, preferably $> 0.8\%$, to have adequate mechanical characteristics, but should not exceed 1% if a deterioration in toughness and fatigue resistance are to be avoided. The addition of zinc combined with manganese has been found to have a beneficial effect on the mechanical characteristics of welded sheets and joints. However, it is better not to exceed 0.4% because problems can then be encountered in welding.

The magnesium is preferably kept $> 4.3\%$, because it has a favourable effect on the yield stress and fatigue resistance, but beyond 5% the corrosion resistance is less good. The addition of Cu and Cr are also favourable to the yield stress, but Cr is preferably kept $< 0.15\%$ to maintain good resistance to fatigue.

The mechanical strength of the sheets depends both on the magnesium content in solid solution and on the manganese dispersoids. It has been found that the volumetric fraction of these dispersoids, which is linked to the iron and manganese contents, should preferably be kept above 1.2% . This volumetric fraction is calculated from the average of the surface fractions measured on polished cuts produced in three directions (length, width and thickness) by scanning electron microscopy and image analysis.

The products according to the invention can be rolled or extruded products such as hot- or cold-rolled sheets, wires, profiles or extruded and optionally drawn tubes.

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The sheets according to the invention, which are assembled by butt welding by a MIG or TIG process and with a bevel of the order of 45% over about 2/3 of the thickness have, in the welded region, a yield stress $R_{0.2}$ which can be at least 25 MPa higher than that of a conventional alloy having the same magnesium content, that is a gain of about 20%.

The width of the thermally affected region is reduced by about one third relative to a conventional 5083 alloy, and the hardness of the welded joint increases from about 75 Hv to more than 80 Hv. The welded joints also have a tensile strength exceeding the minimum imposed by organizations monitoring unwelded cold-worked crude sheets.

The sheets according to the invention have fatigue resistance, measured by plane bending with a stress ratio wherein $R = 0.1$ on samples taken in the cross-longitudinal direction, higher than:

10⁵ cycles with a maximum stress > 280 MPa

10⁶ cycles with a maximum stress > 220 MPa

10⁷ cycles with a maximum stress > 200 MPa.

The fissure propagation rate ΔK , measured when $R = 0.1$, is > 22 MPa $\sqrt{m}$ when $da/dN = 5 \times 10^{-4}$ mm/cycle and > 26 MPa $\sqrt{m}$ when $da/dN = 10^{-3}$ mm/cycle.

The sheets according to the invention usually have a thickness greater than 1.5 mm. With thicknesses greater than 2.5 mm they can be obtained directly by hot rolling, without the need for subsequent cold rolling and, furthermore, these hot-rolled sheets are less distorted on cutting than cold-rolled sheets.

The products according to the invention have corrosion resistance which is as good as that of normal alloys having the same magnesium content, for example 5083 of common composition, widely used in naval construction.

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Example

Thirteen samples of sheets were prepared by conventional semi-continuous casting in the form of plates, were heated for 20 h at a temperature $> 500^{\circ}\text{C}$ and were then cold-rolled to the final thickness of 6 mm. The reference 0 corresponds to a conventional 5083 composition and reference 1 to a composition slightly outside the invention. The 11 others (references 2 to 12) have a composition according to the invention.

The compositions were as follows (% by weight):

Ref	Mg	Cu	Mn	Fe	Cr	Zn	Ti	Zr
0	4.40	< 0.01	0.50	0.27	0.09	0.01	0.01	0.11
1	4.68	< 0.01	0.72	0.12	0.05	< 0.01	0.01	
2	4.56	< 0.01	0.83	0.12	0.13	0.01	0.01	
3	4.60	< 0.01	0.85	0.17	0.10	0.16	0.01	
4	4.62	< 0.01	0.96	0.10	0.05	0.02	0.01	
5	4.80	0.09	0.80	0.11	0.03	0.02	0.01	
6	4.72	< 0.01	0.87	0.13	0.03	0.02	0.01	
7	4.88	0.05	0.78	0.16	0.02	0.01	0.09	
8	4.92	0.06	0.94	0.08	0.02	0.19	0.01	
9	4.69	< 0.01	0.72	0.07	0.02	0.10	0.01	
10	4.71	< 0.01	0.82	0.06	0.02	< 0.01	0.01	
11	4.73	< 0.01	0.95	0.17	0.03	< 0.01	0.01	
12	4.70	< 0.01	0.92	0.22	0.03	0.01	0.01	

The samples all have, after rolling, a yield stress $R_{0.2} > 220$ MPa in the L direction.

The mechanical strength of the joints welded from these sheets was measured under the following conditions: continuous automatic MIG butt welding with a symmetrical bevel having an inclination of 45° to the vertical over a thickness of 4 mm and filler wire of 5183 alloy.

The mechanical characteristics (tensile strength R_m , yield

stress $R_{0.2}$) were obtained by pulling over samples standardized by the Norwegian monitoring organization DNV for naval construction having a length of 140 mm and a width of 35 mm, the weld bead with a width of 15 mm being in the centre and the length of the narrow portion of the sample being 27 mm, that is the sum of the width of the bead and twice the thickness (15 + 12 mm).

The volumetric fractions of manganese dispersoids was also measured.

The results are as follows (in MPa for resistances and % for fractions):

Ref.	R_m	$R_{0.2}$	Fractions
0	285	141	0.62
1	292	144	1.2
2	302	150	1.4
3	300	146	1.6
4	310	158	1.7
5	309	149	1.4
6	305	155	1.5
7	315	166	1.3
8	318	164	1.9
9	310	153	1.5
10	312	150	1.5
11	315	153	1.6
12	315	151	1.5

The resistance to fatigue of unwelded sheets subjected to plane bending wherein $R = 0.1$ was also measured for references 0 to 5, while determining the maximum stress (in MPa) corresponding to 10^6 and 10^7 cycles respectively, as well as the fissure propagation rate ΔK measured when $da/dn = 5 \times 10^{-4}$ mm/cycle (in MPa $\sqrt{m}$).

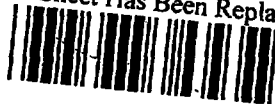
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The results were as follows:

Ref.	10^6 cycles	10^7 cycles	ΔK
0	220	200	22
1	235	205	22
2	230	200	23
3	225	200	23
4	230	205	22
5	225	200	22

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Claims

1. Product for a welded construction made of AlMgMn aluminium alloy composed of (% by weight):

3.0 < Mg < 5.0

0.5 < Mn < 1.0

Fe < 0.25

Si < 0.25

Zn < 0.40

optionally one or more of the elements Cr, Cu, Ti, Zr such that:

Cr < 0.25

Cu < 0.20

Ti < 0.20

Zr < 0.20

other elements < 0.05 each and < 0.15 in total, wherein Mn + 2Zn > 0.75 and preferably > 0.8%.

2. Product according to Claim 1, characterized in that Mg > 4.3%.

3. Product according to one of Claims 1 and 2, characterized in that Mn > 0.8%.

4. Product according to one of Claims 1 to 3, characterized in that Fe < 0.20%.

5. Product according to Claim 4, characterized in that Fe < 0.15%.

6. Product according to one of Claims 1 to 5, characterized in that the volumetric fraction of dispersoids is greater than 1.2%.

7. Sheet according to one of Claims 1 to 6, characterized in that it has a thickness > 2.5 mm and is merely hot rolled.

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8. Unwelded sheet according to any one of Claims 1 to 7, characterized in that it has fatigue resistance, measured by plane bending wherein $R = 0.1$ in the cross-longitudinal direction, higher than:

10⁵ cycles with a maximum stress > 280 MPa

10⁶ cycles with a maximum stress > 220 MPa

10⁷ cycles with a maximum stress > 200 MPa.

9. Sheet according to any one of Claims 1 to 8, characterized in that it has a fissure propagation rate ΔK , measured when $R = 0.1$, higher than:

22 MPa $\sqrt{m}$ when $da/dn = 5 \cdot 10^{-4}$ mm/cycle

26 MPa $\sqrt{m}$ when $da/dn = 10^{-3}$ mm/cycle

10. Use of a product according to one of Claims 1 to 9 in naval construction.

11. Use of a product according to one of Claims 1 to 9 for the construction of industrial vehicles.

12. Use of extruded tubes according to one of Claims 1 to 6 for the manufacture of welded bicycle frames.

13. Sheet according to one of Claims 1 to 9 welded by fusion and having a hardness > 80 Hv in the welded zone.

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Product for a welded construction made of AlMgMn alloy having improved mechanical strength

Technical sphere

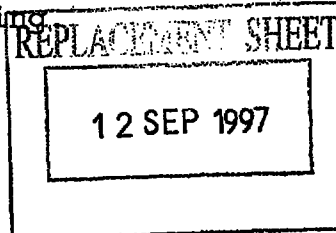
The invention relates to the sphere of rolled or extruded products such as sheets, profiles, wires or tubes made of AlMgMn-type aluminium alloy containing more than 3% by weight of Mg, intended for welded constructions having a high yield stress, good resistance to fatigue and good toughness for structural applications such as ships, industrial vehicles or welded bicycle frames.

State of the art

The optimum dimensioning of welded structures made of aluminium alloy leads to the use of 5,000 series AlMg alloys according to the Aluminium Association nomenclature, such as, for example, the alloy 5083 of which the composition lodged at the Aluminium Association is (% by weight):

Mg:	4.0 - 4.9
Mn:	0.4 - 1.0
Fe	< 0.40
Si	< 0.40
Zn	< 0.25
Cu	< 0.10
Cr:	0.05 - 0.25
Ti	< 0.15

These alloys are used in the cold-worked state (state H1 according to the standard NF-EN-515) or partially softened state (state H2), or stabilized state (state H3), while maintaining high resistance to corrosion (state H116) rather than the annealed state (state O). However, the improvement in the mechanical characteristics relative to the state O does not usually remain after welding, and certifying and monitoring organizations generally recommend that only the characteristics in state O be taken into consideration for welded structures. The resistance to fatigue and the fissure propagation rate should also be taken into consideration for dimensioning.



In this sphere, research has concentrated mainly on the implementation of the welding operation itself. There have also been attempts to improve the corrosion resistance of the article by appropriate thermomechanical treatments.

Japanese patent application JP 06-212373 proposes the use of an alloy containing 1.0 to 2.0% of Mn, 3.0 to 6.0% of Mg and less than 0.15% of iron to minimize the reduction in the mechanical strength due to welding. However, the use of an alloy having such a high manganese content leads to a reduction in the resistance to fatigue and in the toughness.

Object of the invention

The object of the invention is significantly to improve the mechanical strength and fatigue resistance of welded structures made of AlMgMn alloy, under predetermined welding conditions, without unfavourable consequences for other parameters such as toughness, corrosion resistance and cutting deformation, due to internal stresses.

An invention relates to products for welded constructions made of AlMgMn aluminium alloy composed of (% by weight):

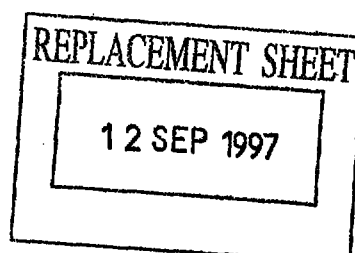
3.0	< Mg < 5.0
0.5	< Mn < 1.0

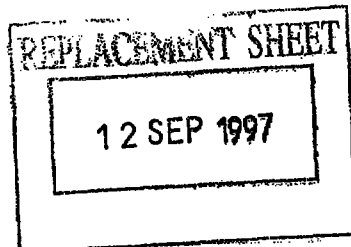
containing Fe, Si and Zn in a quantity such that:

Fe < 0.25
Si < 0.25
Zn < 0.40

optionally one or more of the elements Cr, Cu, Ti, Zr such that:

Cr < 0.25
Cu < 0.20
Ti < 0.20
Zr < 0.20





other elements < 0.05 each and < 0.15 in total, wherein $Mn + 2Zn > 0.75$.

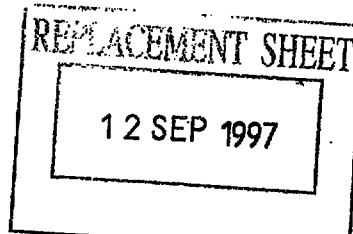
Description of the invention

Contrary to earlier research which concentrated on the welding process and the thermomechanical treatments, the inventors have found a particular range of composition for minor alloying elements, in particular iron, manganese and zinc, leading to an interesting set of properties combining static mechanical characteristics, toughness, resistance to fatigue, resistance to corrosion and cutting deformation, this set of properties being particularly well adapted to the use of these alloys for naval construction, utility vehicles or the welded frames of bicycles.

This set of properties is obtained by combining a low iron content, $< 0.25\%$, preferably $< 0.20\%$, and even 0.15% , and a manganese and zinc content such that $Mn + 2Zn > 0.75\%$, preferably $> 0.8\%$. The Mn content should be $> 0.5\%$, preferably $> 0.8\%$, to have adequate mechanical characteristics, but should not exceed 1% if a deterioration in toughness and fatigue resistance are to be avoided. The addition of zinc combined with manganese has been found to have a beneficial effect on the mechanical characteristics of welded sheets and joints. However, it is better not to exceed 0.4% because problems can then be encountered in welding.

The magnesium is preferably kept $> 4.3\%$, because it has a favourable effect on the yield stress and fatigue resistance, but beyond 5% the corrosion resistance is less good. The addition of Cu and Cr are also favourable to the yield stress, but Cr is preferably kept $< 0.15\%$ to maintain good resistance to fatigue.

The mechanical strength of the sheets depends both on the magnesium content in solid solution and on the manganese dispersoids. It has been found that the volumetric fraction of these dispersoids, which is linked to the iron and manganese contents, should preferably be kept above 1.2% . This volumetric fraction is calculated from the average of the surface fractions measured on polished cuts produced in three directions (length,



width and thickness) by scanning electron microscopy and image analysis.

The products according to the invention can be rolled or extruded products such as hot- or cold-rolled sheets, wires, profiles or extruded and optionally drawn tubes.

The sheets according to the invention, which are assembled by butt welding by a MIG or TIG process and with a bevel of the order of 45% over about 2/3 of the thickness have, in the welded region, a yield stress $R_{0.2}$ which can be at least 25 MPa higher than that of a conventional alloy having the same magnesium content, that is a gain of about 20%.

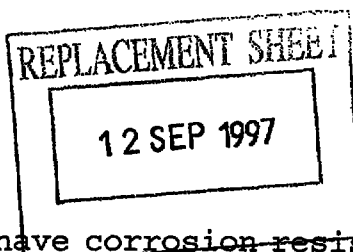
The width of the thermally affected region is reduced by about one third relative to a conventional 5083 alloy, and the hardness of the welded joint increases from about 75 Hv to more than 80 Hv. The welded joints also have a tensile strength exceeding the minimum imposed by organizations monitoring unwelded cold-worked crude sheets.

The sheets according to the invention have fatigue resistance, measured by plane bending with a stress ratio wherein $R = 0.1$ on samples taken in the cross-longitudinal direction, higher than:

- 10^5 cycles with a maximum stress > 280 MPa
- 10^6 cycles with a maximum stress > 220 MPa
- 10^7 cycles with a maximum stress > 200 MPa.

The fissure propagation rate ΔK , measured when $R = 0.1$, is > 22 MPa $\sqrt{m}$ when $da/dN = 5 \times 10^{-4}$ mm/cycle and > 26 MPa $\sqrt{m}$ when $da/dN = 10^{-3}$ mm/cycle.

The sheets according to the invention usually have a thickness greater than 1.5 mm. With thicknesses greater than 2.5 mm they can be obtained directly by hot rolling, without the need for subsequent cold rolling and, furthermore, these hot-rolled sheets are less distorted on cutting than cold-rolled sheets.



The products according to the invention have ~~corrosion resistance~~ which is as good as that of normal alloys having the same magnesium content, for example 5083 of common composition, widely used in naval construction.

Example

Thirteen samples of sheets were prepared by conventional semi-continuous casting in the form of plates, were heated for 20 h at a temperature $> 500^{\circ}\text{C}$ and were then cold-rolled to the final thickness of 6 mm. The reference 0 corresponds to a conventional 5083 composition and reference 1 to a composition slightly outside the invention. The 11 others (references 2 to 12) have a composition according to the invention.

The compositions were as follows (% by weight):

Ref	Mg	Cu	Mn	Fe	Cr	Zn	Ti	Zr
0	4.40	< 0.01	0.50	0.27	0.09	0.01	0.01	0.11
1	4.68	< 0.01	0.72	0.12	0.05	< 0.01	0.01	
2	4.56	< 0.01	0.83	0.12	0.13	0.01	0.01	
3	4.60	< 0.01	0.85	0.17	0.10	0.16	0.01	
4	4.62	< 0.01	0.96	0.10	0.05	0.02	0.01	
5	4.80	0.09	0.80	0.11	0.03	0.02	0.01	
6	4.72	< 0.01	0.87	0.13	0.03	0.02	0.01	
7	4.88	0.05	0.78	0.16	0.02	0.01	0.09	
8	4.92	0.06	0.94	0.08	0.02	0.19	0.01	
9	4.69	< 0.01	0.72	0.07	0.02	0.10	0.01	
10	4.71	< 0.01	0.82	0.06	0.02	< 0.01	0.01	
11	4.73	< 0.01	0.95	0.17	0.03	< 0.01	0.01	
12	4.70	< 0.01	0.92	0.22	0.03	0.01	0.01	

The samples all have, after rolling, a yield stress $R_{0.2} > 220 \text{ MPa}$ in the L direction.

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The mechanical strength of the joints welded from these sheets was measured under the following conditions: continuous automatic MIG butt welding with a symmetrical bevel having an inclination of 45° to the vertical over a thickness of 4 mm and filler wire of 5183 alloy.

The mechanical characteristics (tensile strength R_m , yield stress $R_{0.2}$) were obtained by pulling over samples standardized by the Norwegian monitoring organization DNV for naval construction having a length of 140 mm and a width of 35 mm, the weld bead with a width of 15 mm being in the centre and the length of the narrow portion of the sample being 27 mm, that is the sum of the width of the bead and twice the thickness (15 + 12 mm).

The volumetric fractions of manganese dispersoids was also measured.

The results are as follows (in MPa for resistances and % for fractions):

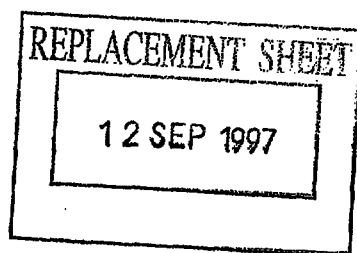
Ref.	R_m	$R_{0.2}$	Fractions
0	285	141	0.62
1	292	144	1.2
2	302	150	1.4
3	300	146	1.6
4	310	158	1.7
5	309	149	1.4
6	305	155	1.5
7	315	166	1.3
8	318	164	1.9
9	310	153	1.5
10	312	150	1.5
11	315	153	1.6
12	315	151	1.5

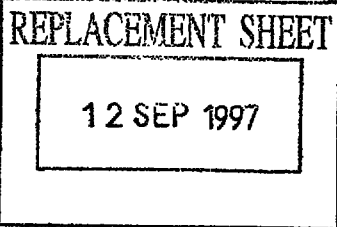
The resistance to fatigue of unwelded sheets subjected to plane bending wherein $R = 0.1$ was also measured for references 0 to 5, while determining the maximum stress (in MPa) corresponding to

10^6 and 10^7 cycles respectively, as well as the fissure propagation rate ΔK measured when $da/dn = 5 \times 10^{-4}$ mm/cycle (in MPa $\sqrt{m}$).

The results were as follows:

Ref.	10^6 cycles	10^7 cycles	ΔK
0	220	200	22
1	235	205	22
2	230	200	23
3	225	200	23
4	230	205	22
5	225	200	22



**Claims**

1. Product for a welded construction made of AlMgMn aluminium alloy composed of (% by weight):

3.0 < Mg < 5.0

0.5 < Mn < 1.0

containing Fe, Si and Zn in a quantity such that:

Fe < 0.25

Si < 0.25

Zn < 0.40

optionally one or more of the elements Cr, Cu, Ti, Zr such that:

Cr < 0.25

Cu < 0.20

Ti < 0.20

Zr < 0.20

other elements < 0.05 each and < 0.15 in total, wherein $Mn + 2Zn > 0.75$ and preferably $> 0.8\%$, said product having a volumetric fraction of dispersoids greater than 1.2%

2. Product according to Claim 1, characterized in that $Mg > 4.3\%$.

3. Product according to Claim 1 or Claim 2, characterized in that $Mn > 0.8\%$.

4. Product according to one of Claims 1 to 3, characterized in that $Fe < 0.20\%$.

5. Product according to Claim 4, characterized in that $Fe < 0.15\%$.

6. Sheet according to one of Claims 1 to 5, characterized in that it has a thickness > 2.5 mm and is merely hot rolled.



7. Use of a product according to one of Claims 1 to 6 in naval construction.
8. Use of a product according to one of Claims 1 to 6 for the construction of industrial vehicles.
9. Use of extruded tubes according to one of Claims 1 to 5 for the manufacture of welded bicycle frames.
10. Unwelded product made of AlMgMn aluminium alloy composed of (% by weight):

3.0	< Mg < 5.0
0.5	< Mn < 1.0

containing Fe, Si and Zn in a quantity such that:

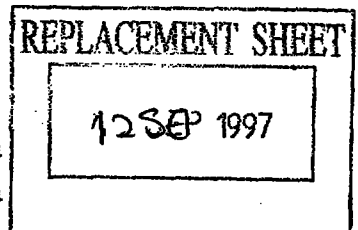
Fe < 0.25
Si < 0.25
Zn < 0.40

optionally one or more of the elements Cr, Cu, Ti, Zr such that:

Cr < 0.25
Cu < 0.20
Ti < 0.20
Zr < 0.20

other elements < 0.05 each and < 0.15 in total, wherein $Mn + 2Zn > 0.75$ and preferably > 0.8 , having fatigue resistance, measured by plane bending wherein $R = 0.1$ in the cross-longitudinal direction, higher than:

10^5 cycles with a maximum stress > 280 MPa
10^6 cycles with a maximum stress > 220 MPa
10^7 cycles with a maximum stress > 200 MPa.



11. Sheet according to Claim 10, characterized in that Mg is > 4.3%.



12. Sheet according to Claim 10 or Claim 11, characterized in that Mn is $> 0.8\%$.
13. Sheet according to one of Claims 10 to 12, characterized in the Fe is $< 0.20\%$ and preferably $< 0.15\%$.
14. Sheet according to one of Claims 10 to 13, characterized in that its thickness is > 2.5 mm and it is merely hot rolled.
15. Use of a sheet according to one of Claims 10 to 14 in naval construction.
16. Use of a sheet according to one of Claims 10 to 14 for the construction of industrial vehicles.
17. Sheet for a welded construction made of AlMgMn alloy composed of (% by weight):

3.0	$< \text{Mg} < 5.0$
0.5	$< \text{Mn} < 1.0$

containing Fe, Si and Zn in a quantity such that:

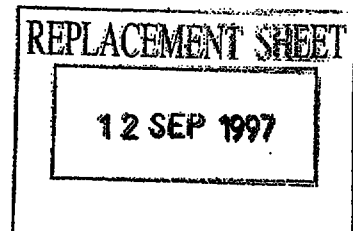
$\text{Fe} < 0.25$
$\text{Si} < 0.25$
$\text{Zn} < 0.40$

optionally one or more of the elements Cr, Cu, Ti, Zr such that:

$\text{Cr} < 0.25$
$\text{Cu} < 0.20$
$\text{Ti} < 0.20$
$\text{Zr} < 0.20$

other elements < 0.05 each and < 0.15 in total, wherein $\text{Mn} + 2\text{Zn} > 0.75$ and preferably > 0.8 , having a fissure propagation rate ΔK , measured when $R = 0.1$, higher than:

22 MPa $\sqrt{\text{m}}$ when $da/dn = 5 \times 10^{-4}$ mm/cycle





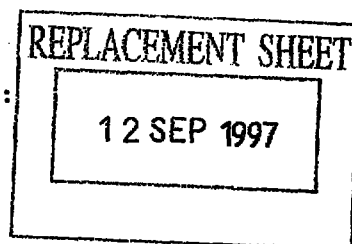
26 MPa/m when $da/dn = 10^{-3}$ mm cycle.

18. Sheet according to Claim 17, characterized in that Mg is > 4.3%.
19. Sheet according to Claim 17 or Claim 18, characterized in that Mn is > 0.8%.
20. Sheet according to one of Claims 17 to 19, characterized in that Fe is < 0.20 and preferably < 0.15%.
21. Sheet according to one of Claims 17 to 20, characterized in that its thickness is > 2.5 mm and that it is merely hot rolled.
22. Use of a sheet according to one of Claims 17 to 21 in naval construction.
23. Use of a sheet according to one of Claims 17 to 21 for the construction of industrial vehicles.
24. Sheet for a welded construction made of AlMgMn aluminium alloy composed of (% by weight):

3.0	< Mg < 5.0
0.5	< Mn < 1.0

containing Fe, Si and Zn in a quantity such that:

Fe < 0.25
Si < 0.25
Zn < 0.40



optionally one or more of the elements Cr, Cu, Ti, Zr such that:

Cr < 0.25
Cu < 0.20
Ti < 0.20
Zr < 0.20

other elements < 0.05 each and < 0.15 in total, wherein $Mn + 2Zn$



> 0.75 and preferably > 0.8, welded by fusion and having a hardness > 80 Hv in the welded zone.

25. Sheet according to Claim 24, characterized in that Mg > 4.3%.

26. Sheet according to Claim 24 or Claim 25, characterized in that Mn is > 0.8%.

27. Sheet according to one of Claims 24 to 26, characterized in that Fe is < 0.20% and preferably < 0.15%.

28. Sheet according to one of Claims 24 to 27, characterized in that its thickness is > 2.5 mm and it is merely hot rolled.

29. Use of a sheet according to one of Claims 24 to 28 in naval construction.

30. Use of a sheet according to one of Claims 24 to 28 for the construction of industrial vehicles.

