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MICROACTUATOR-INDUCED REACTIVE FORCES FOR FINE POSITIONING A SENSOR

Field of the Invention

The present invention relates to servo control systems incorporating both microactuators and position sensors, and more particularly to controlling the movement of position sensors accurately enough for use in an electromechanical information handling system.

Background of the Invention

Precise control of a transducer or similar sensor is becoming more important, particularly in the field of mass storage. Optical and magnetic discs often contain tens of thousands of tracks per radial inch. This density continues to increase rapidly, requiring greater precision in head positioning. In the past, head positioning was typically accomplished by operating an actuator arm with a large-scale motor, such as a voice coil motor, to position a head on a gimbal at the end of an actuator arm. Unfortunately, such large-scale motors often lack sufficient resolution to effectively accommodate high track-density discs. Thus, a high-resolution head positioning mechanism is necessary to accommodate the more densely spaced tracks.

One promising class of head positioning system involves using a high resolution microactuator in addition to the conventional low resolution actuator, thereby effecting head positioning through dual-stage actuation. Various microactuator designs have been considered to accomplish high-resolution head positioning, including piezoelectric, electromagnetic, electrostatic, capacitive, fluidic, and thermal actuators. An example of such structures is provided in U.S. Patent 4,431,934 ("Electrically Actuated Piezoelectric Control Element") issued to Peter Kleinschmidt et al. on Feb. 14, 1984.

Various locations for such microactuators along each actuator arm have been suggested, including at the interface between the gimbal and the head. Such systems are exemplified in U.S. Patent 5,189,578 ("Disk System with Sub-Actuators for Fine Head Displacement") issued to Kenji Mori et al. on Feb. 23, 1993; and in U.S. Patent 5,657,188 ("Head Suspension with Tracking Microactuator") issued to Ryan A. Jurgenson et al. on Aug. 12, 1997.

More pertinent for present purposes is the structure provided in U.S. Patent 6,002,549 ("Dither Microactuators for Stiction Release in Magnetic Disc Drives") issued to Alan David Berman et al. on December 14, 1999. There, a piezoelectric element 26 exemplified relatively near to the rotational axis 14 of the actuator arm 16. The piezoelectric element 26 is employed for fine positioning of a slider 24 relative to tracks 34 on disc 30. A voltage applied to piezoelectric element 26 causes selective expansion or contraction of the piezoelectric element, thereby causing distortion of actuator arm 16 to effect fine positioning of slider 24 over a selected track of rotatable disc 30.

Various methods of contructing and configuring microactuators have been known for some time, and they continue to advance. Computational and cost constraints have nevertheless limited their use in many aspects of position control. Moreover, previous microactuator

control systems have not addressed reactive forces that Applicant has found to frustrate fast, dynamic position control. Consequently, existing servo positioning systems will not permit continued increases in performance, such as will be required for further increasing the density of recorded data. There is a therefore a need in the art for efficient servo positioning systems that are effective for preventing or reducing mechanical resonances selectively.

Summary of the Invention

The present invention provides a novel way to control a servo system of two or more masses bendably coupled to a primary body by microactuators. The controller receives a position signal from a sensor on the first mass, from which it generates a signal to control the microactuator(s) coupling the second mass to the body. The movement of the second mass(es) thereby exerts a controlled reactive force upon the body and upon the first mass that is useful for reducing unwanted components of vibration.

As used herein, "primary" microactuators refer to those coupled between a first mass and a (larger) body, and "secondary" microactuators refer to those coupled between a second mass and the body. Devices of the present invention include at least one primary microactuator and one secondary microactuator. Except as noted, any reference to "moving" a mass will refer to controlling the mass with respect to the body.

In a first embodiment, each mass is coupled to two piezoelectric elements and one flexible pivot, which are also coupled to the body. The piezoelectric elements are biased in compression on each side of the flexible pivot, which is in tension. The first and second mass each include a distal end having a position sensor. The pivots are arranged for substantially paralled operation, allowing each position sensor to move along a

curvilinear path defining a respective surface, the surfaces being substantially parallel. The controller oppositely actuates each pair of microactuators simultaneously so that each mass accelerates to induce an equal-magnitude reactive force upon the actuator body. Preferably, the masses are selected so that they have substantially equal rotational inertia and can therefore be driven by a common control signal. Alternatively, at least one of the signals is derived with a predetermined multiplier related to the inertia ratios between the respective masses.

In a second embodiment, data storage discs are interleaved between the several arms of an actuator body. Each of the arms between the discs is coupled to a pair of head-carrying load beams having transverse motion control via a respective microactuator. A selected head follows a track on its disc surface by controlling a voice coil motor and the primary microactuator. At least one secondary microactuator on another arm is accelerated oppositely so as to counteract the primary microactuator's tendency to rotate the actuator body parallel to the disc surface. In a preferred system, two such secondary microactuators are used, and the "tertiary" microactuator (on the same arm as the primary) moves in phase with the primary microactuator. In this way, the tertiary microactuator counteracts the primary microactuator's tendency to twist the shared arm (about an axis parallel to the disc), and the secondary microactuators counteract the shared arm's tendency to rotate the actuator body about its spindle.

In a third embodiment, also with data storage discs interleaved between the several arms of an actuator body, two selected heads transduce signals simultaneously on two data surfaces. Primary microactuators simultaneously provide control signals so that each selected head follows its respective track. At least one unwanted oscillation is systematically reduced by applying a fixed gain amplified version of an existing control signal to at least one microactuator not being used for track

following. This improves performance on both selected heads without requiring an additional servo channel.

Further features and benefits of the present invention will become apparent to one of ordinary skill upon a careful review of the following drawings and accompanying detailed description.

Brief Description of the Drawings

Fig. 1 is a top view of an information handling system with an actuator assembly, with mechanical features substantially to scale.

Fig. 2 is a side view of the system of **Fig. 1**.

Fig. 3 shows how the system of **Fig. 1** can be used to cause a body of an actuator assembly to settle at its destination position more quickly.

Fig. 4 shows another information handling system incorporating a servo positioning system of the present invention.

Fig. 5 shows a flowchart of a method of the present invention.

Fig. 6 is a schematic depiction of the third embodiment of the present invention, using more than one servo channel for improved microactuator control.

Detailed Description

Numerous aspects of servo positioning that are not a part of the present invention (or are well known in the art) are omitted for brevity, avoiding needless distractions from the essence of the present invention. These include (1) specific circuitry for mathematically combining received sensor signals to derive servo control signals; (2) techniques for constructing microactuators, including parallel or serial arrangements of piezoelectric elements; and (3) biasing and sensor/channel selection mechanisms. Although the examples below show more than enough detail

to allow those skilled in the art to practice the present invention, subject matter regarded as the invention is broader than any single example below. The scope of the present invention is distinctly defined, however, in the claims at the end of this document.

Fig. 1 is a top view of a disc drive **10** with an actuator assembly **110** suitable for use with the present invention. A stack of one or more discs **210** is mounted so that it can be rotated about axis **214**. To read data from track **216**, the center of transducer head **171** must be positioned near the center **218** of the track. For coarse adjustment, the body **114** of actuator assembly **110** is rotated about axis **117** so that transducer head **171** moves toward target track **216**. Transducer head **171** is supported by load beam **118**, which is supported by actuator arm **116** by conventional means. In a portion of the actuator arm **116** that is nearer to the axis **117** than to the head **171**, a mechanism for fine adjustment includes a piezoelectric microactuator **160** able to rotate the head **171** in a horizontal plane about flexible pivot **128**.

Disc drive **10** also includes disc controller **220**. When active, transducer head **171** provides signals to the read channel **222**, which provides a signal to servo controller **224** indicating the head's position. Servo controller then causes driver/receiver **226** to activate one or more microactuators **160**. With head **171** selected, microactuator control may hold head **171** stationary or move head **171** in a first direction **81** according to art-known methods. Simultaneously, according to a first embodiment of the present invention, another portion **111** of the actuator assembly **110** may be moved in an opposite direction **82** to reduce the net lateral reaction of actuator assembly body **114**. Body **114** is a rigid structure having a larger angular inertia about axis **117** than the counterweight portion **111**. Portion **111** has an angular inertia that is at least as large as that of actuator arm **116** and load beam **118** combined.

Microactuator "movements" are described herein with respect to a "body" that is much more massive than the "mass" that is moved. The microactuator is said to move with respect to the body, also, despite the fact that a portion of it remains stationary. As described herein, this movement is measured by the portion of the microactuator that moves the greatest distance relative to the body.

Fig. 2 is a side view of the disc drive **10** of **Fig. 1**, showing more explicitly a conventional arrangement of a motor comprising a voice coil **192** and a pair of magnets **194**. When selected, heads **171,172,173,174** are each configured to read or write from a respective surface of a stack of data storage discs **210**. First, head **171** is selected. Signals travel to and from selected head **171** via read channel **222**, which also provides servo information to servo controller **224**. When head **171** has approached a predetermined target (such as track center **218**) to within the range that head **171** can be moved by microactuator control, servo controller **224** responds by providing a control signal via driver receiver **226** so as to move selected head **171** toward the target (i.e., clockwise).

One inherent effect of this motion of head **171** is the counterclockwise horizontal reactive torque exerted upon the body **114**. In practice, taking this torque into account for precise control of the voice coil motor can be cumbersome. Rather than tolerate this reactive-torque-induced error, according to the first embodiment, servo controller **224** reduces this error by causing a counterweight to move in direction **82**. One way to accomplish this is for servo controller **224** to counter-drive microactuator **140**, which is coupled to a mass of about the same rotational inertia as that coupled to microactuator **160**. This reduces the reactive-torque-induced error as long as microactuator **140** moves mass **141** less than twice as far counterclockwise as microactuator **160** moves mass **161** clockwise.

Optionally, at least one of the microactuators **140** is unavailable for use to control the movement of its respective mass **141**. This may be desired if microactuator **140** is being used for sensing shocks, for example, or to conserve current. Because no mass of about the same rotational inertia as that including the selected head is available for use in microactuator counter-balancing control, another mass is used to reduce the reactive-torque-induced error. In **Fig. 2**, the rotational inertia (J) of mass **151** about axis **117** is more than 50% greater than the rotational inertia (j) of mass **161**. Accordingly, a control signal is desirably provided to microactuator **150** so as to move mass **151** about j/J times the distance that mass **161** is moved by microactuator **160**. So long as mass **151** is moved within 50% of this "perfect counterbalance" distance, the approximate effect of this control signal will be to halve the error that might otherwise result from the reactive torque exerted upon body **114**.

In another embodiment, 100% of the non-selected microactuators **140,150** are driven so as to urge selected head **171** toward the destination track center **218**. The additional inertia provided by the counter-movement of these microactuators **140,150** can increase the microactuator bandwidth by at least a few percent, as compared with the response of the selected microactuator **160** alone. Alternatively, where the corresponding masses **141,151** have a combined angular inertia on the order of that of the body **114**, in a sufficiently stable track follow mode, microactuators **140,150** can be used in lieu of selected microactuator **160**. This allows the selected microactuator **160** to perform other functions, such as controlling the horizontal skew angle during a servo track writing operation or a read retry operation.

Fig. 3 shows how the second embodiment of the present invention can be used to cause a body of an actuator assembly to settle at its destination position more quickly. Curve **310** shows an actuator body's movement from start position **301** to target position **302**, at least partially

compensated according to the present invention. Curve **310** thus resembles the movement of an actuator body that is not affected by reactive forces arising from microactuator movements. According to conventional servo control methods, a microactuator **160** linking the active head **171** to the body **114** is rapidly deformed from longest position **351** to shortest position **352**. This places head **171** near its target position **218** quickly. Unfortunately, the inertial forces of the selected mass **171** cause excitation in the uncompensated actuator, as shown in curve **330**. According to the first embodiment of the present invention, these errors are at least partially compensated. Because the body converges to the target position **302** more precisely, the present embodiment allows the sensor to settle more quickly to its target position **302**. Sensor signal **370** indicates a sensor's location with respect to its target position, and shows some microactuator-induced offsets that are reduced by the compensation scheme of the present embodiment.

For disc drives that implement the present invention, microactuators should be selected that can respond several times faster than the corresponding actuator motor. For a VCM capable of moving a head 0.5 track widths from a stationary position in a minimum time T, for example, the microactuators coupled from the body to the rigid mass comprising that head should be able to move the head 0.5 track widths in less than T/3.

Fig. 4 shows another information handling system **400** incorporating a servo positioning system of the present invention. Controller **420** is configured to receive signal **418** from sensor **471** and to generate control signals **419** that expand and contract microactuators **431,432,441,442**. Physically, the paths for signals **418,419** are housed within conduits **468** affixed to positionable body **414**. Microactuators **431,441** are coupled between mass **421** and body **414**. Microactuators **432,442** are coupled between mass **422** and body **414**. Parallel tracks **415,416** on a medium **410**

such as a tape or disc surface move longitudinally **411** with respect to the sensor **471**. In response to a sensor signal **418** indicating a need to move from a present position (e.g. track **415**) to another position (e.g. track **416**), control signals are selectively provided to expand microactuator **432** and to contract microactuator **442**, urging body **414** in direction **481**. These same respective signals may be provided to expand microactuator **441** and to contract microactuator **431**.

Fig. 5 shows a flowchart of a method of the present invention featuring steps **510** through **570**. An actuator body is moved to within a few tracks of the target **520**, methods for which are known in the art. As illustrated in **Figs. 3&4**, these can include steps of obtaining a difference signal between the sensed location and the target location. This difference signal can then be used to generate (e.g. through a driver/receiver or similar current amplifier) one or more control signals, one of which controls a motor.

At a desired distance from the destination, microactuators are controlled in preparation for entry into the destination track **530**. As shown in **Figs. 1& 4**, this can include situating a selected head toward the destination and/or moving non-selected heads away from the destination. A short seek is performed **540** to enter the destination track, after which a position error signal (PES) is available. First and second control signals based on the PES are then calculated **550** and used to actuate secondary and primary microactuators **560**, respectively.

Fig. 6 is a schematic depiction of an embodiment of the present invention using two servo channels to allow simultaneous track following on two data surfaces of a disc stack. The actuator assembly includes a block **680** coupled to four arms **610,620,630,640**. Optionally, the two end arms **610,640** have about 50 to 70% of the rotational inertia of the middle arms **620,630**, each pair being about equal in size and configuration.

A servo controller **600** includes a circuit **697** for deriving servo control signals for coarse control by motor **699**, and for deriving fine control signals on two additional channels, systems for which are known in the art. According to the present invention, the servo controller passes these signals each through a power amplifier. The amplified signals **601,602** are then received by a selectable channel coupling mechanism **660**.

For clarity and explicitness, the mechanism **660** is depicted schematically to include a double-pole double-throw switch **661**, two inverting amplifiers **676,677**, a unity gain buffer **678** and another switch **662**. In practice, this mechanism **660** is easily and preferably replaced by a MUX/DEMUX arrangement or similar circuit or by software. With the aid of present teachings, this substitution is an ordinary matter of design choice. As shown, each switch **661,662** has an upper position and a lower position.

Irrespective of the position of switch **661**, signal **601** passes directly to control microactuators **621,622**, so that these two always operate in phase with one another. In systems vulnerable to arm torsion excitation, this in-phase motion may be preferable to the arm-level scissors-like motion described conjunction with **Fig. 4**.

With switch **661** in its upper position, control signal **601** also passes through inverting amplifier **676**, so that an inverted signal is received by the microactuators coupled to arm **630**. If the delay induced by inverting buffer **676** is suitably short, the masses **627,633** of arm **630** move substantially out of phase with the masses **617,623** of arm **620**. Their net torque on block **680** about its axis is therefore canceled (i.e. opposed so as to reduce its net magnitude). Note that many actuator assemblies (including that of **Fig. 1**) are vulnerable to lateral rotational vibrations. Because of their mass and bearing construction, however, they are not ordinarily vulnerable to roll excitations being transmitted between arms **620,630**.

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It is assumed that **Fig. 6** depicts a microactuator configuration like that of **Fig. 4**, where the effective pivot of each actuator **621** is less than ten times closer to its corresponding sensor **616** than to the axis of rotation of the actuator assembly. It is also assumed that J/j is less than about 500, where J is the combined rotational inertia of the arms **610,620,630,640** together with the block **680**, and j is the rotational inertia of each mass **623**, about the actuator's axis of rotation. More preferably, J/j is less than 100. With these assumptions, the net torque cancellation described in the foregoing paragraph can be important.

It should be noted that with switch **661** in its upper position, the second microactuator control signal **602** passes through unity gain buffer **678** to microactuator **641**, provided that switch **662** is in its lower position. This allows rotary compensation between mass **613** and mass **637**, despite the fact that the arm associated with each **610,640** has only one microactuator. With suitable DEMUX circuitry between the signals received from the heads, any one of the four middle heads **616,624,626,634** can track follow simultaneously with either the top or the bottom heads **614,636**.

With switch **661** in its upper position, control signal **601** can be derived from the position signal **696** received from head **634**. Configuring circuitry **697** to provide a suitable control signal **601** for this purpose is optionally conventional and in any event is not a critical part of this invention. Note that G_1 can be -1 if the circuitry **697** is conventional. What is extraordinary about this configuration is its specific use of the position-indicative signal **696** received from a sensor **634** on a first mass **633** to control the movement of at least one other mass **623,627** advantageously.

With suitable read channel circuitry, head **636** can track follow simultaneously with head **634**. Signal **602** is derived from a position-indicative signal **696** received from head **634** by ordinary methods and is

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provided to microactuator **641**. Note that this will ordinarily require a second read channel.

With switch **661** in its lower position, heads **616,624** move independently of heads **626,634**. In fact, the depicted configuration is switchable so that any two non-successive heads can track follow simultaneously.

Fig. 6 further includes at least one microactuator that can be used as an acceleration sensor. With switch **662** in its upper position, microactuator **641** is configured to provide an output signal **665** indicative of a component of vibration aligned with the plane of the discs **615**. A preferred embodiment of the present invention provides switching circuitry that allows at least one microactuator **641** on an arm **640** to be used as either a tracking control or as an acceleration sensor.

The depicted configuration can alternatively be used so that both servo channel control signals **601,602** are used to enhance the track following performance of head **616** with the aid of unconventional information sources. With switch **661** in its lower position, for example, gains G_2 and G_3 could each be computed as a sum with one term derived from acceleration sense signal **665**. It should therefore be understood that the broad general meaning encompassed in signals "derived from" other signals is not confined to conventional analog methods.

By way of review in conjunction with **Fig. 6**, certain aspects of the present invention relate to an apparatus including a large, fairly rigid body **620** flexibly coupled to two or more masses **617,623**. By "fairly rigid," it is meant that the large rigid pieces of the body **620** are coupled together by joints having an effective spring constant more than double that of joints **619** joining a mass **617** to the body **620**. As shown in **Fig. 6**, each flexible joint is shown as a (negligible) damper **638** in parallel with a spring **639**. In typical disc drive actuator assemblies, each arm **630** is affixed to its block **680** by a joint properly represented as a stiff spring **683**. In effect, the arms

and block thus combine to form a fairly rigid composite body. This composite body will be affected by an active microactuator **621** moving a sufficiently large distal mass **617** in a circumferential direction.

Sensor **616** is able to sense its radial position relative to a disc **615** and to generate a position-indicative signal **696**. When sensor **616** is selected for track following, the microactuator(s) **621** between the sensor **616** and the body **620,680** are defined to be "primary." Control circuitry including controller **600** is configured to derive a control signal based on the signal **696** from the selected sensor **616**, and to provide the signal to at least one secondary microactuator **631,632**. The control circuitry similarly derives a second control signal that is received by a tertiary microactuator **622**. The selection of a particular circuits for controller **600**, amplifiers **601,602**, and selectable channel coupling mechanisms **661** within the scheme of the present invention are matters of design choice, and can optionally use art-known circuits and/or software.

For example, the sensor **616** of **Fig. 6** optionally provides a sensor signal **696** indicative of an offset from a target position (such as a track center **218** of **Fig. 1**). In this case, secondary microactuators **631,632** are preferably configured to receive inverted signals from inverting buffers **674,675** so that they are actuated in a direction that tends to reduce the offset. In another aspect, one of ordinary skill can alter the selectable channel coupling mechanism **661** of **Fig. 6** so that one or two of the masses **617,623** are moved in phase, but that substantially all of the others **613,627,633,637** urge their respective masses in a direction that tends to reduce the offset.

With or without secondary microactuators **631,632** the apparatus of **Fig. 6** desirably includes another microactuator **622** in contact with the same arm **620** as the primary microactuator **621**. Microactuators **621,622** are both in contact with and able to move arm **620**. By operating these microactuators **621,622** in substantially parallel directions, substantially in

phase, the tendency of the arm **620** to roll is reduced. Note that "roll" refers to a rotation of a portion of arm **620** in a plane that is roughly perpendicular to the discs **615**.

Further elaborating on the method of **Fig. 5**, the depicted step **550** of deriving control signals **601,602** from the difference signal can be performed conventionally by the circuitry **697** in controller **600**. According to the present invention, for example, head **616** is selected and generates a signal **696** indicative of position such as a Gray code signal, a digitally encoded track number identifier. The target track is subtracted from the track number to calculate an offset. With switch **661** in its upper position, a VCM control signal is derived from this offset and is provided to motor **699** to seek to the desired track. When the offset is sufficiently small, signal **601** is derived so that microactuator **621** performs a short seek to move head **616** over the target track.

As a result of the depicted circuitry, another control signal **603** is derived to control secondary microactuators **631,632** so as to cancel the torque exerted by microactuator **621** upon body (i.e., the actuator assembly including the arms **610,620,630,640** and the block **680**). Tertiary microactuator **622** also receives a signal to cancel an unwanted excitation, the roll torque exerted upon arm **620** by microactuator **621**.

All of the structures and methods described above will be understood to one of ordinary skill in the art, and would enable the practice of the present invention without undue experimentation. It is to be understood that even though numerous characteristics and advantages of various embodiments of the present invention have been set forth in the foregoing description, together with details of the structure and function of various embodiments of the invention, this disclosure is illustrative only. Changes may be made in the details, especially in matters of structure and arrangement of parts within the principles of the present invention to the full extent indicated by the broad general meaning of the terms in which

the appended claims are expressed. For example, steps of the above methods can be reordered while maintaining substantially the same functionality, without departing from the scope and spirit of the present invention. In addition, although the preferred embodiments described herein are largely directed to moving sensors along a fixed curvilinear path, it will be appreciated by those skilled in the art that many teachings of the present invention can be applied to other systems such as two-dimensional micropositioning systems without departing from the scope and spirit of the present invention.

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Claims

What is claimed is:

1. A servo positioning apparatus comprising:

a positionable body;

a first mass and a second mass, the first mass including a first sensor configured to generate a sensor signal indicative of the first sensor's position;

one or more primary microactuator(s) coupled between the first mass and the body;

one or more secondary microactuator(s) coupled between the second mass and the body, the secondary microactuator(s) being configured to move the second mass relative to the first mass; and

a controller configured to derive a first control signal from the sensor signal and to provide the first control signal to at least one of the secondary microactuator(s).

2. The servo positioning apparatus of claim 1 in which the first mass and the second mass are about equal in size.

3. The servo positioning apparatus of claim 1 in which the sensor signal is indicative of an offset from a target position and in which the first control signal is configured to urge the secondary microactuator(s) in a direction that tends to reduce the offset.

4. The servo positioning apparatus of claim 1, in which an unwanted vibration is induced in the body by the primary microactuator(s), and in which the unwanted vibration is reduced by actuation of the secondary microactuator(s).

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5. The servo positioning apparatus of claim 1 in which the body has an axis of rotation and a rotational inertia J about the axis, and in which the second mass has a rotational inertia j about the axis, J/j being less than 100.

6. The servo positioning system of claim 1 in which the primary and secondary microactuators comprise piezoelectric transducers.

7. An information handling system including:

a voice coil magnet generating a magnetic field;

at least one rotatable data storage disc; and

the servo positioning apparatus of claim 1, in which the positionable body includes a voice coil positioned across a part of the magnetic field, in which the controller is configured to provide a coarse control signal able to actuate the voice coil, and in which the first sensor is a transducer head able to read data from the data storage disc.

8. A method of using the servo positioning system of claim 1 comprising steps of:

(a) calculating a difference between the sensor signal and a target value to derive a difference signal;

(b) deriving a first control signal from the difference signal; and

(c) actuating at least one of the secondary microactuators with the first control signal.

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9. In a system including a positionable body, a first mass and a second mass each coupled indirectly to the body, the first mass including a first sensor configured to generate a sensor signal indicative of the first sensor's position, a method for positioning comprising steps of:

(a) calculating a difference between the sensor signal and a target value to derive a difference signal;

(b) deriving a first control signal from the difference signal;

(c) actuating at least one microactuator coupled between the second mass and the body in response to the first control signal to move the second mass relative to the body and the first mass, so that a reactive force is exerted upon the body.

10. An actuator assembly comprising:

a first mass and a second mass each pivotably coupled to a third mass, the first mass including a sensor able to generate a signal indicative of the sensor's position; and

means for selectively pivoting the second mass relative to the third mass and the first mass based upon the position-indicative signal.