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(54) MAGNETIC RECORDING AND/OR REPRODUCING APPARATUS

(71) We, SONY CORPORATION, a Japanese Body Corporate of 7-35 Kitashinagawa, 6-chome, Shinagawa-ku, Tokyo, Japan, do hereby declare the invention for which we pray that a patent be granted to us, and the method by which it is to be performed, to be particularly described in and by the following statement:—

The present invention relates to apparatus for processing periodic information signals such as the recording and reproduction of information signals, for example, color video signals, and more particularly is directed to the reduction of cross-talk in the reproduction of signals recorded in adjacent tracks, even though the relatively low frequency chrominance signal components of color video signals are recorded for every line interval and the tracks are very close together, or even may be overlapping.

It is well-known to record video signals on magnetic tape or other forms of record medium by scanning successive parallel tracks on the record medium with one or more transducers energized by the video signals. There has been a constant effort to improve the efficiency of use of the record medium by packing the tracks as close together as possible. The packing density has always been limited by, among other things, the fact that, during reproduction of the recorded signals, a reproducing transducer scanning each of the tracks in order could pick up signals or cross-talk from adjacent tracks.

One effort made to minimize cross-talk has been to use two transducers having air gaps with different azimuth angles for successive lines. This is relatively easy to do because most magnetic recording apparatus for video signals includes a rotary drum provided with two transducers or heads which can have gaps with different azimuth angles. The tape is wrapped helically about a portion of the perimeter of the drum and moved longitudinally along this helical path while the

transducers or heads are rotated, thus bringing the heads alternately into recording relationship with the tape and allowing each head to trace out a respective one of the tracks. Each transducer or head has a finite width and thus produces magnetization of those magnetic domains in the material on the tape in what would appear to be, if such domains were visible, a series of parallel lines or stripes, each having a length as great as the width of the track, and each having an orientation that corresponds to the azimuth angle of the gap of the transducer or head used to record that track.

By recording successive alternate tracks with transducers or heads having different azimuth angles, and in view of the fact that the reproducing transducers or heads would also have corresponding azimuth angles, the gap of each reproducing transducer or head would be aligned with the parallel, but fictitious, lines of the track being scanned thereby, but, because of the difference in azimuth angles, would extend at an angle to such lines of the next adjacent track. If the reproducing transducer overlapped that adjacent track, the well-known azimuth loss would result in attenuation of the signal reproduced from the adjacent track. Even if the reproducing transducer accurately scans a track recorded with the same azimuth, the reproducing transducer may still be influenced by the signals recorded in adjacent tracks with different azimuths, but the azimuth loss will decrease or eliminate the effect of such signals recorded in adjacent tracks on the output signal of the transducer.

Even in the above type of recording with different azimuth angles, there is still a limit to the overlapping or abutting of adjacent tracks. This is due in part to the fact that some of the recorded information may include relatively low frequencies, and the azimuth loss is generally proportional to the frequency of the signals. Thus, interference due to cross-

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talk from low frequency signals, such as, a frequency converted chrominance signal component, is not reduced to the same degree by the use of transducers having different azimuth angles as cross-talk from high frequency signals, such as, a frequency modulated luminance signal component.

One important step in minimizing cross-talk of low frequency information is disclosed in British Patent Application No. 37435/72 (Serial No. 1,407,036). In some embodiments of that earlier application, the relatively high frequency luminance components were recorded during every line increment on every track, but the low frequency chrominance components were not recorded in adjacent line increments of adjacent tracks. The chrominance components were recorded intermittently, usually in alternate line intervals, but also permissibly for every third or fourth line interval or for two or more successive line intervals followed by at least the same number of line intervals in which the chrominance components were not recorded, and in all cases the recording in adjacent tracks was such that chrominance components would not be recorded in adjacent line increments of the respective tracks. If this type of recording were visible, the chrominance components would appear to be recorded in a checkerboard-like pattern. Furthermore, the luminance components could also be recorded intermittently in this same way to permit even further overlapping of adjacent tracks.

In the reproduction of signals recorded with this checkerboard-like pattern, the components that were recorded only intermittently would be utilized directly upon reproduction and would also be delayed for the length of time necessary to permit them to be used during the next succeeding interval in which similar information was not recorded. This system reduced the cross-talk interference but at some sacrifice in the quality of the reproduced image, due to the fact that less information was recorded than was available.

According to one aspect of the present invention there is provided apparatus for processing periodic information signals comprised of first intervals, each of which includes a predetermined number of second intervals, said second intervals being recorded in respective areas of successive, substantially parallel tracks on a record medium, the apparatus including a recording circuit including means for providing different first and second information-modulated carriers alternately; said recording circuit including selecting means and control means for the selecting means operative to cause the recording of the first and second information-modulated carriers, respectively, in tracks which are next adjacent each other.

According to the second aspect of the present invention there is provided apparatus

for processing periodic information signals comprised of first intervals, each of which includes a predetermined number of second intervals, said second intervals being recorded in respective areas of successive, substantially parallel tracks on a record medium, the apparatus including a recording circuit including means for providing two different signals to be used in deriving first and second information modulated carriers to be recorded; selecting means for alternately selecting the two signals, deriving means for deriving respective first and second information-modulated carriers from said selected two signals and said information signals, and control means for the selecting means operative to cause the recording of the first and second information-modulated carriers, respectively in tracks which are next adjacent each other.

The present invention may further comprise a reproducing circuit comprising transducer means for reproducing information signals recorded in each of the tracks and simultaneously reproducing cross-talk signals from the tracks next adjacent thereto, and means for providing the information signals reproduced from each of said tracks with a common carrier and for eliminating the cross-talk signals therefrom on the basis of said different first and second information-modulated carriers which are recorded in the tracks which are next adjacent each other.

In accordance with an embodiment of this invention, periodic information signals having first intervals and second intervals which are subdivisions of the first intervals, for example, color video signals having field and line intervals, are recorded in respective areas of successive parallel tracks on a record medium with the ends of the margins between the areas in which the second or line intervals are recorded in each of the tracks being aligned, in the direction transverse to the lengths of the tracks, with the adjacent ends of such margins in the next adjacent tracks, and interference or cross-talk between signals recorded in adjacent tracks is reduced or eliminated during reproduction of the recorded information signals, and more particularly the chrominance signal components in the case of recording of color video signals after they have been combined with different first and second carriers, respectively. Such first and second carriers modulated by information signals and recorded in adjacent tracks, respectively, may be distinguished from each other by their respective frequency and/or polarity characteristics so that, upon reproduction of the signals recorded in a particular track, the cross-talk signals from the tracks next adjacent thereto can be conveniently suppressed or eliminated by reason of the different frequency and/or polarity characteristics of the carriers with which the signals were combined prior to being recorded in

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5 that particular track and in the next adjacent tracks, respectively. In any case, when recording color video signals in accordance with this invention, both the chrominance and luminance components are recorded as continuous signals, the word "continuous" being used in the sense that the blanking portion of each line interval is part of the continuous signal.
10 In the recording and/or reproducing of color video signals according to a particular embodiment of this invention, the chrominance signal components of the video signal to be recorded may be frequency converted so as to selectively produce first and second frequency converted signals which respectively have different carrier frequencies selected to interleave with each other and with any luminance and original chrominance component frequencies with which they might otherwise interfere. Switching or selecting means are provided to allow one or the other of the two frequency converted signals to be recorded in each line increment of each track, and such switching or selecting means is controlled to provide a pattern of recording in which the frequency converted signal recorded in each line increment will be different from the frequency converted signal recorded in the adjacent line increment that would otherwise produce an interfering cross-talk signal.
20 In the simplest pattern of such recording, one of the two frequency converted signals may be recorded in each line increment of one track and the other frequency converted signal may be recorded in each line increment of the next adjacent tracks. However, other, more complex patterns could also be selected. During reproducing of the signals thus recorded, the frequency-interleaved relation of the carriers of the frequency-converted signals recorded in adjacent tracks makes it possible to simply minimize or eliminate the cross-talk interference signals, for example, by means of a simple comb filter including a one line delay. However, with the described frequency-interleaved relation of the carriers of the frequency-converted signals with respect to each other and with respect to the luminance and original chrominance signal components, the carrier of one of the reproduced frequency converted signals, as reconverted and supplied to the comb filter, may reverse its phase or polarity for successive line intervals, and this polarity reversal may further account for the suppression by the comb filter of the cross-talk interference signals during reproduction.
30 In accordance with another embodiment of this invention for recording and/or reproducing color video signals, the chrominance signal components of the video signal to be recorded may be frequency converted so as to selectively produce first and second frequency converted signals which, when considered instantaneously, have the same carrier

frequency, but differ from each other in their phase or polarity characteristics. In this case, switching or selecting means are provided to receive both of these frequency converted signals having different polarity characteristics and to allow one or the other of them to be recorded during every line interval. For example, each of the line areas or increments of one track may have recorded therein a frequency converted signal with a carrier of constant polarity, while, in the next adjacent tracks, the carrier of the frequency converted signal recorded therein reverses its polarity for successive line intervals. Again, the pattern of recording is such that, during reproduction, cross-talk effects can be minimized or eliminated, and the carrier-frequency of each frequency converted signal is preferably such as to interleave with potentially interfering signals. Although the first and second frequency converted signals of this embodiment, when considered instantaneously, have the same carrier frequency but differ from each other in their phase and polarity characteristics, the effect appears to be the same as that of balanced-modulating that carrier with a signal having a repetition rate which is one-half the video line repetition rate, and this balanced-modulation effect results in frequency-interleaving of the carriers of the frequency-converted signals recorded in adjacent tracks. In any case, during reproduction of the recorded signals, the reproduced signals of two successive line intervals may be added together by means of suitable delay means, for example, as by a simple comb filter, to cancel out, or at least minimize cross-talk interference signals.
40 According to a third aspect of the present invention there is provided apparatus for processing periodic information signals comprised of first intervals, each of which includes a predetermined number of second intervals, the second intervals having been recorded in respective areas of successive parallel tracks on a record medium with the information signals recorded in next adjacent tracks modulated onto different first and second carriers; the apparatus including a reproducing circuit including transducer means for scanning along the tracks one at a time so as to reproduce the information signals recorded in each of the tracks along with cross-talk signals from the tracks next adjacent thereto, and means for providing the information signals reproduced from each of said tracks with a common carrier and for eliminating the cross-talk signals therefrom on the basis of the different first and second carriers which have been modulated by the information signals prior to being recorded in the tracks which are next adjacent to each other.
50 The present invention will now be described, by way of example, with reference to the accompanying drawings, wherein:
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Fig. 1 shows a fragment of a record medium illustrating portions of two tracks in which signal information may be recorded;

5 Fig. 2 is a block diagram of basic components of a recording apparatus for minimizing cross-talk interference between frequency converted chrominance components of a video signal;

10 Fig. 3 is a block diagram of a recording apparatus embodying one of the modes of operation suggested in Fig. 2;

Figs. 4A and 4B respectively show a comb filter and its frequency response characteristic;

15 Figs. 5A—5C are frequency response curves for sections of the circuit shown in Fig. 3;

Fig. 6 is a chart of frequency relationships for Figs. 3 and 7;

20 Fig. 7 is a block diagram of a playback or reproducing apparatus to be used for reproducing signals recorded by the apparatus of Fig. 3;

Figs. 8A and 8B are response curves for Figs. 3 and 7;

25 Figs. 9A and 9B show the transducers used in Figs. 3 and 7;

Fig. 10 shows a fragment of a recording made by the transducers of Figs. 9A and 9B;

30 Fig. 11 is a block diagram of another embodiment of a recording apparatus;

Fig. 12 is a block diagram of a playback apparatus for reproducing signals recorded with the apparatus of Fig. 11;

35 Fig. 13 is a graph of a frequency spectrum illustrating a difference between the apparatus of Figs. 3 and 11;

Fig. 14 is a block diagram of still another embodiment of a recording apparatus;

40 Fig. 15 shows a fragment of a recording made by the apparatus of Fig. 14;

Fig. 16 is a set of waveforms to which reference will be made in explaining the operation of the apparatus of Fig. 15; and

45 Fig. 17 is a block diagram of a playback apparatus for reproducing video signals recorded by the apparatus of Fig. 14.

50 Fig. 1 shows a section of a record medium 21 on which there are two tracks 22 and 23 recorded in that order due to relative movement in the directions of the arrows 24 and 26 between the medium 21 and recording transducers (not shown). Only two tracks 22 and 23 are shown, although in the normal recording of signal information there would be a large number of such tracks. Each track is divided into areas or increments of which the increments 27—32 are illustrative. Each of these areas or increments has recorded on it the signal information of one interval, for example a line interval of a video signal that is divided into line intervals and field intervals. Usually, but not necessarily, each track 22 and 23 includes a line increment for each line interval of one field of the television signal.

Each line interval and each field interval contains a blanking and synchronizing portion, and in accordance with accepted practice, the tracks 22 and 23 are shown with the increments 27—32, as well as all of the other increments, arranged in a pattern referred to as H-alignment. This is achieved by regulating the relative movements along the directions 24 and 26 in accordance with the synchronizing portions of the video signal to be recorded so that the section of the increment or area 27, for example, on which the blanking and synchronizing signal is recorded in the track 22 is aligned with the section of the abutting increment or area 28 on which the blanking and synchronizing signal for that line interval is recorded. This reduces the cross-talk of blanking and synchronizing signal information from one track to the other.

55 The tracks 22 and 23 in Fig. 1 are shown recorded in such a way that they are contiguous. It is assumed that the width of each of the transducers (not shown) used to record the tracks is exactly equal to the width of the respective track 22 or 23. Signals recorded on contiguous tracks as shown in Fig. 1 would produce cross-talk interference from one track to the other during reproduction or playback, because the reproducing transducer (not shown) scanning track 22 would unavoidably be energized slightly by the magnetic field of the adjacent edge of the track 23.

60 In accordance with accepted practice, the luminance components of a color video signal can be treated separately from the chrominance components. More specifically, the luminance components modulate a carrier so that they are recorded in a higher frequency portion of the available frequency band. If the tracks 22 and 23 are then recorded by respective transducers having different azimuth angles of their respective gaps, and the same azimuth angles are used in transducers respectively reproducing video information recorded in tracks 22 and 23, then the well-known azimuth loss would result in attenuation of the signal reproduced from track 23 during the scanning of track 22. However, the chrominance signal components, in accordance with well-known practice, are frequency converted from a band around the normal chrominance carrier frequency, which in the case of the NTSC signal is approximately 3.58 MHz, to a relatively low frequency of about 600 or 700 KHz. Since the azimuth loss is generally proportional to the frequency of the signals, the interference due to cross-talk from low-frequency signals, such as the frequency-converted chrominance signal components, is not reduced to the same degree, by the use of transducers having different azimuth angles, as is cross-talk from high frequency signals, such as the frequency-modulated luminance signal components. Thus, even if transducers having different azimuth angles are used for

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the recording of tracks 22 and 23 on Fig. 1, and then for the reproducing of the recorded signals, chrominance information recorded in the area or increment 28 of track 23 would be picked up by the transducer traversing the area or increment 27 when scanning track 22 and would interfere with the chrominance signal reproduced from the area or increment 27. The reverse would also be true.

In the co-pending British Application No. 37435/72 (Serial No. 1,407,036) supra, such interference between signals from adjacent areas is eliminated by not recording a chrominance signal in the area or increment 28 if a chrominance signal is recorded in the area or increment 27, and vice versa. In accordance with the invention in that application, the recording of chrominance information is alternated such that chrominance information is not recorded in the increment 29 but is recorded in the increment 30. Preferably, but not necessarily, there is chrominance information recorded in the increment 31, and if there is, there would be no chrominance information recorded in the area 32. Under certain conditions it would be preferable not to record information in the increment 31, but instead to record chrominance information in two successive increments 30 and 32. Various other patterns of recording chrominance information are encompassed within that application, but all of them depended upon reproducing the chrominance information that was recorded in one line area or increment, utilizing that information and simultaneously delaying it and then utilizing the delayed replica to fill in the gap in the next line interval, or line intervals, for which the chrominance signal was not recorded. While the chrominance signal does not vary much from line to line, it does vary somewhat, and this use of the same information twice or even more times reduces to some degree the quality of reproduction of a color television image, especially the signal-to-noise ratio.

Fig. 2 shows basic components of a circuit in accordance with the present invention to permit successive tracks, such as the tracks 22 and 23 in Fig. 1, to be recorded and to include in every line area or increment of each track both luminance information and chrominance information. The luminance signal is supplied from an input terminal 34 to an angular modulator 36 in which it modulates the phase or frequency of a carrier signal produced within the angular modulator 36. This angular modulated signal is connected to a transducer 37 for recording by the latter on a record medium 38. There is relative movement between the transducer 37 and the medium 38 which may be resolved into movement of the medium along the direction of the arrow 39.

Chrominance components of the video signal corresponding to the luminance components

applied to the input terminal 34 are applied to an input terminal 41. This input terminal is connected to carrier control means 42 that includes a frequency converter 43, and the output of which is supplied to the transducer 37. In accordance with the usual practice, the chrominance components include a carrier originally having a frequency in the upper part of the video signal band. The chrominance components are clustered around this carrier at frequencies such as to interleave with components in the same part of the frequency band of the original luminance components applied to the input terminal 34. The carrier control means 42 is shown generally to include a signal generator 46 that produces either one or two frequency converting signals, depending upon the mode of operation of the system. The frequency converting signal or signals is or are connected to the frequency converter 43 to shift the carrier of the chrominance components to a relatively low frequency band below the band of frequencies occupied by the modulated carrier from the angular modulator 36.

The basic system further includes a synchronizing signal input terminal 47 and a synchronizing circuit 48 to receive synchronizing signals synchronous with selected synchronizing signals of the video signal to be recorded. The synchronizing circuit is connected to switching or selecting circuit means 49 or 51, which are alternatively provided according to embodiments of the invention hereinafter described in detail. Either the switching circuit means 49 is used to control the converting signal input to the frequency converter 43 or the switching circuit means 51 is used to modify the output signal of the frequency converter 43 in the carrier control means 42. In one mode of operation, the signal generator 46 produces two frequency converting signals of different frequency, and the switching means 49 is used to apply these two signals, alternately, to the frequency converter 43 to convert the chrominance components to one or the other of two frequency bands. As will be described hereinafter, these bands may be almost completely overlapping or they may be substantially separated from each other in frequency. In the case of a system utilizing two different converting frequencies, the frequency-converted chrominance signal recorded on track 22 in Fig. 1 would have one carrier frequency, and the frequency-converted chrominance signal recorded on track 23 would have another carrier frequency. Not only would these carrier frequencies be different from each other but they would be selected to interleave with each other and with the chrominance and luminance components, or at least with the frequencies that those components would occupy if the components were present. As is well-known, if two signals have frequency-interleaving rela-

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tion therebetween with regard to line synchronizing frequency, these two signals can be separated by using a comb-filter having a 1H delay line and either an adder or subtractor, even though frequency ranges of these signals are overlapped. This means that after suitable frequency changing one of the two signals changes its polarity between successive two line intervals, while the other keeps its polarity unchanged.

If the system is used in such a way that the signal generator 46 produces only a single frequency converting signal, the frequency converter 43 is arranged to provide two output signals to the switching means 51, one of these output signals being out of phase, or, more correctly, of inverse polarity, to the other. In that case, the signal from the synchronizing circuit 48 controls the switching means 51 to select one of these frequency converted signals of opposite polarity on every other track and to switch over one to another on the remaining track to apply the properly arranged frequency converted signal to the output terminal 44 to be recorded by the transducer 37. The action of the switching means acts as a balanced modulator as will be described in the later part of the specification. The selection of one or the other of these frequency converted signals would produce a pattern of recording, although not a visible pattern, of the chrominance components in the increments in the tracks 22 and 23. A pattern suitable for minimizing cross-talk between contiguous increments such as the increments 27 and 28 in the tracks 22 and 23 will be described in greater detail hereinafter.

In the more detailed illustration in Fig. 3 of a video tape recording system a color video signal input terminal 53 is provided to receive a composite video signal that includes both luminance and chrominance components and is composed of line field, and frame intervals with blanking and synchronizing portions in each of those intervals. A low pass filter 54 connects the input terminal 53 to a delay circuit 56 that, in turn, supplies a signal to a frequency modulator 57. The frequency modulator includes a source for generating a carrier, the frequency of which is to be modulated. The output of the frequency modulator 57 is fed through a high pass filter 58 to a mixing circuit 59.

The input terminal 53 is also connected to a comb filter 61 that separates out the chrominance signal components of the composite video signal. The output of the comb filter 61 is connected to a frequency converter 62, and a frequency converting carrier signal is supplied to the frequency converter 62 from a second frequency converter 63. The frequency converted output signal is supplied from the converter 62 through a band pass filter 64 to mixer 59.

The input terminal 53 is also connected to a horizontal synchronizing signal separator 65, the output of which is connected to a phase comparison circuit 66 that also receives signals via a frequency divider 67 from an oscillator 68. The phase comparator circuit 66 has its output connected to the oscillator 68 to control the frequency thereof, and the output of oscillator 68 is connected to frequency converter 63.

The input terminal 53 is also connected to a vertical synchronizing signal, or as it is more commonly called, sync, separator circuit 69, the output of which is applied to a flip-flop circuit 71. This flip-flop circuit is connected to a switching or selecting circuit 72 that operates, in effect, as if it were a single-pole, single-throw switch having its poles respectively connected to output circuits of two oscillators 73 and 74.

The flip-flop 71 is also connected to a servo-control circuit 76 that controls the operation of a transducer driving motor 77 in the mechanical part of the system in accordance with standard practice. In addition to being connected to the servo-circuit 76, the flip-flop 71 is also connected to a control signal transducer 78 located to record control signals along one edge of a magnetic tape record medium 79 that is wrapped helically part of the way around a drum 81. This drum comprises an upper portion 82 and a lower portion 83 with a slot 84 therebetween. Two transducers 86 and 87 are located at opposite ends of an arm 88 affixed to the end of a shaft 89 driven by the motor 77. An amplifier 91 connects the mixing circuit 59 to the transducers 86 and 87.

Before describing in detail the operation of this circuit and apparatus in Fig. 3, it is desirable to consider briefly the comb filter 61 which is shown in somewhat greater detail in Fig. 4A. As may be seen, it comprises an input terminal 92 connected to a delay line 93 that delays signals passing through it by one horizontal line interval, which in the case of the NTSC signal is approximately $1/15,750$ th of a second. Both the input terminal 92 and the output of the 1H delay means 93 are connected to input terminals of a combining circuit 94 that has an output terminal 96.

The response characteristic of the comb filter 61 of Fig. 4A is illustrated in Fig. 4B. As may be seen, the filter 61 transmits most readily those signals close to a frequency f_c , which is the carrier frequency of the chrominance components and in the case of the NTSC signal is approximately 3.58 MHz. The filter also transmits, with somewhat greater attenuation, signals whose frequency differs from the frequency f_c by a frequency f_h , which is the fundamental frequency of the line repetition rate of approximately 15.750 KHz. The filter also transmits signals that differ

connected to oscillator 65, to a phase locked oscillator 66 has its control signal of oscillator 66 connected to a circuit 69, a flip-flop connected to it 72 that single-pole, less respectively of two controls the motor 77 in accordance with it 76, the control signals are recorded on a drum component a lower between. Two at opposite end of an amplifier to the trans- operation of Fig. 3, it is a comb filter water detail comprises an delay line through it by in the case approximately the input a 1H delay terminals an output the comb in Fig. 4B. emits most frequency f_c , the chrominance NTSC. The filter attenuates from f_c , which is the line 5.750 KHz. that differ

from the frequency f_c by other integral multiples of the frequency f_h . These are the frequencies of components of the chrominance signal. However, the filter 61 substantially completely rejects signals having frequencies that differ from the frequency f_c by odd multiples of $1/2 f_h$. These are exactly the frequencies of the luminance signal components in the composite video signal. Thus a comb filter is well suited to separate luminance components from chrominance components.

In describing the operation of the circuit in Fig. 3, reference will be made to Figs. 5A—5C and 6. The band of frequencies of a typical video signal to be applied to the input terminal 53 of the circuit in Fig. 3 is shown in Fig. 5A in which the section indicated as S_c is the band of the luminance components and S_c' is the frequency band of the chrominance components clustered around the chrominance carrier having the frequency f_c .

For reasons that will be described hereinafter, the frequency of the signal generated by the oscillator 73 is $f_c + 1/4 f_h$ and that of the oscillator 74 is $f_c - 1/4 f_h$.

The switching circuit 72 is controlled by a pulse signal P_s that originates in the flip-flop 71 and is illustrated in line A of Fig. 6. The pulse signal P_s is a square wave that has a negative interval T_a which, in the case of recording a field in each of the parallel tracks, is equal in duration to a television field and a positive interval T_b of the same duration as the interval T_a . Thus the switching circuit 72 connects the oscillators 73 and 74 alternately to the frequency converter 63 for one field interval at a time. As a result, the frequency of the signal applied through the switching circuit 72 to the frequency converter 63 is illustrated in line B of Fig. 6 as being $f_c - 1/4 f_h$ for each of the intervals T_a , and $f_c + 1/4 f_h$ for each of the intervals T_b . As mentioned, this is in accordance with the common practice of recording one field interval, which has a duration equal to the interval T_a , on one track, for example the track 22 shown in Fig. 1, and the next field interval, which has a duration equal to the interval T_b , on the next track, for example, the track 23.

The oscillator 68 produces a signal having a frequency f_c which is selected to be nf_h . A suitable value for n has been found to be 44, so that the frequency of the oscillator 68 is approximately 693 KHz. This signal is maintained constant by dividing its frequency by n , that is, by 44, in the frequency divider 67 to produce a signal having a frequency f_h and comparing the phase of this signal in the phase comparator 66 with the horizontal sync signal from the separator 65. The output of the phase comparator circuit 66 is applied to control the oscillator 68. The controlled signal at the frequency f_c from the oscillator

68 is applied to the frequency converter 63. This frequency converter 63 is, typically, a balanced modulator, which is arranged to add the frequencies of the signals supplied thereto. For one field interval, indicated in Fig. 6 as the interval T_a , the output signal of the frequency converter 63, as indicated in line C of Fig. 6 has frequency $f_c + f_c - 1/4 f_h$, and for the next field interval T_b , the frequency of the output signal of the frequency converter is $f_c + f_c + 1/4 f_h$. These two signals are applied, during alternate field intervals, to the frequency converter 62, which is, typically, another balanced modulator arranged to subtract the frequencies of the signals supplied thereto.

The other input signal to the frequency converter 62 is the chrominance signal comprising components clustered around the original carrier frequency f_c and having frequencies that differ from f_c by integral multiples of f_h . Thus, in the frequency converter 62 a signal S_c' is produced having components clustered around the frequency $f_c - 1/4 f_h$ during the field interval T_a , as shown in line D of Fig. 6, and around the frequency $f_c + 1/4 f_h$ during the interval T_b . The frequency band occupied by this signal S_c' is illustrated in Figs. 5B and 5C. Actually, these are two bands slightly different in frequency from each other. The frequency $f_c - 1/4 f_h$ may be written as f_{c1} and the frequency $f_c + 1/4 f_h$ may be written as f_{c2} . Fig. 5C shows the relationship between these frequencies, and both Figs. 5B and 5C show the band of the frequency modulated signal S_c' produced in the frequency modulator 57 as being almost entirely above the band of the signal S_c' .

The purpose of the delay circuit 56 is to assure that the frequency modulated signal S_c' applied through the high pass filter 58 to the mixing circuit 59 arrives at the mixing circuit exactly in time with the frequency converted signal S_c' from the frequency converter 62 as filtered by the bandpass filter 64. The resulting mixed signal is amplified by the amplifier 91 and applied to the transducers 86 and 87 to be recorded on the tape 79.

Face views of the transducers 86 and 87 are shown in Figs. 9A and 9B to clarify the difference in azimuth angles of their respective gaps g_1 and g_2 . The azimuth angle of the transducer 86 is θ_1 and is 90° in the example shown, while the azimuth angle θ_2 of the transducer 87 is approximately 60° .

Fig. 10 illustrates the recording of several tracks 92—98 on a piece of tape 79 in which the even-numbered tracks are recorded by the transducer 86 of Fig. 9A and the odd-numbered tracks are recorded by the transducer 87 of Fig. 9B. These tracks are recorded by wrapping the tape 79 approximately half-way around the drum 81 in Fig. 3 along a

helical path as illustrated. The tape is moved lengthwise at a certain speed and the motor 77 rotates the arm 88 on which the transducers 86 and 87 are mounted. The relative speed of movement of the tape 79 and rotation of the transducers 86 and 87, and the angle of the helix are such that the tracks recorded by the two transducers are contiguous with each other or may even overlap somewhat. At one edge of the tape are control pulses 99 recorded by the control signal transducer 78 in Fig. 3. The tracks 92-98 in Fig. 10 are not to scale, but are illustrative of the recording of several line intervals in respective areas or increments of each track and further illustrative of the effect of the difference in azimuth angles of the transducers 86 and 87. It will be seen that, in this case, the ends of the margins between the areas in which the line intervals are recorded in each of the tracks, for example, in the track 93, are aligned, in the direction transverse to the lengths of the tracks, with the adjacent ends of such margins in the next adjacent tracks, for example, the tracks 92 and 94. Except for the fact that the apparatus in accordance with the present invention permits both luminance and chrominance components to be recorded in every line increment of each of the tracks 92-98 even though the tracks are contiguous with each other, the azimuth relationship of the transducers 86 and 87 and the mechanical structure shown in Fig. 3 are in accordance with known practice.

Fig. 7 shows a playback apparatus suitable for reproducing video signals that have been recorded by means of the apparatus of Fig. 3. The mechanical components of the playback apparatus and some of the electrical components are identical with those in Fig. 3 and will be given similar reference numerals. Among these elements are the transducers 86 and 87, which are operated as playback transducers in Fig. 7 and are connected to the input of an amplifier 101. The output circuit of this amplifier is connected through a high pass filter 102 to a limiter 103 that supplies an amplitude-limited signal to a frequency demodulator 104. The demodulator is connected to another amplifier 106 that supplies a signal to a mixing circuit 107.

The amplifier 101 is also connected through a low pass filter 108 to a frequency converter 109, which is connected through a bandpass filter 111 and a comb filter 112 to the mixing circuit 107. The output of the mixing circuit 107 is connected to a reproduced composite video signal output terminal 113 of the playback or reproducing apparatus.

The amplifier 106 is also connected to a horizontal sync separator circuit 65 that may be the same as the correspondingly numbered circuit in Fig. 3. As in Fig. 3, the horizontal sync separator circuit 65 is connected to a phase comparison circuit 66 that receives a

signal from the frequency divider 67. The signal to be applied to the frequency divider 67 is generated in the oscillator 68, which is, in turn, controlled by the phase comparator 66.

The output of amplifier 106 is also connected to the vertical sync separator circuit 69, which supplies signals to a flip-flop 114. The flip-flop 114 also receives signals from the control signal transducer 78 via a waveform circuit 116 that may be, for example, a rectifier.

The output of the flip-flop 114 is applied to the switching or selecting circuit 72, which is similar to the switching circuit in Fig. 3 and which receives signals from two oscillators 117 and 118, respectively. The output signal of the switching circuit 72 is connected to the frequency converter 63 that corresponds to the frequency converter 63 in Fig. 3, and the output signal of the frequency converter 63 in Fig. 7 is connected to the frequency converter 109.

The comb filter 112 is also connected to a burst-gate 119, which is connected to a phase comparator circuit 121 that also receives signals from a fixed oscillator 122. The phase comparator 121 is connected to both of the oscillators 117 and 118 to control their operation.

In the operation of the system in Fig. 7, demodulation of the frequency-modulated luminance signal reproduced from the tape 79 by the transducers 86 and 87 and passed through the circuit that includes the amplifier 101, the filter 102, the limiter 103, the demodulator 104, and the amplifier 106 is well-known. The advantage of the invention concerns mainly the handling of the frequency converted chrominance signal components.

The oscillator 68 produces a signal f_c at the frequency nf_c , where n is the same integral number 44 as was used in the system in Fig. 3. The oscillators 117 and 118 produce signals having frequencies $f_c - 1/4(f_h)$ and $f_c + 1/4(f_h)$, respectively. The latter signals are applied alternately to the frequency converter 63 by means of the switching or selecting circuit 72 that reverses at the field repetition rate for the intervals T_a and T_b as shown in Fig. 6 at line A. These signals are alternately combined in the frequency converter 63 with the signal from the oscillator 68 to produce alternately frequency converting signals having the frequencies listed in line C of Fig. 6 as $f_c + f_h - 1/4(f_h)$ during the interval T_a and $f_c + f_h + 1/4(f_h)$ during the interval T_b . These signals are applied alternately to the frequency converter 109 which is arranged to subtract the frequencies of the signals applied thereto.

The frequency converter 109 also receives during alternate field intervals the signals S_c' clustered around the respective carrier frequencies

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$$f_{ca} = f_c - 1/4 (f_h) \text{ and } f_{cb} = f_c + 1/4 (f_h),$$

as shown in Figs. 5B and 5C. The relative
timing of the two sets of signals applied to
the frequency converter 109 corresponds to
the timing of the control signal pulses 99
recorded along the edge of the tape 79 (Fig.
10) by the transducer 78 when it is operating
as a recording device in the system in Fig. 3.
When the same control transducer 78 is
operating as a playback device, the control
pulses from it are the pulses P_c in line E
of Fig. 6. These pulses are rectified in the
waveform circuit 116 so that only the pulses
of one polarity are allowed to pass through
to the flip-flop 114 where they cooperate with
vertical sync pulses from the vertical sync
separator 69 to control the phase of the pulse
signal P_s in line A of Fig. 6. As a result
of this interrelation, during the interval T_s
when the signal S_c' in line D of Fig. 6
applied to the frequency converter 109 from
the low pass filter 108 has the carrier fre-
quency $f_{ca} = f_c - 1/4 (f_h)$, the switching circuit
72 will be conductive to signals from the
oscillator 117, and as a result the signal
supplied by the frequency converter 63 to
the frequency converter 109 will have the
frequency $f_s + f_c - 1/4 (f_h)$. These two signals,
when subtracted by the frequency converter
109, result in an output signal S_s that includes
the original carrier frequency f_s and side
bands spaced therefrom by integral multiples
of the frequency f_h . The signal S_s is referred
to on line G of Fig. 6. This frequency
reconverted chrominance signal passes through
the bandpass filter 111 and through the comb
filter 112 to the mixing circuit 107 where
it mixes with the demodulated luminance
signal from the amplifier 106 to form a reconsti-
tuted composite video signal at the output
terminal 113.

At the same time that the reproduced
chrominance component signal having the
carrier frequency $f_c - 1/4 (f_h)$ characteristic of
the track being scanned is applied to the
frequency converter 109, a cross-talk inter-
ference signal picked up from the adjacent
recorded track and having frequency con-
verted chrominance components with a carrier
frequency $f_c + 1/4 (f_h)$ is also being applied
to the frequency converter 109. The cross-
talk interference signal is identified in line F
of Fig. 6 and in Fig. 8A as the signal S_k' .
As shown in Fig. 8A, the amplitude of the
cross-talk signal S_k' is substantially less than
the amplitude of the desired signal S_c' , and
this difference in amplitude is beneficial in
avoiding an interference effect from the signal
 S_k' . Of more significance is the frequency
interleaving relationship between the signals
 S_c' and S_k' .

This frequency interleaving relationship
causes the incorrect, or undesired, frequency
converted chrominance component signal, that

is, the cross-talk signal, applied to the fre-
quency converter 109 to be converted therein
from the signal S_k' in line F of Fig. 6 to the
signal S_k in line G of Fig. 6, where it is
shown to have a carrier frequency $f_s - 1/2 (f_h)$.
As may be seen in Fig. 4B, such a carrier
frequency corresponds to a node in the
response curve of the comb filter 112 and
therefore will be greatly attenuated by the
filter. The frequency response of this filter is

$$\sqrt{2(1 - \cos w/f_h)}.$$

In addition, all of the side bands of the
undesired frequency converted signal S_k will
be at frequencies that are greatly attenuated
by the comb filter 112.

The comb filter 112 produces the same
beneficial elimination of interference or cross-
talk chrominance component signals during
the interval T_b as during the interval T_a .
During the interval T_b , the desired frequency
converted chrominance component signal S_c'
in lines D and F of Fig. 6 has the carrier
frequency $f_{cb} = f_c + 1/4 (f_h)$ while the cross-
talk signal S_k' in line F of Fig. 6 and shown
in Fig. 8B has the carrier frequency
 $f_{ca} = f_c - 1/4 (f_h)$. The desired signal is con-
verted by the frequency converting signal
 $f_c + f_s + 1/4 (f_h)$ from frequency converter 63,
that is, the sum of the signal $f_s + 1/4 (f_h)$ from
the oscillator 118 and the signal f_c from the
oscillator 68, to produce, at the output of the
frequency converter 109 the desired chromin-
ance signal S_s having the original carrier
frequency f_s as illustrated in line G of Fig. 6.
At the same time the undesired chrominance
component signal picked up as cross-talk inter-
ference, and having the carrier frequency of
 $f_c - 1/4 (f_h)$, is frequency converted in fre-
quency converter 109 into the signal S_k in
line G of Fig. 6 with a carrier frequency
 $f_s + 1/2 (f_h)$. As may be seen in Fig. 4B, this
carrier frequency is above the frequency f_s ,
but is also a frequency that is greatly
attenuated by the comb filter 112, as are all
of the side bands of the frequency converted
cross-talk signal.

Thus, the comb filter 112 greatly attenuates
cross-talk interference chrominance signals
while transmitting the desired chrominance
component signals, no matter whether the
desired signals have a higher or a lower
carrier frequency than the undesired inter-
ference signals. The only requirement is that
the carriers of the desired and undesired
signals have a frequency-interleaving rela-
tionship with each other. This relationship
requires that the two carrier signals of the
frequency converted chrominance components
have the relationship:

$$f_{cb} - f_{ca} = 1/2 (2k - 1) f_h$$

In the system of Figs. 3 and 7, k , which

could be any integer, is 1. The frequencies f_{ca} and f_{cb} are:

$$f_{ca} = nf_h - 1/4 f_h$$

$$f_{cb} = nf_h + 1/4 f_h$$

The output signal of the comb filter 112 is also applied to the burst gate 119 that passes only the burst signals that have been reconverted to the frequency f_a . These signals are compared in the phase comparison circuit 121 with a fixed frequency signal f_s from the oscillator 122 and the output of the phase comparator 121 is applied to both of the oscillators 117 and 118. It does not matter that the oscillators 117 and 118 have different frequencies. The correction signal applied to both of these oscillators during the period that the oscillator 117 is connected to the frequency converter 63 by the switching means 72 is determined by the phase comparator 121 as if the oscillator 118 did not exist. In a corresponding manner, the control signal applied to both of the oscillators by the phase comparator 121 during the time that the oscillator 118 is connected to the frequency converter 63 is determined as if the oscillator 117 did not exist.

Fig. 11 shows a modified recording system in which many of the components are identical with those in Fig. 3 and will not be described again. The components that do differ from those in Fig. 3 are the components associated with the production of the frequency converting signals to be applied to the frequency converter 62.

The system in Fig. 11 has an oscillator 123 that produces a signal that is connected directly to one of the input terminals of the switching or selecting circuit 72 and is also connected to a frequency divider 124. A frequency multiplier 126 connects the output of the frequency divider 124 to the other input terminal of the switching circuit 72. The output terminal of the switching circuit 72 is connected to a frequency converter 127 that also receives a frequency converting signal from a fixed frequency oscillator 128. Due to the frequency selected for the oscillator 123, a frequency divider 129 is connected between the frequency converter 127 and the frequency converter 62.

The output of the frequency divider 124 is also connected to a frequency divider 131, which is connected in turn to the phase comparator 66. The output of the phase comparator 66 is supplied back to the oscillator 123 to control its operation.

As in the system in Fig. 3, the frequency converter 62 alternately produces frequency converted chrominance signals S_c' shown in Figs. 5B and 5C to have the carrier frequencies F_{ca} and F_{cb} , respectively, that have an interleaving relationship so that the side

bands of these frequency converted carriers interleave with each other. For simplicity of the circuits, the frequencies F_{ca} and F_{cb} produced by the system in Fig. 11 are not as close as the frequencies f_{ca} and f_{cb} in the system in Fig. 3. The oscillator 123 is chosen to have a frequency $4F_{cb}$. This signal is divided by 7 in the frequency divider 124 and the divided frequency is multiplied by 5 in the frequency multiplier 126 to produce a signal having a frequency defined as $4F_{ca}$, which is 5/7th as great as the frequency $4F_{cb}$ from the oscillator 123. These signals having frequencies $4F_{cb}$ and $4F_{ca}$ are applied during alternate field intervals T_b and T_a shown in Fig. 6 to the frequency converter 127 that also receives a fixed signal having a frequency $4f_s$ from the oscillator 128 and is arranged to add the frequencies of the signals supplied thereto. Thus, the output signal of the frequency converter 127 during one field interval includes the component $4(f_s + F_{cb})$ and, during the next field interval, has a component with a frequency $4(f_s + F_{ca})$. The frequency of the output signal of the frequency converter 127 is divided by 4 in the frequency divider 129 so that the signal applied to the frequency converter 62 is either $f_s + F_{ca}$ or $f_s + F_{cb}$. These signals produce a converted chrominance component signal at the output of the bandpass filter 64 which, during successive field intervals, has the carrier frequency F_{ca} and the carrier frequency F_{cb} , respectively.

The output signal of the frequency divider 124 is divided by 29 in the frequency divider 131 to an output frequency of f_h . This output signal is compared with the line frequency f_h in the phase comparator 66 to produce a control signal that is fed back to the oscillator 123 to control its operation.

Instead of connecting the switching circuit 72 directly to the frequency converter 127 and dividing the frequency of the output signal of the frequency converter in the divider 129, the frequency divider 129 may be connected between the switching circuit 72 and the frequency converter 127. In that case, the oscillator 128 must produce a signal having a frequency f_s instead of $4f_s$.

The frequencies F_{ca} and F_{cb} although generally related in the same manner as the frequencies f_{ca} and f_{cb} in the system in Fig. 3, are somewhat farther apart in actual frequency. However, they still retain the interleaving relationship. Where the frequencies f_{ca} and f_{cb} in the system in Fig. 3 differed only by $1/2 (f_h)$, the frequency $4F_{cb}$ generated by the oscillator 123 is $203 (f_h)$, which corresponds to the fact that it is divided by 7 in the frequency divider 124 and the output of that divider is further divided by 29 in the frequency divider 131 to reach the frequency f_h . The frequency $4F_{ca}$ is 5/7th the frequency $4F_{cb}$ or $145 (f_h)$. Thus, the frequency difference between the frequencies

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$4F_{cb}$ and $4F_{ca}$ is $58(f_h)$, and when this difference is divided by 4 in the frequency divider 129, it turns out that the frequency difference between F_{cb} and F_{ca} in Fig. 11 is

$$5 \quad 14 \frac{1}{2} (f_h).$$

The response curves shown in Figs. 5B, 5C, 8A, and 8B are still applicable to the signals produced by the system in Fig. 11, since the response curves are not drawn to a precise frequency scale. The frequency F_{cb} produced in the system in Fig. 11 is

$$10 \quad 50 \frac{3}{4} (f_h),$$

which is approximately 799 KHz. Even with a frequency converted carrier of 799 KHz, there is still an acceptable separation between the frequency modulated luminance band S_y' and the frequency converted chrominance S_c' .

$$35 \quad F_{ca} = \frac{1}{4} (2 \times 73 - 1) f_h = \frac{1}{4} \times 145 f_h = \frac{1}{4} \times 5 \times 29 f_h$$

and

$$F_{cb} = \frac{1}{4} (2 \times 102 - 1) f_h = \frac{1}{4} \times 203 f_h = \frac{1}{4} \times 7 \times 29 f_h.$$

Fig. 12 shows an apparatus for reproducing signals recorded by the apparatus of Fig. 11. Many of the components of Fig. 12 are identical with those in the playback or reproducing apparatus in Fig. 7 and others are identical with components in Fig. 11. The description of such components and their operation will not be unnecessarily repeated.

In order to reconvert the frequency converted chrominance signal components of signals recorded by the apparatus of Fig. 11, the frequency converter 109 in Fig. 12 is supplied during alternate field intervals with frequency converting signals having frequencies $f_s + F_{ca}$ and $f_s + F_{cb}$, respectively. These frequency converting signals are generated in the same way as in the system in Fig. 11 by means of the oscillator 123 that produces a signal having a frequency $4F_{cb}$ which is applied to one input terminal of the switching circuit 72 and is divided by 7 in the frequency divider 124 and is multiplied by 5 in the frequency multiplier 126 to produce a signal having the frequency $4F_{ca}$ at the other input terminal of the switching circuit 72. The output signal of the switching circuit is divided by 4 by the frequency divider 129 to produce signals having frequencies F_{ca} and F_{cb} to be applied to the frequency converter 63. The frequency converter 63 also receives signals from an oscil-

The equation for determining interleaving of the signals F_{cb} and F_{ca} in the system of Fig. 11 is still:

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$$F_{cb} - F_{ca} = \frac{1}{2} (2k - 1) f_h,$$

but whereas k was 1 in the system in Fig. 3, it has been selected to be 15 in the system in Fig. 11. In order to produce a frequency difference which is an odd multiple of $1/2 (f_h)$, as is required for interleaving, both the frequencies F_{cb} and F_{ca} must be odd multiples of $1/4 (f_h)$. The frequencies are:

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$$F_{ca} = \frac{1}{4} (2x - 1) f_h$$

and

$$F_{cb} = \frac{1}{4} (2y - 1) f_h$$

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where x is 73 and y is 102. Thus,

lator 132 at the frequency f_s , thus causing the frequency converter 63 to produce the required two output signals alternately having the frequency $f_s + F_{ca}$ and the frequency $f_s + F_{cb}$, respectively.

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The switching circuit 72 is controlled by the flip-flop 71 which in turn is controlled by the waveform circuit 116. This circuit 116 operates in the same manner as the corresponding circuit in Fig. 7 to rectify pulses picked up by the control signal transducer 78 and to select pulses of only one polarity occurring at alternate field intervals. As a result, the proper frequency converting signals are applied to the frequency converter 109 to produce reconverted chrominance signals that have the correct carrier frequency f_s to pass through the comb filter 112. The undesired cross-talk interference signals applied to the frequency converter 109 at the same time have a carrier frequency that differs from the correct carrier frequency by $29/2 (f_h)$. These signals may be partially attenuated by the bandpass filter 111 because of their substantial difference in frequency, and, since they differ from the frequencies of the desired chrominance components by an odd multiple of $1/2 (f_h)$, they will also be strongly attenuated by the comb filter 112.

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As in the circuit in Fig. 7, the burst signals of the reconverted chrominance signal

components are allowed to pass through the burst gate 119 to the phase comparator 121, which is also supplied with a signal having the same frequency f_c from the oscillator 122. The output of the phase comparator 121 is used to control the operation of the oscillator 132.

Fig. 13 illustrates the difference between the frequencies f_{ca} and f_{cb} of the frequency converted carriers of the apparatus of Figs. 3 and 7 as compared with the frequencies F_{ca} and F_{cb} of the frequency converted carriers of the apparatus in Figs. 11 and 12. The frequencies f_{ca} and f_{cb} are spaced $1/4(f_h)$ on each side of the 44th harmonic of the line frequency f_h , while the frequency F_{ca} is $1/4(f_h)$ above the 36th harmonic and the frequency F_{cb} is $1/4(f_h)$ below the 51st harmonic.

Fig. 14 shows another embodiment of an apparatus in accordance with the invention for recording video signals on closely spaced tracks on a record medium while minimizing the interference of cross-talk signals from adjacent tracks during reproducing even though both luminance components and chrominance components are recorded in each line area or increment of each of the tracks. The part of the apparatus of Fig. 14 for frequency modulating a carrier by means of the luminance signal component and recording the frequency modulated signal is the same as that shown in Figs. 3 and 11 and need not be described again.

In Fig. 14 the composite video signal is also applied to the comb filter 61 which passes the chrominance signal components to a balanced modulator 133. An oscillator 134 is also connected to the balanced modulator 133. The modulator 133 has two output terminals connected to the fixed terminals of the single-pole, double-throw switch or selecting device 72 and the arm of this switch is connected to a low pass filter 136 which is connected in turn to the mixing circuit 59.

The composite video signal is also supplied from the input terminal 53 to the horizontal sync separator 65 and to the vertical sync separator 69. The horizontal sync separator 65 is connected to a flip-flop 137 and the vertical sync separator 69 is connected to the flip-flop 71. Both of these flip-flops are connected to an AND gate 138 the output of which is connected to control the switching or selecting circuit 72. The flip-flop 71 is also connected to the servo-circuit 76 and to the control signal transducer 78 to record control signals along one edge of the tape 79.

In the operation of the apparatus shown in Fig. 14, the oscillator 134 generates a signal having a fixed frequency f_c and this signal combines, in the balanced modulator 133, with the chrominance signal components that pass through the comb filter 61 to the balanced modulator. The balanced modulator 133, which is arranged to subtract the frequencies

of the signals supplied thereto, produces two output signals indicated as C_a and $-C_a$ which are, as the minus sign indicates, of opposite polarity, although they may be considered to be 180° out of phase. Each of these signals has the same carrier frequency f_c , when considered instantaneously, and they are selected alternately by the switching circuit 72 to be applied to the low pass filter 136 that eliminates undesired side bands and applies only the proper frequency converted chrominance component signal to the mixing circuit 59.

The operation of the switching circuit 72 to select either signal C_a or signal $-C_a$ is controlled by the AND gate 138 in response to output signals from the flip-flops 71 and 137. The selected pattern of recording of the signals C_a and $-C_a$ is illustrated in Fig. 15 which shows a short length of the tape 79 with two adjacent tracks 139 and 140 recorded on it. The track 139 is shown with four line areas or increments 141—144 and the track 140 is shown with four line areas or increments 146—149 which are disposed so that the ends of the margins therebetween are aligned, transversely to the lengths of the tracks, with the adjacent ends of the margins between line areas 141—144, respectively, of the track 139. Each of the line areas 141—144 and 146—149 has two arrows in it, the larger of which indicates the polarity of the carrier of the frequency converted chrominance component recorded therein, and the smaller of which indicates the polarity of the carrier of the cross-talk interference signal, which is the frequency converted chrominance components signal in the next adjacent line area of the adjacent track.

Examination of track 139 indicates that all of the frequency converted chrominance component signals recorded therein have a carrier of the same polarity. This may be either the polarity of the signal C_a or of the signal $-C_a$. For the sake of simplifying the explanation it will be assumed that the polarity of the larger arrows in the track 139 indicates that the signal C_a is recorded in all of the line increments 141—144. In the track 140 the polarity of the carrier is reversed in alternate line areas or increments, that is, in line areas 146 and 148 the signal C_a is recorded and in line areas 147 and 149 the signal $-C_a$ is recorded.

In order to record the signals C_a and $-C_a$ in the pattern set forth in Fig. 15, the simple logic circuit involving the AND gate 138 is used. Line A of Fig. 16 shows the output signal P_a of the flip-flop 137 as being a square wave having high and low intervals, each equal to one line interval, or 1H. One complete cycle of the signal in line A of Fig. 16 thus has a fundamental frequency $1/2(f_h)$. The output signal of the flip-flop 71 is shown in line B of Fig. 16 as a square

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Since the AND gate 138 can produce a high output only when both of the applied signals P₁ and P₂ are high, the output of the AND gate, as is shown in line C of Fig. 16, remains low during one entire field interval T₁ and goes high only during alternate line intervals of the alternate field interval T₂. The pattern shown in Fig. 15 corresponds to having the arm of the switching circuit 72 apply the signal C_a to the low pass filter 136 when the output of the AND gate 138 is low and having the arm apply the signal -C_a to the low pass filter 136 when the output of the AND gate 138 is high.

Fig. 17 shows a playback apparatus for reproducing video signals recorded by the apparatus of Fig. 14. Many of the components in Fig. 14 are identical with those in Fig. 12 and others are identical with those in Fig. 14. Such identical components are indicated by the same reference numerals as in the earlier figures and descriptions of such elements and their operation will not be unnecessarily repeated.

The reproduced frequency converted chrominance signal separated by the low pass filter 108 and made up, alternately, of the signals C_a and C_b is applied to a balanced modulator 133 along with a signal from an oscillator 139. The signal from oscillator 139 has a frequency f_s+f_c and is constant during all line and field intervals. The phase comparator circuit 121 is connected to the oscillator 139 to control its operation.

The operation of the system in Fig. 17, insofar as the chrominance component signal is concerned, consists in applying the signal having the frequency f_s+f_c from the oscillator 139 to the balanced modulator 133 to convert the frequency f_c of the signals C_a and C_b which are applied alternately to the balanced modulator back to the original chrominance carrier frequency f_c. The two output terminals of the balanced modulator 133 provide signals of opposite polarity. One of them includes the desired signal C_a and the undesired or cross-talk signal C_{ab}, while the other includes the desired signal -C_a and the undesired or cross-talk signal -C_{ab}. The switching circuit 72 is controlled by the horizontal and vertical sync separators 65 and 69 and the respective flip-flop circuits 137 and 71 controlling the AND gate 138 to produce exactly the same switching pattern as is shown in line C of Fig. 16. As in previous playback systems, the waveform circuit 116 assures that the operation of the flip-flop 71 in the playback unit corresponds to the operation of the flip-flop 71 in the recording system of Fig. 14.

The output of the switching circuit 72 is applied to the comb filter 112. It will be recalled that the comb filter, as shown in Fig. 4A, includes both a direct signal path and a

path in which the signal is delayed by one horizontal line interval, these respective signal paths being applied to a subtractor. In the embodiment of Fig. 17 this subtractor is replaced by an adder. Thus, when the chrominance component signals of the track 139 of Fig. 15 are being reproduced, the desired chrominance component signals in two successive line areas 141 and 142 or 142 and 143 or 143 and 144 are combined with the polarities of their carriers being the same, at the output of the comb filter. However, the undesired or cross-talk components indicated by the small arrows in the line increments have carriers of opposite polarities in successive pairs of lines, and thus cancel each other when combined at the output of the comb filter 112. As a result, the output signal of the comb filter 112 in Fig. 17 during the reproduction of the track 139 consists substantially only of the desired chrominance components C_a having the proper carrier frequency f_c. During the reproduction of the track 139, the switching circuit 72 does not switch back and forth between its two input terminals but remains on only one terminal as indicated during the interval T₁ in Fig. 16.

During reproduction of the track 140, the switching circuit 72 does switch back and forth at the end of each line interval of time in accordance with the output signal of the AND gate 138 during the interval T₂ as indicated in line C of Fig. 16. Thus, the comb filter 112 receives the signals C_a and C_{ab} during one line interval, for example, corresponding to the line area 146, and the signals -C_a and -C_{ab} during the next succeeding line interval, for example, corresponding to the line area 147. This is the equivalent of inverting the signal received during the line interval that corresponds to the line area 147. Since the chrominance signal components recorded in line areas 146 and 147 have carriers with reversed polarities, respectively, such inverting of the signal reproduced from line area 147 causes the chrominance components signal reproduced from line area 147 to be combined, in phase, with the delayed chrominance component signal reproduced from line area 146 at the output of comb filter 112. However, since the chrominance component signals are recorded in all line areas of the next adjacent track 139 with carriers of the same polarity, the cross-talk signals from track 139 which are reproduced with the chrominance component signals recorded in the successive line areas of the track 140 also have carriers of the same polarity. Therefore, the above mentioned inverting of the signal reproduced from line area 147 of track 140 causes the cross-talk signal reproduced with the signal recorded in line area 147 to be combined, with its phase or polarity reversed, with the delayed cross-

talk signal reproduced with the signal recorded in line area 146, whereby the combined cross-talk signals cancel each other at the output of comb filter 112.

Although in the embodiments of the invention described above with reference to Figs. 3 and 7 and Figs. 11 and 12, it has been indicated that the comb filter 112 achieves suppression or elimination of cross-talk interference primarily by reason of the different frequency characteristics of the carriers with which the chrominance components signals are recorded in adjacent tracks, for example, the tracks 92 and 93 on Fig. 10, and although in the embodiment of the invention described above with reference to Figs. 14 and 17 it has been indicated that the comb filter 112 achieves suppression or elimination of cross-talk interference primarily by reason of the different polarity characteristics of the carriers with which the chrominance components signals are recorded in adjacent tracks, for example, the tracks 139 and 140 on Fig. 15, it is to be understood that, in both types of the described apparatus, the suppression or elimination of cross-talk or interference signals by comb filter 112 may result in differences in both the frequency and polarity characteristics of the carriers of the reproduced signals, either as actually reproduced or as supplied to the input of comb filter 112.

For example, in the case of the embodiment of Figs. 3 and 7, in which the carriers of the chrominance component signals, as recorded in adjacent tracks, have different frequencies of $f_c - 1/4(f_h)$ and $f_c + 1/4(f_h)$, respectively, it has already been indicated that the desired signal supplied from the frequency converter 109 to the input of the comb filter 112 has the carrier frequency f_s during each of the field intervals T_a and T_b , while the cross-talk signal, as supplied to the input of comb filter 112, has a carrier frequency $f_s - 1/2(f_h)$ during the field interval T_a and a carrier frequency of $f_s + 1/2(f_h)$ during the field interval T_b . Since f_s is related to f_h so that the phase or polarity of the carrier with the frequency f_s will not change in successive line intervals, it will be apparent that the carriers supplied to the input of comb filter 112 with the frequency $f_s \pm 1/2(f_h)$ will change polarity in successive line intervals. Accordingly, at the output of comb filter 112, the cross-talk signals with carrier frequencies of $f_s \pm 1/2(f_h)$ will be combined with opposite polarities, and hence will cancel each other so as to eliminate the cross-talk signals from the signals passed to mixing circuit 107.

In the case of the embodiment of Figs. 14 and 17, the frequency converted chrominance signals alternately recorded in the line areas of Fig. 15 have carriers with the same frequencies, when considered instantaneously. However, this is not the case when the carrier of the frequency converted chromin-

ance signals recorded in track 140, that is, during the field interval T_b on Fig. 16, is considered as a whole. This may be explained by considering a simplified situation in which signals C_a and $-C_a$, both of which have the carrier frequency f_a , are not modulated by chrominance components but are available at the two output terminals of the balanced modulator 133 as pure sine waves of opposite polarity. During the field interval T_b when signals C_a and $-C_a$ are selected alternately by the switching circuit 72, the output signal of the switching circuit is no longer a single signal but is a sine wave whose polarity reverses, or whose phase shifts 180° , at a repetition rate of $1/2(f_h)$. When a Fourier analysis is made of such a signal over a complete cycle of the interval of two horizontal lines, it will be found that the carrier frequency f_a is no longer present, but has been replaced by first upper and lower side bands spaced by $1/2(f_h)$ from the original carrier frequency and by additional upper and lower side bands spaced from the first mentioned side bands and from each other, in order, by f_h . Therefore, in effect, the single-pole, double-throw switching circuit 72 operates as a balanced modulator, and the modulating signal is the switching signal that takes two horizontal line intervals for a complete cycle and therefore has a frequency of $1/2(f_h)$. Being, in effect, a balanced modulator, the switching circuit 72 produces a balanced output signal without a carrier. This balanced output signal, since it interleaves with the signal C_a may be referred to as the signal C_{ab} and thus there is, in fact, an interleaving relationship between the carriers of the frequency converted carrier components of the signal recorded on the track 139 and that recorded on the track 140 in Fig. 15. Such interleaving relationship provides for an interleaving relationship between the previously referred to cross-talk or interference signals C_{ab} and $-C_{ab}$ and the desired signals C_a which further improves the cancellation of the cross-talk signals.

A possible modification of the apparatus in accordance with this invention, as described above, involves the changes necessary to record a television signal produced according to the PAL system. As is known, the chrominance carrier in the PAL system is offset from one of the high harmonics of the line frequency f_h by only $1/4(f_h)$ instead of $1/2(f_h)$, as in the NTSC system. Thus, in order to achieve an interleaving effect for recording signals of the PAL system, the difference between the carriers f_{cb} and f_{ca} (or F_{cb} and F_{ca}) must follow the equation:

$$f_{cb} - f_{ca} = \frac{1}{4}(2k-1)f_h.$$

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40, that is, Fig. 16, is be e... in which ch have the 70 modulated by available at be balanced of opposite al T_1 when 75 i alternately output signal ger a single ose polarity 180°, at a 80 n a Fourier gnal over a f two hori- nt, but has 85 lower side the original al upper and e first men- 90 other, in , the single- circuit 72 or, and the g signal that 95 for a com- frequency of d modulator, a balanced his balanced es with the 100 e signal C_0 , interleaving of the fre- quents of the 105 39 and that g. 15. Such for an inter- previously ence signals signals C_1 110 cillation of

apparatus in as described 115 ary to record ding to the chrominance et from one e frequency 120 $2(f_h)$, as in r to achieve g signals of between the F_{ca} must 125

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This relationship can be achieved using the recording apparatus disclosed in Figs. 3 and 11 (and their corresponding playback apparatus in Figs. 7 and 12). For the apparatus in Figs. 14 and 17, the pulsing signal applied during the interval T_1 must have a repetition rate of $1/4(f_h)$. This corresponds to recording two line intervals in one polarity and the succeeding two line intervals in the opposite polarity, and is consistent with the fact that the carrier of one of the chrominance components in a PAL television signal is inverted in alternate line intervals.

All of the embodiments of the invention are also capable of being used with a mechanical recording system in which one field interval is broken up to be recorded on more than one track or in which an entire frame interval may be recorded on a single track.

WHAT WE CLAIM IS:—

1. Apparatus for processing periodic information signals comprised of first intervals, each of which includes a predetermined number of second intervals, said second intervals being recorded in respective areas of successive, substantially parallel tracks on a record medium, the apparatus including a recording circuit including means for providing different first and second information-modulated carriers alternately; said recording circuit including selecting means and control means for the selecting means operative to cause the recording of the first and second information-modulated carriers, respectively, in tracks which are next adjacent each other.

2. Apparatus according to claim 1, in which the first and second information-modulated carriers have different polarity characteristics.

3. Apparatus according to claim 2, in which the polarity of the first information-modulated carrier is constant during successive second intervals of the information signals being recorded in one track, and the polarity of the second information-modulated carrier is reversed after a second predetermined number of second intervals of the information signals being recorded in the next adjacent track.

4. Apparatus according to claim 3, in which said means for providing said first and second information-modulated carriers includes a balanced modulator receiving the information signals and having first and second output signals of opposite polarity, said selecting means includes switching means for alternately passing the first and second output signals from the balanced modulator, and said control means in use actuates said switching means so that the latter continuously passes the first output signal during recording in said one track and passes the first and second output signals, alternately, during successive periods of said second predetermined number of said second intervals during recording in said other track.

5. Apparatus for processing periodic information signals comprised of first intervals, each of which includes a predetermined number of second intervals, said second intervals being recorded in respective areas of successive, substantially parallel tracks on a record medium, the apparatus including a recording circuit including means for providing two different signals to be used in deriving first and second information-modulated carriers to be recorded; selecting means for alternately selecting the two signals, deriving means for deriving respective first and second information-modulated carriers from said selected two signals and said information signals, and control means for the selecting means operative to cause the recording of the first and second information-modulated carriers, respectively in tracks which are next adjacent each other.

6. Apparatus according to claim 5, in which the first information-modulated carrier and side bands of the information signals thereon have different frequencies from the second information-modulated carrier and side bands of the information signals thereon and are in frequency-interleaving relationship therewith.

7. Apparatus according to claim 6, in which the information signals have an original carrier frequency which is in frequency-interleaving relationship to the repetition rate of the second intervals, and the different carrier frequencies of the first and second information-modulated carriers are also in frequency-interleaving relationships to the original carrier frequency and to the repetition rate of the second intervals.

8. Apparatus according to claim 6, in which the information signals have an original carrier frequency; said deriving means includes a frequency converter receiving the information signals with the original carrier frequency, and means for producing from said selected two signals first and second frequency converting signals which are supplied to the frequency converter for causing the latter to convert the carrier of the information signals from said original frequency to the carrier frequencies of the first and second information-modulated carriers, respectively.

9. Apparatus according to claim 8, in which said means for providing said two signals includes first and second oscillators the outputs of which are selectively supplied by the selecting means.

10. Apparatus according to claim 8, in which said means for providing the two signals includes an oscillator having an output used to derive one of the signals, and frequency-dividing and frequency-multiplying means for frequency-dividing the output frequency of the oscillator by a non-integral number; and in which said selecting means alternately connects the output of the oscillator and the output of the frequency-dividing and

frequency-multiplying means to the frequency converter.

11. Apparatus according to any one of the preceding claims, further comprising means for recording on the record medium control signals which are in predetermined positional relation to said tracks and which identify the tracks having first and second information-modulated carriers, respectively, recorded therein.

12. Apparatus according to any one of the preceding claims, in which the ends of the margins between successive areas in which said second intervals are recorded in each of said tracks are aligned, in the direction transverse to the lengths of the tracks, with the respective adjacent ends of the margins between the successive areas in which said second intervals are recorded in the next adjacent tracks.

13. Apparatus according to any one of the preceding claims, in which said successive parallel tracks are arranged without guard bands therebetween.

14. Apparatus according to any one of the preceding claims, in which said periodic information signals are chrominance signal components of color video signals which are comprised of field intervals and line intervals respectively constituting said first and second intervals.

15. Apparatus according to claim 14, wherein the first and second information-modulated carriers have the carrier frequencies $f_c - 1/4 f_h$ and $f_c + 1/4 f_h$, respectively, in which f_h is the line interval frequency and f_c is nf_h where n is an integer.

16. Apparatus according to claim 15, in which said video signals are NTSC color video signals, and said first and second information-modulated carriers have carrier frequencies that differ from each other by $1/2 (2k-1) f_h$, where k is an integer.

17. Apparatus according to claim 14, in which said video signals are PAL color video signals, and said first and second information-modulated carriers have carrier frequencies that differ from each other by $1/4 (2k-1) f_h$, where k is an integer and f_h is the line interval frequency.

18. Apparatus according to any one of claims 14 to 17 in which said color video signals also contain a luminance signal component to be recorded with the chrominance signal components; and further comprising means for frequency modulating said luminance signal component on a carrier prior to the recording of said video signals on the record medium, and said carrier frequencies of the first and second information-modulated carriers for the chrominance signal components are below the band of frequencies of the frequency modulated luminance signal component.

19. Apparatus according to claim 18, in which said record medium is magnetic, first

and second magnetic transducers are provided for recording the video signals in adjacent tracks, respectively, and said first and second transducers have gaps with substantially different azimuth angles.

20. Apparatus according to any one of claims 14, 15, 16, 18 and 19 when appended to claim 3, in which said video signals are NTSC color video signals, and in which the polarity of the first information-modulated carrier is constant during successive line intervals of the video signals recorded in one track, and the polarity of the second information-modulated carrier is reversed for successive line intervals of the video signals recorded in the next adjacent track.

21. Apparatus according to claim 20, in which said means for providing the first and second information-modulated carriers further includes means for separating horizontal synchronizing signals and vertical synchronizing signals from the video signals to be recorded, and said control means is operated by the separated horizontal and vertical synchronizing signals.

22. Apparatus according to any one of claims 14, 17, 18 and 19, when appended to claim 3, in which said video signals are PAL color video signals, the polarity of said first information-modulated carrier is constant during successive line intervals of the video signals being recorded in one track, and the polarity of said second information-modulated carrier is reversed after each two line intervals of the video signals being recorded in the next adjacent track.

23. Apparatus according to any preceding claim, further comprising a reproducing circuit comprising transducer means for reproducing information signals recorded in each of the tracks and simultaneously reproducing cross-talk signals from the tracks next adjacent thereto, and means for providing the information signals reproduced from each of said tracks with a common carrier and for eliminating the cross-talk signals therefrom on the basis of said different first and second information-modulated carriers which are recorded in the tracks which are next adjacent each other.

24. Apparatus according to claim 23, in which said means for eliminating the cross-talk signals includes a comb filter.

25. Apparatus according to claim 24 when appended to claim 7, in which the different carrier frequencies of the first and second information-modulated carriers are reconverted to the common carrier having a frequency which is the same as the original carrier frequency; and in which said comb filter has a frequency response characteristic with a peak response at the frequency of the common carrier and nodes spaced from the peak response at odd multiples of one-half the repetition rate of the second intervals, while

are provided in first and second substantially any one of an appended signals are in which the n-modulated cessive line rded in one the second reversed for video signals ck. claim 20, in the first and rriers further rizontal syn- ynchronizing be recorded, ated by the ynchronizing any one of appended to als are PAL of said first is constant f the video ck, and the n-modulated ine intervals l in the next y preceding reproducing as for repro- ed in each reproducing ext adjacent the informa- ach of said r and for herefrom on and second which are ext adjacent claim 23, in the cross-talk im 24 when the different and second :reconverted a frequency l carrier fre- filter has a with a peak the common n the peak one-half the ervals, while

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the cross-talk signals are reconverted to have carrier frequencies at the nodes so as to be eliminated by the comb filter.

26. Apparatus according to claim 23 when appended to claim 3, in which said means for providing the reproduced information signals with a common carrier and for eliminating the cross-talk signals includes processing means for the reproduced signals having a first output terminal at which processed signals are derived with the polarities of their information-modulated carriers as recorded and a second output terminal at which the information-modulated carriers of the processed signals are derived with inverted polarities, a comb filter having a delay equal to the duration of each of the second intervals, and switching means for continuously connecting said first output terminal of the processing means to the comb filter during the reproduction of the first information-modulated carrier and for alternately connecting the first and second output terminals of the processing means to the comb filter after each said second predetermined number of said second intervals of the information signals during the reproduction of the second information-modulated carrier.

27. Apparatus according to claim 23 when appended to claim 11, in which said reproducing circuit further comprises means for reproducing said control signals so as to identify the information-modulated carrier signals being reproduced by said transducer means, and said means for providing the reproduced information signals with said common carrier is controlled on the basis of said identifying control signals.

28. Apparatus according to claim 23, when appended to claim 18 or 19, in which said reproducing circuit further comprises filter means for separating the chrominance signal components from the luminance signal components in the reproduced signals; a frequency converter for providing the separated chrominance signal components of the video signals reproduced from each of the tracks with the common carrier; and a filter for said eliminating of the chrominance signal components of the cross-talk signals from the separated chrominance signal components on said basis of the different frequencies of the first and second information-modulated carriers which have been recorded in the tracks which are next adjacent to each other.

29. Apparatus according to claim 28 when appended to claim 19, in which said reproducing transducer means includes first and second magnetic reproducing transducers for reproducing the signals recorded by the first and second recording transducers, respectively, and the first recording and reproducing transducers have gaps with the same azimuth angles that are substantially different from the azimuth angles of the gaps of the second

recording and reproducing transducers so as to suppress the luminance signal components of the cross-talk signals.

30. Apparatus according to claim 28, when appended to claim 3, in which the said frequency converter for providing the separated chrominance signal components with a common carrier includes processing means for the chrominance signal components of the reproduced signals having a first output terminal at which processed signals are derived with the polarities of their information-modulated carriers as recorded and a second output terminal at which the processed signals are derived with inverted polarities, the filter is in the form of a comb filter having a delay period equal to one of the line intervals, and switching means are provided for continuously connecting the first output terminal of the processing means to the comb filter during the reproducing of video signals having the first information modulated carrier and for alternately connecting the first and second output terminals of the processing means to the comb filter after each said second predetermined number of the line intervals during the reproducing of video signals having the second information modulated carrier.

31. Apparatus for processing periodic information signals comprised of first intervals, each of which includes a predetermined number of second intervals, the second intervals having been recorded in respective areas of successive parallel tracks on a record medium with the information signals recorded in next adjacent tracks modulated onto different first and second carriers; the apparatus including a reproducing circuit including transducer means for scanning along the tracks one at a time so as to reproduce the information signals recorded in each of the tracks along with cross-talk signals from the tracks next adjacent thereto, and means for providing the information signals reproduced from each of said tracks with a common carrier and for eliminating the cross-talk signals therefrom on the basis of the different first and second carriers which have been modulated by the information signals prior to being recorded in the tracks which are next adjacent to each other.

32. Apparatus according to claim 31, in which said first and second carriers of the recorded information signals are in frequency interleaving relation to each other and to the repetition rate of the second intervals; and in which the means for providing the reproduced information signals with a common carrier and for eliminating said cross-talk signals includes a comb filter having a frequency characteristics to pass signals in the frequency spectrum of the common carrier, and frequency converting means receiving the reproduced information and cross-talk signals and being operative to convert the first and

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second carrier frequencies selectively, to the frequency of the common carrier for passage through the comb filter while converting the cross-talk signals to frequencies at nodes of said frequency characteristic of the comb filter so as to be eliminated by the latter.

33. Apparatus according to claim 31, in which said modulated first and second carriers of the recorded information signals have different polarity characteristics with the polarity of said first modulated carrier being constant and the polarity of said second modulated carrier being reversed after each second predetermined number of the second intervals of the information signals modulated onto said second carrier; and in which said means for providing the reproduced information signals with a common carrier and for eliminating the cross-talk signals includes processing means for the reproduced signals having a first output condition in which the processed signals are derived with the polarities of their respective carriers as recorded and a second output condition in which the processed signals are derived with inverted polarities, a comb filter with a delay-period equal to each of said second intervals and receiving said processed signals, and a switching device for continuously establishing said first output condition of the processing means during the reproducing of information signals modulated onto said first carrier and for alternately establishing said first and second output conditions of the processing means for said second predetermined number of said second intervals of the information signals during the reproducing of the latter modulated onto said second carrier.

34. Apparatus according to claim 31, 32 or 33, in which the ends of the margins between successive areas in which said second intervals have been recorded in each of said tracks are aligned, in the direction transverse to the lengths of the tracks, with the respective adjacent ends of the margins between the successive areas in which said second intervals have been recorded in the next adjacent tracks.

35. Apparatus according to any one of claims 31 to 34, in which control signals have also been recorded on the record medium in predetermined positional relation to said tracks so as to identify the tracks having information signals modulated onto said first and second carriers, respectively, and recorded therein; and in which said reproducing circuit further comprises means for reproducing said control signals, and means for controlling said means by which the reproduced information signals are provided with a common carrier on the basis of the reproduced identifying control signals.

36. Apparatus according to claim 31, in which said periodic information signals are the chrominance signal components of color video signals formed of field intervals and line

intervals respectively constituting said first and second intervals, and the color video signals further have luminance signal components which have also been recorded in said tracks with the frequency band of the luminance signal components, as recorded, being higher than those of said first and second modulated carriers of the chrominance signal components; and in which said reproducing circuit further comprises filters for separating the chrominance signal components from the luminance signal components in the reproduced signals.

37. Apparatus according to claim 36, in which the record medium is magnetic, the next adjacent tracks have had the video signals magnetically recorded therein with different azimuths, and said transducer means includes first and second reproducing magnetic transducers having gaps with different azimuths corresponding to the azimuths of the next adjacent tracks and respectively reproducing video signals recorded in the latter so as to suppress the luminance signal components of the cross-talk signals.

38. Apparatus according to claim 36, in which the modulated first and second carriers and respective side bands are in frequency interleaving relation to each other and to the line frequency and harmonics thereof; and in which a comb filter has a frequency transmission characteristic to pass signals in the frequency spectrum of the common carrier, and a frequency converter receives the separated chrominance signal components of the reproduced video signals and cross-talk signals and is operative to convert the modulated first and second carriers, selectively, to the common carrier frequency for passage through the comb filter while converting the cross-talk signals of the chrominance signal components to carrier frequencies at nodes of the frequency transmission characteristic of the comb filter so as to be blocked by the comb filter.

39. Apparatus according to claim 36, in which said first and second modulated carriers have different polarity characteristics with the polarity of said first modulated carrier being constant and the polarity of said second modulated carrier being reversed after every second predetermined number of line intervals of the video signals modulated onto said second carrier; and in which said means for providing the separated chrominance signal components with a common carrier and for eliminating therefrom the chrominance signal components of the cross-talk signals includes a signal processor for the chrominance signal components of the reproduced signals having a first output condition in which processed signals are derived with the polarities of their modulated carriers as recorded and a second output condition in which the processed signals are derived with inverted polarities, a comb filter having a delay period equal to one of

said first and video signals components said tracks the luminance being higher d modulated components; circuit further the chrominance luminance signals. claim 36, in magnetic, the video signals with different trans includes genetic trans-ent azimuths of the next reproducing iter so as to mponents of

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said line intervals and receiving said processed signals, and a switching control for continuously establishing said first output condition of the signal processor during the reproducing of video signals having the chrominance signal components modulated onto said first carrier and for alternately establishing said first and second output conditions of the signal processor after said second predetermined number of line intervals during the reproducing of video signals having the chrominance signal components thereof modulated onto said second carrier.

40. Apparatus according to claim 39, in which said second predetermined number is 1 when said video signals are NTSC color video signals and said second predetermined number is 2 when said video signals are PAL color video signals.

41. Apparatus according to claim 39 or 40, in which said switching control includes means for separating horizontal synchronizing signals and vertical synchronizing signals from the reproduced video signals, and control elements operated by the separated horizontal and vertical synchronizing signals for actuating a switch which determines the output condition of the signal processor.

42. Apparatus for processing periodic information signals, substantially as hereinbefore described with reference to, and as illustrated in, Figures 1 to 8 of the accompanying drawings.

43. Apparatus for processing periodic information signals, substantially as hereinbefore described with reference to, and as illustrated in, Figures 11 to 13 of the accompanying drawings.

44. Apparatus for processing periodic information signals substantially as hereinbefore described with reference to, and as illustrated in, Figures 14 to 17 of the accompanying drawings.

45. Apparatus according to claim 42, 43 or 44, including transducers substantially as hereinbefore described with reference to Figures 9 and 10 of the accompanying drawings.

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