

CMOS Analog Multiplying Circuit

5 This invention relates to a CMOS analog multiplying circuit which provides a current output whose magnitude is proportional to the product of the values of two input variables. CMOS stands for complementary metal-oxide-semiconductor structure.

10 Analog multiplying circuits are, of course, well known. One such circuit is described at pages 1158-1168 of IEEE Journal of Solid-State Circuits, Vol. SC-20, No.6, December 1985. This circuit, as do others, performs multiplication of variables which are present in the form of differential
15 voltages and can consequently be handled by amplifiers having a differential input. Such circuits are conceived to achieve high precision multiplication of input variables whose sign can be positive or negative, i.e. they are four-quadrant multipliers. Due to their working mechanisms, the input
20 variables have to be voltages whose DC component is of a predetermined value in order to bias correctly the differential input amplifiers. This fact and the fact that the input variables have to be present in the form of differential voltages constitute a drawback in application.
25 Also, to achieve four-quadrant multiplication with high precision, their complexity is high which results in relatively high manufacturing costs.

 It is thus desirable to produce a one-quadrant multiplier which does not necessarily achieve high precision,
30 which is of low complexity and consequently has low manufacturing costs.

 Accordingly, the invention provides a CMOS analog multiplying circuit comprising a first transistor having its current electrodes coupled between a first reference voltage
35 line and a first node and its gate electrode coupled to a first input node having, in use, an input voltage such that said first transistor operates in its triode region, a second transistor having its current electrodes coupled between said first node and an output node, and a comparator for comparing

a first voltage at said first node with a second voltage at a second input node and for controlling the gate electrode of said second transistor to keep said first and second voltages substantially equal, whereby the current through said second transistor is proportional to the product of the voltages at said first input and second input nodes.

In one embodiment of the invention, the comparator comprises a differential amplifier having its inverting input coupled to said first node and its non-inverting input coupled to said second input node and whose output is coupled to the gate of said second transistor.

In a second embodiment of the invention, the comparator comprises a long-tailed pair of transistors, the node formed by their source electrodes being coupled to a constant current source, the gate of the first of the transistors forming said long-tailed pair being coupled to said second input node, the gate of the second transistor forming said long-tailed pair being coupled to said first node, the drain of said first transistor of said long-tailed pair being coupled to the input of a current mirror whose output is coupled to the drain of the second transistor of said long-tailed pair, the drain of said second transistor of said long-tailed pair constituting the output of the comparator and being coupled to the gate electrode of said second transistor.

In a preferred embodiment of the invention, said output node is coupled to a second reference line via a current mirror.

It will be appreciated that the voltages applied to the input nodes may constitute the input variables or that one or both of them may result from an appropriate conversion of current to voltage if the variables to be multiplied are currents.

The invention will now be more fully described by way of examples with reference to the drawings of which:

Figure 1 shows a simplified version of a CMOS analog multiplying circuit according to the invention;

5 Figure 2 shows a preferred embodiment of the comparator used in the invention;

Figure 3 shows a variation of the circuit of Figure 1 used to produce an output current having a value between approximately zero and a predetermined value; and

10 Figure 4 shows a further variation of the circuit of Figure 1 for providing an output current which compensates for variations in the transconductance of further transistors.

Thus, there is shown in Figure 1 a simplified version
15 of a CMOS analog multiplying circuit according to the invention. This circuit comprises a first transistor 1 whose source electrode is coupled to a first voltage reference line and whose drain electrode is coupled to the source electrode of a second transistor 2 via node B, the
20 drain electrode of the second transistor 2 being coupled to an output node D. The gate electrode of the transistor 1 is coupled to a first input node C and the gate electrode of the transistor 2 is coupled to the output of a
comparator 3. Node B is coupled to the inverting input of
25 the comparator whereas node A is coupled to its non-inverting input.

The comparator 3 ensures that the voltage at node A and that at node B are kept substantially equal by controlling the gate of transistor 2. Due to the fact that
30 transistor 1 operates in triode region, for an input voltage V_C the current through transistor 1 will be proportional to $V_A \cdot V_C$ provided that the voltage V_C is noticeably higher than the threshold voltage of transistor 1. The current I_D through transistor 2 can
35 then be fed to other parts of the circuit by means of a current mirror formed by transistors 8 and 9 as shown in Figure 3.

If only relatively low precision has to be realised the circuit shown in Figure 2 can be used as comparator 3. This circuit comprises a pair of long-tailed transistors 4 and 5 whose gates are coupled to node B for transistor 5 and to node A for transistor 4. The common source of these transistors is supplied by constant current source 6. The drain of transistor 4 is coupled to the input of a current mirror 7 whose output representing the output of the comparator is coupled to the drain of transistor 5 and to the gate of transistor 2.

The circuit of Figure 1 may be used in a number of applications. One such application is shown in Figure 3 where the output current of the current mirror 8, 9 supplied by the current through transistor 2 can be adjusted to have any value between zero and a value predetermined by the current I_0 . In this arrangement, the input current I_0 is mirrored by a current mirror 13 to provide current I_1 through transistor 12. The voltage at node A will be proportional to the current I_0 when transistor 12 is biased by a supply voltage on the second reference line whose value is noticeably higher than the threshold voltage of transistor 12 so that it operates in its triode region. The input voltage V_0 is supplied to node C via a transistor 14 acting as a transmission gate element. The transistor 14 is coupled in parallel with a further transistor 16 connected as a diode and supplied by a current I_T . This configuration allows the voltage V_0 whose value varies between 0 and that of the supply voltage V_{DD} applied to the second reference line to control the value of the output current at node D in the range between approximately 0 and a value determined by I_0 regardless of the threshold voltage of transistor 1.

A second application of the circuit of Figure 1 is shown in Figure 4. In this case the circuit is used to control the transconductance of further transistors in the circuit by supplying them with a current whose value varies with process and temperature variations.

The transconductance g_m of a transistor whose current is described by

$$I = K(V - V_T)^2$$

can be expressed as

$$g_m = 2\sqrt{I \cdot K}$$

where K is a constant of the transistor depending on its geometry, on process parameters and on the temperature. V is the voltage on its gate electrode and V_T is its threshold voltage.

Changes of g_m due to process or temperature fluctuations can be compensated for by appropriate control of current I . A constant g_m can be achieved if current I varies inversely to K . Such a current I is generated by the circuit shown in Figure 4.

In this circuit the input current I_0 is constant or very nearly so. Currents I_1 and I_3 are provided by current mirrors 13 and 19 so that they are proportional to current I_0 . The voltage V_A at node A is given by

$$V_A \approx \frac{I_1}{2K_{12} (V_{DD} - V_T)}$$

Thus V_A is in good approximation proportional to $1/K_{12}$. In the same way V_C is given by

$$V_C \approx \frac{I_3}{2K_{17} (V_{DD} - V_T)} + V_T$$

Now, the value of the control current I_2 is given by

$$I_2 = K_1 [2(V_C - V_T) - V_A] V_A$$

For

$$\frac{I_1}{K_{12}} \ll \frac{2I_3}{K_{17}}$$

so that

$$I_2 \approx \left[\frac{I_1}{2(V_{DD} - V_T)} \right]^2 \frac{2K_1}{K_{12} K_{17}}$$

5 For transconductance g_{m18} of transistor 18 one can write

$$g_{m18} = 2 \sqrt{I_2 K_{18}} \approx \frac{I_1}{V_{DD} - V_T} \sqrt{\frac{K_1 K_{18}}{K_{12} K_{17}}}$$

10 For $V_{DD} \gg V_T$ we thus have that

$$g_{m18} \approx \frac{I_O}{V_{DD}} \sqrt{\frac{K_1 K_{18}}{K_{12} K_{17}}}$$

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Thus the transconductance of a transistor supplied with a current proportional to I_2 is then proportional to the square root of its own K-value multiplied by

$$20 \quad \sqrt{\frac{K_1}{K_{12} K_{17}}}$$

i.e. independent or very nearly independent of process and
25 or temperature variations.

The circuit thus mirrors current I_2 by means of transistors 8 and 9 and passes this mirrored current to transistor 18 or to other transistors not shown whose transconductance will now be held constant.

30 It has to be pointed out that the current I_2 which controls the transconductance of a transistor of type n (transistor 18) depends exclusively on the characteristics of transistors of the same conductivity type. For this reason the control does not depend on the ratio of
35 threshold voltages of the n and p type transistors.

Although the above description of the invention only describes how the multiplication of two parameters can be achieved by using n-channel MOS transistors which operate

in their triode regions, it is obvious that the same features can be realised converting the described circuits into their complementary ones, e.g. that the transistors n will be replaced by p-type transistors, the p-type ones by n-types inverting at the same time also the polarity of voltages.

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CLAIMS

- 5 1. A CMOS analog multiplying circuit comprising a first transistor having its current electrodes coupled between a first reference voltage line and a first node and its gate electrode coupled to a first input node having, in use, an input voltage such that said first transistor operates in its triode region, a second transistor having its
10 current electrodes coupled between said first node and an output node, and a comparator for comparing a first voltage at said first node with a second voltage at a second input node and for controlling the gate electrode of said second transistor to keep said first and second voltages substantially equal, whereby the current
15 through said second transistor is proportional to the product of the voltages at said first input and second input nodes.
2. A CMOS analog multiplying circuit according to claim 1 wherein the comparator comprises a differential amplifier having its
20 inverting input coupled to said first node, and its non-inverting input coupled to said second input node and whose output is coupled to the gate of said second transistor.
3. A CMOS analog multiplying circuit according to claim 1
25 wherein said comparator comprises a long-tailed pair of transistors, the node formed by their source electrodes being coupled to a constant current source, the gate of the first of the transistors forming said long-tailed pair being coupled to said second input node, the gate of the second transistor forming said long-tailed pair
30 being coupled to said first node, the drain of said first transistor of said long-tailed pair being coupled to the input of a current mirror whose output is coupled to the drain of the second transistor of said long-tailed pair, the drain of said second transistor of said long-tailed pair constituting the output of the comparator and being
35 coupled to the gate electrode of said second transistor.



4. A CMOS analog multiplying circuit according to any preceding
claim wherein said output node is coupled to a second reference
5 voltage line via a current mirror.

5. A CMOS analog multiplying circuit according to any preceding
claim wherein at least one of said input nodes is coupled to the
output node of a current source and is coupled, directly or indirectly,
10 to the drain of a third transistor whose source is coupled to said first
reference voltage line and whose gate is coupled to a second
reference voltage line on which, in use, the voltage is such that said
third transistor operates in its triode region.

15 6. A CMOS analog multiplying circuit according to claim 5
wherein said at least one input node is coupled directly to the drain
of said third transistor.

7. A CMOS analog multiplying circuit according to claim 5
20 wherein said at least one input node is coupled to the gate and to
the drain of a further transistor whose source is coupled to the drain
of said third transistor.

8. A CMOS analog multiplying circuit according to any one of
25 claims 1 to 4 wherein at least one of said input nodes is connected to
an auxiliary input node via an auxiliary transistor whose drain and
gate are connected to said at least one input node and are supplied
by a further current source, and said at least one input node being
further coupled to said auxiliary input node via a complementary
30 transistor forming an element of a transmission gate.

9. A CMOS analog multiplying circuit substantially as
hereinbefore described with reference to any one of the Figures of
the drawings.
