

Description

The present invention relates to bypass devices for relieving pressure on inflatable packers in a tool string.

In testing a well formation, a testing string is lowered into a well bore such that packers are positioned above and below the formation to be tested. The packers are typically of the inflatable type and a pump in the testing string is actuated for pumping fluid to inflate the packers into sealing engagement with the well bore for isolation of the formation. When testing is completed, it is necessary to bypass or vent the fluid in the packers back to the well annulus so that the testing string may be moved to a different location in the well bore or removed therefrom.

A typical packer used is the Halliburton Hydroflate (trade mark) packer which is described in Halliburton Services Catalog 43, pages 2537-2538. The pump previously used with this packer has a built-in packer bypass which releases fluid from the packers when pull is exerted on the bypass from the surface. We have now devised an improved such packer bypass.

US-A-4424860 describes a pressure equalising and packer deflating valve apparatus useful in an inflatable packer straddle testing system, which comprises case means defining a central opening therethrough; piston means reciprocally disposed in said central opening of said case means and movable between a first position and a second position; and mandrel means disposed in said central opening of said case means and having a bypass position for providing communication between said packer and a well annulus and further having a sealed position preventing communication between said packer and said well annulus.

According to the present invention, there is provided a packer bypass apparatus for use in a testing string with a pump and an inflatable packer, said apparatus comprising: case means defining a central opening therethrough; piston means reciprocally disposed in said central opening of said case means and movable between a first position and a second position; mandrel means disposed in said central opening of said case means and having a bypass position for providing communication between said packer and a well annulus and further having a sealed position preventing communication between said packer and said well annulus; characterised by pivotable latching means in operative association with said piston means for latchingly engaging said mandrel means when said mandrel means is in said sealed position and said piston means is in said second position, whereby said mandrel means may be moved from said sealed position to said bypass position by moving said

piston means from said second position to said first position.

One particular problem with certain prior known packer bypass units is that overpull on the tester valve can result in premature actuation of the packer bypass with resulting premature deflation of the packers. In accordance with a preferred feature of the present invention, this problem can be reduced or avoided by using a mandrel having a pressure differential thereacross which requires approximately 10,000 pounds pull (44,000N) to actuate during a packer deflation operation. This force is greatly more than is needed to operate the tester valve. Thus, even if there is some overpull on the tester valve, premature actuation of the packer bypass is not likely to occur.

The mandrel in the packer of the present invention is preferably automatically released when in a bypass position so that it can reclose if pump pressure is reapplied. In this way, the packer bypass may be used for sequential tests with the testing string.

The packer bypass of the present invention is used to vent fluid from an inflatable packer used in a testing string so that the packer will deflate, allowing movement of the testing string within the well bore. The packer bypass comprises latching means in operative association with the piston means for latchingly engaging the mandrel means when the mandrel is in the sealed position and the piston means is in the second position. After latching, the mandrel means may be moved from the sealed position to the bypass position thereof by moving the piston means from the second position to the first position. Releasing means are preferably provided for disengaging the latching means and releasing the mandrel means when in the bypass position. The mandrel means may be moved back from the bypass position to the sealed position in response to a differential pressure between the pump and well annulus acting across a differential area defined by a portion of the mandrel means.

The packer bypass also preferably includes overpull prevention means for preventing actuation of the piston until a predetermined force is overcome. The overpull prevention means may, for example, be characterized by annular shoulder means on the mandrel means, and the shoulder means is exposed to pump pressure on one side thereof and well annulus pressure on an opposite side thereof, resulting in a predetermined force acting on the mandrel means which must be overcome before the mandrel means can be moved to the bypass position.

Pressure balancing means is also preferably included in the packer bypass for balancing pressure between the case means and the piston

means for minimizing downward force on the packer. The pressure balancing means can comprise a recess defined in the case means and annular shoulder means on the piston means extending into the recess such that a cavity is formed therebetween with an upper portion in communication with the pump and the lower portion in communication with the well annulus.

In a preferred embodiment, the packer bypass further comprises inner flow tube means disposed in the case means such that an annular flow passageway is defined between the case means and flow tube means. The piston means has an annular portion disposed in the flow passageway, and the mandrel means is characterized by a generally annular mandrel disposed in the flow passageway.

The latching means preferably comprises a releasable latch assembly with at least one latch pivotally attached to the lower portion of the piston means. The latch may comprise a lower end having a latching position and a release position and biasing means for biasing the lower end of the latch toward the latching position. The latch is preferably one of a plurality of angularly spaced latches, and the biasing means includes at least one garter spring disposed around the latches. The releasing means comprises a tapered surface in the case means for engaging an upper end of the latch and pivoting the lower end of the latch to the released position.

Sealing means are provided for sealing between the mandrel means and the flow tube means when the mandrel means is in the bypass position such that the flow passageway is separated into upper and lower portions. The mandrel means comprises check valve means for venting the upper portion of the flow passageway through a bypass passageway in the mandrel means when a differential pressure between the upper portion of the flow passageway and the well annulus exceeds a predetermined level.

The packer bypass of the present invention is used as a portion of a downhole testing tool which includes a pump attached to an upper testing string portion and an inflatable packer disposed below the pump and positionable adjacent the well formation to be tested. The packer bypass is disposed between the pump and packer and allows communication between the pump and packer when the mandrel means is in the sealed position and vents the pump through the upper portion of the flow passageway to the well annulus and vents the packer through the lower portion of the flow passageway to the well annulus when the mandrel means is moved to the open position.

One feature of the present invention is the provision of a packer bypass having a bypass mandrel therein which may be selectively posi-

tioned between a bypass position for venting a packer to a well annulus and a sealed position preventing such venting.

In order that the invention may be more fully understood, one embodiment thereof will now be described by way of example only, with reference to the accompanying drawings, in which:

FIGS. 1A-1B show the embodiment of packer bypass of the present invention as part of a testing string in position in a well bore for testing a well formation.

FIGS. 2A-2D show a partial longitudinal cross section of the packer bypass in a closed, sealed position.

FIG. 3 is a side elevation of a latching assembly used in the packer bypass.

FIG. 4 is a cross section taken along lines 4-4 in FIG. 3.

FIG. 5 shows an elevation of a lower end of a flow tube in the packer bypass.

FIGS. 6A-6D show the packer bypass in a position in which a piston therein is latched to a bypass mandrel and ready for actuation from the closed position to the open position.

FIGS. 7A-7D show a partial longitudinal cross section of the packer bypass in an open, bypassing position.

Referring now to the drawings, and more particularly to FIGS. 1A-1B, the packer bypass is shown and generally designated by the numeral 10. Packer bypass 10 forms part of a testing apparatus or tool 12. Testing apparatus is shown in position in a well bore 14 for use in testing a well formation 16.

Testing apparatus 12 is attached to the lower end of the tool string 18 and includes a reversing sub 20, a tester valve 22 such as the Halliburton Hydrospring® tester, an extension joint 24, and a pump 26 of a type having a pressure limiter means 28, all of which are positioned above packer bypass 10.

Disposed below packer bypass 10 is a string bypass 30 and a safety joint 32. An upper packer 34 is attached to the lower end of safety joint 32 and is disposed above well formation 16. String bypass 30 is used for bypassing fluid around upper packer 34 as tool string 18 is lowered into, or raised out of, well bore 14. A lower packer 36 is positioned below well formation 16. A porting sub 38 interconnects upper packer 34 and lower packer 36. Spacers (not shown) may also be used between upper packer 34 and lower packer 36 depending upon the longitudinal separation required therebetween.

Pump 26 is preferably a positive displacement pump and is used to inflate upper packer 34 and lower packer 36 in a manner known in the art such that the packers may be placed in sealing engage-

ment with well bore 14, thus isolating well formation 16 as shown in FIGS. 1A-1B so that a testing operation may be carried out.

A gauge carrier 40 is attached to the lower end of lower packer 36 and includes a plurality of drag springs 42 which are adapted to engage well bore 14 and prevent rotation of a portion of testing apparatus 12 during inflation of upper packer 34 and lower packer 36.

A well annulus 44 is defined between testing apparatus 12 and well bore 14, and when upper packer 34 and lower packer 36 are inflated into sealing engagement with well bore 14, it will be seen that well annulus 44 is divided into an upper portion 46 above upper packer 34 and a lower portion 48 below lower packer 36. Both upper portion 46 and lower portion 48 of well annulus 44 are sealingly separated from well formation 16 by the packers.

Referring now to FIGS. 2A-2D, packer bypass 10 is shown in a closed, sealed position. This is preferably the position in which the apparatus is set as testing apparatus 12 is lowered into well bore 14. However, as will be further discussed herein, packer bypass 10 may also be run into well bore 14 in an open, bypass position.

The major components of packer bypass 10 include a case means 50 with a central opening 52 therethrough, mandrel means 54 disposed in a lower end of central opening 52, and piston means 56 having a lower portion reciprocally disposed in central opening 52 of case means 50 above mandrel means 54.

Referring to FIG. 2B, the upper end of case means 50 is formed by a hydraulic case 58 having an upper end with a first bore 60 therein. Hydraulic case 58 also has a second bore 62 outwardly spaced from first bore 60. A downwardly facing, annular shoulder 64 extends between first bore 60 and second bore 62. A transverse hole 66 provided communication between second bore 62 and well annulus 44.

The lower end of hydraulic case 58 is connected to an upper end of a splined nipple 68 at threaded connection 70.

Referring now to FIG. 2C, the lower end of splined nipple 68 is connected to bypass case 72 at threaded connection 74. Seal 76 insures sealing engagement between splined nipple 68 and bypass case 72.

The lower end of bypass case 72 is connected to the upper end of bottom adapter 78 at threaded connection 80.

As shown in FIG. 2D, bottom adapter 78 has an externally threaded lower end 82 which is adapted for connection to the portion of testing string 12 below packer bypass 10. The lower end of bottom adapter 78 also has an internally threaded portion

84 into which is threadedly engaged the lower end 86 of inner flow tube 88.

Inner flow tube 88 acts as an inner flow tube means and extends through the entire length of packer bypass 10 including central opening 52 of case means 50. As shown in FIGS. 2A and 2B, inner flow tube 88 extends upwardly and outwardly of the case means into piston means 56. It will be seen in FIGS. 2B-2D that case means 50 and inner flow tube 88 define a generally annular flow passageway 90 therebetween. Thus, mandrel means 54 and the substantially annular lower end of piston means 56 are disposed in annular passageway 90.

Referring again to FIGS. 2A and 2B, the upper end of piston means 56 includes a top adapter 92 having an internally threaded portion 94 adapted for attachment to the portion of testing apparatus 12 which is above packer bypass 10. Top adapter 92 has a central bore 96 therein with a plurality of lugs 98 extending radially inwardly therefrom. The lower end of top adapter 92 is connected to hydraulic piston 100 at threaded connection 102. A seal 104 provides sealing between top adapter 92 and hydraulic piston 100.

Positioned above hydraulic piston 100 in top adapter 92 is an upper seal mandrel 106. The lower end of seal mandrel 106 includes a radially outwardly extending flange 108 which is longitudinally positioned between lugs 98 in top adapter 92 and upper end 110 of hydraulic piston 100. The upper end of seal mandrel 106 includes seals 112 and is adapted for engagement with a mandrel (not shown) of a kind known in the art which is in the portion of testing apparatus 12 above packer bypass 10.

Upper seal mandrel 106 has a first bore 114 through the upper end thereof and a second bore 116 outwardly spaced from first bore 114. Second bore 116 is in close, spaced relationship with first outside diameter 118 of inner flow tube 88. Seals 120 provide sliding, sealing engagement between upper seal mandrel 106 and inner flow tube 88.

It will be seen that upper seal mandrel 106 is spaced inwardly from central bore 96 of top adapter 92 such that an annular cavity 122 is defined therebetween. Similarly, first outside diameter 118 of inner flow tube 88 is spaced inwardly from central bore 124 of hydraulic piston 100 such that an annular cavity 126 is defined therebetween throughout the length of hydraulic piston 100. At least one annularly disposed hole 128 extends in a generally longitudinal direction through flange 108 of upper seal mandrel 106 and provides communication between annular cavity 122 and annular cavity 126.

Referring now to FIG. 2B, seals 130 provide sealing engagement between the upper end of hydraulic case 58 and first outside diameter 134 of

hydraulic piston 100. The lower end of hydraulic piston 100 has a second outside diameter 136 which is radially outwardly spaced from first outside diameter 134 and is in close, spaced relationship with second bore 62 of hydraulic case 58. Seals 138 and 140 provide sliding, sealing engagement between hydraulic piston 100 and second bore 62 of hydraulic case 58. It will be seen that hydraulic piston 100 thus has an upwardly facing shoulder 142 between first outside diameter 134 and second outside diameter 136, and shoulder 142 faces shoulder 64 in hydraulic case 58. In the position shown in FIG. 2B, shoulder 142 is in contact with shoulder 64.

Hydraulic piston 100 has at least one substantially transverse hole 144 therethrough. In the preferred embodiment, the central axis of hole 142 is in substantially the same transverse plane as shoulder 140 on hydraulic piston 100.

The lower end of hydraulic piston 100 is attached to the upper end of splined mandrel 146 at threaded connection 148. A seal 150 provides sealing engagement therebetween.

Splined mandrel 146 has a central bore 152 therethrough which is substantially the same diameter as central bore 124 of hydraulic piston 100. Thus, it will be seen that annular cavity 126 continues below hydraulic piston 100 and along the entire length of splined mandrel 146.

Splined mandrel 146 has an outside diameter 154, and seals 156 provide sliding, sealing engagement between outside diameter 154 and the upper end of splined nipple 68. Extending radially outwardly from outside diameter 154 of splined mandrel 146 are a plurality of splines 158 which are engaged with inwardly extending splines 160 in splined nipple 68. It will be seen that the engagement of splines 158 and 160 prevents relative rotation between piston means 56 and case means 50 while allowing relative longitudinal movement therebetween.

Outside diameter 154 of splined mandrel 146 is spaced radially inwardly from second bore 62 of hydraulic case 58. Thus, a substantially annular hydraulic piston chamber 162 is defined radially between outside diameter 154 of splined mandrel 146 and second bore 62 of hydraulic case 58, and longitudinally between bottom face 164 of hydraulic piston 100 and top face 166 of splined nipple 68. Transverse hole 66 through hydraulic case 58 thus provides communication between piston chamber 162 and well annulus 44.

Referring now to FIG. 2C, a latching means, generally designated by the numeral 168, is shown. Latching means 168 includes a latching assembly mandrel 170 which is attached to the lower end of splined mandrel 146 at threaded connection 172.

Referring also to FIG. 3, latching assembly

mandrel 170 includes a plurality of angularly spaced, substantially longitudinal slots 174 therein. A substantially annular latch support flange 176 extends radially outwardly on latching assembly mandrel 170. It will be seen that latch support flange 176 is located at an intermediate position along slots 174, and slots 174 extend through latch support flange 176. An elongated latching finger 178 with a body portion 180 is disposed in each slot 174. In the preferred embodiment, three slots 174 and three latching fingers 178 are used. However, the apparatus is not limited to this configuration.

Body portion 180 of each latching finger 178 defines a hole 182 therethrough which is aligned with a pair of other holes 184 through latch support flange 176 of latching assembly mandrel 170, as best shown in FIG. 4. The central axis of each pair of holes 184 intersects flange 176 in a chord-like manner. A pivot pin 186 is disposed through each corresponding set of holes 182 and 184 such that latching finger 178 is pivotally mounted in slot 174 with pivot pin 186 defining a point of pivotation.

The upper end of each latching finger 176 above pivot pin 186 has a chamfered outer surface which tapers inwardly toward the top. In the uppermost position of piston means 56 with respect to case means 50 as shown in FIGS. 2A-2D, chamfered surface 188 of latching finger 178 engages a corresponding chamfered inner surface 190 at the lower end of splines 160 in splined nipple 68 such that the upper end of each latching finger 178 is pivoted inwardly. The lower end of each latching finger 178 below pivot pin 186 is correspondingly pivoted outwardly.

Latching finger 178 also includes an outwardly facing notch 192 below pivot pin 186. A biasing means, such as a plurality of garter springs 194, is positioned around latching fingers 178 and in notches 192 therein. It will be seen that garter springs 194 tend to bias the lower end of latching fingers 178 radially inwardly.

The lower end of each latching finger 178 has an inwardly extending latching tooth 196 with an inwardly facing notch 198 above and adjacent tooth 196. The lower side of each tooth 196, and thus of each latching finger 178, includes a tapered surface 200 which tapers inwardly toward the top.

As seen in FIGS. 2A-2C, first outside diameter 118 of inner flow tube 88 is substantially constant through the entire length of piston means 56. A second diameter 202 of inner flow tube 88 is larger than first diameter 118. Second outside diameter 202 includes a plurality of wrenching flats 204 thereon which are used when installing lower end 86 of the inner flow tube into threaded portion 84 of bottom adapter 78 of case means 50.

Inner flow tube 88 also has a third outside

diameter 206 which, in the position of packer bypass 10 shown in FIGS. 2A-2D, is longitudinally located between latching means 168 and mandrel means 54. Third outside diameter 206 is shown in FIG. 2C and is larger than second diameter 202 of inner flow tube 88. Inner flow tube 88 also has a fourth outside diameter 208 which is smaller than third outside diameter 206 and extends therebelow. A downwardly facing chamfer 210 on inner flow tube 88 interconnects third outside diameter 206 and fourth outside diameter 208 thereof.

Referring again to FIGS. 2C and 2D, mandrel means 54 is preferably characterized by an elongated, substantially annular mandrel 212 which is annularly disposed between inner flow tube 88 and case means 50. In the position shown in FIGS. 2C-2D, mandrel 212 is in a lowermost position in which a lower end 214 thereof engages upwardly facing shoulder 216 in bottom adapter 78 of case means 50. It will thus be seen that when piston means 56 is in the uppermost position shown in FIGS. 2A-2D, mandrel 212 is spaced below latching fingers 178.

The upper end of mandrel 212 includes a relatively small diameter neck section 218 with a radially outwardly extending flange 220 at the top thereof. Flange 220 is adapted to be engaged by teeth 196 and notches on latching fingers 178 as hereinafter described.

Below neck portion 218, mandrel 212 has a first outside diameter 222 which is in close, spaced relationship to inner bore 224 of bypass case 72. Seals 226 insure sliding, sealing engagement between mandrel 212 and bypass case 72. Bypass case 72 has a transverse hole 228 therethrough which is always located below seals 226, regardless of the position of mandrel 212 within case means 50.

Mandrel 212 has a second outside diameter 230 which is smaller than first outside diameter 222 such that a downwardly facing shoulder 231 is formed. Second outside diameter 230 is in close, spaced relationship to first bore 232 in bottom adapter 78. Upper seals 234 located at the upper end of bottom adapter 78 provide sealing engagement between the bottom adapter and second outside diameter 230 of mandrel 212. It will be seen that seals 234 are fixedly positioned below transverse hole 228 in bypass case 72.

A set of intermediate seals 236 are spaced below upper seals 234 and also seal on second outside diameter 230 of mandrel 212. An annular recess 238 extends outwardly from first bore 232 of bottom adapter 78. Recess 238 is longitudinally positioned below intermediate seals 236. A transverse hole 240 provides communication between recess 238 and well annulus 44. A set of lower seals 242 is positioned below recess 238 and also provides sealing engagement between bottom

adapter 78 and second outside diameter 230 of mandrel 212.

Mandrel 212 has first and second check valve ports 244 and 246 angularly disposed therein. First and second check valve ports 244 and 246 are preferably angularly displaced from one another about a central longitudinal axis of packer bypass 10 at approximately 180°. A first ball check valve 248 is positioned in first check valve port 244, and a first valve retainer 250 is threaded into the first check valve port to hold the first ball check valve in place and act as a seat therefor. A first check valve spring 252 biases first ball check valve 248 into sealing engagement with first valve retainer 250. Similarly, a second ball check valve 254 is held in place by, and normally seated against, a second valve retainer 256 which is threaded into second check valve portion 246, and a second check valve spring 258 biases second ball check valve 254 into sealing engagement with second valve retainer 256.

Extending downwardly from first check valve port 244 below first ball check valve 248 is a substantially longitudinal port 260 with a transverse port 262 intersecting the lower end thereof. It will be seen that, in the position of mandrel 212 shown in FIGS. 2C and 2D, transverse port 262 opens toward first bore 232 of bottom adapter 78 of case means 50 at a longitudinal position between upper seals 234 and intermediate seals 236.

Extending downwardly from second check valve port 246 below second ball check valve 254 is an angularly disposed port 264. It will be seen that port 264 opens on the radially inner side of mandrel 212 toward inner flow tube 88.

Mandrel 212 has a first bore 266, a second bore 268 spaced radially inwardly from first bore 266, and a third bore 270 larger than second bore 268. A sealing means, such as a set of inner seals 272 is disposed on second bore 268 of mandrel 212. In the position shown in FIGS. 2C and 2D, it will be seen that seals 272 are radially outwardly spaced from fourth outside diameter 208 of inner flow tube 88 so that there is no sealing engagement between the inner flow tube and mandrel 212. It will also be seen that inner seals 272 are positioned above the intersection of angularly disposed port 264 with second bore 268 of mandrel 212.

A substantially transverse hole 274 extends through mandrel 212 from third bore 270 thereof. In the position shown in FIGS. 2C and 2D, hole 274 is positioned below lower seals 242 in bottom adapter 78 of case means 50.

Referring now to FIGS. 2D and 5, the lower end of inner flow tube 88 is shown. Inner flow tube 88 includes a fifth outside diameter 276 which is generally adjacent and facing annular recess 278 in bottom adapter 78. A recess or notch 280 is

formed in fifth outside diameter 276 of inner flow tube 88, and it will be seen that this insures fluid communication between recess 278 and annular passageway 90 along second bore 282 of bottom adapter 78. Another flow passageway 284 formed in fifth outside diameter 276 and threaded portion 86 of inner flow tube 88 insures fluid communication between annular recess 278 and the components of testing apparatus 12 attached below packer bypass 10, including upper packer 34 and lower packer 36. As will be discussed in greater details herein, communication is thus provided to the packers for inflation and deflation thereof.

Inner flow tube 88 further includes a second bore 285 at the lower end thereof. Second bore 285 is adapted for receiving a mandrel (not shown) of a kind known in the art which is included in the portion of testing apparatus 12 below packer bypass 10.

Operation Of The Invention

As testing apparatus 12 is lowered into well bore 14 on tool string 18, packer bypass 10 is preferably in the position shown in FIGS. 2A-2D. That is, piston means 56 is in the uppermost position with respect to case means 50, and mandrel means 54 is in the lowermost position with respect to case means 50. When testing apparatus 12 is in the position shown in FIGS. 1A and 1B with upper packer 34 and lower packer 36 located properly with respect to well formation 16, pump 26 is operated to inflate the packers. Fluid is pumped from well annulus 44 downwardly through an annular passageway in testing apparatus 12. A part of this annular passageway passes through packer bypass 10 and includes annular cavity 122, hole 128, annular cavity 126, an upper portion 286 of annular passageway 90 above mandrel 212, annular space 288 between mandrel 212 and inner flow tube 88, a lower portion 290 of annular passageway 90 below mandrel 212, notch 280, recess 278 and flow passageway 284.

When fluid is being pumped from pump 26 to packers 34 and 36 through packer bypass 10, first and second ball check valves 248 and 254 are in their closed positions. It will be seen that transverse hole 228 through bypass case 72 of case means 50 is sealed by seals 226 on mandrel 212 and upper seals 234 on bottom adapter 78. Thus, fluid communication between annular passageway 90 in packer bypass 10 and well annulus 44 through hole 228 is prevented.

Similarly, transverse hole 240 in bottom adapter 78 of case means 50 is sealed by intermediate seals 236 and lower seals 242 on bottom adapter 78, again preventing fluid communication between annular passageway 90 and well annulus 44

through hole 240.

Once upper packer 34 and lower packer 36 are inflated, a test on well formation 16 may be carried out in a manner known in the art. After the test, it is necessary to deflate packers 34 and 36 so that testing apparatus 12 may be removed from well bore 14 or moved to another position in the well bore for testing a different well formation. To accomplish this, weight is set down on testing string 18 so that piston means 56 is moved downwardly with respect to case means 50 to the position shown in FIGS. 6A-6D. As this occurs, of course, splines 158 on splined mandrel 146 slide downwardly with respect to splines 160 in splined nipple 68.

As soon as latching fingers 178 are moved below chamfered surface 190 in splined nipple 68, garter springs 194 act to pivot the lower ends of latching fingers 178 inwardly. Over-pivotation is prevented by the contact of inner surface 292 of latching fingers 178 with outer surface 294 of latching assembly mandrel 170, as best shown in FIG. 6C.

When piston means 56 and latching means 168 are moved to the lowermost position shown in FIGS. 6C and 6D, chamfered surface 200 on the lower end of each latching finger 178 engages flange 220 on the upper end of mandrel 212 so that the lower ends of the latching fingers are again pivoted outwardly until all teeth 196 pass below flange 220, at which point garter springs 194 will snap the lower ends of latching fingers 178 inwardly, so that the latching fingers are in a latching position with teeth 196 thereon positioned below flange 220 on mandrel 212, and flange 220 extends into notch 198 on each latching finger 178.

Downward movement of piston means 56 with respect to case means 50, and thus the downward movement of latching means 168 with respect to mandrel means 54, is limited by the engagement of lower end 296 of top adapter 92 with upper end 298 of hydraulic case 58. This is best seen in FIG. 6A.

Further, as piston means 56 is moved downwardly with respect to case means 50, fluid in piston chamber 162 is displaced through hole 66 in hydraulic case 58 to well annulus 44. In other words, the volume of piston chamber 162 is reduced. Simultaneously, an upper piston chamber 300 is annularly formed between hydraulic piston 100 and hydraulic case 58 and longitudinally between the shoulder 64 on hydraulic case and shoulder 142 on the hydraulic piston. The volume of upper piston chamber 300 increases as piston means 56 is moved downwardly. Fluid is allowed to enter upper piston chamber 300 through hole 144 in hydraulic piston 100.

Once latching means 168 is latchingly engaged with mandrel means 54, the mandrel means may

be raised to an open, bypassing position by lifting on tool string 18 and thus raising piston means 56, and mandrel means 54 latched thereto, with respect to case means 50. When piston means 56 is returned to the uppermost position thereof at which point shoulder 142 on hydraulic piston 100 again contacts shoulder 64 in hydraulic case 58, mandrel means 54 is raised to the uppermost position thereof, as best shown in FIGS. 7A-7D.

It will be seen by those skilled in the art that downwardly facing shoulder 231 defines an annular differential area on mandrel 212 with pump pressure thereabove and well annulus pressure therebelow. Shoulder 231 is preferably sized such that, prior to upward movement of mandrel 212, an upward pull of approximately 10,000 pounds (44,000N) on tool string 18 is required to move the mandrel. Upward movement of tool string 12 is required during a testing operation to actuate tester valve 22, and obviously, it would be undesirable to prematurely relieve the pressure in packers 34 and 36. Therefore, this requirement of 10,000 pounds (44,000N) overpull provides an overpull prevention means so that packer bypass 10 cannot be inadvertently opened during a normal test.

As piston means 56, and mandrel means 54 latched thereto, are moved upwardly, seals 272 on mandrel 212 sealingly engage third outside diameter 206 of inner flow tube 88. This causes second ball check valve 254 to open to maintain an equal pressure in upper portion 286 and lower portion 290 of annular passageway 90.

As transverse port 262 in mandrel 212 is moved above upper seals 234 on bottom adapter 78 of case means 50, first ball check valve 248 will open. As this occurs, the pressure in annular flow passageway 90 will drop rapidly to well annulus pressure, and the force required to raise mandrel 212 will drop accordingly since the pressure across the annular area of shoulder 231 will be essentially balanced.

Continued upward movement of piston means 56 and mandrel 212 will stop when shoulder 142 on hydraulic piston 100 engages shoulder 64 in hydraulic case 58. At this point, piston means 56 and mandrel means 54 are in the position shown in FIGS. 7A-7D. Chamfered surface 188 on latching fingers 178 again contacts chamfered surface 190 at the lower end of splined nipple 68, acting as a releasing means so that the lower end of latching fingers 178 are again pivoted radially outwardly such that teeth 196 are disengaged from flange 220 on mandrel 212.

In the raised position of mandrel 212, it will be seen that annular cavity 231 between second outside diameter 230 of mandrel 212 and inner bore 224 of bypass case 72 is enlarged. Transverse port 262 at the lower end of longitudinal port 260 is

raised above upper seals 234 and placed in communication with annular cavity 231 and hole 228 in bypass case 72, and thus also in communication with well annulus 44.

First check valve 252 stays open, and pump pressure above mandrel 212 is bypassed through packer bypass 10 past first ball check valve 248 and through longitudinal port 260, transverse port 262, annular cavity 231 and hole 228 to well annulus 44.

Simultaneously, transverse hole 274 in mandrel 212 is raised to a position between intermediate seals 236 and lower seals 242 in bottom adapter 78 of case means 50. In this position, transverse hole 274 is thus placed in communication with recess 238 and hole 240 in bottom adapter 78, and thus in communication with well annulus 44.

Because of the sealing engagement of inner seals 272 with third outside diameter 206 of inner flow tube 88, lower portion 290 of annular passageway 90 below inner seals 272 is sealingly separated from upper portion 286 of annular passageway 90 above mandrel 212. In other words, annular space 288 is closed off.

The pressure in packers 34 and 36 is relieved upwardly through the portion of testing apparatus 12 below packer bypass 10 and through flow passageway 284, recess 278, notch 280 to lower portion 290 of annular passageway 90 below inner seals 272. Thus, the inflation chambers of packers 34 and 36 are in communication with hole 274 in mandrel 212, recess 238 and hole 240 in bottom adapter 78, and thus are in bypassing, deflating communication with well annulus 44.

After deflation of packers 34 and 36 by bypassing through packer bypass 10 as above described, testing apparatus 12 may be moved within well bore 14. If it is desired to retest well formation 16 or move testing apparatus 12 for testing another well formation, packer bypass 10 will automatically reset to the position shown in FIGS. 2A-2D when pump pressure is applied by pump 26. As fluid pressure in upper portion 286 of annular passageway 90 above mandrel 212 increases, the pump pressure acting upon the top of mandrel 212 will cause the mandrel to move downwardly to its lowermost position. First check valve spring 252 and second check valve spring 258 are sized such that first ball check valve 248 and second ball check valve 254, respectively, will not open before mandrel 212 is repositioned in the downwardmost, closed position. Once mandrel 212 is again at the downwardmost position, the entire cycle may be repeated.

It will be seen, therefore, that the packer bypass of the present invention is well adapted to carry out the ends and advantages mentioned, as well as those inherent therein. While a presently

preferred embodiment of the invention has been described for the purposes of this disclosure, numerous changes in the arrangement and construction of parts may be made by those skilled in the art, without departing from the invention claimed in the following claims.

Claims

1. A packer bypass apparatus (10) for use in a testing string (18) with a pump (26) and an inflatable packer, said apparatus comprising: case means (50) defining a central opening (52) therethrough; piston means (56) reciprocally disposed in said central opening of said case means and movable between a first position and a second position; mandrel means (54) disposed in said central opening of said case means and having a bypass position for providing communication between said packer and a well annulus and further having a sealed position preventing communication between said packer and said well annulus; characterised by pivotable latching means (168) in operative association with said piston means for latchingly engaging said mandrel means when said mandrel means is in said sealed position and said piston means is in said second position, whereby said mandrel means may be moved from said sealed position to said bypass position by moving said piston means from said second position to said first position.
2. Apparatus according to claim 1, further comprising releasing means (188,190) for disengaging said latching means and releasing said mandrel means when in said bypass position.
3. Apparatus according to claim 1 or 2, wherein said mandrel means is movable from said bypass position to said sealed position in response to a differential pressure between said pump and said well annulus acting across a portion of said mandrel means.
4. Apparatus according to claim 1,2 or 3, further comprising overpull prevention means (231) for preventing movement of said mandrel means until a predetermined force is overcome.
5. Apparatus according to claim 4, wherein said overpull prevention means is characterized by a differential area on said mandrel means, said area being exposed to pump pressure on one side thereof and well annulus pressure on an opposite side thereof.

6. Apparatus according to any of claims 1 to 5, further comprising pressure balancing means (162,300) for balancing pressure between said case means and said piston means for minimizing downward force on said packer.
7. Apparatus according to any of claims 1 to 6, further comprising inner flow tube means (88) disposed in said case means such that an annular flow passageway (90) is defined between said case means and said flow tube means; wherein said piston means has an annular portion disposed in said flow passageway; and said mandrel means is characterized by a generally annular mandrel disposed in said flow passageway.

Patentansprüche

1. Packerumgehungsvorrichtung (10) zur Verwendung in einem Prüfstrang (18) mit einer Pumpe (26) und einem aufblasbaren Packer, enthaltend Gehäusemittel (50), die eine durchgehende Mittelöffnung (52) bestimmen; Kolbenmittel (56), die hin- und herbeweglich in der Mittelöffnung der Gehäusemittel angeordnet und zwischen einer ersten Stellung und einer zweiten Stellung verstellbar sind; und in der Mittelöffnung der Gehäusemittel angeordnete Dornmittel (54), die eine Umgehungsstellung zur Herstellung einer Verbindung zwischen dem Packer und einem Bohrlochringraum und ferner eine abgedichtete Stellung einnehmen, in der sie eine Verbindung zwischen dem Packer und dem Bohrlochringraum verhindern, gekennzeichnet durch den Kolbenmitteln wirkungsmäßig zugeordnete, schwenkbare Riegelmittel (168), die verriegelnd an den Dornmitteln angreifen, wenn sich die Dornmittel in der abgedichteten Stellung und die Kolbenmittel in der zweiten Stellung befinden, wodurch die Dornmittel aus der abgedichteten Stellung dadurch in die Umgehungsstellung bewegt werden können, daß die Kolbenmittel aus der zweiten Stellung in die erste Stellung verstellt werden.
2. Vorrichtung nach Anspruch 1, ferner gekennzeichnet durch Freigabemittel (188, 190) zur Lösung der Riegelmittel und Freigabe der Dornmittel, wenn diese sich in der Umgehungsstellung befinden.
3. Vorrichtung nach Anspruch 1 oder 2, dadurch gekennzeichnet, daß die Dornmittel aus der Umgehungsstellung unter Ansprechen auf einen Differenzdruck zwischen der Pumpe und dem Bohrlochringraum, der einem Teil der

preferred embodiment of the invention has been described for the purposes of this disclosure, numerous changes in the arrangement and construction of parts may be made by those skilled in the art, without departing from the invention claimed in the following claims.

Claims

1. A packer bypass apparatus (10) for use in a testing string (18) with a pump (26) and an inflatable packer, said apparatus comprising: case means (50) defining a central opening (52) therethrough; piston means (56) reciprocally disposed in said central opening of said case means and movable between a first position and a second position; mandrel means (54) disposed in said central opening of said case means and having a bypass position for providing communication between said packer and a well annulus and further having a sealed position preventing communication between said packer and said well annulus; characterised by pivotable latching means (168) in operative association with said piston means for latchingly engaging said mandrel means when said mandrel means is in said sealed position and said piston means is in said second position, whereby said mandrel means may be moved from said sealed position to said bypass position by moving said piston means from said second position to said first position.
2. Apparatus according to claim 1, further comprising releasing means (188,190) for disengaging said latching means and releasing said mandrel means when in said bypass position.
3. Apparatus according to claim 1 or 2, wherein said mandrel means is movable from said bypass position to said sealed position in response to a differential pressure between said pump and said well annulus acting across a portion of said mandrel means.
4. Apparatus according to claim 1,2 or 3, further comprising overpull prevention means (231) for preventing movement of said mandrel means until a predetermined force is overcome.
5. Apparatus according to claim 4, wherein said overpull prevention means is characterized by a differential area on said mandrel means, said area being exposed to pump pressure on one side thereof and well annulus pressure on an opposite side thereof.

6. Apparatus according to any of claims 1 to 5, further comprising pressure balancing means (162,300) for balancing pressure between said case means and said piston means for minimizing downward force on said packer.

7. Apparatus according to any of claims 1 to 6, further comprising inner flow tube means (88) disposed in said case means such that an annular flow passageway (90) is defined between said case means and said flow tube means; wherein said piston means has an annular portion disposed in said flow passageway; and said mandrel means is characterized by a generally annular mandrel disposed in said flow passageway.

Patentansprüche

1. Packerumgehungsvorrichtung (10) zur Verwendung in einem Prüfstrang (18) mit einer Pumpe (26) und einem aufblasbaren Packer, enthaltend Gehäusemittel (50), die eine durchgehende Mittelöffnung (52) bestimmen; Kolbenmittel (56), die hin- und herbeweglich in der Mittelöffnung der Gehäusemittel angeordnet und zwischen einer ersten Stellung und einer zweiten Stellung verstellbar sind; und in der Mittelöffnung der Gehäusemittel angeordnete Dornmittel (54), die eine Umgehungsstellung zur Herstellung einer Verbindung zwischen dem Packer und einem Bohrlochringraum und ferner eine abgedichtete Stellung einnehmen, in der sie eine Verbindung zwischen dem Packer und dem Bohrlochringraum verhindern, gekennzeichnet durch den Kolbenmitteln wirkungsmäßig zugeordnete, schwenkbare Riegelmittel (168), die verriegelnd an den Dornmitteln angreifen, wenn sich die Dornmittel in der abgedichteten Stellung und die Kolbenmittel in der zweiten Stellung befinden, wodurch die Dornmittel aus der abgedichteten Stellung dadurch in die Umgehungsstellung bewegt werden können, daß die Kolbenmittel aus der zweiten Stellung in die erste Stellung verstellt werden.
2. Vorrichtung nach Anspruch 1, ferner gekennzeichnet durch Freigabemittel (188, 190) zur Lösung der Riegelmittel und Freigabe der Dornmittel, wenn diese sich in der Umgehungsstellung befinden.
3. Vorrichtung nach Anspruch 1 oder 2, dadurch gekennzeichnet, daß die Dornmittel aus der Umgehungsstellung unter Ansprechen auf einen Differenzdruck zwischen der Pumpe und dem Bohrlochringraum, der einem Teil der



Dornmittel anliegt, in die abgedichtete Stellung bewegbar ist.

4. Vorrichtung nach Anspruch 1, 2 oder 3, weiter gekennzeichnet durch Mittel (231) zur Verhinderung von übermäßigem Zug, die eine Verstellung der Dornmittel verhindern, bis eine vorgegebene Kraft überwunden ist. 5
5. Vorrichtung nach Anspruch 4, dadurch gekennzeichnet, daß die übermäßigen Zug verhin- 10 dernden Mittel eine Differenzfläche an den Dornmitteln bilden, die auf einer Seite dem Pumpdruck und auf der Gegenseite dem Druck im Bohrlochringraum ausgesetzt ist. 15
6. Vorrichtung nach einem der Ansprüche 1 bis 5, ferner gekennzeichnet durch Druckausgleichsmittel (162, 300) zum Ausgleich des Drucks zwischen den Gehäusemitteln und den Kolbenmitteln zur Minimierung der nach unten gerichteten Kraft auf den Packer. 20
7. Vorrichtung nach einem der Ansprüche 1 bis 6, weiter gekennzeichnet durch Rohrmittel (88) für den Innendurchfluß, die in den Gehäusemit- 25 teln angeordnet sind, derart, daß ein ringförmiger Durchflußkanal (90) zwischen den Gehäusmitteln und den Rohrmitteln bestimmt ist, einen ringförmigen, in dem Durchflußkanal angeordneten Teil der Kolbenmittel und Dornmit- 30 tel, die einen allgemein ringförmigen, in dem Durchflußkanal angeordneten Dorn bilden.

Revendications

1. Appareil (10) bipasse de packer destiné à être 35 utilisé dans un train d'essai (18) comprenant une pompe (26) et un packer gonflable, cet appareil comprenant : un moyen formant (50) 40 boîtier définissant une ouverture centrale (52) qui le traverse ; un moyen (56) formant piston disposé mobile en translation alternative dans cette ouverture centrale du moyen formant boî- 45 tier et pouvant se déplacer entre une première position et une seconde position ; un moyen (54) formant mandrin disposé dans l'ouverture centrale du moyen formant boîtier et pouvant 50 prendre une position de bipasse pour établir la communication entre le packer et un annulaire du puits et pouvant prendre en outre une position de fermeture étanche qui empêche la communication entre le packer et l'annulaire du puits et étant caractérisé par des moyens 55 de verrouillage pivotants (168) en association fonctionnelle avec le moyen formant piston pour entrer en prise par verrouillage avec le moyen formant mandrin lorsque ce moyen for-

mant mandrin se trouve dans la position fermée à joint étanche et que le moyen formant piston se trouve dans sa seconde position, de sorte que le moyen formant mandrin peut être amené de la position fermée à joint étanche à la position de bipasse par déplacement du moyen formant piston de la seconde position à la première position.

2. Appareil selon la revendication 1, comprenant en outre des moyens de relâchement (188, 190) servant à dégager ce moyen de verrouillage et à libérer le moyen formant mandrin lorsqu'il se trouve dans la position de bipasse.
3. Appareil selon la revendication 1 ou 2, dans lequel ce moyen formant mandrin peut être amené de la position de bipasse à la position de fermeture à joint étanche en réponse à une pression différentielle entre la pompe et l'annulaire du puits qui agit de part et d'autre d'une position du moyen formant mandrin.
4. Appareil selon la revendication 1, 2 ou 3, comprenant en outre un moyen (231) de prévention de la traction excessive destiné à empêcher le moyen formant mandrin de se déplacer avant qu'une force prédéterminée n'ait été surmontée.
5. Appareil selon la revendication 4, dans lequel le moyen de prévention de traction excessive est caractérisé par une surface différentielle prévue sur le moyen formant mandrin, cette surface étant exposée à la pression de la pompe sur un côté et à la pression de l'annulaire du puits sur le côté opposé.
6. Appareil selon une quelconque des revendications 1 à 5, comprenant en outre des moyens (162, 300) d'équilibrage de la pression, servant à équilibrer la pression entre le moyen formant boîtier et le moyen formant piston afin de réduire à un minimum la force descendante exercée sur le packer.
7. Appareil selon une quelconque des revendications 1 à 6, comprenant en outre un moyen (88) formant tube d'écoulement intérieur, disposé dans le moyen formant boîtier de manière qu'un passage d'écoulement annulaire (90) soit défini entre le moyen formant boîtier et le moyen formant tube d'écoulement ; dans lequel le moyen formant piston possède une partie annulaire disposée dans le passage d'écoulement ; et le moyen formant mandrin étant caractérisé par un mandrin de forme générale annulaire disposé dans le passage



* C L M S *

d'écoulement.

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