

Workup of a CDON/CDOL mixture by means of a “holed” dividing wall column

The invention relates to a process for removing a cyclododecanone-rich fraction from a dehydrogenation mixture comprising low boilers, cyclododecanone, medium

5 boilers, cyclododecanol and high boilers.

Butadiene is used hereinafter as a short name for the substance 1,3-butadiene, CAS No. 106-99-0.

10 CDT is used hereinafter as an abbreviation for the substance 1,5,9-cyclododecatriene, CAS No. 4904-61-4.

CDEN is used hereinafter as an abbreviation for the substance cyclododecene, CAS No. 1501-82-2.

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CDAN is used hereinafter as an abbreviation for the substance cyclododecane, CAS No. 294-62-2.

CDON is used hereinafter as an abbreviation for the substance cyclododecanone, CAS No. 830-13-7.

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CDOL is used hereinafter as an abbreviation for the substance cyclododecanol, CAS No. 1724-39-6.

25 CDOL t.q. stands for CDOL in technical-grade quality and refers to a mixture containing 75 to 85% by weight of CDOL and 10 to 20% by weight of CDON.

Oxime is used hereinafter as a short name for the oxime of CDON, CAS No. 9466-89-4.

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Lauro lactam is the trivial name of azacyclotridecan-2-one, CAS No. 947-04-6.

Lauro lactam is the starting material of the production of the high-performance polymer nylon-12. Lauro lactam is obtainable on the industrial scale via the following route: butadiene, which is obtained in mineral oil processing, is converted by means of catalytic cyclotrimerization to CDT. Hydrogenation of CDT gives CDAN. Oxidation of CDAN with (atmospheric) oxygen results in a mixture of CDOL and CDON. This mixture is subjected to a dehydrogenation which converts the CDOL present in the mixture to CDON. A dehydrogenation mixture comprising principally CDON is obtained. In addition, the dehydrogenation mixture comprises unconverted CDOL and further components. High-purity CDON is separated from the dehydrogenation mixture. The high-purity CDON is oximated to its oxime. The oxime is subsequently reacted with sulphuric acid to give lauro lactam.

The overall process is described with further evidence in Oenbrink, G. and Schiffer, T. 2009. Cyclododecanol, Cyclododecanone, and Lauro lactam. Ullmann's Encyclopedia of Industrial Chemistry. DOI: 10.1002/14356007.a08_201.pub2.

The invention is concerned with the workup of the CDON/CDOL-containing dehydrogenation mixture with the aim of obtaining high-purity CDON therefrom.

The dehydrogenation mixture obtained by the route described above comprises, as well as CDON and CDOL, further components in the form of low boilers, medium boilers and high boilers.

"Low boilers" in the context of this invention are substances or substance mixtures which have a lower boiling point than CDON under the same pressure conditions and are therefore enriched in the distillate in the course of distillative separation of a mixture of low boilers and CDON. The significant low boilers in this connection are: cyclododecene (CDEN), cyclododecane (CDAN), dodecanal, cyclododecane

epoxide. Cyclododecane epoxide is at the limit of the above definition of the low boilers, since its boiling point of about 150°C at 40 mbar corresponds virtually to that of CDON and it is therefore virtually inseparable in an economically viable manner from the CDON. Smaller amounts (less than 100 ppm) of the low boilers acetic acid and decane are also present, but these are barely of any relevance for the separation tasks.

“Medium boilers” in the context of this invention are substances or substance mixtures which, under the same pressure conditions, have a higher boiling point than CDON and a lower boiling point than CDOL, and are therefore enriched in the middle of the column in the course of distillative separation of a mixture of CDON, medium boilers and CDOL. A medium boiler in this connection is particularly dodecan-1-ol. The fraction of the medium boilers is accompanied by further organic substances which have not been characterized exactly to date.

“High boilers” in the context of this invention are substances or substance mixtures which, under the same pressure conditions, have a higher boiling point than CDOL and therefore remain in the residue in the distillative separation of a mixture of high boilers and CDOL. The high boiler limit is at about 180°C and a pressure of 46 mbar. The high boilers include especially cyclododecanediol. In addition, the fraction of the high boilers comprises further organic substances which have not been characterized specifically to date.

The dehydrogenation of CDOL to CDON has been described in documents DE1568317 and DE1248650. These describe dehydrogenation mixtures containing 74 to 89% by weight of CDON and 25.9 to 21.8% by weight of CDOL. The remaining fraction of the dehydrogenation mixture prepared is accounted for by low boilers and medium boilers. The workup of the dehydrogenation mixture is not described any further.

Japanese patent application JP05-000977A discloses a process for preparing high-purity CDOL from a CDON/CDOL mixture. During the distillative workup of the mixture, a small proportion of alkaline components is added to the mixture to be separated. A dividing wall column is not utilized for workup of the mixture.

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The oxidation of CDAN to an oxidation mixture comprising CDAN and CDOL is described in GB930842. The processing steps which follow are not described.

DE2031782 describes a process for selective preparation of CDON, in which CDAN
10 is oxidized in order to obtain a mixture of CDON and CDOL. The mixture is worked up by distillation, but without more specific description of the distillation operation.

WO2009/092682 discloses a process for workup of a CDON/CDOL-containing mixture, which is worked up with the aid of a dividing wall column. In this process,
15 however, the medium boiler is the main component of the feed, while the low and high boilers are unwanted by-products.

The processing of a laurolactam-containing mixture in a dividing wall column is mentioned in EP2336112A1. Here too, the feed to the dividing wall column consists
20 predominantly of medium boilers.

The CDON used for the preparation of laurolactam should be present in a form of maximum purity, since accompanying components cause lasting damage to the polymers in the nylon-12. These secondary components arise particularly during the
25 oxidation of the CDAN and also during the dehydrogenation of the CDOL.

With regard to this prior art, the problem addressed by the invention is that of specifying a process for workup of a mixture comprising low boilers, CDON, medium boilers, CDOL and high boilers, in which a fraction consisting of CDON of maximum

purity is obtained. The plant for performance of this process should entail a minimum level of capital costs.

This problem is solved by a process having the features of claim 1.

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The invention therefore provides a process for removing a cyclododecanone-rich fraction from a dehydrogenation mixture comprising low boilers, cyclododecanone, medium boilers, cyclododecanol and high boilers, which comprises the following steps:

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- a) providing the dehydrogenation mixture;
- b) distillatively removing the low boilers from the dehydrogenation mixture to obtain a first mixture comprising cyclododecanone, medium boilers, cyclododecanol and
15 high boilers;
- c) feeding the first mixture into a dividing wall column having a left-hand column section and a right-hand column section, in which the two column sections are partly divided by a dividing wall which extends along the dividing wall column such
20 that the top and bottom of the two column sections are combined, and in which a permeable connection between the two column sections which bypasses the dividing wall is provided at a separation stage disposed between the top and bottom;
- 25 d) drawing off the cyclododecanone-rich fraction from the top of the dividing wall column;
- e) drawing off a second mixture comprising cyclododecanone, cyclododecanol and medium boilers from a side draw of the dividing wall column;

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- f) drawing off a fraction comprising cyclododecanol and high boilers from the bottom of the dividing wall column.

The core of the present invention is the use of a "holed" dividing wall column having a permeable connection between the two column sections. The term "hole" in this connection should not be understood in such a way that the dividing wall necessarily has an orifice. Instead, the term "hole" should be understood in the figurative sense, as a connection between the two column sections which allows mass transfer from a point in one column section to the other, which is otherwise prevented by the dividing wall.

Because of this connection, the holed dividing wall column constitutes an integrated construction of two series-connected side draw columns with combined tops and bottoms. The advantage of this combination is the possibility of dispensing with one condenser and one vaporizer overall, such that the holed dividing wall column entails lower capital costs than an equivalent combination of two individual columns. The comparison between the inventive dividing wall column with a "hole" and an arrangement of two sidestream columns with combined top and bottom streams, which is equivalent for separation purposes but more costly, is illustrated in detail by Figures 3 and 4.

In a preferred embodiment of the invention, the first mixture is fed into the left-hand column section of the dividing wall column and the second mixture is drawn off in the right-hand column section from a side draw therein. The connection therefore constitutes a withdrawal on the feed side and an additional feed on the withdrawal side.

In a further preferred embodiment of the invention, the permeable connection is designed to transport liquid medium boilers between the two column sections. The

connection in this case constitutes a liquid connection between the two column sections.

In order to ensure that exclusively liquid substances switch column sides via the permeable connection, the connection should originate at a liquid collector in the left-hand column section. Liquid collectors are commonly known in distillation technology and serve primarily to collect the liquid flowing away from a bed of structured or random packing and to apply it to a liquid distributor which distributes the liquid homogeneously over a bed below. Optionally, a portion of the collected liquid can be withdrawn as a side draw. The connection between the two column sections is thus conventionally drawn off as a side stream on the left and applied like a feed on the right. The requirement that exclusively a liquid stream is exchanged between the two column sections is also a reason why the inventive dividing wall column does not necessarily have a hole in the dividing wall, since a simple hole is also permeable to gaseous media.

In a very particularly preferred embodiment of the invention, the permeable connection is positioned such that it originates at the separation plane of the left-hand column section at which the liquid concentration of the medium boilers in the left-hand column section is at a maximum, and such that the permeable connection opens at the separation plane of the right-hand column section at which the composition of the liquid phase corresponds as far as possible to that of the liquid stream withdrawn from the left-hand column section. This means that, in the left-hand section of the dividing wall column, the medium boilers are concentrated to a few per cent and tapped off at the concentration peak, and this stream is fed back in again on the right-hand side via the connection. On the right-hand side, the column can then be operated with an increased reflux ratio, such that the medium boilers can be concentrated to high values of up to 40% and withdrawn in the side stream.

Preferably, the dividing wall column is run under reduced pressure, i.e. at a pressure below 1 bar absolute. More particularly, the pressure within the dividing wall column should be below 50 mbar absolute.

- 5 The diameter ratio of the right-hand column section to the left-hand column section and the number of any internals in the two column sections should be selected such that the desired flow conditions are established in the two column sections, taking account of the equivalence of the hydraulic resistance for gases.
- 10 Preferably, the process according to the invention serves for workup of a dehydrogenation mixture having the following composition which adds up to 100%:

Low boilers (LB): 1 to 8% by weight, preferably 3% by weight;

Cyclododecanone (CDON): 60 to 90% by weight, preferably 70% by weight;

- 15 Medium boilers (MB): 0 to 1.5% by weight, preferably 1% by weight;

Cyclododecanol (CDOL): 10 to 40% by weight, preferably 24% by weight;

High boilers (HB): 0.1 to 2.5% by weight, preferably 2% by weight.

- The process preferably serves to obtain a cyclododecanone-rich fraction having a particularly high purity. According to the invention, this fraction should have a CDON content of at least 98%, preferably even a target CDON content of 99.5% by weight. In addition, the cyclododecanone-rich fraction drawn off at the top of the dividing wall column should as far as possible be free of CDOL, high boilers and medium boilers. The fraction drawn off at the bottom of the dividing wall column should accordingly be
- 20
- 25 very substantially free of CDON.

If the process according to the invention is used in the course of a laurolactam process, the step of "providing the dehydrogenation mixture" comprises the following component steps:

g) oxidation of cyclododecane with oxygen to obtain an oxidation mixture comprising low boilers, cyclododecanone, medium boilers, cyclododecanol and high boilers;

5 h) distillatively removing a cyclododecanol-rich fraction from the oxidation mixture, said fraction having been depleted of high boilers;

i) dehydrogenating the cyclododecanol-rich fraction to obtain the dehydrogenation mixture.

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If the process according to the invention is part of a lauro lactam process, it is advisable to recycle the bottoms from the dividing wall column into step h). This is because this bottom fraction comprises a large portion of CDOL, which can be made available again to the dehydrogenation operation and converted to CDON in this way. The high boilers are concentrated up to a limiting concentration and are circulated therewith. The high boilers newly introduced into the process via the oxidation leave the process again via the bottom of the preliminary separator column and via the side draw of the dividing wall column.

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20 The top product of the dividing wall column is high-purity CDON, which is of excellent suitability to be oxidized and then processed further to give lauro lactam. The second mixture provided by the dividing wall column can either be worked up further in order to obtain pure CDON and/or CDOL (for example by batch distillation) or utilized thermally. In the simplest case, the latter is accomplished by combustion. The
25 tangible heat can optionally be tapped off beforehand.

The invention also provides the dividing wall column used in the process as such.

This is an apparatus for the distillative workup of substance mixtures into three fractions, comprising a space which is surrounded by a shell and is divided into a left-
30 hand column section, a right-hand column section, a bottom and a top, in which a

dividing wall which separates the left-hand column section from the right-hand column section extends through the dividing wall column within the shell between the bottom and top, and in which a feed for the introduction of the substance mixture, a draw at the top for the removal of the first fraction, a draw at the bottom for the removal of the second fraction and a side draw for the removal of the third fraction are provided, and in which a permeable connection between the two column sections is disposed between the top and bottom. The inventive apparatus thus has a combined top and a combined bottom.

- 10 The permeable connection between the two column sections is preferably disposed outside the shell of the apparatus. The connection is preferably a draw from the left-hand side and a feed for the right-hand side.

Further advantageous features of this apparatus are apparent from the description and the examples.

The invention further provides for the use of this apparatus for workup of a substance mixture comprising low boilers, CDON, medium boilers, CDOL and high boilers.

- 20 The invention is now to be illustrated in detail by working examples. These show:

- Figure 1: Process flow diagram;
- Figure 2: Detail view of dividing wall column;
- Figure 3: Concentration profiles within the dividing wall column;
- 25 Figure 4: Equivalence diagram of the dividing wall column.

The overall workup operation is shown in Figure 1. It commences in an oxidation 1 in which CDAN is oxidized with oxygen. This gives an oxidation mixture 2 comprising low boilers LB, CDON, medium boilers MB, CDOL and high boilers HB. On the basis of the reaction mechanism, the CDON content within the oxidation mixture 2 is much

lower than the CDOL content. Typically, such an oxidation mixture 2 contains about 15% by weight of CDON and about 70% by weight of CDOL.

The oxidation mixture 2 is fed into a preliminary separator column 3. The function of this preliminary separator column 3 is to discharge a large proportion of the high boilers HB. This is done via the bottom. CDOL t.q. is drawn off via the top of the preliminary separator column 3. CDOL t.q. contains about 84% by weight of CDOL and 13% by weight of CDON. CDOL t.q. constitutes a separate saleable product and can optionally be discharged from the process via a branch 4.

For the laurolactam preparation, CDOL t.q. is subjected to a dehydrogenation 5. This dehydrogenates CDOL to CDON, such that the proportion of these two substances is reversed. The dehydrogenation mixture O drawn off from the dehydrogenation 5 typically has the following composition which adds up to 100%:

Low boilers (LB):	1 to 8% by weight, preferably 3% by weight;
Cyclododecanone (CDON):	60 to 90% by weight, preferably 70% by weight;
Medium boilers (MB):	0 to 1.5% by weight, preferably 1% by weight;
Cyclododecanol (CDOL):	10 to 40% by weight, preferably 24% by weight;
High boilers (HB):	0.1 to 2.5% by weight, preferably 2% by weight.

The dehydrogenation mixture O is then fed into a low boiler column 6. The purpose of the low boiler column 6 is to remove the low boilers LB by overhead distillation out of the dehydrogenation mixture O, such that a first mixture ABC1 comprising CDON, medium boilers MB, CDOL and high boilers HB is obtained at the bottom of the low boiler column 6. The low boilers LB are preferably removed completely in this step. The special feature of the bottom product ABC1 is that its content of medium boilers MB is extremely low, namely only about 1% by weight. For the rest, the mixture ABC1 consists essentially of CDON, CDOL and high boilers HB. A typical composition of the mixture ABC1 is as follows:

Low boilers (LB): 0 to 1% by weight, preferably 0% by weight;

Cyclododecanone (CDON): 60 to 90% by weight, preferably 70% by weight;

Medium boilers (MB): 0 to 2% by weight, preferably 1% by weight;

5 Cyclododecanol (CDOL): 10 to 40% by weight, preferably 26% by weight;

High boilers (HB): 0.1 to 3% by weight, preferably 3% by weight.

Mixture ABC1 is then fed into a dividing wall column DWC. The dividing wall column DWC comprises a dividing wall W which separates a left-hand section of the dividing wall column LHS from a right-hand section of the dividing wall column RHS. The top 7 and bottom 8 of the dividing wall column are combined. In a separation plane between the top 7 and bottom 8, there is a connection V between the two halves of the dividing wall column LHS and RHS. The connection V thus constitutes a draw from the left-hand side and a feed for the right-hand side. On the right-hand side of the dividing wall column RHS, a side draw S is also provided. The specific construction of the dividing wall column DWC is apparent from Figure 2.

From the top 7 of the dividing wall column DWC, a CDON-rich fraction A consisting to an extent of 99.5% of CDON is drawn off. From the bottom 8 of the dividing wall column DWC, a fraction C comprising CDOL and high boilers HB is drawn off. This bottom fraction C is recycled and conducted together with the oxidation mixture 2 into the preliminary separator column 3. In this way, the unconverted CDOL is fed back to the dehydrogenation 5. The recycled high boilers HB are concentrated to a certain degree in the process. The high boilers HB freshly introduced from the oxidation 1 are separated out via the bottom of the preliminary separator column 3, such that a steady state is established with regard to the high boiler concentration.

Through the side draw S, a second mixture ABC2 is drawn off, comprising CDON, CDOL and medium boilers. The medium boilers MB constitute the greatest proportion of the side mixture ABC2. The proportion of the product of value CDON

and CDOL is lower. Mixture ABC2 can be purified further, for example, by batch distillation or sent to a thermal utilization. The high-purity CDON in fraction A drawn off from the top 7 of the dividing wall column DWC is used for laurolactam preparation (not shown).

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The schematic structure of the dividing wall column DWC is shown in detail in Figure 2. The dividing wall column DWC comprises a shell 9 which surrounds an inner space. The space is divided into a left-hand column section LHS, a right-hand column section RHS, a top 7 and a bottom 8. A wall W which extends through the
10 dividing wall column DWC within the shell 9 physically separates the left-hand column section from the right-hand column section. In the top 7 and at the bottom 8, the two column sections are physically combined, since the dividing wall W does not extend over the entire height of the dividing wall column DWC. The top 7 and bottom 8 commence where the dividing wall W stops.

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A multitude of internals 10 known per se may be incorporated into the dividing wall column DWC, for example structured packings or random packings from Sulzer or Montz. The purpose of the internals 10 is to achieve a maximum number of theoretical plates.

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In addition, various liquid collectors and distributors 11 may be provided in the dividing wall column DWC, and are of designs customary in the art.

An essential feature of the dividing wall column DWC used in accordance with the
25 invention is a permeable connection V from the left-hand column side LHS to the right-hand column side RHS. The connection V is a liquid conduit provided with a circulation pump, which is not shown, to establish a flow through the conduit. By means of the connection V, a liquid medium boiler is transferred from the concentration maximum thereof on the left-hand side to the right-hand side of the
30 column; in this regard, see also explanation for Figure 4. In order to ensure that

exclusively liquid substances are exchanged via the connection V, the connection V originates from a liquid collector 11 on the left-hand side. The liquid collector 11 is installed at a separation plane at which the liquid concentration of the medium boilers has a maximum. The permeable connection thus originates at the separation plane of the left-hand column section at which the liquid concentration in the medium boiler in the left-hand column section is at a maximum. The permeable connection V opens out at the separation plane of the right-hand column section at which the composition of the liquid phase corresponds as far as possible to that of the liquid stream withdrawn from the left-hand column section. This means that the medium boiler is concentrated to a few per cent in the left-hand section of the dividing wall column and tapped off at the concentration peak, and this stream is fed back in via the connection on the right-hand side. The draw and feed points for the connection V are accordingly selected in accordance with the concentration ratios and need not be on the same plane.

The stream transported via the connection V has the following composition which adds up to 100%:

Cyclododecanone (CDON): 30 to 50% by weight, preferably 43% by weight;

Medium boilers (MB): 0 to 20% by weight, preferably 18% by weight;

Cyclododecanol (CDOL): 30 to 50% by weight, preferably 38.4% by weight;

High boilers (HB): 0.1 to 2% by weight, preferably 0.6% by weight.

From the top 7 of the dividing wall column, a gaseous top product A is drawn off, which comprises almost exclusively CDON (approx. 99.5% by weight). As usual in distillation columns, a condenser 12 and a tops reflux 13 are provided at the top draw. Also disposed at the top is a vacuum system 19 which generates a reduced pressure in the dividing wall column DWC.

At the bottom 8 of the dividing wall column DWC, a fraction C is drawn off, comprising predominantly CDOL and high boilers. As usual in distillation columns, a reboiler/vaporizer 14 is provided here with the corresponding bottoms reflux 15.

- 5 On the right-hand side of the dividing wall column RHS is provided a side draw S through which a second mixture ABC2 rich in medium boilers is drawn off. The mixture ABC2 drawn off from the side draw comprises essentially CDON, CDOL and medium boilers.
- 10 The stream ABC2 withdrawn via the side draw has the following composition which adds up to 100%:

Cyclododecanone (CDON): 20 to 50% by weight, preferably 35% by weight;

Medium boilers (MB): 0 to 60% by weight, preferably 54% by weight;

- 15 Cyclododecanol (CDOL): 10 to 50% by weight, preferably 10% by weight;

High boilers (HB): 0 to 2% by weight, preferably 1% by weight.

- Figure 3 is another drawing of the dividing wall column, but now with the concentration profiles of CDON (solid line, fraction A), CDOL (broken line, fraction C) and medium boilers (line of dashes and dots, fraction B). The connection V is arranged such that it originates at the separation plane of the left-hand column section at which the liquid concentration in the medium boiler in the left-hand column section is at a maximum. The connection opens out at the separation plane of the right-hand column section at which the composition of the liquid phase corresponds as far as possible to that of the liquid stream withdrawn from the left-hand column section. This means that the medium boiler is concentrated to a few per cent in the left-hand section of the dividing wall column and tapped off at the concentration peak, and this stream is fed back via the connection on the right-hand side. In this way, the mixture ABC1 is separated in the left-hand column such that CDON is obtained as a pure distillate and CDOL as a pure high boiler. The medium boiler forms a
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concentration peak within the left-hand section of the dividing wall column. At the point of the concentration maximum, a substream of liquid medium boiler is withdrawn and transferred via the connection V into the right-hand section of the dividing wall column. A sharp separation of CDON and CDOL is again conducted there with elevated reflux. The medium boiler is in turn highly concentrated within the right-hand section of the dividing wall column and can be removed via the side stream S. Since the distillates of the two column sections and the bottoms of the two column sections each have the same concentration (pure products), they can be combined and run through one condensation system 12, one vacuum system 19 and one vaporizer 14.

An equivalent solution for separation purposes is shown in Figure 4: no dividing wall column is employed here; instead, two conventional side draw columns 16 and 17 are connected in series. The first column 16 corresponds to the left-hand section of the dividing wall column, the second section 17 to the right-hand section of the dividing wall column. The function of the connection V is adopted by a side stream 18 between the first column 16 and the second column 17. The bottoms and distillates of the two columns 17 and 18 are combined to give common fractions A and C. The concentration profiles in the two columns 16 and 17 are selected, respectively, as in the left-hand and right-hand sections of the dividing wall column (see Figure 3). In this way, the same separation result is achieved. However, the plant shown in Figure 4 requires greater capital costs, since each of the two columns 16 and 17 requires an individual vaporizer 14 and condenser 12. Since the dividing wall column shown in Figure 3 requires only one vaporizer and one condenser, the inventive execution shown in Figure 3 is much less expensive.

List of reference numerals

	1	Oxidation
	2	Oxidation mixture
5	3	Preliminary separator column
	4	Branch
	5	Dehydrogenation
	6	Low boiler column
	7	Top of dividing wall column
10	8	Bottom of dividing wall column
	9	Shell
	10	Column internals
	11	Liquid collector
	12	Condenser
15	13	Tops reflux
	14	Reboiler/vaporizer
	15	Bottoms reflux
	16	First column
	17	Second column
20	18	Side stream
	19	Vacuum system
	LB	Low boilers
	MB	Medium boilers
	HB	High boilers
25	DWC	Dividing wall column
	RHS	Right-hand section of the dividing wall column
	LHS	Left-hand section of the dividing wall column
	W	Dividing wall
	V	Connection
30	S	Side draw

- O Dehydrogenation mixture
 - A CDON-rich fraction (tops of dividing wall column)
 - B Medium boiler-rich fraction (connection of dividing wall column sides)
 - C CDON/high boiler-containing fraction (bottoms of dividing wall column)
- 5 ABC1 First mixture (feed of dividing wall column)
- ABC2 Second mixture (side draw of dividing wall column)

Claims

1. Process for removing a cyclododecanone-rich fraction (A) from a dehydrogenation mixture (O) comprising low boilers (LB), cyclododecanone (CDON), medium boilers (MB), cyclododecanol (CDOL) and high boilers (HB), characterized by the following steps:
 - a) providing the dehydrogenation mixture (O);
 - b) distillatively removing the low boilers (LB) from the dehydrogenation mixture (O) to obtain a first mixture (ABC1) comprising cyclododecanone (CDON), medium boilers (MB), cyclododecanol (CDOL) and high boilers (HB);
 - c) feeding the first mixture (ABC1) into a dividing wall column (DWC) having a left-hand column section (LHS) and a right-hand column section (RHS), in which the two column sections (LHS, RHS) are partly divided by a dividing wall (W) which extends along the dividing wall column (DWC) such that the top (7) and bottom (8) of the two column sections (LHS, RHS) are combined, and in which a permeable connection (V) between the two column sections (LHS, RHS) which bypasses the dividing wall (W) is provided at a separation stage disposed between the top (7) and bottom (8);
 - d) drawing off the cyclododecanone-rich fraction (A) from the top (7) of the dividing wall column (DWC);
 - e) drawing off a second mixture (ABC2) comprising cyclododecanone (CDON), cyclododecanol (CDOL) and medium boilers (MB) from a side draw (S) of the dividing wall column (DWC);

f) drawing off a fraction (C) comprising cyclododecanol (CDOL) and high boilers (HB) from the bottom (8) of the dividing wall column (DWC).

2. Process according to Claim 1, characterized in that the first mixture (ABC1) is fed
5 into the left-hand column section (LHS), and in that the second mixture (ABC2) is drawn off from the side draw (S) present in the right-hand column section (RHS).

3. Process according to Claim 2, characterized in that the permeable connection (V)
10 between the two column sections (LHS, RHS) is set up for the transport of liquid medium boilers (MB) from the left-hand column section (LHS) to the right-hand column section (RHS).

4. Process according to Claim 3, characterized in that the permeable connection (V)
15 originates at a liquid collector (11) in the left-hand column section (LHS).

5. Process according to Claim 3 or 4, characterized in that the permeable
connection (V) originates at the separation plane of the left-hand column section
(LHS) at which the liquid concentration of the medium boilers (MB) in the left-
hand column section (LHS) is at a maximum, and in that the permeable
20 connection (V) opens at the separation plane of the right-hand column section
(RHS) at which the composition of the stream from the left-hand column section
(LHS) corresponds as far as possible to that of the liquid phase at the separation
plane of the right-hand column section (RHS).

25 6. Process according to any of Claims 1 to 5, characterized in that the dividing wall column (DWC) is operated at a pressure of below 1 bar absolute, especially below 50 mbar absolute.

7. Process according to any of Claims 1 to 6, characterized in that the dehydrogenation mixture (O) has the following composition which adds up to 100%:

Low boilers (LB): 1 to 8% by weight, preferably 3% by weight;
Cyclododecanone (CDON): 60 to 90% by weight, preferably 70% by weight;
Medium boilers (MB): 0 to 1.5% by weight, preferably 1% by weight;
Cyclododecanol (CDOL): 10 to 40% by weight, preferably 24% by weight;
High boilers (HB): 0.1 to 2.5% by weight, preferably 2% by weight.

8. Process according to any of Claims 1 to 7, characterized in that the cyclododecanone-rich fraction (A) has a cyclododecanone (CDON) content of at least 98% by weight, preferably of 99.5% by weight, and/or in that the cyclododecanone-rich fraction (A) is free of cyclododecanol (CDOL), high boilers (HB) and medium boilers (MB).

9. Process according to any of Claims 1 to 8, characterized in that the fraction (C) comprising cyclododecanol (CDOL) and high boilers (HB) is free of cyclododecanone (CDON).

10. Process according to any of Claims 1 to 9, characterized in that the providing of the dehydrogenation mixture (O) comprises the following steps:

g) oxidation of cyclododecane (CDAN) with oxygen to obtain an oxidation mixture (2) comprising low boilers (LB), cyclododecanone (CDON), medium boilers (MB), cyclododecanol (CDOL) and high boilers (HB);

h) distillatively removing a cyclododecanol-rich fraction (CDOL t.q.) from the oxidation mixture (2), said fraction having been depleted of high boilers (HB);

- i) dehydrogenating the cyclododecanol-rich fraction (CDOL t.q.) to obtain the dehydrogenation mixture (O).

- 5 11. Process according to Claim 10, characterized in that the fraction (C) comprising cyclododecanol (CDOL) and high boilers (HB) is recycled into step h).
12. Process according to any of Claims 1 to 11, characterized in that the cyclododecanone-rich fraction (A) is processed further to give lauro lactam and/or
10 in that the second mixture (ABC2) is either separated further or utilized thermally.
13. Apparatus for the distillative workup of substance mixtures into three fractions, called a dividing wall column (DWC), comprising a space which is surrounded by a shell (9) and is divided into a left-hand column section (LHS), a right-hand
15 column section (RHS), a bottom (8) and a top (7), in which a dividing wall (W) which separates the left-hand column section (LHS) from the right-hand column section (RHS) extends through the dividing wall column (DWC) within the shell (9) between the bottom (8) and top (7), and in which a feed for the introduction of the substance mixture (ABC1), a draw at the top for the removal of the first fraction
20 (A), a draw at the bottom for the removal of the second fraction (C) and a side draw (S) for the removal of the third fraction (ABC2) are provided, characterized by
a permeable connection (V) between the two column sections (LHS, RHS) arranged between the top (7) and bottom (8).
- 25 14. Use of an apparatus according to Claim 13 for workup of a substance mixture comprising low boilers (LB), cyclododecanone (CDON), medium boilers (MB), cyclododecanol (CDOL) and high boilers (HB).