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## MASTER INFORMATION CARRIER FOR MAGNETIC TRANSFER

### BACKGROUND OF THE INVENTION

#### Field of the Invention

5           This invention relates to a master information carrier carrying thereon an irregularity pattern representing the information to be transferred to a magnetic medium.

#### Description of the Related Art

          With an increase in information quantity, there is a  
10 demand for a magnetic recording medium which is high in memory capacity, low in cost and preferably requires a short time to read out a necessary part of data (a magnetic recording medium which allows so-called high-speed access). As an example of such a magnetic recording medium, there has been known a high  
15 recording density magnetic medium such as a hard disc or a ZIP (Iomega) in the form of a flexible disc. In such a high recording density magnetic medium, the recording area is formed by narrow data tracks. In order to cause a magnetic head to accurately trace such narrow data tracks and reproduce  
20 the data at a high S/N ratio, the so-called servo tracking technique has been employed.

          In order to perform the servo tracking, it is necessary to write servo information such as servo tracking signals for positioning the data tracks, address signals for the data  
25 tracks and reproduction clock signals on the magnetic recording medium as a preformat upon production thereof. At



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the present, such preformat recording is performed by the use of a specialized servo recording apparatus (a servo track writer). However, the preformat recording by the conventional servo recording apparatus is disadvantageous in that it takes  
5 a long time since the servo information must be recorded on the magnetic recording medium one by one by the use of a magnetic head, which deteriorates the productivity.

As a method of recording the preformat accurately and efficiently, there has been proposed, for instance, in  
10 Japanese Unexamined Patent Publication Nos. 63(1988)-183623, 2001-14667 and U.S. Patent No. 6,347,016, a magnetic transfer method in which a pattern which is formed on a master information carrier and represents servo information is copied to a magnetic recording medium (a slave medium) by magnetic  
15 transfer.

In the magnetic transfer, the magnetization pattern representing the information (e.g., servo information) carried by a master information carrier is magnetically transferred from the master information carrier to a slave  
20 medium by applying a transfer magnetic field to the slave medium and the master information in close contact with each other, and accordingly, the information carried by the master information carrier can be statically recorded on the slave medium with the relative position between the master  
25 information carrier and the slave medium kept constant. Thus, according to the magnetic transfer, the preformat recording

can be performed accurately and the time required for the preformat recording is very short.

The master information carrier employed in the magnetic transfer disclosed in Japanese Unexamined Patent Publication No. 2001-14667 and U.S. Patent No. 6,347,016 comprises a patterned base sheet having on the surface thereof an irregularity pattern representing the information to be transferred and a magnetic layer formed at least on the surface of the protruding portions of the base sheet.

As a method of forming such a patterned base sheet, there has been known a method in which an irregularity pattern is formed on the surface of a non-magnetic flat plate by photolithography which has been employed in the field of semiconductor. However, it has been found that when the signal is transferred to a slave medium from a master information carrier comprising a non-magnetic base sheet, the quality of the transferred signal can greatly deteriorate due to asymmetry.

We, these inventors, have come to conceive that in the conventional master information carrier, where the base sheet is non-magnetic, since only the magnetic layer formed on the base sheet contributes to convergence of magnetic fluxes and convergence of magnetic fluxes concentrates on the magnetic layer, turbulence is generated in the magnetic field established on the slave medium side, which deteriorates symmetry (increases the degree of asymmetry). The magnetic

layer on the base sheet is as thin as several tens to several hundreds nm, and the edges of the protruding portions are sharp. Due to such a small thickness of the magnetic layer and such a shape of the magnetic layer, the transfer magnetic layer is  
5 stabilized in the energy state at the edges of the protruding portions and concentration of magnetic fluxes on the edges occurs, which, we have determined, causes uniformity of the magnetic field in the area of transfer to deteriorate.

Further, we have determined that, in order to suppress  
10 turbulence of the magnetic field in the area of transfer of the slave medium, it is necessary to use a magnetic base sheet to rectify the transfer magnetic field passing through the slave medium.

However our further investigation has revealed that the  
15 transfer magnetic field in the area of transfer of the slave medium cannot be rectified by simply forming the base sheet itself of a magnetic material.

#### SUMMARY OF THE INVENTION

In view of the foregoing observations and description,  
20 the primary object of the present invention is to provide an improved master information carrier for magnetic transfer which allows to obtain a high-quality signal from a slave medium.

In accordance with the present invention, there is  
25 provided a master information carrier for magnetic transfer comprising a base sheet which is formed of a magnetic material

and is provided with an irregularity pattern representing information to be transferred to an in-plane magnetic recording medium, and a magnetic layer formed along the irregularity pattern, wherein the improvement comprises that

5        the saturation magnetization  $M_s$  of the base sheet and the saturation magnetization  $M_m$  of the magnetic layer satisfy the following condition,

$$1.0 < M_m / M_s < 100.$$

It is preferred that the saturation magnetization  $M_s$  of  
10    the base sheet and the saturation magnetization  $M_m$  of the magnetic layer satisfy the following condition,

$$2.0 \leq M_m / M_s < 3.9.$$

The magnetic material for the base sheet is a material which draws the magnetic fluxes into the base sheet when applied  
15    with a magnetic field and may comprise either elements of one kind or elements of a plurality of kinds. So long as the above condition is satisfied in total, the base sheet may contain non-magnetic elements.

It is further preferred that the magnetic layer be of  
20    a body-centered cubic structure (bcc) or a face-centered cubic structure (fcc) or an amorphous structure in crystallographic structure.

It is preferred that the saturation magnetization  $M_s$  of the base sheet be not smaller than 5.65T (4500 Gauss).

25        Further, it is preferred that the height of the protruding portion of the irregularity pattern on the base

sheet be not smaller than 40nm.

Further it is preferred that the height  $h_1$  of the protruding portion of the irregularity pattern on the base sheet and the height  $h_2$  of the magnetic layer on the upper surface of the protruding portion of the irregularity pattern from the surface of magnetic layer on the recessed portion of the irregularity pattern (i.e., the distance between the upper surface of the protruding portion of the irregularity pattern and the surface of magnetic layer on the recessed portion of the irregularity pattern) satisfy the following formula

$$0.2 \leq h_2/h_1 \leq 0.8.$$

More preferably,  $0.3 \leq h_2/h_1 \leq 0.6$ .

The information to be transferred to the magnetic recording medium is, for instance, a servo signal.

According to our investigation, when  $100 \leq M_m/M_s$ , concentration of magnetic fluxes on the edges of the protruding portions cannot be satisfactorily prevented whereas when  $M_m/M_s \leq 1$ , the magnetic fluxes drawn in the master information carrier cannot be satisfactorily released from the protruding portions thereof. When  $1.0 < M_m/M_s < 100$ , concentration of magnetic fluxes on the edges of the protruding portions can be satisfactorily prevented and at the same time, the magnetic fluxes can be sufficiently released from the protruding portions, whereby uniformity of the magnetic field in the area of transfer can be improved and the transfer magnetic field in the slave medium can be rectified.

Thus, when  $1.0 < M_m/M_s < 100$ , the transfer magnetic field in the slave medium can be rectified and the magnetization pattern representing the information carried by the master information carrier is optimally transferred from the master information carrier to a slave medium, whereby a high-quality reproduction signal can be obtained from the slave medium.

We have further found that when  $2.0 \leq M_m/M_s < 3.9$ , the transfer magnetic field in the slave medium can be better rectified and a higher-quality reproduction signal can be obtained from the slave medium.

The aforesaid effect obtained by forming the base sheet of a magnetic material and setting the saturation magnetization  $M_s$  of the base sheet and the saturation magnetization  $M_m$  of the magnetic layer to satisfy the aforesaid condition is remarkable in a master information carrier where the minimum inter-pattern distance (the minimum distance between the protruding portions) of the irregularity pattern is not larger than 300nm.

Further, it has been found that a higher-quality reproduction signal can be obtained from the slave medium when the magnetic layer is of a body-centered cubic structure or a face-centered cubic structure or an amorphous structure in crystallographic structure. In the master information carrier employed in the magnetic transfer disclosed in Japanese Unexamined Patent Publication No. 10(1998)-40544, the magnetic layer is of Co. Co is normally of a hexagonal

close-packed structure having an axis of easy magnetization in a direction of c-axis. In the magnetic transfer, it is necessary to apply a magnetic field in a circumferential direction when the slave medium is an in-plane recording medium and in a perpendicular direction when the slave medium is a perpendicular recording medium. In the case where the magnetic layer of the master information carrier is formed of a magnetic material having an axis of easy magnetization, the intensity of the transferred signal is weakened, which can result in reduction of output of the signal and/or a dull edge of the signal unless the axis of easy magnetization is controlled to be parallel to the direction of the transfer magnetic field. We suppose this is because it is difficult for magnetization to be orientated in the direction of the transfer magnetic field due to misalignment of the direction of the transfer magnetic field and the direction of the axis of easy magnetization. Since a material of a body-centered cubic structure or a face-centered cubic structure or an amorphous structure in crystallographic structure has no axis of easy magnetization, when the magnetic layer is formed of such a material, all the magnetization is more apt to be orientated in the direction of the transfer magnetic field as compared with when the magnetic layer is formed of a hexagonal close-packed structure having an uncontrolled axis of easy magnetization. Since it is difficult to control the axis of easy magnetization, the manufacturing process can be

simplified and the productive efficiency can be improved by using a magnetic material having no axis of easy magnetization.

Our further investigation has revealed that when the height  $h_1$  of the protruding portion of the irregularity pattern on the base sheet and the height  $h_2$  of the magnetic layer on the upper surface of the protruding portion of the irregularity pattern from the surface of magnetic layer on the recessed portion of the irregularity pattern satisfy  $0.2 \leq h_2/h_1 \leq 0.8$ , the transfer magnetic field rectifying effect is further enhanced. That is, we have found that when the ratio  $h_2/h_1$  is smaller than 0.2, the distance by which the transfer magnetic field generated by magnetic fluxes released from edges of the protruding portions spreads in perpendicular to the surface of the magnetic layer is shortened and accordingly, magnetic fluxes cannot sufficiently penetrate into the slave medium as the distance between the master information carrier and the slave medium becomes large, whereas when the ratio  $h_2/h_1$  is larger than 0.8, the transfer magnetic field leaks in the magnetic layer between the protruding portions of the irregularity pattern on the surface of the master information carrier, which results in fear that the transfer magnetic field can be insufficient in intensity.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a plan view partly in a perspective view showing a master information carrier for magnetic transfer in accordance with a first embodiment of the present invention,

Figure 2 is a fragmentary cross-sectional view taken along line II-II in Figure 1,

Figure 3 is an exploded perspective view of a double-sided slave medium and a pair of master information carriers carrying thereon master information to be transferred to opposite sides of the slave medium, and

Figures 4A to 4C are views for illustrating basic steps of magnetic transfer to an in-plane magnetic medium.

#### DESCRIPTION OF THE PREFERRED EMBODIMENTS

10 A master information carrier for preformatting in-plane magnetic recording media in accordance with an embodiment of the present invention will be described first. In Figure 1, a master information carrier 3 in accordance with the embodiment of the present invention is like a disc in shape and comprises a base sheet 3a having a plurality of protruding portions 31 arranged in a pattern formed on the surface thereof (as a result the base sheet 3a has an irregularity pattern) and a magnetic layer 3b formed along the irregularity pattern. The irregularity pattern represents information to be transferred to a magnetic recording media (slave media) and Figure 1 shows a part of the irregularity pattern. In Figure 1, arrow X indicates the circumferential direction (the direction of track) and arrow Y indicates the radial direction. For example, the information to be transferred may be a servo signal.

Figure 2 is a fragmentary cross-sectional view of a part

of the master information carrier 3 including a protruding portion 31 on the base sheet 3a taken along a line parallel to the direction X of track.

In the master information carrier 3 of this embodiment,  
5 the base sheet 3a and the magnetic layer 3b are formed of materials such that the saturation magnetization  $M_s$  of the base sheet 3a and the saturation magnetization  $M_m$  of the magnetic layer 3b satisfy the condition  $1.0 < M_m/M_s < 100$  (preferably  $2.0 \leq M_m/M_s < 3.9$ ). The saturation magnetization  $M_s$  of the base  
10 sheet is not smaller than 5.65T (4500 Gauss). For example, the base sheet 3a of the master information carrier 3 may be formed of nickel or nickel alloy. The magnetic layer 3b may be formed of, for instance, alloys such as FeCo, FeCoNi and FeNi which contain at least one of Fe, Co, Ni, Gd, Dy, Sm, and  
15 Nd and are of a face-centered cubic structure (fcc) in crystallographic structure. So long as exhibiting ferromagnetism in total, the magnetic layer 3b may contain other magnetic elements or non-magnetic elements. Though may be soft, semi-hard or hard, it is preferred in view of obtaining  
20 better magnetic transfer that the magnetic layer 3b be a soft or semi-hard magnetic layer relatively small in coercive force. Further, as described above, it is further preferred that the magnetic layer 3b be of a body-centered cubic structure (bcc) or a face-centered cubic structure (fcc) or an amorphous  
25 structure in crystallographic structure. In the case where the magnetic layer 3b is of a body-centered cubic structure

(bcc) or a face-centered cubic structure (fcc), it is preferred that the magnetic layer 3b has a particle structure where fine particles are arranged at random and each particle is not larger than 100nm in size as observed from the surface of the magnetic layer.

The height  $h_1$  of the protruding portion 31 of the irregularity pattern on the base sheet 3a is not smaller than 40nm. The height  $h_1$  of the protruding portion of the irregularity pattern on the base sheet and the height  $h_2$  of the magnetic layer on the upper surface of the protruding portion of the irregularity pattern from the surface of magnetic layer on the recessed portion of the irregularity pattern satisfy the formula,  $0.1 \leq h_2/h_1 \leq 0.8$ . More preferably,  $0.3 \leq h_2/h_1 \leq 0.6$ .

When the magnetic base sheet 3a and the magnetic layer 3b satisfy the aforesaid conditions, the magnetization pattern representing the information carried by the master information carrier is optimally transferred from the master information carrier to a slave medium 2, whereby a high-quality reproduction signal can be obtained from the slave medium 2. Further, when the height  $h_1$  of the protruding portion 31 of the irregularity pattern on the base sheet 3a is not smaller than 40nm and the height  $h_1$  of the protruding portion of the irregularity pattern on the base sheet and the height  $h_2$  of the magnetic layer on the upper surface of the protruding portion of the irregularity pattern from the surface of

magnetic layer on the recessed portion of the irregularity pattern satisfy the formula,  $0.2 \leq h_2/h_1 \leq 0.8$ , absorption and release of the magnetic fluxes at the edges of the protruding portions 31 can be improved and a higher-quality reproduction  
5 signal can be obtained from the slave medium 2. When the height  $h_1$  of the protruding portion 31 of the irregularity pattern is smaller than 40nm, there arises a fear that magnetic fluxes cannot be sufficiently released from the protruding portions 31 to the space (toward the slave medium 2) and a sufficient  
10 intensity of the transfer magnetic field cannot be ensured.

The base sheet 3a having thereon the irregularity pattern or the pattern of the protruding portions 31 can be formed, for instance, by the use of stamper method or photolithography.

A photo-resist layer is first formed on a smooth glass  
15 plate (or a smooth crystal plate), for instance, by spin coating, and a laser beam (or an electron beam) modulated according to the servo signal is projected onto the photo-resist layer while rotating the glass plate so that the photo-resist layer is exposed to the laser beam in a predetermined pattern, e.g.,  
20 a pattern of servo signals each extending in a radial direction in one track. Thereafter the photo-resist layer is developed and the part exposed to the laser beam is removed with an irregularity pattern of the photo-resist left on the glass plate, thereby obtaining a matrix. Then the surface of the  
25 matrix is plated (electroforming), and a Ni base sheet having a positive irregularity pattern is formed on the matrix and

separated from the matrix. The Ni base sheet as it is may be used as a master information carrier or may be used as a master information carrier after forming a magnetic layer and a protective layer along the irregularity pattern as desired.

5           Otherwise, the matrix may be plated to form a second matrix and the second matrix may be plated to form a base sheet having a negative irregularity pattern. Further, a third matrix may be formed by plating the second matrix or pressing a resin syrup against the surface of the second matrix and  
10       curing the resin syrup, and a base sheet having a positive irregularity pattern may be formed by plating the third matrix.

          Further, a matrix without photo-resist layer may be first formed by etching the glass plate with an irregularity pattern of the photo-resist to make holes in the glass plate, and a  
15       base sheet may be formed by the use of the matrix in the manner described above.

          The base sheet may be formed of metal such as Ni or Ni alloy as described above, and as the aforesaid plating for forming the metal base sheet, various metal film forming  
20       techniques such as electroless plating, electroforming, sputtering, or ion plating can be employed. The height of the protruding portion (the depth of the irregularity pattern) should be not smaller than 40nm, preferably in the range of 50 to 800nm and more preferably 80 to 600nm. When the  
25       irregularity pattern represents a sample servo signal, each of the protruding portions is rectangle having longer sides

in a radial direction of the base sheet and shorter sides in a circumferential direction of the same. When the irregularity pattern represents a sample servo signal, each of the protruding portions is preferably 0.05 to 20  $\mu\text{m}$  in the longer sides and 0.05 to 5  $\mu\text{m}$  in the shorter sides.

The magnetic layer 3b may be formed on the irregularity pattern by various vacuum film forming techniques or plating methods such as vacuum deposition, sputtering, ion plating and the like of magnetic material. The thickness of the magnetic layer 3b is preferably 50 to 500nm and more preferably 80 to 300nm. As described above, the ratio  $h_2/h_1$  of the height  $h_1$  of the protruding portion of the irregularity pattern on the base sheet to the height  $h_2$  of the magnetic layer on the upper surface of the protruding portion of the irregularity pattern from the surface of magnetic layer on the recessed portion of the irregularity pattern is not smaller than 0.2 and not larger than 0.8.

It is preferred that a protective film 5 to 30nm thick such as of DLC (diamond-like carbon) be provided on the magnetic layer on the upper surface of the protruding portion 31. A lubricant layer may be further provided on the protective film. A reinforcement layer such as a Si layer may be provided between the magnetic layer 3b and the protective film to enhance the contact therebetween. The lubricant layer suppresses deterioration in durability of the magnetic layer 3b, such as scores due to friction, which occurs in correcting for a shift

generated when the magnetic layer 3b is brought into contact with the slave medium.

Magnetic transfer of information to a slave medium by the use of a master information carrier in accordance with the present invention will be described, hereinbelow.

As shown in Figure 3, a pair of master information carriers 3 and 4 are disposed on opposite sides of a slave medium 2. The slave medium 2 may be, for instance, a hard disc or a flexible disc. In this particular embodiment, the slave medium 2 is provided with a pair of in-plane recording magnetic layers 2b and 2c formed on lower and upper sides of a disc-shaped base sheet 2a though the slave medium 2 may be provided with a single recording layer on one side thereof.

Both the master information carriers 3 and 4 are in accordance with the present invention and respectively provided with irregularity patterns formed on the upper side of a base sheet 3a and the lower side of a base sheet 4a representing pieces of information to be transferred to the lower and upper magnetic layers 2b and 2c. Magnetic layers 3b and 4b are formed along the irregularity patterns.

Though, in Figure 3, the lower and upper master information carriers 3 and 4 and the slave medium 2 are away from each other, in the actual magnetic transfer process, the magnetic layer 3b of the lower master information carrier 3 is brought into contact with or to the vicinity of the lower magnetic layer 2b of the slave medium 2 and the magnetic layer

4b of the upper master information carrier 4 is brought into contact with or to the vicinity of the upper magnetic layer 2c of the slave medium 2.

Basic steps of magnetic transfer to an in-plane magnetic recording medium will be described with reference to Figures 4A to 4C, hereinbelow. In Figures 4A to 4C, only the lower magnetic layer 2b is shown.

An initial DC magnetic field  $H_{in}$  is first applied to the slave medium 2 in one direction parallel to the recording tracks thereof, thereby magnetizing the magnetic layer 2b of the slave medium 2 in an initial DC magnetization as shown in Figure 4A. Thereafter, the magnetic layer 3b of the lower master information carrier 3 is brought into close contact with the lower magnetic layer 2b of the slave medium 2. In this state, a transfer magnetic field  $H_{du}$  is applied in the direction opposite to the initial DC magnetic field  $H_{in}$  as shown in Figure 4B, thereby magnetically transferring the information on the master information carrier 3 to the lower magnetic layer 2b of the slave medium 2. As a result, information represented by the irregularity pattern on the master information carrier 3 is transferred to the lower magnetic layer 2b as shown in Figure 4C. The information represented by the irregularity patterns on a pair of master information carriers may be transferred to opposite sides of the slave medium either simultaneously or in sequence.

In the case where the irregularity pattern representing

information to be transferred is a negative pattern reverse to the positive pattern shown in Figures 4A to 4C, the information can be magnetically transferred to the slave medium 2 by reversing the directions of the initial DC magnetic field  $H_{in}$  and the transfer magnetic field  $H_{du}$ . The intensities of the initial DC magnetic field and the transfer magnetic field are determined on the basis of the coercive force of the slave medium 2, the specific permeabilities of the master information carrier and the slave medium, and the like.

10        A magnetic recording disc such as a hard disc or a high-density flexible disc is generally employed as the slave medium 2. The magnetic layer thereof is generally of a coated magnetic material or a metal film.

         In the case of a slave medium having a magnetic layer of metal film, the material of the magnetic layer may be Co, Co alloy (e.g., CoPtCr, CoCr, CoPtCrTa, CoPtCrNbTa, CoCrB, CoNi, Co/Pd), Fe or Fe alloy (e.g., FeCo, FePt, FeCoNi). It is preferred in view of obtaining clearer magnetic transfer that the magnetic layer be higher in magnetic flux density and has a magnetic anisotropy conforming to the recording system of the slave medium, that is, in the case of an in-plane recording medium, in a direction parallel to the direction of tracks and in the case of a perpendicular recording medium, in a direction perpendicular to the direction of tracks. The magnetic layer of the slave medium is preferably not smaller than 10nm and not larger than 500nm in thickness, and more

preferably not smaller than 20nm and not larger than 200nm in thickness.

It is further preferred that the magnetic layer of the slave medium 2 be provided with a non-magnetic primer layer on the base sheet side thereof in order to give the magnetic layer a necessary magnetic anisotropy. The primer layer may be, for instance, of Cr, CrTi, CoCr, CrTa, CrMo, NiAl, Ru or Pd, but should match to the magnetic layer in crystallographic structure and lattice constant. The thickness of the primer layer is preferably not smaller than 10nm and not larger than 150nm, and more preferably not smaller than 20nm and not larger than 80nm.

Though, in the embodiment described above, the slave medium is an in-plane recording medium, the present invention can be applied to the case where the slave medium is a perpendicular recording medium.

#### Examples

Master information carriers in accordance with first to eighth embodiments of the present invention and first to third comparative examples were made in the following way and the signal was transferred from the master information carriers to the slave media produced in the manner described later. Then transferred signal quality was evaluated in the following manner. The result is shown in the following table. In the table, "emb" is an abbreviation of "embodiment", "c/e" is an abbreviation of "comparative example", "CS" is an abbreviation

of "crystallographic structure", "ev" is an abbreviation of "evaluation", and "ASY" is an abbreviation of "asymmetry".

#### Evaluation of the transferred signal quality

Quality of the signal reproduced from the slave medium  
5 was evaluated by the use of electromagnetic conversion  
property meter (SS-60: KYODO Electronics). A GMR head which  
was  $0.12\mu\text{m}$  in reproducing head gap,  $0.41\mu\text{m}$  in reproducing  
track width,  $0.2\mu\text{m}$  in recording head gap and  $0.67\mu\text{m}$  in  
recording track width was employed.

10 The read signal was divided into frequencies by a  
spectro-analyzer, and the difference C/N between the peak  
intensity C of the primary signal and the medium noise N  
obtained by extrapolation was measured. The quality of the  
signal reproduced from the slave medium was evaluated on the  
15 basis of the relative values  $\Delta\text{C/N}$  with the difference C/N  
between the peak intensity C of the primary signal and the  
medium noise N obtained from the same slave medium by recording  
and reproducing the same signal by the use of the same GMR head  
instead of magnetic transfer taken as 0 db. When the relative  
20 value  $\Delta\text{C/N}$  is larger than -1.5 db, the transferred signal  
quality was evaluated as an excellent state ○, when the  
relative value  $\Delta\text{C/N}$  is not smaller than -3.0 db and not smaller  
than -1.5 db, the transferred signal quality was evaluated as  
a good state △ and when the relative value  $\Delta\text{C/N}$  is smaller  
25 than -3.0 db, the transferred signal quality was evaluated as  
a poor state ×.

Second, asymmetry ASY is calculated according to the output of positive polarity (TAA+) and the output of negative polarity (TAA-) on the basis of the following formula.

$$ASY = \{ [(TAA+) - (TAA-)] / [(TAA+) + (TAA-)] \} * 100 \quad (5)$$

5 Then if the value of ASY was not smaller than 0% and smaller than 5%, the asymmetry was evaluated as excellent ○, if the value of ASY was not smaller than 5% and smaller than 10%, it was evaluated as good △ and if the value of ASY was 10% or more, it was evaluated as poor ×.

#### 10 First embodiment

In the master information carrier in accordance with a first embodiment of the present invention, the base sheet was formed of Ni by the use of stamper method. An irregularity pattern signal which were 1.0 μm in track width and 1.1 μm in  
15 track pitch and extended from an innermost position at a distance of 20mm from the center to an outermost position at a distance of 40mm from the center was formed on the base sheet in a height of 0.2 μm of the protruding portions. The bit length was 0.2 μm in the innermost position.

20 A magnetic layer of FeCO (30at%) having a bcc structure was formed on the Ni base sheet at 25°C. The Ar sputtering pressure was  $1.44 \times 10^{-1}$  Pa (1.08mTorr), and the power supplied was 2.80W/cm<sup>2</sup>.

In the master information carrier of the first embodiment,  
25 Mm/Ms=3.8 and h2/h1=0.7.

The master information carriers of the second to eighth

embodiments and the first to third comparative examples were produced in manners similar to the first embodiment except that the base sheet and the magnetic layer were formed of different material and in different thickness so that the  
5 crystallographic structure of the magnetic layer, the value of  $M_m/M_s$  and the value of  $h_2/h_1$  differ from those of the first embodiment.

#### Second embodiment

The master information carrier of the second embodiment  
10 was produced in the same manner as the first embodiment except that the magnetic layer was of Co having a hcp structure and  $M_m/M_s$  was 2.8.

#### Third embodiment

The master information carrier of the third embodiment  
15 was produced in the same manner as the first embodiment except that the magnetic layer was of CoNi50 having a fcc structure and  $M_m/M_s$  was 2.0.

#### Fourth embodiment

The master information carrier of the fourth embodiment  
20 was produced in the same manner as the first embodiment except that the magnetic layer was of FeMn50 having a bcc structure and  $M_m/M_s$  was 2.5.

#### Fifth embodiment

The master information carrier of the fifth embodiment  
25 was produced in the same manner as the first embodiment except that  $h_2/h_1$  was 0.1.

#### Sixth embodiment

The master information carrier of the sixth embodiment was produced in the same manner as the first embodiment except that  $h_2/h_1$  was 0.9.

#### 5 Seventh embodiment

The master information carrier of the seventh embodiment was produced in the same manner as the first embodiment except that the base sheet was of  $(\text{FeCO}_2)\text{P}$  alloy and  $M_m/M_s$  was 92.

#### Eighth embodiment

10 The master information carrier of the eighth embodiment was produced in the same manner as the first embodiment except that the magnetic layer was of Co FeB amorphous alloy and  $M_m/M_s$  was 2.0.

#### Comparative example 1

15 The master information carrier of the first comparative example was produced in the same manner as the first embodiment except that the magnetic layer was of Ni having a fcc structure and  $M_m/M_s$  was 1.0.

#### Comparative example 2

20 The master information carrier of the second comparative example was produced in the same manner as the first embodiment except that the magnetic layer was of CuNi80 having a fcc structure and  $M_m/M_s$  was 0.8.

#### Comparative example 3

25 The master information carrier of the third comparative example was produced in the same manner as the first embodiment except

that the base sheet was of NiP alloy having a fcc structure and  $M_m/M_s$  was 113.

The slave media were produced in the following manner. That is, 3.5" disc-shaped in-plane magnetic recording media  
5 were prepared by a sputtering apparatus (S-50S: Shibaura Mechatronics). The sputtering apparatus was evacuated to  $1.33 \times 10^{-5}$  Pa ( $1.0 \times 10^{-4}$  Torr) at the room temperature and then argon was introduced into the apparatus to a pressure of 0.4 Pa (3.0 mTorr). Under these conditions, glass discs were heated  
10 to 200°C and a magnetic layer consisting of a 30 nm thick CrTi and 30 nm thick CoCrPt layer was formed on each of the glass discs. Each of the slave media was 5.65 T (4500 Gauss) in saturation magnetization  $M_s$  and 199 kA/m (2500 e) in coercive force.

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20

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Table

|        | Mn/Ms | h2/h1 | CS        | $\Delta$<br>(dB) / (ev) | ASY<br>(%) / (ev) |
|--------|-------|-------|-----------|-------------------------|-------------------|
| emb. 1 | 3.8   | 0.7   | bcc       | -0.2 (○)                | 2 (○)             |
| emb. 2 | 2.8   | 0.7   | hcp       | -1.7 (△)                | 7 (△)             |
| emb. 3 | 2.0   | 0.7   | fcc       | -2.0 (△)                | 3 (○)             |
| emb. 4 | 2.5   | 0.7   | bcc       | +0.2 (○)                | 3 (○)             |
| emb. 5 | 3.8   | 0.1   | bcc       | -1.2 (○)                | 8 (△)             |
| emb. 6 | 3.8   | 0.9   | bcc       | -1.6 (△)                | 1 (○)             |
| emb. 7 | 92    | 0.7   | bcc       | -1.4 (○)                | 5 (△)             |
| emb. 8 | 2.0   | 0.7   | amorphous | -0.7 (○)                | 1 (○)             |
| c/e. 1 | 1.0   | 0.7   | fcc       | -4.2 (×)                | 11 (×)            |
| c/e. 2 | 0.8   | 0.7   | fcc       | -4.5 (×)                | 15 (×)            |
| c/e. 3 | 113   | 0.7   | bcc       | -3.1 (×)                | 26 (×)            |

As can be understood from the table, in the first to eighth embodiments which satisfied  $1.0 < Mm/Ms < 100$ , both the transferred signal quality and the asymmetry were  $\Delta$  or  $\bigcirc$ . On the other hand, in the first to third comparative examples which did not satisfy  $1.0 < Mm/Ms < 100$ , both the transferred signal quality and the asymmetry were  $\times$ .

In the fifth and sixth embodiments which were the same as the first embodiment except that they did not satisfy  $0.2 \leq h2/h1 \leq 0.8$ , one of the transferred signal quality and the asymmetry were  $\Delta$  whereas in the first embodiment, both the transferred signal quality and the asymmetry were  $\bigcirc$ , which indicated that it is necessary to satisfy  $0.2 \leq h2/h1 \leq 0.8$  in

order to form a better magnetization pattern.

Further, even if  $1.0 < M_m/M_s < 100$  and  $0.2 \leq h_2/h_1 \leq 0.8$  were both satisfied, the embodiment which was a hcp structure in crystallographic structure as the second embodiment could not  
5 obtained  $\bigcirc$  and could obtained only  $\triangle$  in both the transferred signal quality and the asymmetry, which indicated that the magnetic layer which was a bcc, a fcc or an amorphous in crystallographic structure was better than that which was a hcp in crystallographic structure.

What is claimed is:

1. A master information carrier for magnetic transfer comprising a base sheet which is formed of a magnetic material and is provided with an irregularity pattern representing  
5 information to be transferred to a magnetic recording medium, and a magnetic layer formed along the irregularity pattern, wherein the improvement comprises that

the saturation magnetization  $M_s$  of the base sheet and the saturation magnetization  $M_m$  of the magnetic layer satisfy  
10 the following condition,

$$1.0 < M_m / M_s < 100.$$

2. A master information carrier as defined in Claim 1 in which the saturation magnetization  $M_s$  of the base sheet and the saturation magnetization  $M_m$  of the magnetic layer satisfy  
15 the following condition,

$$2.0 \leq M_m / M_s < 3.9.$$

3. A master information carrier as defined in Claim 1 or 2 in which the magnetic layer is of a body-centered cubic structure or a face-centered cubic structure or an amorphous  
20 structure in crystallographic structure.

4. A master information carrier as defined in any one of Claims 1 to 3 in which a magnetic layer is formed also on the recessed portion of the irregularity pattern on the base sheet and the height  $h_1$  of the protruding portion of the  
25 irregularity pattern and the height  $h_2$  of the magnetic layer on the upper surface of the protruding portion of the

irregularity pattern from the surface of magnetic layer on the recessed portion of the irregularity pattern satisfy the following formula

$$0.2 \leq h_2/h_1 \leq 0.8.$$

5

5. A master information carrier as defined in Claim 4 in which  $0.3 \leq h_2/h_1 \leq 0.6$ .

6. A master information carrier as defined in any one of Claims 1 to 5 in which the saturation magnetization  $M_s$  of the base sheet is not smaller than 5.65T (4500 Gauss).

7. A master information carrier as defined in any one of Claims 1 to 6 in which the height of the protruding portion of the irregularity pattern on the base sheet be not smaller than 40nm.

15 8. A master information carrier as defined in any one of Claims 1 to 7 in which the information to be transferred to the magnetic recording medium is a servo signal.

9. A magnetic recording medium having information transferred thereto from a master information carrier as defined in any one of the preceding claims.