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TOTAL ELECTRICAL TRANSIENT ELIMINATOR

BACKGROUND OF THE INVENTION

5 1. Field of the invention:

 This invention relates generally to transient
elimination or suppression systems and more
particularly, it relates to an improved apparatus and
10 method for attenuating high frequency transients in the
range of 50 KHz to 200 MHz on AC power lines from
damaging sensitive electrical and electronic circuits
in equipment coupled to the AC power lines.

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 2. Description of the Prior Art:

 As is generally well-known in the art, modern
electrical and electronic circuits in equipment, such
20 as those that exist in microprocessors and computer
systems, can be damaged or destroyed by voltage surges,
transients, atmospheric discharges (i.e., lightning
strikes), and other forms of undesirable electrical
noise generated by motors, generators and the like
25 which can cause interferences. As a consequence, there
have been developed heretofore many types of transient
suppression apparatuses for eliminating unwanted

transient voltages or currents and for isolating such
transients appearing
on the AC external power lines so as to protect
sensitive electrical and electronic circuits and
5 equipment coupled to the external power lines.

A prior art search directed to the subject matter
of this application in the U.S. Patent and Trademark
10 Office revealed the following U.S. Letters Patent:

1,730,881	5,650,908
4,019,122	5,671,110
4,802,055	5,737,161
15	5,532,897

In U.S. Patent No. 5,532,897 to Carpenter, Jr.
issued on July 2, 1996, there is taught a high voltage
substation level surge suppression system which
20 includes a high energy surge arrestor and a low energy
surge arrestor. A surge interceptor is interconnected
between the two surge arrestors. The surge interceptor
includes an inductor interconnected in parallel with a
high energy resistor.

In U.S. Patent No. 5,671,110 to McCartney et al. issued on September 23, 1997, there is disclosed an apparatus for protecting a non-isolated data communication cable against ground skew used with an AC power source. A current summing transformer is coupled to the AC power source. The current summing transformer includes a single transformer core and a plurality of coils. One of the coils is connected with each phase, neutral and ground line in the AC power source. The current summing transformer provides a high impedance to surge current in the data cable ground of one or many non-isolated data cables.

In U.S. Patent No. 5,737,161 to Thomas issued on April 7, 1998, there is disclosed an overcurrent protection device which includes a relay having two coils wound on a common magnetic core and a PTC device coupled in parallel with the relay contacts. The first coil is a low impedance current coil, and the second coil is a high impedance voltage coil.

The remaining patents listed above but not specifically discussed are deemed to be of general

interest and to show the state of the art pertaining to transient surge suppressors utilizing coils and cores.

Further, there is known in the prior art of U.S. Patent No. 5,689,130 to Carlson issued on November 18, 1997. This '180 patent teaches an isolated electrical power supply for protecting electrical devices from transient voltages and currents. A filter is provided which includes a toroid and a resistor which are used in conjunction with an isolator transformer. The filter is coupled between the secondary neutral lead of the transformer and the secondary ground lead so as to shunt the current or voltage spikes. A ferrite bead is connected between earth ground and a binding post for filtering current in the 70-200 KHz range.

However, none of the prior art discussed above teach an apparatus for attenuating high frequency transients on AC power lines like that of the present invention which includes a continuous attenuator circuit for attenuating high frequency transients in the frequency range of 50 KHz to 200 MHz electrically coupled between earth ground and an electrical load ground. The present invention represents significant improvement over the prior art discussed above.

SUMMARY OF THE INVENTION

Accordingly, it is a general object of the present
5 invention to provide an improved apparatus for
attenuating high frequency transients over a wider
frequency range than has been traditionally available.

10 It is an object of the present invention to
provide an improved method and apparatus for
attenuating high frequency transients in the range of
50 KHz to 200 MHz on AC power lines from damaging
sensitive electrical and electronic circuits and
15 equipment coupled to the AC power lines.

It is another object of the present invention to
provide an improved method and apparatus for
20 attenuating high frequency transients which includes a
continuous attenuator circuit formed of a plurality of
toroid cores.

25 It is still another object of the present
invention to provide any improved method and apparatus

for attenuating high frequency transients which includes an isolation transformer and a continuous attenuator circuit.

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It is yet still another object of the present invention to provide an improved apparatus and method for attenuating high frequency transients which includes a Ground Fault Circuit Interruptor and a
10 continuous attenuator circuit.

In accordance with a preferred embodiment of the present invention there is provided an apparatus for
15 attenuating high frequency transients on AC power lines from damaging sensitive electrical and electronic circuits in an electrical load coupled to the AC power line. The AC power line has an earth ground and the electrical load has an electrical load ground. An
20 isolation transformer is provided which has a primary winding and a secondary winding. The primary winding has a primary source lead, a primary neutral lead, and a primary electrostatic shield lead. The secondary winding has a secondary source lead, a secondary
25 neutral lead, and a secondary electrostatic shield lead. The primary source lead, primary neutral lead,

and primary electrostatic shield lead are electrically coupled to the AC power lines.

5 The secondary source lead, secondary neutral lead, and secondary electrostatic shield lead are electrically coupled to the electrical load. The primary electrostatic shield lead and the secondary electrostatic shield lead are electrically connected
10 together and to the earth ground. A continuous attenuator circuit is used to attenuate high frequency transients in the frequency range of 50 KHz to 200 MHz electrically coupled between the earth ground and the electrical load ground.

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BRIEF DESCRIPTION OF THE DRAWINGS

These and other objects and advantages of the
20 present invention will become more fully apparent from the following detailed description when read in conjunction with the accompanying drawings with like reference numerals indicating corresponding parts throughout, wherein:

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Figure 1 is a schematic circuit diagram of an apparatus for attenuating high frequency transients, constructed in accordance with the principles of the present invention;

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Figure 2 is a schematic circuit diagram of a second embodiment of an apparatus for attenuating high frequency transients in accordance with the present invention; and

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Figure 3 is a detailed diagram of a continuous attenuator circuit formed of a plurality of toroid cores for use in the apparatus of Figure 1 or Figure 2.

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DESCRIPTION OF THE PREFERRED EMBODIMENTS

Referring now in detail to the drawings, there is shown in Figure 1 a schematic circuit diagram of an improved apparatus **110** for attenuating high frequency transients, constructed in accordance with the principles of the present invention. The apparatus **110** is used to attenuate high frequency transients in the range of 50 KHz to 200 MHz and for isolating such transients from an electrical load **112** due to an external AC (alternating current) power source **114**.

The apparatus 110 includes an isolation transformer 116 having a primary winding 118 and a secondary winding 120. Typically, the primary-to-secondary winding ratio is 1:1.

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The external AC power source 114 is connected to the primary winding 118 of the transformer 116 by a standard three-prong electrical plug 122. The isolation transformer 116 has a primary source lead 124
10 connected to the line lead L of the plug 122, a primary neutral lead 126 connected to the line lead N of the plug 122, and a primary electrostatic shield lead 128 connected to the line lead EG of the plug 122. The isolation transformer 116 also has a secondary source
15 lead 130, a secondary neutral lead 132, and a secondary electrostatic shield lead 134. The primary electrostatic shield 128 and the secondary electrostatic shield 134 are connected together and to a line lead 136 which serves as a primary earth ground
20 GND.

A metal oxide varistor (MOV) 138 has its ends connected across the secondary source lead 130 and the
25 secondary neutral lead 132 of the isolation transformer 116. The metal oxide varistor 138 functions to clamp

any high voltages which may be coupled through the secondary winding of the transformer to the electrical load **112**. A filter capacitor **140** is connected in parallel with the MOV **138** and has its ends also
5 connected across the secondary source lead **130** and the secondary neutral lead **132** of the isolation transformer **116**. The purpose of the capacitor **140** is to attenuate high frequency voltage and current pulses in the 100 KHz frequency range.

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Further, one end of the capacitor **140** is connected to a load source lead **142** of the electrical load **112**, and its other end is connected to a load neutral lead
15 **144** of the electrical load **112** at a node **A**. The node **A** is also connected to the primary earth ground **GND** via a lead line **146**. An electrical load ground line **148** of the electrical load is connected to a node **B** which is joined to a floating ground **FG** via lead line **150**.

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In order to attenuate high frequency transient voltages and currents generated on the electrical load line **148** of the electrical load **112** from being passed
25 straight back to the primary winding of the transformer, a continuous attenuator circuit **152** of the

present invention is interconnected between the floating ground **FG** at the node **B** and the primary earth ground **GND** at the node **A**. Unlike the '180 patent of the prior art which has a filter circuit formed of a ferrite bead, resistor, and toroid for filtering
5 current in the 70 - 200 KHz range, the instant continuous attenuator circuit **152** has been designed to filter high frequency transients in the range of 50 KHz to 200 MHz before they reach the secondary winding of
10 the transformer.

With reference now to Figure 3, there is shown a detailed diagram of the continuous attenuator circuit
15 **152** which includes a plurality of sections **154a**, **154b**, and **154c**. The first section **154a** includes three series-connected toroids **T1**, **T2** and **T3** which are tuned to a frequency range between 50 KHz and 100 KHz. The second section **154b** includes two series-connected
20 toroids **T4** and **T5** which are tuned to a frequency of 100 MHz. The third section **154c** includes two series-connected toroids **T6** and **T7** which are tuned to a frequency of 200 MHz.

Each of the toroids **T1-T7** has a cylindrical core which is typically on the order of one to six inches in diameter. The diameter of each toroid is dependent upon the magnitude of the high frequency transients to
5 be eliminated. While the core is shown to be cylindrical in shape, it should be apparent that other shapes may be also used. Further, the toroid may be of the split ring type. The toroid core is formed of a magnetic material such as iron and ferrite which is
10 overwrapped with an epoxy. A single long continuous copper strand of wire **156** is wound individually and sequentially a number of turns around each core of the toroids **T1-T7** which are disposed in close proximity to each other in either an end-to-end, side-by-side, or
15 stacked fashion. In this manner, a "braided wire" effect is achieved by using the unbroken and continuous strand of wire **156**.

20 As will be noted, one end of the copper wire **156** adjacent to the toroid **T1** is connected to a lug **158** and the other end thereof adjacent to the toroid **T7** is connected to a lug **160**. A shrink tubing **162** may be placed over the toroids **T1-T7** so as to package them into a
25 single housing. In the preferred embodiment, the wire size as measured by the American Wire Gauge (AWG) is

preferably a No. 12, 14 or 16 size and is most preferably a 16 AWG size. However, it should be clearly understood by those skilled in the art that different wire sizes, number of turns, and core sizes
5 may be used to accommodate the various magnitude and frequencies of the transient voltages and currents. The total impedance of the continuous attenuator circuit **152** is in compliance with the National Electronic Code (NEC) and Underwriters Laboratories
10 (UL) requirements of being safe for a ground conductor of an electrical product.

In Figure 2, there is illustrated a second embodiment of an apparatus **210** for attenuating high frequency
15 transients in accordance with the present invention. The apparatus **210** is substantially identical in its construction to the apparatus **110** of Figure 1, except that a Ground Fault Current Interruptor (GFCI) **216** has been used instead of the isolation transformer **116**.
20 The GFCI **216** has an input source lead **224** connected to the line lead **L** of the plug **122**, an input neutral lead **226** connected to the line lead **N** of the plug, and a ground fault line **228** connected to the line lead **EG** of the plug. The GFCI **216** has also an output source lead
25 **230** and an output neutral lead **232** which are coupled to the electrical load **114**.

The GFCI 216 electrically couples the output source and neutral leads to the input source and neutral leads in a first mode of operation and electrically isolates the output source and neutral leads from the input source and neutral leads in a second mode of operation. Except for these differences, the apparatus 210 for attenuating high frequency transients operates and functions in the same manner as just previously described with respect to Figure 1. Thus, a detailed description of the interconnection of the components and their operation will not be repeated.

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From the foregoing detailed description, it can thus be seen that the present invention provides an improved method and apparatus for attenuating high frequency transients on AC power lines from damaging sensitive electrical and electronic circuits in an electrical load coupled to the AC power line. The AC power line has an earth ground and the electrical load has an electrical load ground. A continuous attenuator circuit for attenuating high frequency transients in the frequency range of 50 KHz to 200 MHz is

electrically coupled between the earth ground and the electrical load ground.

5 While there has been illustrated and described
what are at present considered to be preferred
embodiments of the present invention, it will be
understood by those skilled in the art that various
changes and modifications may be made, and equivalents
10 may be substituted for elements thereof without
departing from the true scope of the invention. In
addition, many modifications may be made to adapt a
particular situation or material to the teachings of
the invention without departing from the central scope
15 thereof. Therefore, it is intended that this invention
not be limited to the particular embodiments disclosed
as the best modes contemplated for carrying out the
invention, but that the invention will include all
embodiments falling within the scope of the appended
20 claims.



CLAIMS

WHAT IS CLAIMED IS:

1. An apparatus for attenuating high frequency transients on AC power lines from damaging sensitive electrical and electronic circuits in an electrical load coupled to the AC power lines, said AC power lines
5 having an earth ground and said electrical load having an electrical load ground, said apparatus comprising:

an isolation transformer having a primary winding and a secondary winding, said
10 primary winding having a primary source lead, a primary neutral lead, and a primary electrostatic shield lead, said secondary winding having a secondary source lead, a secondary neutral lead, and a secondary
15 electrostatic shield lead;

said primary source lead, primary neutral lead and primary electrostatic shield lead being electrically coupled to the AC
20 power lines;



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25 said secondary source lead, secondary
 neutral lead and secondary electrostatic
 shield lead being electrically coupled to the
 electrical load;

30 said primary electrostatic shield lead
 and said secondary electrostatic shield lead
 being electrically connected together and to
 the earth ground; and

35 continuous attenuator means for attenu-
 ating high frequency transients electrically
 coupled between the earth ground and the
 electrical load ground.

2. An apparatus as claimed in Claim 1, wherein
said continuous attenuator means is comprised of a
plurality of toroid cores and a single continuous
strand of wire being wound individually and
5 sequentially a number of turns around each of said
plurality of toroid cores, said strand of wire having a
first end connected to the earth ground and a second
end connected to the electrical load ground.



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3. An apparatus as claimed in Claim 2, wherein a first three of said plurality of toroid cores are tuned to a frequency range between 50 KHz and 100 KHz, a second two of said plurality of toroid cores are tuned
5 to a frequency of 100 MHz, and a third two of said plurality of toroid cores are tuned to a frequency of 200 MHz.

4. An apparatus as claimed in Claim 3, further comprising high voltage clamping means coupled between said secondary source lead and said secondary neutral lead of said isolation transformer for clamping a
5 voltage therebetween to a predetermined level.

5. An apparatus as claimed in Claim 4, wherein said clamping means is a metal oxide varistor.

6. An apparatus as claimed in Claim 5, further comprising filter capacitor means also coupled between said secondary source lead and said secondary neutral lead of said isolation transformer for attenuating high
5 frequency voltage and current pulses.



7. An apparatus for attenuating high frequency
transients on AC power lines from damaging sensitive
electrical and electronic circuits in an electrical
load coupled to the AC power lines, said AC power lines
5 having an earth ground and said electrical load having
an electrical load ground, said apparatus comprising:

ground fault current interruptor means
having input leads and output leads for elec-
10 trically coupling said output leads to said
input leads in a first mode of operation and
for electrically isolating said output leads
from said input leads in a second mode of
operation;

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said input leads being electrically
coupled to the AC power lines;

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said output leads being electrically
coupled to the electrical load;

said ground fault current interruptor
being electrically connected to the earth
ground; and

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continuous attenuator means for attenuating high frequency transients electrically coupled between the earth ground and the electrical load ground.

8. An apparatus as claimed in Claim 7, wherein said continuous attenuator means is comprised of a plurality of toroid cores and a single continuous strand of wire being wound individually and
5 sequentially a number of turns around each of said plurality of toroid cores, said strand of wire having a first end connected to the earth ground and a second end connected to the electrical load ground.

9. An apparatus as claimed in Claim 8, wherein a first three of said plurality of toroid cores are tuned to a frequency range between 50 KHz and 100 KHz, a second two of said plurality of toroid cores are tuned
5 to a frequency of 100 MHz, and a third two of said plurality of toroid cores are tuned to a frequency of 200 MHz.



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10. An apparatus as claimed in Claim 9, further comprising high voltage clamping means coupled between said secondary source lead and said secondary neutral lead of said isolation transformer for clamping a
5 voltage therebetween to a predetermined level.

11. An apparatus as claimed in Claim 10, wherein said clamping means is a metal oxide varistor.

12. An apparatus as claimed in Claim 11, further comprising filter capacitor means also coupled between said secondary source lead and said secondary neutral lead of said isolation transformer for attenuating high
5 frequency voltage and current pulses.



13. A method for attenuating high frequency
transients on AC power lines from damaging sensitive
electrical and electronic circuits in an electrical
load coupled to the AC power lines, said AC power lines
5 having an earth ground and said electrical load having
an electrical load ground, said method comprising the
steps of:

coupling electrically input leads of an
10 isolation device to the AC power source;

coupling electrically output leads of
the isolation device to the electrical load;

15 coupling electrically the isolation
device to the earth ground; and

attenuating high frequency transients in
a continuous attenuator circuit electrically
20 coupled between the earth ground and the
electrical load ground.

14. A method as claimed in Claim 13, wherein said
continuous attenuator means is comprised of a plurality



of toroid cores and a single continuous strand of wire being wound individually and sequentially a number of turns around each of said plurality of toroid cores, said strand of wire having a first end connected to the earth ground and a second end connected to the electrical load ground.

15. A method as claimed in Claim 14, wherein a first three of said plurality of toroid cores are tuned to a frequency range between 50 KHz and 100 KHz, a second two of said plurality of toroid cores are tuned to a frequency of 100 MHz, and a third two of said plurality of toroid cores are tuned to a frequency of 200 MHz.

16. A method as claimed in Claim 15, further comprising high voltage clamping means coupled between said secondary source lead and said secondary neutral lead of said isolation transformer for clamping a voltage therebetween to a predetermined level.

17. A method as claimed in Claim 16, wherein said clamping means is a metal oxide varistor.



18. A method as claimed in Claim 17, further comprising filter capacitor means also coupled between said secondary source lead and said secondary neutral lead of said isolation transformer for attenuating high
5 frequency voltage and current pulses.

19. A method as claimed in Claim 13, wherein said isolation device is an isolation transformer.

20. A method as claimed in Claim 13, wherein said isolation device is a ground fault current interruptor.