

Description

This invention relates to a method and circuitry for detecting and removing additive transient disturbances in a data channel, and more particularly, to a method and circuitry for suppressing electrical transients caused by a temperature change in a magneto-resistive (MR) sensor due to physical contact of said sensor with the recording surface of a rotating magnetic disk.

Disturbances which occur in a data channel can be categorized as either additive or multiplicative. An undesirable additive disturbance signal is simply added to the information (data) signal. An undesirable multiplicative disturbance or data density change causes a modulation of the data signal.

In a data channel where the signal sensing transducers are magneto-resistive (MR) sensors exposed to the air in the air bearing surface of a slider assembly and a rotating magnetic disk, additive disturbances can occur due to physical frictional contact of the sensor(s) with the moving recording surface of the disk. The disturbances result from the friction-generated elevated temperature (up to 120°C) at the contact spot. This produces a small yet sudden increase in temperature of the MR sensor; e.g., in the order of 1°C averaged over the entire sensor within about 50 to 100 nanoseconds. Due to the nonzero temperature coefficient of resistance of the MR sensor (approximately 0.003/°C for permalloy), the sensor resistance will increase with this sudden temperature rise. The heat conducted into the MR sensor from the hot spot will diffuse slowly to the environment of the sensor, causing the resistance increase to decay slowly to the original value. Typically, a drop to about 30% of the thermally induced resistance change will occur in 1.5 to 5 μs. The MR sensor is used for detecting magnetic signals by the magneto-resistive effect. The sensor is biased with a constant direct current (DC) to convert the resistance changes due to the magnetic information into a data voltage signal for later amplification. The thermally induced resistance change will then lead to an additive disturbance upon which the data signal is superimposed. The nonlinearity of such an MR sensor increases with increasing magnetic signal excursions around its bias point. Therefore, these magnetic excursions are kept sufficiently small giving at most a relative change in sensor resistance of ± 0.3%. Therefore thermal disturbance signals can be up to four times the base-to-peak data amplitude and possibly even greater.

Such a combination of signal and disturbance causes many problems with signal detection in the data channel. The automatic gain control (AGC) circuit in the channel may fade out quickly during the transient and recover only slowly. Even if the

AGC circuit were to accommodate the disturbed signal, the thermal transient would still result in a peak shift; i.e., the data signal is differentiated for peak detection; and as a result of this the thermal transient will also be differentiated. This leads to an extra zero crossing and a shift of the zero-crossing level directly after the thermal transient.

There is a need for a method and apparatus for suppressing additive transient disturbances that are caused in a data channel by a temperature change (hereinafter referred to as a thermal asperity) in an MR sensor due to frictional contact with the moving recording surface of a magnetic disk. Such suppression cannot be achieved by the prior art approaches known to the applicants because the MR sensor as used in hard disk products is not provided with a center tap (which could be utilized to balance out thermal transients), the spectral content of the thermal transient disturbance is too close to the spectral content of the data signal to be filtered out, and the problems associated with high-frequency AC biasing are for all practical purposes unsolvable.

In addition to the prior art approaches above described, US-A-3,566,281 discloses positive and negative peak detectors which are offset by a constant voltage and averaged and subtracted from a delayed input signal. Note that the outputs of each detector are cross connected for resetting each detector to zero after the pulse has been processed. That patent document merely describes clipping level circuitry in which, as the positive peak detector detects a positive peak, the negative peak detector is reset to zero, and vice versa. That patent document and others (such as US-A-3,473,131 and US-A-4,356,389) less pertinent do not and cannot solve the problem to which the applicants' invention is directed. They do not disclose means for ensuring that both detectors respond rapidly to the onset of an additive disturbance, or means to reduce residue components and produce an output signal free of the additive disturbance.

The invention provides circuitry for suppressing an additive transient disturbance in an input data signal, comprising a positive envelope detector and a negative envelope detector, both having the data signal as their inputs, and providing respective outputs containing an envelope component and a residue component; summing means for summing the envelope components; the circuitry being characterised by: means interconnecting said detectors for insuring that both envelope detectors respond rapidly to the onset of the additive disturbance; nonlinear signal-adaptive filter means connected to the summed output from said summing means for reducing the residue component; and second summing means for summing or subtracting

ting the input data signal with an output derived from said filter means for producing an output signal free of the additive disturbance.

A method and circuit are disclosed hereinafter for suppressing additive transient disturbances in a data channel. These disturbances may be due to thermal asperity transients caused by an MR transducer contacting a moving storage surface.

How the invention can be carried out will now be described by way of example, with reference to the accompanying drawings, in which:-

Fig. 1 depicts an input data signal, and an additive transient disturbance superimposed on the data signal in a data channel;

Fig. 2 is a schematic diagram of a circuit embodying the invention for suppressing the additive transient disturbance superimposed on the data signal in the data channel;

Fig. 3 depicts negative and positive envelope signals and an estimated disturbance signal resultant from the sum thereof divided by two;

Fig. 4 depicts an estimated disturbance signal after the application of non-linear signal adaptive filtering;

Fig. 5 depicts an output signal from which the estimated disturbance signal (i.e. the output of the non-linear signal adaptive filter) has been subtracted; and

Fig. 6 depicts a more detailed schematic diagram of the circuitry illustrated in Fig. 2.

A data signal I, without and with an additive transient disturbance superimposed thereon, are depicted in Fig. 1. The circuit illustrated in Fig. 2, which embodies the invention, suppresses such additive transient disturbances to provide output signals free of additive disturbances. This circuit ensures that only the additive component (such as due to thermal transients) will be detected and not the multiplicative component (due to density modulation resulting from bit density variations).

Referring to Fig. 2, assume initially that the input signal I contains both data and a superimposed additive disturbance due, for example, to a thermal asperity. Signal I is fed via line 10 to both a positive envelope detector 11 and a negative envelope detector 12. The positive envelope 11' and negative envelope 12' of signal I (Fig. 3) are summed at block 13 to produce a summed signal 13' (Fig. 3). Envelope signals 11', 12' contain not only an envelope component but also a residue component that is pattern dependent and correlated to the input data in signal I. These correlated residue components result from the small time constant used in the envelope detectors 11, 12. Detectors 11, 12 are connected in a "peristaltic" fashion; i.e., the positive envelope signal pulls up the negative envelope signal simultaneously at the onset of a thermal transient disturbance, causing

the negative envelope detector 12 to follow the fast positive signal excursions that then occur. This peristaltic connection alters the residue profile of the negative envelope signal 12' with respect to that of the positive envelope signal 11'.

A buffer 14 is preferably interposed between the outputs of detectors 11, 12 in parallel with summing block 13 to accomplish the peristaltic connection. The signals 11', 12' are added by the summing block. To reduce the correlated residue in the first estimate of the additive disturbance as denoted by the signal in 13', a nonlinear signal-adaptive filter 15 is preferably used. Filter 15 is constructed as a low-pass network with a single pole that is a function of the difference in voltage between the filter output 15' and input 13' (the DC gain of the filter being unity).

When the signal across filter 15 is low in amplitude, the pole frequency is low and the aforementioned correlated residue is filtered out. When this signal is high in amplitude, as it is when a thermal asperity occurs, then the pole frequency moves up to track the fast rise time that occurs at the onset of the thermal transient disturbance. During decay of the transient disturbance, this signal difference becomes small again, permitting the pole frequency to assume its normal low value. This filtered signal 15' is then attenuated two times by attenuator 16 to the appropriate level and used as the estimated disturbance signal 16' (Fig. 4). A delay means 17, having a delay time equal to that of the disturbance estimating circuitry just described, preferably is interposed between a branch of input line 10 and a summing block 18. Depending upon whether the gain blocks 20, 29 and 16 are of the inverting or noninverting type, block 18 adds to or subtracts from the delayed version of input signal I the estimated disturbance signal 16' to produce an output signal O in line 19 which is free of additive disturbances (see Fig. 5). Note that Fig. 5 shows the estimated disturbance signal obtained without use of the delay means 17; however, by use of the delay means the glitch at X can desirably be eliminated.

Assume now that the input signal I consists solely of data and noise; i.e., no additive disturbance. Under the assumed condition, the signal will still be fed through the envelope detectors 11, 12. With no additive disturbance, the output from block 13 will constitute only the residue component. Thus the estimated disturbance signal 16', which represents only what is left over after the nonlinear filter 15 filters out the residue component, will be summed at block 18 with the delayed input signal 17' from delay element 17.

A more detailed schematic representation of the circuitry of Fig. 2 is shown in Fig. 6 in which identical reference numerals are used, where ap-

propriate.

Input signal I in line 10 is amplified by a gain block 20. Current sources 21, 22 are used to bias diodes 23, 24, respectively, used in the envelope detectors 11, 12. Positive envelope detector 11 comprises diode 24 and capacitor 25. Negative envelope detector 12 comprises diode 23 and capacitor 26. Capacitor 26 would normally be connected to ground as capacitor 25 is; however, because the onset of a thermal asperity transient has a very fast associated rise time, diode 23 would normally be temporarily shut off and thus not permit the negative envelope to follow the signal. Since a thermal asperity-induced event produces a signal excursion in one polarity only, the previously described "peristaltic" connection is accomplished by connecting capacitor 26 to capacitor 25 preferably by way of buffer 14 instead of to ground. This connection permits both envelope detectors 11, 12 to follow fast positive signal excursions. However, the charging and discharging of both capacitors 25, 26 is now coupled due to the peristaltic connection. To prevent such coupling of charge paths and also minimize the amplitude of the aforementioned residue component, buffer 14 is inserted between capacitors 25, 26, as shown.

Summing block 13 comprises resistors 27, 28. The resultant summed signal is amplified by gain block 29 and fed into the nonlinear filter 15. Filter 15 comprises resistors 30, 31, 32, 33, diodes 34, 35 and capacitor 36. Current sources 37, 38, bias diodes 34, 35 to an optimal operating point by generating a bias voltage with resistors 30, 32. Capacitor 36 sets the time constant of the nonlinear filter 15 with the differential resistance associated with diodes 34, 35, the resistance of resistor 33 being much larger than said differential resistance. The impedance of diodes 34, 35 therefore determines the overall pole location of filter 15. As a result, it is adaptive to the voltage between the input and output of the filter. If this voltage difference is high, a high filter roll-off frequency will result, whereas a low voltage difference will yield a low filter roll-off frequency. Resistor 31 is preferably provided to limit the minimum filter roll-off frequency (i.e., the maximum time constant).

Attenuator 16 comprises a gain block that provides a negative-going output disturbance signal estimate. Summing block 18 comprises resistors 40, 41. The estimated disturbance signal 16' is summed with the delayed input signal 17' from delay means 17, and the resultant signal is amplified by a gain block 42 to produce in line 19 the data output signal 0 free of the additive disturbance.

In a preferred embodiment of the invention, the circuitry above described would be interposed in the data channel between an arm select amplifier

(not shown) and an automatic gain control (AGC) circuit (not shown) by connecting line 10 to the select amplifier and line 19 to the AGC circuit. A switch 50 is preferably provided which, when in the position shown, provides the data output signal in line 19 free of additive disturbances. However, switch 50 is preferably normally connected to ground via line 51 and actuated to its shown position by suitable means (not shown) only when uncorrectable errors are detected during a retry operation; such arrangement is especially desirable when data errors due to additive disturbances occur very infrequently, as will usually be the case.

The apparatus as thus far described may be used to warn of an imminent "head crash" by adding the optional circuitry now to be described. ("Head crash" is defined as near continuous contact of the MR head or sensor with the surface of the rotating disk.) This optional circuitry comprises a buffer 60 having its input commoned to the input to attenuator 16. The output of buffer 60 is compared at 61 with a reference voltage V_{ref} to provide an output to counter 62 whenever a thermally induced additive disturbance is sensed. Counter 62 will generate a warning signal in line 63 to initiate a desired control operation, such as shutting down the disk file to prevent further damage, whenever there is more than a preselected number of counted disturbances (or, if preferred, more than a preselected number per predetermined period of time).

This optional circuitry may also be used for asperity mapping of the disk surface and/or MR sensor glide height testing during manufacture.

It will now be apparent that a simple and effective method and circuitry has been described herein for removing additive transient disturbances in a data channel; e.g., such as due to a thermal asperity resulting from contact of the head or sensor with the surface of the rotating disk. Also, optionally, the number and/or frequency of these disturbances can be counted and used to trigger a desired control operation.

If desired, the delay means 17 may be eliminated. However, if this is done, there will be a difference in the timing of the estimated disturbance signal 16' with respect to the input data signal I in line 10 containing the unprocessed asperity. This difference will cause in the output signal 0, an amplitude disturbance the length of which is proportional to said timing difference.

Claims

1. Circuitry for suppressing an additive transient disturbance in an input data signal, comprising a positive envelope detector (11) and a negative envelope detector (12), both having



propriate.

Input signal *I* in line 10 is amplified by a gain block 20. Current sources 21, 22 are used to bias diodes 23, 24, respectively, used in the envelope detectors 11, 12. Positive envelope detector 11 comprises diode 24 and capacitor 25. Negative envelope detector 12 comprises diode 23 and capacitor 26. Capacitor 26 would normally be connected to ground as capacitor 25 is; however, because the onset of a thermal asperity transient has a very fast associated rise time, diode 23 would normally be temporarily shut off and thus not permit the negative envelope to follow the signal. Since a thermal asperity-induced event produces a signal excursion in one polarity only, the previously described "peristaltic" connection is accomplished by connecting capacitor 26 to capacitor 25 preferably by way of buffer 14 instead of to ground. This connection permits both envelope detectors 11, 12 to follow fast positive signal excursions. However, the charging and discharging of both capacitors 25, 26 is now coupled due to the peristaltic connection. To prevent such coupling of charge paths and also minimize the amplitude of the aforementioned residue component, buffer 14 is inserted between capacitors 25, 26, as shown.

Summing block 13 comprises resistors 27, 28. The resultant summed signal is amplified by gain block 29 and fed into the nonlinear filter 15. Filter 15 comprises resistors 30, 31, 32, 33, diodes 34, 35 and capacitor 36. Current sources 37, 38, bias diodes 34, 35 to an optimal operating point by generating a bias voltage with resistors 30, 32. Capacitor 36 sets the time constant of the nonlinear filter 15 with the differential resistance associated with diodes 34, 35, the resistance of resistor 33 being much larger than said differential resistance. The impedance of diodes 34, 35 therefore determines the overall pole location of filter 15. As a result, it is adaptive to the voltage between the input and output of the filter. If this voltage difference is high, a high filter roll-off frequency will result, whereas a low voltage difference will yield a low filter roll-off frequency. Resistor 31 is preferably provided to limit the minimum filter roll-off frequency (i.e., the maximum time constant).

Attenuator 16 comprises a gain block that provides a negative-going output disturbance signal estimate. Summing block 18 comprises resistors 40, 41. The estimated disturbance signal 16' is summed with the delayed input signal 17' from delay means 17, and the resultant signal is amplified by a gain block 42 to produce in line 19 the data output signal 0 free of the additive disturbance.

In a preferred embodiment of the invention, the circuitry above described would be interposed in the data channel between an arm select amplifier

(not shown) and an automatic gain control (AGC) circuit (not shown) by connecting line 10 to the select amplifier and line 19 to the AGC circuit. A switch 50 is preferably provided which, when in the position shown, provides the data output signal in line 19 free of additive disturbances. However, switch 50 is preferably normally connected to ground via line 51 and actuated to its shown position by suitable means (not shown) only when uncorrectable errors are detected during a retry operation; such arrangement is especially desirable when data errors due to additive disturbances occur very infrequently, as will usually be the case.

The apparatus as thus far described may be used to warn of an imminent "head crash" by adding the optional circuitry now to be described. ("Head crash" is defined as near continuous contact of the MR head or sensor with the surface of the rotating disk.) This optional circuitry comprises a buffer 60 having its input commoned to the input to attenuator 16. The output of buffer 60 is compared at 61 with a reference voltage V_{ref} to provide an output to counter 62 whenever a thermally induced additive disturbance is sensed. Counter 62 will generate a warning signal in line 63 to initiate a desired control operation, such as shutting down the disk file to prevent further damage, whenever there is more than a preselected number of counted disturbances (or, if preferred, more than a preselected number per predetermined period of time).

This optional circuitry may also be used for asperity mapping of the disk surface and/or MR sensor glide height testing during manufacture.

It will now be apparent that a simple and effective method and circuitry has been described herein for removing additive transient disturbances in a data channel; e.g., such as due to a thermal asperity resulting from contact of the head or sensor with the surface of the rotating disk. Also, optionally, the number and/or frequency of these disturbances can be counted and used to trigger a desired control operation.

If desired, the delay means 17 may be eliminated. However, if this is done, there will be a difference in the timing of the estimated disturbance signal 16' with respect to the input data signal *I* in line 10 containing the unprocessed asperity. This difference will cause in the output signal 0, an amplitude disturbance the length of which is proportional to said timing difference.

Claims

1. Circuitry for suppressing an additive transient disturbance in an input data signal, comprising a positive envelope detector (11) and a negative envelope detector (12), both having

the data signal as their inputs, and providing respective outputs containing an envelope component and a residue component;

summing means (13) for summing the envelope components;

the circuitry being characterised by:

means (14) interconnecting said detectors for insuring that both envelope detectors respond rapidly to the onset of the additive disturbance;

nonlinear signal-adaptive filter means (15) connected to the summed output from said summing means (13) for reducing the residue component; and

second summing means (18) for summing or subtracting the input data signal with an output derived from said filter means for producing an output signal free of the additive disturbance.

2. Circuitry as claimed in claim 1, including attenuation means (16) for attenuating the output of said filter means; and

delay means (17) for delaying the input signal to said second summing means.

3. Circuitry as claimed in claim 1 or claim 2, including delay means (17) having a delay time corresponding to the cumulative time delays in processing the data signal through the circuitry previously described for correspondingly delaying said input data signal to said second summing means.

4. Circuitry as claimed in any preceding claim, including means responsive to a preselected number of additive disturbances to initiate a desired control operation.

5. Circuitry as claimed in any of claims 1 to 3, including means responsive to a preselected number of additive disturbances per predetermined unit of time to initiate a desired control operation.

6. Circuitry as claimed in any of claims 1 to 3, including means for detecting a counting the number of additive disturbances.

7. Circuitry as claimed in any preceding claim, wherein said interconnecting means comprises a buffer (14) to ensure substantially simultaneous response to the onset of the additive disturbance.

8. Circuitry as claimed in any preceding claim, including at least one magnet-resistive (MR) transducer for producing the input data signal

and wherein the disturbances are due to thermal asperity transients caused by an MR transducer contacting a storage surface moving relative to said transducer.

9. A method of suppressing an additive disturbance signal in an input data signal, comprising the steps of:

deriving from the input signal positive and negative envelope signals each having a respective pattern-dependent residue component correlated to the input signal; and

summing the envelope signals;

the method being characterised by the steps of:

constraining the negative envelope signals to follow fast positive signal excursions at the onset of a disturbance-causing event,

filtering the summed signal using a nonlinear signal-adaptive filter to reduce its residue content; and

adding or subtracting the input data signal with the output of the filtering means for producing an output signal free of the additive disturbance.

10. A method as claimed in claim 9, further including the step of:

attenuating the filtered signal for estimating the magnitude and shape of the disturbance signal; and

adding to or subtracting from the input signal the estimated disturbance signal.

11. A method as claimed in claim 9 or claim 10, further including the step of:

detecting the number of additive disturbances.

12. A method as claimed in claim 9 or claim 10, further including the steps of:

counting the number of additive disturbances; and

initiating a desired control operation whenever said number exceeds a preselected value.

Patentansprüche

1. Eine Schaltung zur Unterdrückung einer kurzzeitigen additiven Störung in einem Eingangssignalsignal, welche folgendes umfaßt:
einen Detektor für positive Hüllkurven (11) und einen Detektor für negative Hüllkurven (12), bei denen jeweils am Eingang das Datensignal anliegt und die entsprechende Ausgangssignale liefern, die eine Hüllkurvenkomponente und eine Restkomponente enthalten,
ein Summiermittel (13) zur Addition der Hüll-



- kurvenkomponenten,
wobei die Schaltung gekennzeichnet ist durch:
ein Mittel (14), das die Detektoren untereinander verbindet und gewährleistet, daß beide Hüllkurvendetektoren bei Einsetzen der additiven Störung rasch ansprechen,
ein nichtlineares signaladaptives Filtermittel (15), das mit dem Summenausgang des Summiermittels (13) verbunden ist und dazu dient, die Restkomponente zu verringern, und
ein zweites Summiermittel (18) zur Addition oder Subtraktion des Eingangsdatensignals zu oder von einem Ausgangssignal, das von dem Filtermittel abgeleitet wird, zur Erzeugung eines Ausgangssignals, das von der additiven Störung frei ist.
2. Eine Schaltung nach Anspruch 1 mit einem Dämpfungsmittel (16) zur Dämpfung des Ausgangssignals des Filtermittels und ein Verzögerungsmittel (17) zur Verzögerung des Eingangssignals für das zweite Summiermittel.
 3. Eine Schaltung nach Anspruch 1 oder Anspruch 2 mit einem Verzögerungsmittel (17), dessen Verzögerungszeit den kumulierten Zeitverzögerungen entspricht, die bei der Verarbeitung des Datensignals durch die vorstehend beschriebene Schaltung entstehen, so daß das Eingangsdatensignal für das zweite Summiermittel entsprechend verzögert wird.
 4. Eine Schaltung nach den vorstehenden Ansprüchen mit einem Mittel, das auf eine vorgegebene Anzahl additiver Störungen anspricht und damit eine bestimmte Steuerungsoperation auslöst.
 5. Eine Schaltung nach den vorstehenden Ansprüchen 1 bis 3 mit einem Mittel, das auf eine vorgegebene Anzahl additiver Störungen innerhalb einer festzulegenden Zeiteinheit anspricht und damit eine bestimmte Steuerungsoperation auslöst.
 6. Eine Schaltung nach den vorstehenden Ansprüchen 1 bis 3 mit einem Mittel zur Erkennung und Zählung der Anzahl additiver Störungen.
 7. Eine Schaltung nach den vorstehenden Ansprüchen, wobei das Verbindungsmittel einen Puffer (14) umfaßt, der das annähernd zeitgleiche Ansprechen auf das Einsetzen der additiven Störung gewährleistet.
 8. Eine Schaltung nach den vorstehenden Ansprüchen mit mindestens einem magnetoresi-

stiven (MR-) Wandler zur Erzeugung des Eingangsdatensignals, wobei die Störungen durch kurzzeitige thermische Rauheit verursacht werden, die dadurch entsteht, daß ein MR-Wandler eine Aufzeichnungsoberfläche berührt, die sich relativ zu dem Wandler bewegt.

9. Ein Verfahren zur Unterdrückung eines additiven Störsignals in einem Eingangsdatensignal, das folgende Schritte umfaßt: Ableiten von positiven und negativen Hüllkurvensignalen von dem Eingangssignal, wobei die Hüllkurvensignale jeweils eine entsprechende verlaufsabhängige Restkomponente aufweisen, die mit dem Eingangssignal korreliert, und Addieren der Hüllkurvensignale, wobei das Verfahren durch folgende Schritte gekennzeichnet ist:
Veranlassen der negativen Hüllkurvensignale, schnellen positiven Signalauslenkungen bei Einsetzen eines störungsauslösenden Ereignisses zu folgen,
Filtern des Summensignals mit Hilfe eines nichtlinearen signaladaptiven Filters, um dessen Restanteil zu verringern und
Addieren oder Subtrahieren des Ausgangssignals aus dem Filterschritt zu dem oder von dem Eingangsdatensignal, um eine Ausgangssignal zu erhalten, das von der additiven Störung frei ist.
10. Ein Verfahren nach Anspruch 9, welches weiterhin die folgenden Schritte umfaßt:
Dämpfen des gefilterten Signals zur Abschätzung von Intensität und Form des Störsignals und
Addieren oder Subtrahieren des geschätzten Störsignals zu dem oder von dem Eingangssignal.
11. Ein Verfahren nach Anspruch 9 oder Anspruch 10, welches weiterhin den folgenden Schritt umfaßt:
Erkennen der Anzahl additiver Störungen.
12. Ein Verfahren nach Anspruch 9 oder Anspruch 10, welches weiterhin die folgenden Schritte umfaßt:
Zählen der Anzahl additiver Störungen und
Auslösen einer bestimmten Steuerungsoperation, sobald diese Anzahl einen vorgegebenen Wert überschreitet.

Revendications

1. Circuit pour supprimer une perturbation transitoire d'addition dans un signal de données d'entrée, comprenant



un détecteur (11) d'enveloppe positive et un détecteur (12) d'enveloppe négative, ayant tous les deux le signal de données sur leurs entrées, et délivrant des sorties respectives contenant une composante d'enveloppe et une composante résiduelle;

des moyens de sommation (13) pour additionner les composantes d'enveloppe;

le circuit étant caractérisé par:

des moyens (14) interconnectant lesdits détecteurs pour assurer que les deux détecteurs d'enveloppe répondent rapidement à l'établissement de la perturbation d'addition;

des moyens (15) formant filtre linéaire adaptatif pour signaux connectés à la sortie additionnée en provenance desdits moyens (13) de sommation pour réduire la composante résiduelle; et

des seconds moyens (18) de sommation pour additionner ou soustraire le signal de données d'entrée avec une sortie en provenance des moyens de filtrage pour produire un signal de sortie sans la perturbation d'addition.

2. Circuit selon la revendication 1, comportant des moyens (16) d'atténuation pour atténuer la sortie desdits moyens de filtrage; et

des moyens (17) à retard pour retarder le signal d'entrée desdits seconds moyens de sommation.

3. Circuit selon la revendication 1 ou la revendication 2, comprenant des moyens à retard (17) ayant un retard correspondant aux retards cumulés lors du traitement du signal de données par le circuit précédemment décrit pour retarder de manière correspondante ledit signal de données d'entrée desdits seconds moyens de sommation.

4. Circuit selon l'une quelconque des revendications précédentes, comportant des moyens sensibles à un nombre présélectionné de perturbations d'addition afin d'amorcer une opération de commande souhaitée.

5. Circuit selon l'une quelconque des revendications 1 à 3, comportant des moyens sensibles à un nombre présélectionné de perturbations d'addition par unité de temps prédéterminée afin d'amorcer une opération de commande souhaitée.

6. Circuit selon l'une quelconque des revendications 1 à 3, comportant des moyens pour détecter un comptage du nombre de perturbations d'addition.

7. Circuit selon l'une quelconque des revendications précédentes, dans lequel lesdits moyens d'interconnexion comportent un tampon (14) pour assurer une réponse sensiblement simultanée à l'établissement de la perturbation d'addition.

8. Circuit selon l'une quelconque des revendications précédentes, comportant au moins un transducteur à aimant-résistance (MR) pour produire le signal de données d'entrée et dans lequel les perturbations sont dues à des transitoires d'élévation thermique causés par un transducteur MR en contact avec une surface d'enregistrement se déplaçant par rapport audit transducteur.

9. Procédé de suppression d'un signal de perturbation d'addition dans un signal de données d'entrée, comprenant les étapes suivantes:

obtention à partir du signal d'entrée de signaux d'enveloppe positive et négative ayant chacun une composante résiduelle respective fonction de la configuration, corrélée au signal d'entrée; et

addition des signaux d'enveloppe;

le procédé étant caractérisé par les étapes suivantes:

contrainte des signaux d'enveloppe négative pour qu'ils suivent des excursions de signal positif rapide lors de l'établissement d'un événement conduisant à la perturbation;

filtrage du signal additionné en utilisant un filtre non linéaire adaptatif aux signaux afin de réduire son contenu résiduel; et

addition ou soustraction du signal de données d'entrée avec la sortie de l'étape de filtrage pour produire un signal de sortie sans la perturbation d'addition.

10. Procédé selon la revendication 9, comprenant en outre l'étape de:

atténuation du signal filtré pour estimer l'amplitude et la forme du signal de perturbation; et

addition au, ou soustraction du, signal d'entrée du signal de perturbation estimé.

11. Procédé selon la revendication 9 ou la revendication 10, comprenant en outre l'étape de:

détection du nombre de perturbations d'addition.

12. Procédé selon la revendication 9 ou la revendication 10, comprenant en outre les étapes de:

comptage du nombre de perturbations d'addition; et

amorce d'une opération de commande



souhaitée lorsque ledit nombre excède une valeur présélectionnée.



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