

DESCRIPTION

FILLED FLUORORESIN SHEET, PROCESS FOR PRODUCING THE SAME, AND
GASKET

5

TECHNICAL FIELD

[0001]

The present invention relates to a filled fluororesin
sheet, a process for producing the same, and a gasket.

10

BACKGROUND ART

[0002]

A filled fluororesin sheet is a sheet of a fluororesin
containing a filler. The sheet shows chemical resistance and
15 heat resistance of the fluororesin as well as the inherent
functions and properties of the filler. In addition, the
filler improves poor creep resistance of the fluororesin. The
sheet thus has wide applications including sealing materials.

[0003]

20

For use as sealing materials, the properties of
fluororesins, for example creep properties, are improved by
the addition of fillers such as metals, graphite and inorganic
fillers. Such materials are used as gaskets and the like.

[0004]

Filled fluororesin sheets suited as gasket materials are known in the art. For example, JP-A-2004-323717 (Patent Literature 1) discloses a filled fluororesin sheet suited as a gasket material which contains a swelling mineral and a filler
5 (except swelling minerals).

[0005]

JP-A-2007-253519 (Patent Literature 2) discloses a process for producing fluororesin sheets which includes a step of rolling a sheet-forming resin composition containing a
10 fluororesin, a filler (such as talc or clay) and a specific solvent under specific conditions. The literature describes that the filled fluororesin sheet obtained by the process achieves high stress relaxation properties and high airtightness and is suited as a gasket material.

15 [0006]

Further, fluororesin materials that contain a filler having a specific Mohs hardness are known in the art. For example, JP-B-H06-74810 (Patent Literature 3) discloses a slide member material that contains a polytetrafluoroethylene
20 resin as a main component and 0.5 to 10 wt% of powder of at least one abrasive selected from chromium oxide, silicon carbide, aluminum oxide and mixtures containing at least one of these compounds, the abrasive powder having a Mohs hardness of not less than 5 and an average particle diameter of less

than 5 μm . The literature describes that the use of the specific abrasive improves abrasive resistance properties of PTFE.

[0007]

5 JP-A-H08-239682 (Patent Literature 4) discloses a slide member composition which is based on a synthetic resin including PTFE and contains 0.003 to 0.3% by volume of inorganic fine particles having a Mohs hardness of not less than 9 and an average particle diameter of not more than 10 μm . The
10 literature describes that the addition in the trace amount of the inorganic fine particles having a high Mohs hardness to various synthetic resin materials realizes synthetic resin slide materials which have excellent abrasion resistance without damaging a mating member or increasing the friction
15 therebetween.

Citation List

Patent Literatures

[0008]

20 Patent Literature 1: JP-A-2004-323717
Patent Literature 2: JP-A-2007-253519
Patent Literature 3: JP-B-H06-74810
Patent Literature 4: JP-A-H08-239682

SUMMARY OF INVENTION

Technical Problem

[0009]

However, gaskets that are composed of the conventional
5 filled fluoro-resin sheets, for example clay- or talc-filled
fluoro-resin sheets described in Patent Literatures 1 and 2,
are still insufficient in terms of stress relaxation properties,
in particular at a high temperature.

[0010]

10 The present invention has been made in view of the problems
in the art described above. It is therefore an object of the
invention to provide a filled fluoro-resin sheet excellent in
stress relaxation properties, in particular stress relaxation
properties at a high temperature, a process for the production
15 thereof, and a filled fluoro-resin sheet gasket having excellent
stress relaxation properties.

[0011]

Patent Literatures 3 and 4 do not teach or suggest that
the high-hardness filler is added to the fluoro-resin (such as
20 PTFE) to improve stress relaxation properties of the
fluoro-resin sheet, or the fluoro-resin containing the
high-hardness filler is used as a gasket material.

Solution to Problem

[0012]

The present inventor carried out studies and has found that a fluororesin sheet containing a specific filler solves the problems described above. The present invention has been
5 completed based on the finding.

[0013]

A filled fluororesin sheet according to the invention comprises a fluororesin and an inorganic filler having a revised Mohs hardness of not less than 8, in a fluororesin:inorganic
10 filler volume ratio of 30-55:70-45 (wherein the total of the two is 100).

[0014]

A process for producing filled fluororesin sheets according to the invention comprises a step of rolling a
15 sheet-forming resin composition which comprises a fluororesin, an inorganic filler having a revised Mohs hardness of not less than 8 and a processing aid and in which the volume ratio of the fluororesin and the inorganic filler (fluororesin:
inorganic filler) is 30-55:70-45 (wherein the total of the two
20 is 100).

[0015]

The inorganic filler may be at least one material selected from the group consisting of diamond, hexagonal boron nitride, boron carbide, silicon carbide, silicon nitride, tungsten

carbide, α -alumina, tantalum carbide, fused zirconia, garnet, topaz and zirconia.

[0016]

A gasket according to the invention comprises the filled
5 fluororesin sheet of the invention.

Advantageous Effects of Invention

[0017]

The filled fluororesin sheet of the invention has
10 excellent stress relaxation properties, in particular at a high temperature.

[0018]

The inventive process for producing filled fluororesin sheets can produce filled fluororesin sheets which have
15 excellent stress relaxation properties, in particular excellent stress relaxation properties at a high temperature.

[0019]

The gasket of the invention has excellent stress relaxation properties, in particular at a high temperature.

20

DESCRIPTION OF EMBODIMENTS

[0020]

The present invention will be described in greater detail hereinbelow.

[0021]

[Filled fluororesin sheets]

A filled fluororesin sheet according to the invention contains a fluororesin and an inorganic filler having a revised
5 Mohs hardness of not less than 8, in a fluororesin:inorganic filler volume ratio of 30-55:70-45 (wherein the total of the two is 100).

[0022]

(Fluororesins)

10 Examples of the fluororesins include
polytetrafluoroethylene resins (PTFEs), modified PTFEs,
polyvinylidene fluoride resins (PVDFs),
ethylene/tetrafluoroethylene copolymer resins (ETFEs),
polychlorotrifluoroethylene resins (PCTFEs),
15 tetrafluoroethylene/hexafluoropropylene ethylene copolymer
resins (FEPs) and tetrafluoroethylene/perfluoroalkyl
copolymer resins (PFAs). Of these, the
polytetrafluoroethylene resins (PTFEs) are preferable in terms
of processability in extrusion, rolling and the like, and PTFE
20 obtained by emulsion polymerization is particularly
preferable.

[0023]

When PTFE is used as the fluororesin, any of the fluororesins mentioned above except PTFEs may be used in

combination therewith in a small amount, for example 10% by mass (based on 100% by mass of the total of the fluororesins).

[0024]

The fluororesin may be in the form of powder.

5 Alternatively, a dispersion of the fluororesin fine particles in water may be mixed with an inorganic filler described later, and thereafter water may be removed from the dispersion.

[0025]

The fluororesin and an inorganic filler described later
10 are used in a fluororesin:inorganic filler volume ratio of 30-55:70-45, and preferably 40-55:60-45 (wherein the total of the two is 100). This volume ratio ensures that the obtainable filled fluororesin sheet shows excellent stress relaxation properties at a high temperature. If the proportion of the
15 inorganic filler is much smaller than the above range (if the proportion of the fluororesin is much larger than the above range), the inorganic filler will not be able to suppress sufficiently the flow of the fluororesin at a high temperature, resulting in a deterioration in stress relaxation properties
20 of the fluororesin sheet at a high temperature (the stress relaxation percentage is increased).

[0026]

<Fillers>

The filler used in the invention is an inorganic filler

having a revised Mohs hardness of not less than 8, and preferably not less than 12. The filler allows the filled fluororesin sheet of the invention to show excellent stress relaxation properties at high temperatures.

5 [0027]

Specific examples of the inorganic fillers include diamond (revised Mohs hardness = 15), hexagonal boron nitride (revised Mohs hardness = 14), boron carbide (revised Mohs hardness = 14), silicon carbide (revised Mohs hardness = 13),
10 silicon nitride (revised Mohs hardness = 12), tungsten carbide (revised Mohs hardness = 12), α -alumina (revised Mohs hardness = 12), tantalum carbide (revised Mohs hardness = 11), fused zirconia (revised Mohs hardness = 11), garnet (revised Mohs hardness = 10), topaz (revised Mohs hardness = 9) and zirconia
15 (revised Mohs hardness = 8). These may be used singly, or two or more may be used in combination.

[0028]

The inorganic fillers preferably have an average particle diameter of 3 to 30 μm , and more preferably 4 to 20 μm . Herein,
20 the value of the average particle diameter is a value measured by a laser diffraction scattering method (measurement range (particle diameters): 0.03 to 1000 μm).

[0029]

<Filled fluororesin sheets>

The filled fluororesin sheets of the invention that have the above configuration are excellent in stress relaxation properties, in particular stress relaxation properties at a high temperature. In detail, the stress relaxation percentage
5 at 200°C (in accordance with JIS R3453 except that the heating temperature is changed from 100°C to 200°C) is preferably not more than 40%, and more preferably not more than 35%.

[0030]

The filled fluororesin sheets of the invention may be used
10 as gaskets because of their excellent stress relaxation properties, in particular excellent stress relaxation properties at a high temperature. A gasket composed of the filled fluororesin sheet of the invention can be used over a long term at a high temperature (for example, 200°C or above).

15 [0031]

The gasket of the invention may be easily manufactured by cutting the inventive filled fluororesin sheet to the desired shape.

[0032]

20 [Processes for producing filled fluororesin sheets]

The filled fluororesin sheet of the invention may be produced by a known process except that the specific filler described above is used.

[0033]

The production process may be a rolling process or a skiving process. A rolling process is preferable.

[0034]

An exemplary rolling process includes a rolling step of
5 rolling an extrudate of a raw material composition that includes
the fluoro-resin, the inorganic filler and a processing aid
containing not less than 30% by mass (based on 100% by mass
of the processing aid) of a petroleum hydrocarbon solvent having
a fractionation temperature of not more than 120°C. In the
10 rolling step, the composition is rolled at a roll temperature
of 40 to 80°C. Details in this process such as the processing
aids and the production conditions are described in Patent
Literature 2.

[0035]

15 The rolling process for the production of the filled
fluoro-resin sheets generally includes a stirring step, a
preforming step, the rolling step, a drying step and a calcining
step in this order.

[0036]

20 (Stirring step)

In the stirring step, the fluoro-resin, the inorganic
filler and the processing aid are stirred and mixed together
in an arbitrary order to give a sheet-forming resin composition.
When a bad stirring efficiency is encountered, the processing

aid may be added in a large amount and the extra portion of the processing aid may be removed by filtration after the completion of the stirring.

[0037]

5 The kinds and the amounts of the fluororesin and the inorganic filler may be determined appropriately in accordance with the target composition of the fluororesin sheet to be manufactured.

[0038]

10 The processing aids may be known processing aids such as petroleum hydrocarbon solvents, alcohols and water. Commercial petroleum hydrocarbon solvents include Isoper C, Isoper G and Isoper M (Exxon Mobil Corporation).

[0039]

15 <Preforming step>

 In the preforming step, the sheet-forming resin composition is extruded into a preform (an extrudate).

[0040]

 A known extruder may be used in the extrusion.

20 [0041]

 In the extrusion, the composition may be heated as required at a temperature that will not cause the volatilization of much of the processing aid and other components contained in the composition.

[0042]

The shape of the extrudate (preform) is not particularly limited. However, a rod-like or ribbon-like shape is desirable in consideration of the efficiency in the subsequent sheet
5 production and the homogeneity of the sheet properties.

[0043]

In the production process of the present invention, it is preferable that the processing aid is gradually volatilized in the rolling step described below. Accordingly, the stirring
10 step and the preforming step are preferably carried out at a temperature that is lower than the roll temperature in the rolling step in order to avoid the volatilization of the processing aid.

[0044]

15 <Rolling step>

In the rolling step that is performed after the preforming step, the preform is passed through rollers such as a two-roll mill and is thereby rolled and shaped into a sheet.

[0045]

20 The production process of the invention preferably includes a step of further rolling the rolled sheet resulting from the rolling step. Namely, the rolling step is preferably repeated several times (for example, 3 to 50 times), thereby further densifying the fluororesin sheet. In repeating the

rolling step, the distance between the rolls is narrowed after each rolling.

[0046]

When the preform is rolled into a sheet with a two-roll mill, the distance between the rolls may be set at 0.5 to 20 mm and the roll surface moving speed (the sheet extrusion rate) may be 5 to 50 mm/sec.

[0047]

⟨Drying step⟩

10 In the drying step, the rolled sheet is allowed to stand at ordinary temperature or is heated at a temperature not more than the melting point of the fluororesin, thereby removing the processing aid.

[0048]

15 ⟨Calcining step⟩

In the calcining step, the dried sheet is heated at a temperature not less than the melting point of the fluororesin and is thereby sintered. In consideration that the entire sheet has to be calcined homogeneously and that a
20 fluorine-containing harmful gas is generated at an excessively high temperature, the heating temperature is appropriately in the range of, for example, 340 to 370°C, although slightly variable in accordance with the kind of the fluororesin.

EXAMPLES

[0049]

The production process according to the present invention will be described in detail by presenting examples hereinbelow without limiting the scope of the invention.

[0050]

<Testing methods>

Stress relaxation properties:

A test piece was obtained from a 1.5 mm thick sheet. The test piece was tested in accordance with JIS R3453 except that the heating temperature was changed from 100°C to 200°C, thereby determining the stress relaxation percentage.

[0051]

[Example 1]

PTFE fine powder (CD-1, manufactured by ASAHI GLASS CO., LTD., density: 2.2 g/cm³) 1,000 g;

silicon carbide (No. 1200, manufactured by SHOWA DENKO K. K., revised Mohs hardness: 13, average particle diameter: approximately 10 μm, density: 3.2 g/cm³) 1,450 g;

Isoper C (a hydrocarbon organic solvent, fractionation temperature: 97-104°C, Exxon Mobil Corporation) 250 g; and

Isoper G (a hydrocarbon organic solvent, fractionation temperature: 158-175°C, Exxon Mobil Corporation) 250 g

were mixed together in a kneader for 5 minutes. The

resultant mixture was aged by being allowed to stand at room temperature (25°C) for 16 hours, thereby preparing a sheet-forming composition.

[0052]

5 The composition was extruded at room temperature (25°C) using an extruder having a 300 mm x 20 mm orifice. Thus, a preform was prepared.

[0053]

10 The preform was rolled with a two-roll mill having a roll diameter of 700 mm, at a roll interval of 20 mm, a roll speed of 6 m/min and a roll temperature of 40°C. Immediately after this rolling, the sheet was rolled again at a roll interval of 10 mm. Immediately thereafter, the sheet was rolled at a roll interval of 5 mm. Immediately after this rolling, the
15 sheet was rolled for the last time at a roll interval of 1.5 mm. Thus, a 1.5 mm thick sheet was obtained.

[0054]

20 The sheet was allowed to stand at room temperature (25°C) for 24 hours and thereby the solvent was removed. The sheet was calcined in an electric furnace at 350°C for 3 hours. A sheet gasket was thus manufactured.

[0055]

 The stress relaxation percentage of the sheet gasket was 29%.

[0056]

[Example 2]

A sheet gasket was manufactured in the same manner as in Example 1, except that the silicon carbide was replaced by 1,770 g of α -alumina (A-42, manufactured by SHOWA DENKO K. K., revised Mohs hardness: 12, average particle diameter: approximately 4 μm , density: 3.9 g/cm³). The stress relaxation percentage of the sheet gasket was 31%.

[0057]

10 [Comparative Example 1]

A sheet gasket was manufactured in the same manner as in Example 1, except that the silicon carbide was replaced by 1,180 g of clay (NK-300, manufactured by SHOWA KDE CO., LTD., revised Mohs hardness: 2.5, average particle diameter: 10 μm , density: 2.6 g/cm³). The stress relaxation percentage of the sheet gasket was 50%.

[0058]

[Comparative Example 2]

20 A sheet gasket was manufactured in the same manner as in Example 1, except that the silicon carbide was replaced by 1,270 g of talc (K-1, manufactured by Nippon Talc Co., Ltd., revised Mohs hardness: 1, average particle diameter: 7 μm , density: 2.8 g/cm³). The stress relaxation percentage of the sheet gasket was 58%.

[0059]

[Comparative Example 3]

A sheet gasket was manufactured in the same manner as in Example 1, except that the amount of the α -alumina was changed
5 from 1,770 g to 1,090 g.

[0060]

The stress relaxation percentage of the sheet gasket was 51%.

[0061]

Table 1

Items			unit	Ex. 1	Ex. 2	Comp. Ex. 1	Comp. Ex. 2	Comp. Ex. 3
PTFE		CD-1	g	1,000	1,000	1,000	1,000	1,000
	Inorganic fillers	silicon carbide	g	1,450				
α -alumina		g		1,770				1,090
clay		g			1,180			
talc		g				1,270		
PTFE volume proportion (relative to 100% by volume of PTFE and filler combined)			% by volume	50	50	50	50	62
Aids		Isoper C	g	125	125	125	125	125
		Isoper G	g	125	125	125	125	125
Thickness			mm	1.5	1.5	1.5	1.5	1.5
Stress relaxation percentage			%	29	31	50	58	51

CLAIMS

1. A filled fluororesin sheet, comprising a fluororesin and an inorganic filler having a revised Mohs
5 hardness of not less than 8, in a fluororesin:inorganic filler volume ratio of 30-55:70-45 (wherein the total of the two is 100).

2. The filled fluororesin sheet according to claim 1,
10 wherein the inorganic filler comprises at least one material selected from the group consisting of diamond, hexagonal boron nitride, boron carbide, silicon carbide, silicon nitride, tungsten carbide, α -alumina, tantalum carbide, fused zirconia, garnet, topaz and zirconia.

15 3. A gasket comprising the filled fluororesin sheet of claim 1 or 2.

4. A process for producing filled fluororesin sheets,
20 comprising a step of rolling a sheet-forming resin composition which comprises a fluororesin, an inorganic filler having a revised Mohs hardness of not less than 8 and a processing aid and in which the volume ratio of the fluororesin and the inorganic filler (fluororesin:inorganic filler) is

30-55:70-45 (wherein the total of the two is 100).

5. The process for producing filled fluororesin sheets according to claim 4, wherein the inorganic filler comprises at least one material selected from the group consisting of diamond, hexagonal boron nitride, boron carbide, silicon carbide, silicon nitride, tungsten carbide, α -alumina, tantalum carbide, fused zirconia, garnet, topaz and zirconia.