

AN APPARATUS FOR CLAMPING A WORK PIECE

The present invention refers to an apparatus for clamping a work piece in a well defined position within the operating area of a machine tool, comprising a chuck member adapted to be fixed within the operating area of the machine tool, a work piece carrier adapted to be fixed to the chuck member and to be clamped thereto, and a clamping mechanism for clamping the workpiece carrier to the chuck member.

Such an apparatus, well known in the art, primarily serves for clamping a work piece to be machined in the operating area of a machine tool with very high accuracy. It is particularly important that also the repetitive accuracy is ensured. In other words, the work piece received on the work piece carrier has to be clamped subsequently many times on a chuck member adapted to the work piece carrier and shall thereby have always a precisely defined position in X-direction, in Y-direction, in Z-direction and also regarding the angular orientation around the Z-axis, for example in circumstances if the work piece carrier bearing the work piece to be machined has to be clamped in different machine tools that subsequently perform different machining operations and are each equipped with an identical chuck member, or in measuring and test stations equipped with the same chuck member as well.

Such an apparatus is disclosed, for example, in the European Patent Nr.0,255,042. That apparatus comprises two pairs of positioning strip members towering above the surface of the chuck member, equipped with contact surfaces for the orientation of the work piece carrier in X- and Y-directions. Moreover, four pins are provided also towering above the surface of the chuck member. These pins are responsible for defining the Z-position of the work piece carrier. The matching work piece carrier comprises a plane surface adapted to rest against the afore mentioned pins provided

on the chuck member. Furthermore, the surface of the work piece carrier is provided with two pairs of grooves in a layout corresponding to the one of the afore mentioned positioning strip members. The grooves have flexible lips that are intended to rest against the contact surfaces of the afore mentioned strip members of the chuck member. Finally, the work piece carrier has a central aperture for receiving a pulling bolt member by means of which the clamping force required to maintain the defined position between work piece carrier and chuck member is transferred. Thereby, the chuck member comprises a centrally located ball lock mechanism co-operating with that pulling bolt member.

A disadvantage of such a known apparatus may be seen in the fact that it cannot resist high tilting momenta or torque forces that especially can occur in the case of cutting operations or if the work piece to be machined is relatively big.

Thus, it is an object of the present invention to provide an apparatus for clamping a work piece in a well defined position within the operating area of a machine tool in which the work piece carrier clamped to the chuck member and, thereby, the work piece to be machined has an substantially increased resistance against tilting momenta and torque forces, simultaneously avoiding the danger that the work piece carrier and, thereby, the work piece is displaced relative to the chuck member, all this by maintaining a very high accuracy as far as the positioning of the work piece carrier relative to the chuck member is concerned, particularly also in the case of repetitive clamping, as explained herein before.

In order to meet these and other objects, the invention provides an apparatus for clamping a work piece in a well defined position within the operating area of a machine tool, comprising a chuck member adapted to be fixed within the operating area of the machine tool, a work piece carrier adapted to be fixed to the

chuck member and to be clamped thereto, and a clamping mechanism for clamping the workpiece carrier to the chuck member and adapted to be switched from a released condition to a clamping condition and vice versa.

The chuck member comprises first positioning members and the work piece carrier comprises second positioning members. The first and second positioning members cooperate such as to define the position of the work piece carrier relative to the chuck member along three coordinate axes each running perpendicular to each other, i.e. the X-axis, the Y-axis and the Z-axis, as well as with regard to the angular orientation around the Z-axis.

The clamping mechanism thereby fixes the work piece carrier to the chuck member once it is switched to the clamping condition to maintain the defined position. It comprises a plurality of clamping devices each having a direction of activity along a linear path. All these linear paths are located on or next to an imaginary cylindrical nappe intersecting the first and second positioning members.

By the provision of a plurality of individual clamping devices that are arranged, generally said, for example along a circle, the clamping forces act exactly at those locations where they can develop their greatest effect, i.e. in the region of the first and second positioning members. The result is that the length of the levers essential for the occurrence of a tilting momentum and a torque momentum are zero or at least extremely small; this fact explains the high resistance of the apparatus according to the invention against unintentional positional changes caused by tilting and torque momenta occurring under heavy load.

In order to even increase the desired high resistance against unintentional positional changes caused by tilting and torque momenta occurring under heavy load, it is provided in a preferred embodiment that the afore mentioned linear paths of activity of

the individual clamping devices are located slightly outside of the afore mentioned imaginary cylindrical nappe intersecting the first and second positioning members. This may be realized, for example, with a chuck member of essentially cylindrical shape and a work piece carrier of essentially hollow cylindrical shape, whereby the clamping mechanism comprises a plurality of clamping balls evenly distributed along the periphery of the chuck member, and whereby the work piece carrier comprises a circular groove located at its inner cylindrical surface; thereby, the clamping balls cooperate with that circular groove.

In the following, an embodiment of the apparatus according to the invention will be further described, with reference to the accompanying drawings, in which:

Fig. 1 shows a perspective view of a chuck member;

Fig. 2 shows a top view of the chuck member of Fig. 1;

Fig. 3 shows a sectional view of the chuck member of Fig. 1 taken along the line III-III in Fig. 2;

Fig. 4 shows a sectional view of the chuck member of Fig. 1 taken along the line IV-IV in Fig. 2;

Fig. 5 shows a sectional view of the chuck member of Fig. 1 taken along the line V-V in Fig. 2;

Fig. 6 shows a perspective view of a work piece carrier member;

Fig. 7 shows a bottom view of the work piece carrier member of Fig. 6;

Fig. 8 shows a sectional view of the work piece carrier member of Fig. 6 taken along the line VIII-VIII in Fig. 7; and

Fig. 9 shows a schematical partial sectional view of a centering aperture and a centering pin in an enlarged scale.

The apparatus for clamping a work piece in a well defined position within the operating area of a machine tool shown as an embodiment in the drawings comprises, on the one hand, a chuck mem-

ber, generally designated with reference numeral 1 and shown in Figs. 1-5 and, on the other hand, a work piece carrier member, generally designated with reference numeral 25 and shown in Figs. 6-8. While the chuck member is essentially adapted to be fixed within the operating area of a machine tool (not shown in the drawings), the work piece carrier member 25 serves for receiving and holding a work piece to be machined. It should be emphasized that the expression "work piece" shall be understood in a general sense; particularly, a work piece could also be a tool to be machined, for example an electrode for an electro erosive machining device.

As can be seen particularly in Figs. 3-5, the chuck member 1 essentially comprises three portions, i.e. a base portion or base element 2, an intermediate portion 3 and a head portion 4. In the embodiment shown in the drawings, the base element 2 has the shape of a circular disc or plate member provided with a central aperture 5; the purpose of that aperture will be explained further herein after. The intermediate portion 3 is provided with a central aperture 6 having the same diameter as the aperture 5 and has the shape of a cylindrical or tube-like element. It is connected to the base element 2 by means of screws 7. Finally, the head portion 4 has a central aperture 8 as well, again with the same diameter as the apertures 5 and 6. It has essentially pot-like or hat-like shape with an inner diameter that is greater than the outer diameter of the intermediate portion 3. The head portion, on the one hand, is connected to the base element 2 by means of screws 9 and, on the other hand, is connected to the intermediate portion 3 by means of screws 10. By virtue of the afore mentioned design, an extremely stiff and flexurally rigid chuck housing is realized that moreover can be easily disassembled, for example for maintenance reasons.

Due to the fact that the inner diameter of the head portion 4 is larger than the outer diameter of the intermediate portion 3, a circular chamber 11 is created between these two portions 3 and 4. The circular chamber 11 is sealed by means of suitable sealing elements indicated in the drawings (cf. Figs. 3-5), but not referenced in detail. In the interior of this circular chamber 11, a circular piston 12 is received in such a manner that it can be moved along the central axis Z of the chuck member 1. The circular piston 12 is provided with a plurality of blind holes 13 that are evenly distributed along its circumference and that are adapted each to receive a tensioning or clamping spring 14. The springs 14 rest against the bottom surface of the head portion 4 and bias the circular piston 12 to move downwards. Moreover, the circular piston 12 is provided with an outer peripheral groove 15. The lower lateral wall of that groove 15 slopes outwardly downwards. That groove 15 serves for partially receiving a plurality of clamping ball members 18.

Below the circular piston 12, there is provided a hollow circular chamber 16 communicating with a connecting bore 17 provided in the base element 2. By means of this connecting bore 17, the circular chamber 16 can be filled with pressurized air, acting against the circular piston 12 and moves the latter one upwards against the pressure of the springs 14.

The head portion 4 is provided with a plurality of radially extending bores 19 having a diameter that essentially corresponds to the diameter of the clamping ball members 18 and serving for receiving these clamping ball members 18. The height level of these bores 19 and the height level of the afore mentioned peripheral groove 15 are in such a relation that the clamping ball members 18 inserted into the bores 19 can enter the peripheral groove 15 if the circular piston 12, under the influence of the pressurized air in the circular chamber 16 and against the force of the

springs 14, is moved in its topmost position. Thereby, the clamping balls 18 can penetrate the peripheral groove 15 to such an extent that the clamping balls no longer tower above the outer periphery of the head portion 4. Finally, the head portion 4 is provided with an outer peripheral shoulder 20. Inserted into the top surface of that shoulder 20 is a sealing member 21.

The upper surface 24 of the head portion 4 is provided with four protruding centering pins 22 that have essentially prismatic shape and that are located evenly distributed along the edge region of the upper surface 24 of the head portion 4. Two opposite centering pins 22 define the extension of the X-axis, while the remaining two opposite centering pins 22 define the extension of the Y-axis running perpendicularly to the X-axis. The point of intersection of the X-axis and the Y-axis defines the Z-axis (Fig. 3-5) running perpendicularly both to the X-axis and the Y-axis. As will be further explained herein after, at least the two peripherally opposite lateral surfaces of the centering pins 22 are somewhat inclined with regard to the Z-axis.

Moreover, the top surface 24 of the head portion 4 is provided with four plane surface portions 23 each of them extending, in the present embodiment, radially between two adjacent centering pins 22. The surface portions 23 slightly tower above the top surface 24 of the head portion 4. These surface portions 23 serve as Z-references, as will be further explained herein after.

The design of the work piece carrier 25 is shown in Figs. 6-8. As can be seen particularly in Figs. 6 and 8, the one-piece work piece carrier 25 comprises a peripheral portion 26 having essentially cylindrical or tube-like shape as well as an annulus-shaped top portion 27. The inner diameter of the peripheral portion 26 essentially corresponds to the outer diameter of the head portion 4 of the chuck member 1, of course with a reasonable

clearance such that the work piece carrier 25 can be put onto the chuck member 1.

The inner wall of the peripheral portion 26 of the work piece carrier 25 is provided with a circular groove 28, whereby the two side walls of the circular groove 28 extend conically away from each other as seen in a direction towards the interior of the peripheral portion 26. In other words, the circular groove 28 has an essentially V-shaped cross section. The axial position of the circular groove 28, i.e. the height level with reference to the Z-axis, is defined such that the clamping balls 18, schematically indicated in Fig. 8, can penetrate the groove 28 if the work piece carrier is loosely laid onto the chuck member 1. In this situation, the clamping balls 18 are somewhat axially offset downwardly with regard to the axially extending symmetry plane S-S of the circular groove 28. In other words: If the work piece carrier 25 is loosely laid onto the chuck member 1, the afore mentioned symmetry plane S-S of the circular groove 28 is located somewhat above the center of the balls 18 inserted into the bores 19 of the intermediate portion 3 of the chuck member 1.

The upper portion 27 of the work piece carrier 25 is provided with an annulus-shaped shoulder 29 protruding towards the interior of the peripheral portion 26. Thereby, the mean diameter of this shoulder 29 essentially corresponds to the diameter of the circle along which the four centering pins 22 provided on the head portion 4 of the chuck member 1 are located. The front surface of that shoulder 29 that protrudes towards the interior of the peripheral portion 26 of the work piece carrier 25 is smoothly plane ground and serves as a Z-reference of the work piece carrier 25. It is adapted to cooperate with the afore mentioned plane surface portions 23 provided on the top surface 24 of the head portion 4 of the chuck member 1. Moreover, the aforementioned front surface is provided with four recesses 30 evenly distributed along the pe-

riphery of that front surface. The exact design of these recesses will be further explained herein after. Anyway, these four recesses 30 are adapted to cooperate with the afore mentioned four centering pins 22 provided on the top surface 24 of the head portion 4 of the chuck member 1.

Even if four centering pins 22 and four recesses 30 cooperating therewith are shown and described in the present example, it is understood that it is also possible to provide three, six, eight or a greater number, being a mathematical sub-set of a Hirth gearing, of centering pins 22 and recesses 30 in order to ensure the positioning of the work piece carrier 25 with regard to the chuck member 1 in X- and Y-directions as well as regarding the angular orientation.

Fig. 9 shows a schematical partial sectional view of a centering recess 30 and a centering pin 22 in an enlarged scale. The recess 30 is designed as a two stage groove and comprises two shoulders 31a and 31b. As already mentioned before, the centering pins 22 are slightly conical by the fact that at least the two peripherally opposite lateral surfaces of the centering pins 22 are somewhat inclined with regard to the Z-axis. In practice, the angle of inclination can be in the region of between 3° and 9° . The edges 32a and 32b of the shoulders 31a and 31b protruding towards the interior of the groove 30 are authoritative for the definition of the position of the work piece carrier 25 with regard to the chuck member 1 in X- and Y-direction as well as regarding the angular orientation. Thus, the distance between these edges 32a and 32b is somewhat less than the width of the conical centering pin 22 engaging that recess 30, measured between the contact points or lines of the two opposite lateral surfaces of the pin 22 when the work piece carrier 25 is firmly clamped to the chuck member 1.

The mutual dimensions of the work piece carrier 25 and the chuck member 1 are chosen such that the following consequence results:

If the work piece carrier 25 is loosely laid onto the chuck member 1, the centering pins 22 engage the corresponding centering recesses 30, whereby the lateral surfaces 22a of the centering pins 22 get into line contact with the edges 32a and 32b, respectively, of the shoulders 31a and 31b, respectively. In this condition, the plane ground end surface of the shoulder 29 of the work piece carrier 25, serving as the Z-reference of the carrier 25, does not yet abut against the plane surface portions 23 provided on the head portion 4 of the chuck member 1, towering somewhat above its top surface and serving as the Z-reference of the chuck member 1. Rather, in this situation, there is a gap between the end surface of the shoulder 29 and the surface of the portions 23 with a width of some $\frac{1}{100}$ of a millimeter. On the other hand, and this fact has to be emphasized, the position of the work piece carrier 25 with regard to the chuck member 1 in X- and Y- directions as well as regarding the angular orientation is finally set.

As has also already been mentioned, the axial position of the circular groove 28 in the work piece carrier 25 is located in such a way that the clamping balls 18 of the chuck member 1 can penetrate the groove 28 if the work piece carrier 25 is loosely laid onto the chuck member 1, whereby the symmetry plane S-S of the circular groove 28 is located somewhat above the centers of the clamping balls 18 inserted into the radially extending bores 19 of the intermediate portion 3 of the chuck member 1. On the other hand, in order to enable the work piece carrier 25 to be loosely laid onto the chuck member 1, the clamping balls 18 of the chuck member 1 have to be in their retracted position. This is accomplished (cf. Figs.3-5) by feeding pressurized air into the circu-

lar chamber 16 below the circular piston 12, with the result that the circular piston 12 is forced to an upward movement against the pressure of the springs 14. Thus, the peripheral groove 15 provided in the circular piston 12 is moved into a position where it is aligned with the clamping balls 18 such that the latter ones can penetrate the groove 15 and do not tower above the surface of the intermediate portion 3 of the chuck member 1.

Once the work piece carrier 25 is loosely laid onto the chuck member 1 and finally positioned with regard to the X- and Y-directions as well as with regard to its angular orientation, the overpressure in the circular chamber 16 is removed with the result that the circular piston 12 is moved downwards under the influence of the force exerted by the springs 14. Thus, the clamping balls 18 are pressed into the circular groove 28 of the work piece carrier 25. Due to the afore mentioned slightly asymmetric rest position between clamping balls 18 and circular groove 28 and due to the V-shaped design of the circular groove 28, as seen in a cross sectional view, the work piece carrier 25 is pulled against the chuck member 1, in practice with a force in the region of between 2000 and 3000 Newtons. Under the influence of this clamping force acting in Z-direction, the shoulders 31a and 31b, respectively, are elastically deformed in the region of their edges 32a and 32b, respectively, particularly to such an extent until the end surface of the shoulder 29 of the work piece carrier 25 abuts against the slightly elevated surface portions 23 of the head portion 4 of the chuck member 1. The result is that the work piece carrier 25 is exactly positioned with regard to the chuck member 1 in Z-direction as well.

From these explanations, it is clearly evident that the clamping force acting parallel to the Z-direction is transferred by means of the clamping balls 18 to the work piece carrier 25 to clamp the latter one against the chuck member 1, particularly, in

the present example, at twelve locations evenly distributed along the periphery of the intermediate portion 3 of the chuck member 1. In other words, the entire clamping force acting onto the work piece carrier 25 is summed up of twelve individual clamping force components each transferred by one of the twelve clamping balls 18. Thereby, the lines of activity of these clamping force components are located on a cylindrical nappe MF (cf. Figs. 2-5 and 8) that runs, depending on the chosen dimensioning of chuck member 1 and work piece carrier 25 as well as depending on the exact position of the centering pins 22, the recesses 30 and the end surface of the shoulder 29, through these elements 22, 30 and 29, i.e. intersects these elements, or runs immediately next to these elements, preferably slightly outwards thereof. Thereby, it is ensured that the clamping force acts exactly at those locations where it is really required, with the consequence that the flexural stress present in the work piece carriers of the prior art is drastically reduced and entirely avoided, respectively. Moreover, tilting momenta occurring during the machining of a work piece are much better absorbed than in the case of a work piece carrier of the prior art with a central clamping device.

It is understood that the circular piston 12 can be operated, instead by means of pressurized air, also hydraulically.

The final shaping of the recesses 30 of the work piece carrier 25 preferably is performed by plastic deformation, for example by stamping. Thereby, a very high accuracy can be achieved, even in series production. The massive centering pins 22 having slightly sloped lateral surfaces ensure, in cooperation with the recesses 30, that even very high torques can be transmitted.

To the stability and the rigidity of the system chuck member/work piece carrier in the clamped condition contributes also the circumstance that the work piece carrier, including its centering elements in X-, Y, Z- and angular directions, is of a one

piece construction. By virtue of the essentially pot- or hat-like shape of the work piece carrier 25, the essential parts and elements of the chuck member 1 are enclosed once the system is in operation, whereby particularly the centering elements 22, 23 and 30 are well protected against contamination. Such protection is even improved by the provision of the sealing member 21 (cf. Figs. 3-5) located at the top side of the shoulder 20, against which the lower end surface of the peripheral portion 26 of the work piece carrier 25 rests.

The provision of the central apertures 5, 6 and 8, respectively, in the base element 2, in the intermediate portion 3 and in the head portion 4, respectively, in connection with the generally annular shaped design of the work piece carrier 25, enable also elongate work pieces to be clamped and machined. For example, the turbine blades of turbine rotors can be received in the aforementioned apertures in order to machine the so-called "fir tree" of the turbine blades.

If one can go without the afore mentioned central openness of the clamping system according to the present invention, it is possible to provide an additional central clamping mechanism in order to further increase the clamping force exerted to the work piece carrier, or to provide a further, independent clamping system known in the prior art, for example to clamp smaller work pieces.



PATENT CLAIMS

1. An apparatus for clamping a work piece in a well defined position within the operating area of a machine tool, comprising a chuck means adapted to be fixed within the operating area of the machine tool, a work piece carrier means adapted to be fixed to said chuck means and to be clamped thereto, and clamping means for clamping said workpiece carrier means to said chuck means and adapted to be switched from a released condition to a clamping condition and vice versa, whereby said chuck means comprises first positioning means and said work piece carrier means comprises second positioning means, said first and second positioning means being adapted to cooperate such as to define the position of said work piece carrier means relative to said chuck means along three coordinate axes each running perpendicular to each other as well as with regard to the angular orientation, and whereby said clamping means fixes said work piece carrier means to said chuck means once it is switched to said clamping condition to maintain said defined position, characterized in that said clamping means comprises a plurality of clamping device means each having a direction of activity along a linear path, whereby each of said linear paths is located on or next to an imaginary cylindrical nappe intersecting said first and second positioning means.

2. An apparatus according to claim 1, characterized in that said directions of activity of said clamping device means are located outside of said cylindrical nappe intersecting said first and second positioning means.

3. An apparatus according to claim 1, characterized in that said chuck means is of essentially cylindrical shape and said work piece carrier means is of essentially hollow cylindrical shape.



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4. An apparatus according to claim 1 and 3, characterized in that said clamping device means comprises a plurality of clamping ball means evenly distributed along the periphery of said chuck means and said work piece carrier means comprises a circular groove means located at its inner cylindrical surface, said clamping ball means being adapted to cooperate with said circular groove means.

5. An apparatus according to claim 1, 3 and 4, characterized in that said chuck means comprises a circular chamber means and said clamping means comprises a circular piston means biased by spring means and being axially movably mounted in said circular chamber means, said clamping ball means resting against said circular piston means, whereby said circular piston means is adapted to press said clamping ball means into said circular groove means provided in said work piece carrier means once said circular piston means is axially moved.

6. An apparatus according to claim 5, characterized in that said circular piston means is adapted to be pneumatically or hydraulically moved from an operating position, in which it is biased by said spring means and presses said clamping ball means into said circular groove means provided in said work piece carrier means, into a rest position in which said clamping ball means are released.

7. An apparatus according to claim 6, characterized in that said circular piston means comprises a peripheral groove means that is located such that said clamping ball means penetrate said circular groove means provided in said work piece carrier means when said circular piston means is in its rest position.



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8. An apparatus according to claim 1, characterized in that said clamping ball means are received in radially extending bores provided in said chuck means and evenly distributed along its periphery.

9. An apparatus according to claim 4, characterized in that said clamping device means comprises twelve clamping ball means.

10. An apparatus according to claim 4, characterized in that said circular groove means provided in said work piece carrier means is of essentially V-shaped cross section.

11. An apparatus according to claims 4 and 8, characterized in that the axial location of said circular groove means provided in said work piece carrier means is defined such that said clamping ball means can penetrate said circular groove means provided in said work piece carrier means when said work piece carrier means is loosely laid onto said chuck means, whereby the plane of symmetry of said circular groove means provided in said work piece carrier means is located slightly above the centers of said clamping ball means inserted into said radially extending bores.

12. An apparatus according to claim 1, characterized in that said chuck means is of essentially cylindrical shape and said work piece carrier means essentially has the shape of a hollow cylinder that is covered at one end by an essentially annulus-shaped plate member, such that said chuck means is enclosed by said work piece carrier means once the apparatus is in its clamped condition.



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13. An apparatus according to claim 1, characterized in that both said chuck means and said work piece carrier means have central aperture means for receiving elongate work pieces.

AN APPARATUS FOR CLAMPING A WORK PIECE

Abstract of the Disclosure

The apparatus for clamping a work piece in a well defined position within the operating area of a machine tool comprises a chuck member to be mounted within the operating area of the machine tool and a work piece carrier that can be put onto the chuck member and clamped thereto. First positioning members provided on the chuck member and second positioning members provided on the work piece carrier cooperate to define the position of the work piece carrier along three coordinate axes each running perpendicular to each other as well as with regard to the angular orientation. A clamping mechanism fixes the work piece carrier member to the chuck member in the afore mentioned defined position. In order to ensure an increased resistance against tilting momenta and torque occurring during the machining of a work piece, the clamping mechanism comprises a plurality of clamping devices each having a linear direction of activity, whereby all these linear directions of activity are located on or next to an imaginary cylindrical nappe intersecting the first and second positioning members.

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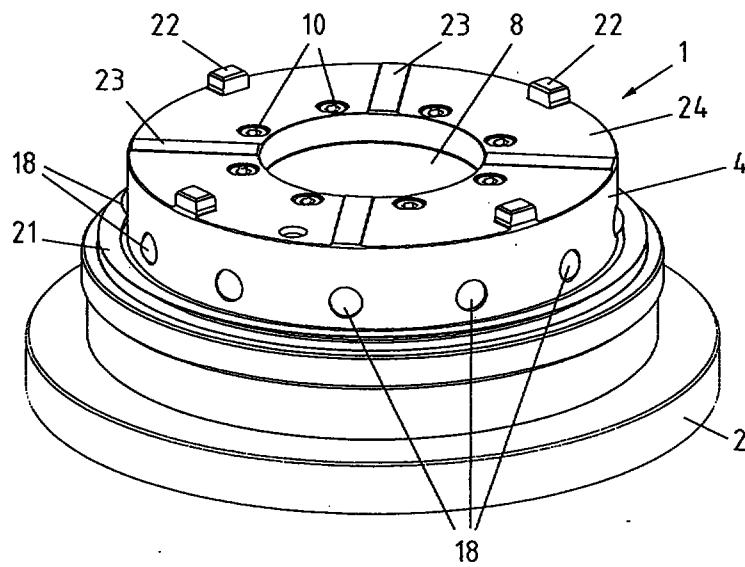


Fig.1

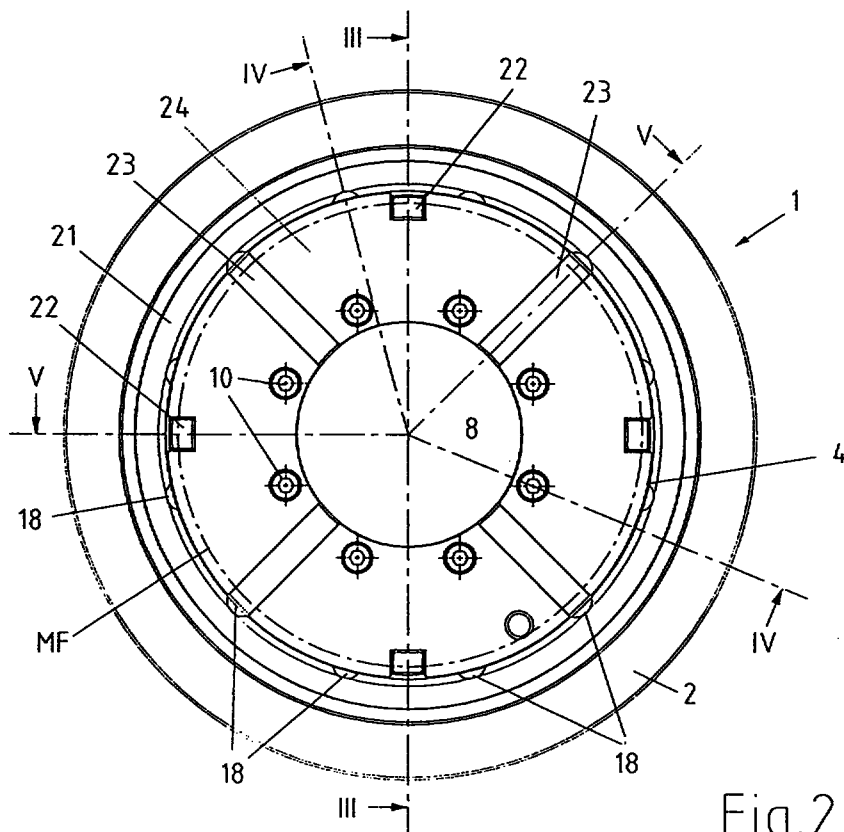
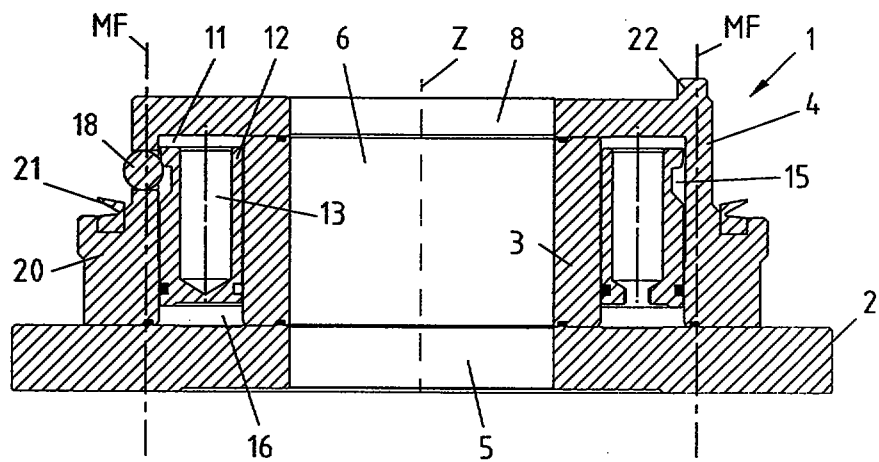
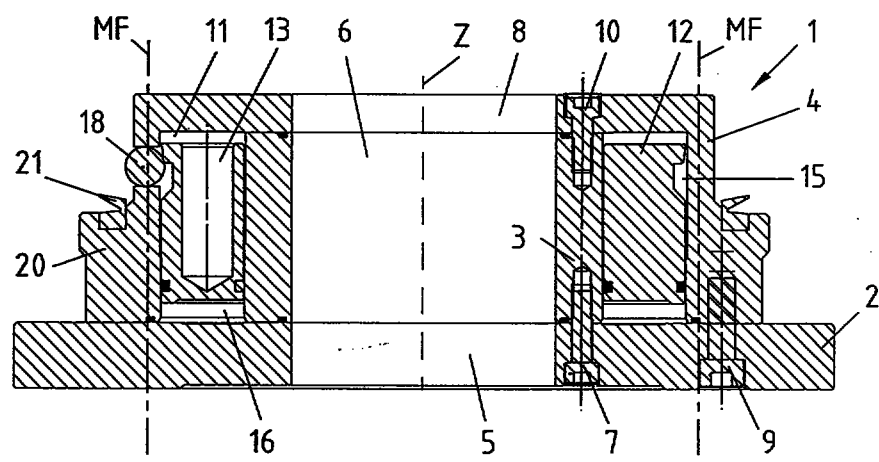
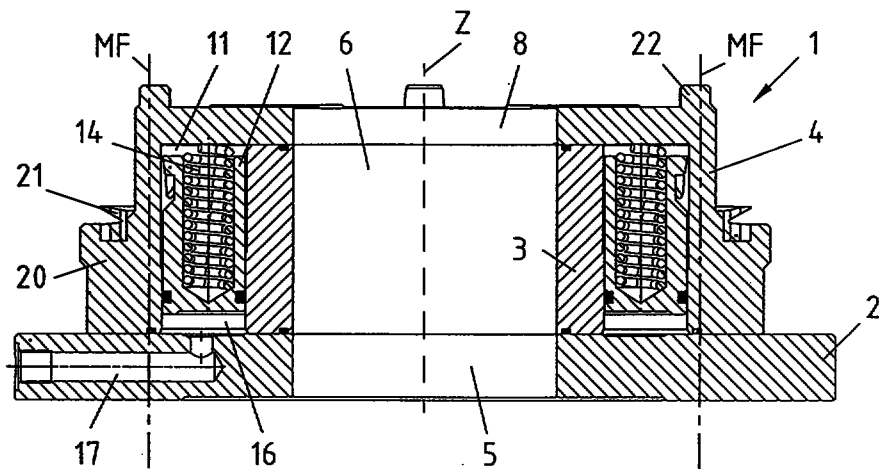


Fig.2



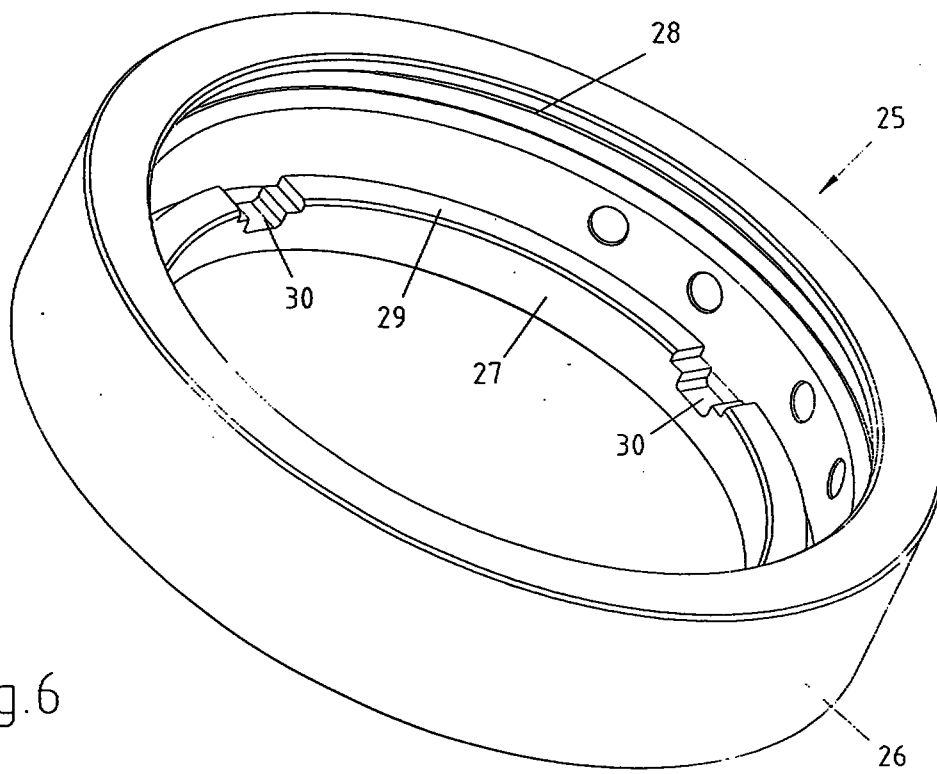


Fig.6

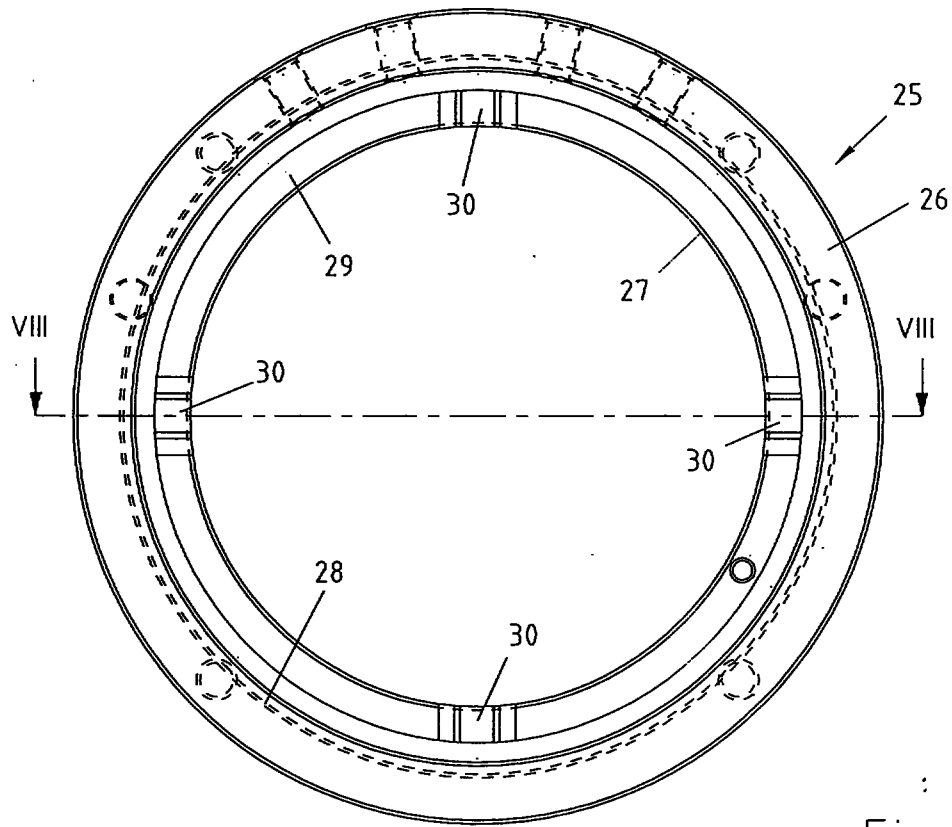


Fig. 7

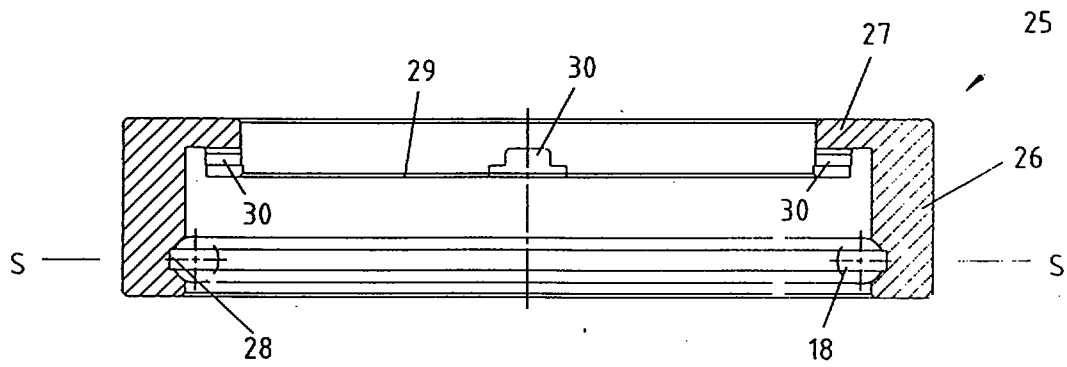


Fig. 8

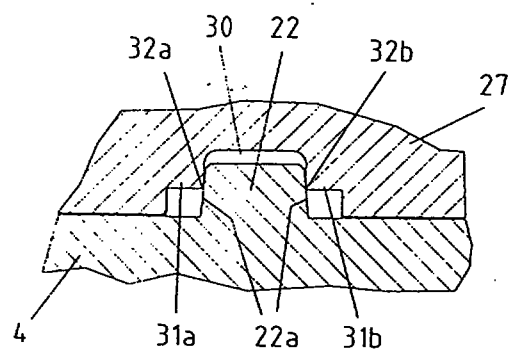


Fig.9