

A SUPPORT INSTALLED AT SEA AND FITTED WITH EXTERNAL CONTAINERS

The present invention provides a support installed at sea, either in open sea, or in a protected zone such as a port, and in grounded or floating manner, i.e. either resting on, or anchored to the sea bottom, the support including both an installation on its deck for processing a liquid that is dangerous and/or corrosive, preferably liquefied natural gas (LNG), and also at least one tank for storing said liquid and incorporated within the hull of said support under said deck.

This type of support may in particular be a barge of the FPSO or FSRU type for processing and storing LNG, or it may be a ship, in particular having a hull and storage tanks made of steel or of concrete as described in WO 01/30648, and as explained below.

The methane-based natural gas is either a by-product of oil fields, being produced in small or medium quantities, in general in association with crude oil, or else it is a major product from a gas field, where it is to be found in combination with other gases, mainly C-2 to C-4 alkanes, CO₂, nitrogen, and traces of other gases. More generally, the natural gas comprises a majority of methane, preferably at least 85% methane, with the other main constituents being selected from nitrogen and C-2 to C-4 alkanes, i.e. ethane, propane, and butane.

When the natural gas is associated in small quantities with crude oil, it is generally processed and separated and then used on site as fuel in boilers, gas turbines, or piston engines in order to produce electricity and heat for use in the separation or production processes.

When the quantities of natural gas are large, or indeed substantial, they need to be transported so that they can be used in regions far away, in general on other continents, and in order to do this the preferred method is to transport the gas while it is in the cryogenic

liquid state (-165°C) and substantially at ambient atmospheric pressure. Specialized transport ships known as "methane tankers" possess containers of very large dimensions with extreme insulation in order to limit
5 evaporation while traveling.

On oil fields in open sea, situated a long way off-shore, petroleum fluids such as crude oil or gas are generally recovered, processed, and stored on board a said floating support often referred to as an FPSO
10 (floating-production-storage-offloading). Petroleum fluids such as crude oil and/or gas are then transferred to offloading ships that call regularly, e.g. every week, to recover the production from the oil field and to export it to places where it is consumed.

15 When transferring liquefied gas of the LNG type at -165°C , transfer devices include at least one go connection pipe for the liquefied gas and a return connection pipe, in general of smaller diameter, for removing gas from the tanks of the offloading ship
20 progressively as they are filled with LNG, and in particular for removing methane gas so that it can be reliquefied on board the FPSO, as described below with reference to Figure 1A.

Another technical field is one in which LNG is
25 stored at sea close to a utilization site, e.g. in order to deliver gas to land after it has been regasified, or else to transform it on site, on-board the floating support, into electricity and for delivering said electricity to the local network on land. Under such
30 circumstances, the ship comes to unload its cargo of LNG and the floating support is referred to as an FSRU (floating storage regasification unit), as described below with reference to Figure 1B.

Concerning LNG, the term "processor installation" is
35 used more particularly below to designate any installation for liquefying natural gas into LNG, any installation for regasifying LNG, and/or any installation

for transferring LNG between said support and a methane tanker type ship for offloading and storing LNG, which tanker may be positioned in tandem or else drawn up alongside said support.

5 Processor installations of this type have means or components such as pumps, flow pipes, compressors, heat exchangers, expander devices, in general decompression turbines, cryogenic heat exchangers, and containers, and also connection pipes and connection elements between
10 these various devices.

 Leaks of the processed and stored liquid, and in particular LNG liquefied gas where applicable, may arise either from valves, pumps, heat exchangers, containers, or pipes, or else more particularly from gaskets in
15 coupling elements or in said components, or indeed by breakage of one or more of these various components.

 Leaks of LNG are particularly dangerous for three reasons:

- 20 1. Spilt LNG gasifies quickly on making contact with air and solid surfaces, and by mixing with ambient air it creates a very dangerous mixture that explodes in the presence of the slightest spark or slightest hot point.
- 25 2. Equipment conveying or containing LNG (-165°C) is made out of material capable of withstanding such cryogenic temperatures, in general nickel-based steels or indeed Invar. Such special steels are very expensive, and in general they are not used for support elements or for the structure of the FPSO,
30 which are generally made out of ordinary steels. However, such ordinary steels become brittle on contact with very low temperatures and they lose their mechanical strength, thus running the risk of structural elements breaking, and possibly even of
35 the deck of the FPSO breaking in the event of a major leak directly onto said deck, unless critical locations are protected by insulating materials that

are themselves very good at withstanding cryogenic temperatures.

3. Contact between LNG and seawater is very dangerous and leads to a very high risk of immediate explosion, since the cold LNG (-165°C) is heated suddenly by seawater at a temperature in the range 10°C to 20°C , and it is heated in the presence of air, and thus in the presence of oxygen.

The object of the present invention is to remedy the consequences associated with these problems of leaks of liquid, in particular of liquefied gas, onto the deck of such a support at sea.

To do this, the present invention provides a support installed at sea, in grounded or floating manner, the support including both a processor installation on its deck for processing a first liquid that is dangerous and/or corrosive, preferably liquefied natural gas (LNG), and also at least one tank for storing said first liquid, preferably an LNG tank incorporated within the hull of said support under said deck, the support being characterized in that it includes at least one container situated outside said support and situated at least in part, and preferably completely, below the deck of said support on which said installation is supported, said container being fastened to said support, preferably in reversible manner, said deck including or supporting first transfer means suitable for transferring towards said container any leakage liquid flowing from at least a portion of said installation, in particular in the event of a leak.

These first transfer means may comprise gutter-forming structures and possibly also pipe elements and/or liquid pumping means.

Positioning and reversibly fastening containers outside the support of the present invention presents the advantages of:

· being able to build said support in a dry dock of dimensions that are standard in terms of width or length, i.e. without requiring a dry dock of excessive dimensions, with this being advantageous since the size of a dry dock is a factor that is very limiting on the size of a support and thus also on the storage capacity of the tanks it contains; and

· being able to build said containers separately, where applicable, closer to the site at sea than said dry dock in which the support is built, and to fasten said containers on said support, either before it is towed to a site, or else on site after said support has been towed and anchored or grounded on the sea bottom; and above all

· improving safety on board said support concerning the risks of incident and/or explosion, in particular by quickly removing any leakage liquid away from said support and then emptying said container in such a manner as to return the entire installation as quickly as possible to maximum safety.

More particularly, said first transfer means for transferring leakage liquid comprise at least one collector device for collecting said leakage liquid and extending from under a said portion at least of the installation to over a first upper orifice of said container, said collector device being suitable for collecting said leakage liquid flowing from said portion of the installation and for directing it merely under gravity towards said first upper orifice of said container situated below said collector device.

It can be understood that using said first transfer means firstly avoids any contact of the leakage liquid with the deck of the support for example, and more generally with any structure of the support, and secondly avoids prolonged contact with atmospheric air.

The present invention thus advantageously consists essentially in collecting leakage flows and directing them to external containers, i.e. containers situated

outside the barge and lower down, so that the flows take place naturally merely by gravity and as quickly as possible without making contact with the structure of the support and in particular with its deck, and without
5 prolonged contact with the base of the processor installations, thereby limiting the quantity of LNG that runs the risk of vaporizing and creating an explosive gas mixture in contact with ambient air.

Still more particularly, said container is fastened
10 in reversible manner against a side of said support.

The term "side of said support" is used herein to mean the longitudinally-extending side walls, and also the front and rear transverse walls (bow and stern).

Under such circumstances, reversible fastener means
15 for fastening the container on the hull may be constituted merely by hooks enabling said container to be suspended from eyelets against said side. Furthermore, said first transfer means may comprise a sloping gutter or a said sloping deck sloping down from the longitudinal
20 middle axis XX' of said deck towards the side of said support against which said container is fastened.

Specifically, and in general, the deck is itself gently sloping at 1% to 2% down towards the longitudinal side edges of the support and is suitable for allowing a
25 liquid to flow towards a discharge outlet at and above the lateral longitudinal sides. Nevertheless, such a slope may not be sufficient for causing the flow to be fast.

Preferably, said first transfer means for
30 transferring leakage liquid comprise a liquid collector device comprising at least one decking element fitted over said deck, said decking element comprising a sloping central plane structure preferably bordered laterally by lateral rims, the angle of inclination (α_2) of said
35 central plane structure of said decking element being greater than the angle of inclination (α_1) of said deck where applicable, preferably by an angle of inclination

(α_2) lying in the range 1% to 5%, preferably in the range 2% to 4%.

When said container is fastened against the side of the support, it can be understood that said decking
5 element presents an angle of inclination with a high point beside the decking closest to said middle longitudinal axis XX' of said support and with a low point beside the decking closest to said side.

More particularly, the support of the invention
10 comprises:

- a plurality of elements of said decking, said decking elements together preferably covering at least the entire surface of the portion of the deck that supports a said processor installation presenting risks
15 of LNG leaking; and
- a plurality of containers, each said decking element co-operating with at least one said container.

It can be understood that the term "decking element co-operating with a said container" is used to mean that
20 said container is suitable for collecting said liquid flowing from said portion of the insulation situated above said decking element, said decking element directing the liquid merely under gravity towards said first upper orifice of said container situated below the
25 bottom end of said decking element, preferably via a first transfer duct element.

A plurality of containers may thus be installed on the port and starboard walls of the hull, and where applicable, on the stern and bow walls, each of them
30 collecting liquid coming from one or more decking elements covering a small area of the deck.

Advantageously, the walls or the surfaces of said collector device that might come into contact with said leakage liquid that it collects, in particular the top
35 surface of the central portion of said decking, are constituted by or covered in a layer of material that withstands the cryogenic temperatures (less than or equal

to -160°C) of said leakage liquid such as LNG, in particular a composite material such as the Chartek®-Intertherm® 7050 sandwich sold by the supplier International (UK) of the AKZO-NOBEL group, and more particularly suitable for providing cryogenic thermal insulation for LNG at -165°C.

Still more particularly, said support of the invention includes attachment means suitable for fastening a plurality of said containers along its sides, and each of said containers presents a volume of no more than 300 cubic meters (m^3), and preferably lying in the range 50 m^3 to 300 m^3 .

Containers of this volume can be built using a structure of smaller size than is needed for building the internal tanks since there is no need for a high degree of insulation, but rather a need for limited heat transfer through the wall to enable the recovered LNG to vaporize quickly but without causing the metal structure of the container or of its supports to drop below a temperature in the range -20°C to -40°C, since that would run the risk of leading to brittle fracture of the material of said structure.

Still more particularly, said container has an elongate cylindrical shape with a vertical longitudinal axis (YY') with only a portion of said container being immersed, and in particular with a horizontal cross-section that is square or rectangular or circular.

The term "vertical axis" is used herein to mean that the axis of the container is substantially perpendicular to the horizontal longitudinal axis XX' of the support and substantially perpendicular to the level of the sea when the sea is flat.

A portion of said container remains immersed even when it is empty, and a portion of the container remains above the level of the sea even when said container is full.

The vertical elongate shape of the containers is advantageous in comparison with containers of greater horizontal size in that pumping out LNG leaves a residue of LNG at the end of pumping that is proportional to the horizontal section of said container, and thus smaller than for a container of large horizontal size. With a large horizontal size, it is advantageous for the bottom of the container to be sloping, so that the pumping device can be placed at its low point.

10 In a first variant embodiment, said container has a bottom constituted by the top surface of a float inside the container and of a shape that fits against the internal outline of the cylindrical side wall of said container, the bottom surface of said cylindrical side wall defining a bottom opening in such a manner that said cylindrical side wall is filled with seawater beneath said float and is suitable for moving vertically relative to said float.

20 It can be understood that said float always remains at the level of the surface of the water, and thus that the side wall of the container moves vertically as a function of the level of the waterline of the support, which itself is a function of the extent to which said tanks and said container(s) are filled.

25 This embodiment is advantageous in that it makes it possible to use a container structure that is even lighter, because the side wall does not need to withstand the hydrostatic pressure of the surrounding seawater, nor does it need to withstand the buoyancy thrust that acts on a container presenting a bottom wall that is stationary and leaktight.

In a second variant embodiment, said container includes a leaktight stationary bottom wall at the bottom end of its cylindrical side wall.

35 Preferably, the walls of said container are thermally insulated, and preferably insulated internally, in particular with polyurethane foam. This thermal

insulation seeks to limit heat transfer due to the LNG rising in temperature, so as to keep the temperature of the steel walls of the container, and in particular the side walls situated above sea level, at a temperature
5 that is higher than the brittle fracture temperature of said steel, and in particular a temperature that is higher than -10°C . If this is not done, said heat transfer runs the risk of cooling the steel structural elements of the container to below a temperature at which
10 the steel presents risks of brittle fracture, i.e. a temperature below a temperature in the range -20°C to -40°C .

Advantageously, said container comprises or co-operates with second transfer means comprising a pump and
15 a second connection pipe suitable for transferring said leakage liquid contained in said container to a tank, preferably a said tank within the hull of said support.

In particular, said container possesses an internal pipe going down to the bottom, which pipe is connected to
20 a pump enabling said container to be emptied and delivering the liquefied gas to a storage tank of the floating support.

Also advantageously, said container further comprises heater means for heating said liquid contained
25 in said container, said heater means preferably being joule effect heater means, said heater means more preferably being incorporated in or against said cylindrical side wall of the container or of its thermal insulation layer.

30 More particularly, a heater device is a device for heating electrically or by circulating hot water or steam. In the event of the liquid phase being emptied out by pumping, said heater device is advantageously situated in the bottom portion of the container, thus
35 making it possible after emptying to finish off complete purging of said container by vaporizing and eliminating

the remaining methane gas in a flare, or merely to the open air.

When there is no device for emptying by pumping, said heater device is advantageously arranged over all or
5 a fraction of the height of the wall of the container, and where applicable, over the bottom of said container.

More particularly, said container further comprises a second upper orifice for discharging gas, in the top portion of a side wall or in a cover-forming top wall of
10 the container, and suitable for enabling the liquid contained in the container, once it has evaporated, to be discharged out from the container, preferably with the help of a third connection pipe, towards a burn-off
15 flare, or towards the gas ceiling of a said tank within the hull, or to the open air.

Still more particularly, said container includes or is suitable for co-operating with a device for injecting a foaming agent, preferably via a third upper orifice in the top portion of a side wall or in a cover-forming top
20 wall of the container. This injection of foaming agent seeks to create an inert medium inside the container when the container begins to fill with LNG. In other words, said foaming agent is injected when a leak is detected in said installation. Preferably, said containers are
25 initially filled with an inert gas such as nitrogen.

Preferably, said support of the invention it is a floating support anchored at sea or resting on the sea bottom and supporting a unit for liquefying LNG and/or for regasifying LNG and producing electricity, said
30 liquid being LNG.

Other characteristics and advantages of the present invention appear in the light of the following detailed description of one or more particular embodiments given with reference to the following figures, in which:

35 · Figure 1A is a side view of an FPSO type floating support supporting a processor unit 1b on a deck 1a, said processor unit 1b comprising LNG liquefaction equipment

1-2 and means for transferring LNG between said floating support 1 and an offloading ship 15;

· Figure 1B is a side view of an FSRU type support resting on the sea bottom 12, the support including a processor unit 1b on its deck 1a, said processor unit
5 having regasification and electricity production equipment 1-3 and means 1-1 for transferring LNG to an offloading ship 15;

· Figure 2 is a plan view of the Figure 1 FPSO type
10 floating support;

· Figure 3 is a cross-section view in a vertical plane perpendicular to the longitudinal direction XX' of said floating support through decking 4-1 and a container 3 of the present invention, said container in a first
15 variant having a solid bottom 3b that is closed in leaktight manner;

· Figures 3A, 3B, and 3C show a second variant embodiment of a container of the invention having a bottom opening 3-4 and an internal float 6 having a top
20 surface 6a defining a variable inside volume of said container; and

· Figure 4 is a section view on AA of a decking element 4-1 of Figure 3A.

In Figure 1A, the FPSO type floating support 1 is
25 anchored to the sea bottom 12 by anchor lines 10a. It receives natural gas extracted from wells in the sea bottom via production pipes 10b connecting the bottom to the surface. It includes storage tanks 2 for storing LNG 2a, and also transfer pipes 1-1a, here shown offloading
30 towards a ship of the methane tanker type, referred to herein as an offloading ship 15, and shown in a so-called "tandem" configuration. Said FPSO 1 possesses equipment 1-2 for processing and liquefying natural gas, and tanks 2 for storing LNG incorporated within its hull 1e. Said
35 FPSO is fitted with a device 1-1 for storing and guiding a flexible transfer hose 1-1a for offloading LNG to the offloading ship 15.

Figures 1 and 2 show and FPSO type floating support having four cylindrical containers 3 on a first side 1c of the hull 1e, each container having a vertical axis YY' and a horizontal cross-section that is square, and each being attached in reversible manner by respective reversible attachment means 5 arranged against each said side 1c. Three containers 3 on each side 1c receive leakage liquid 2a' coming from the processor installation 1b resting on the deck 1a of the floating support. More precisely, each of these six containers 3 receives leakage liquid 2a' collected from a decking element 4-1 collecting the leakage liquid coming from a portion of said installation 1b. In this example, the portion of the deck 1a supporting the liquefaction unit 1-2 is thus covered by a set of six decking elements 4-1 covering all of said portion of the surface of the deck that might receive leakage liquid coming from said liquefaction unit 1-2, with three decking elements 4-1 pouring the liquid towards each of said opposite sides 1c in such a manner as to be capable of pouring the leakage liquid 2a' into a respective container 3 for each decking element 4-1. A seventh decking element 4-1 covers the rear portion of the surface of the deck 1a supporting the device 1-1 for storing and guiding the transfer pipe 1-1a arranged close to the rear wall 1d of the hull 1g, suitable for pouring the leakage liquid coming from the installation 1-1 towards one of the sides 1c fitted with a fourth container of similar shape.

In Figure 1B, the support 1 of the FSRU type rests on the sea bottom 12. It includes an installation 1b comprising a unit 1-3 for regasifying LNG and for producing electricity, the unit including a transformer station for delivering electricity to land. The support 1 includes LNG storage tanks 2. In this example they are shown being loaded from a methane tanker type ship 15, referred to herein as a supply ship, that is in a so-called "tandem" configuration, said support 1 also being

fitted with a device 1-1 for storing and guiding a flexible transfer pipe 1-1a for loading LNG from a supply ship 15.

5 In Figures 1A and 1B, the support 1 has three storage tanks 2 of substantially rectangular parallelepiped shape that are arranged side-by-side in succession in the longitudinal direction XX' extending along the entire width of the floating support inside its hull 1e in the transverse direction that is horizontally
10 perpendicular to the direction XX'

In Figure 3, the steel walls of the tanks 2 are covered in an internal thermally insulating layer 2a-1 constituted by polyurethane foam and by a thin internal membrane of stainless steel in contact with the LNG and
15 capable of withstanding cryogenic temperatures, such that the tanks may be considered as being cryogenic tanks suitable for maintaining the LNG 2a that they contain in the liquid state. Likewise, the external containers 3 present walls of steel fitted on their inside faces with
20 the same thermally insulating material 3-5 so that said containers may also be considered as cryogenic containers suitable for containing LNG in the liquid state at -165°C while nevertheless having a much lower degree of insulation, so as to encourage the LNG to evaporate and
25 nevertheless avoiding the structural elements of said containers reaching temperatures lower than a temperature in the range -20°C to -40°C , so as to avoid any brittle fractures in said structural elements. Thus, in this figure, the bottom portion of the container (its walls
30 and its bottom) that is permanently in contact with seawater may present a low level of insulation, since there is no risk of the temperature of the bottom structure dropping below -20°C , because of its direct and permanent contact with seawater at a temperature in the
35 range 10°C to 20°C . In contrast, the top portion that emerges permanently or temporarily (due to variations in draft as a function of loading) is in contact with

ambient air that is likewise at a temperature in the range 10°C to 20°C. Because less heat is exchanged with air than when making contact with seawater, it is appropriate to have a higher performance insulation system so that heat exchange through said insulation system does not lead to structural elements being cooled to such an extent that their temperature drops below a temperature in the range -20°C to -40°C, thereby avoiding brittle fractures of the steel wall of said structures.

10 The outer side walls 1c and 1d, and also the bottom wall 1e and the deck 1a defining the hull 1g constitute the "hull girder", i.e. the overall strong structure 1f of the floating support.

15 In Figure 3, the plane of the deck 1a is shown as being inclined with a downward slope from the horizontal middle axis XX' of the support and of the deck towards the sides 1c constituting the longitudinal side walls of the hull at an angle α_1 of about 1°. The top wall or cover 3c of the containers is a little below the top ends of the sides 1c. The vertical cylindrical side walls 3a of the containers 3 present respective side faces 3a-1 each having two hooks 5-1 arranged in a high portion and in a low portion and suitable for being suspended from sockets 5-2, i.e. parts presenting respective hollow shapes complementary to said hooks or "hinge pins", that are applied against the outside faces of said sides 1c in such a manner that said containers can be suspended therefrom and thus attached reversibly when the hooks 5-1 co-operate with said parts 5-2. Collecting and
25 transferring the leakage liquid 2a' from the processor installation 1b towards the inside of the container 3 takes place with the help of a collector device constituted by a plurality of decking elements 4-1. Each decking element 4-1 comprises a carrier structure 4a made of steel or of duck board and covered in a layer of
35 strong and insulating composite material 4a-1, e.g. a sandwich made of Chartek®-Intertherm® 7050 from the

supplier International (UK) of the AKZO-NOBEL group. The central portion 4a-1 is inclined at an angle α_2 corresponding to a slope lying in the range 1% to 5%, and preferably in the range 2% to 4% relative to the horizontal. It is fastened on top of the deck 1a with a downward slope from the end of the decking closest to the longitudinal middle axis XX' towards the low end of the decking extending beyond the side 1c, i.e. outwards from the floating support 1 above a first upper opening 3-1 through the cover 3c of the container 3. The leakage liquid flowing over the decking 4-1 at its lower end towards said first opening 3-1 of the container is channeled with the help of a device 4-2 having a small upper chamber 4-2a and a lower pipe element 4-2b enabling the leakage liquid 2a' to flow into the inside of the container 3.

The containers 3 are advantageously installed on the hull 1g after the hull has been floated in a shipyard, but before it has been towed to site at sea. In the event of towing taking place over very long distances, such as several thousands of kilometers, they may advantageously be installed only after reaching the site, and they may be fabricated in a shipyard closer to the site.

In the plan view shown in Figure 2 each decking element co-operating with at least one container 3 presents a trapezoidal shape with its side rims 4b tapering towards the portion 4-2 of the device for collecting and transferring liquid to the container 3. It can be understood that the rims 4b seek to prevent leakage liquid from leaving the central portion of the decking 4a and to channel the flow of leakage liquid towards the container 3 by the tapering width of the central portion 4a towards the side.

In Figure 4 there can be seen a section view on plane AA of Figure 3A showing a decking element 4-1 comprising a steel support structure 4a, strong and

insulating composite material 4a-1, and raised edges 4b for channeling the LNG towards the container situated below.

5 The decking elements 4-1 thus constitute gutters collecting and channeling the liquid leaking from the processor installation 1d towards and up to the top orifices 3-1 of the containers 3.

10 Once the leak(s) is/are under control, the containers 3 are full of leakage liquid 2a' at various levels, and it is then desired to empty them as quickly as possible in order to return the entire installation to a maximum level of safety. Several variants are possible. In a first variant embodiment, second transfer means 8 are used that comprise a pump 8-1 serving to
15 cause the leakage liquid 2a' to flow inside a second connection pipe 8-2 extending from close to the bottom 3b of the container up to and through the cover 3c and extending beyond that, e.g. towards and into the gas ceiling 2a-1 of an LNG storage tank 2.

20 In a second variant embodiment, the liquid 2a' is regasified, if necessary, with the help of a heater device 9 that may be immersed in the leakage liquid 2a' inside the container 3, or that may be incorporated against the side wall of the container 3, and/or in or
25 against the internal thermal insulation layer 3-5 of the container 3. Once regasified, the LNG 2a' may be discharged through a third pipe element 3-6 passing through a second upper opening 3-2 of the cover 3c of the container 3. The third pipe element 3-6 thus enables the
30 gas to be discharged, either merely into the atmosphere, or else by means of pipes (not shown) to a burn-off flare 14 installed at one end of the floating support, as shown in Figure 2. Even when a heater device 9 is not used, the second opening 3-2 and the second pipe element 3-6
35 make it possible to discharge the gas either to the open air or else to the flare, as explained above.

In the embodiment of Figure 3, the container 3 has a portion that always remains immersed, representing a fraction of the height H of the container 3 starting from its bottom 3b that lies in the range $\frac{1}{4}$ to $\frac{3}{4}$, and more particularly in the range $\frac{1}{3}$ to $\frac{1}{2}$ of the height H of the container 3 from its bottom 3b, i.e. below the sea surface 11. It can be understood that the height H varies as a function of the level of the waterline of the hull, which in turn varies depending on whether the tanks 2 are empty (waterline at about $\frac{1}{4}$ of the height of the container above its bottom wall 3b) or the tanks 2 are full of liquid 2a (waterline at about $\frac{1}{4}$ of the height of the container below its top wall 3c, or about $\frac{3}{4}$ above its bottom wall 3b). In this embodiment, buoyancy acts on the entire immersed volume of the container, and in addition the structure of said container must be capable of withstanding pressure, more particularly in its bottom portion. Thus, the attachment points need to withstand forces that are directed mainly downwards when the container is full of leakage liquid and when the FPSO is partially or completely empty, and to forces that are directed upwards when the container is empty and the FPSO is completely full.

In Figures 3A, 3B, and 3C, there can be seen a second embodiment of the container 3 in which the bottom end of the cylindrical side wall 3a defines a bottom opening 3-4 of the container. In this second embodiment, the container 3 contains a float 6 having a top surface 6a that defines the bottom surface of the container, it nevertheless being understood that the float 6 presents a shape, in particular a substantially rectangular block shape, and an outline, in particular of substantially square section, that matches the shape of the inside surface of the cylindrical side wall 3a so as to allow the reservoir at 3 to slide vertically relative to the float 6, which float presents buoyancy so as to remain continuously substantially level with the top surface 11

of the sea. Thus, the height H of the immersed portion of the container 3 varies as a function of the height of the waterline of the floating support between a maximum value H_1 corresponding to an FPSO in which the tanks are full (Figure 3B), and a minimum height H_2 corresponding to an FPSO in which the tanks are empty (Figure 3C). The portion of the container between the undersurface 6b of the float 6 and the bottom opening 3-4 of the container 3 is filled with a varying height of seawater 13. This second embodiment presents the advantage that the empty volume of the container, if any, is always situated below the level 11 of the sea, such that the structure of the side walls of the container can present strength that is relatively weak, since there is no need to withstand the hydrostatic pressure of seawater, unlike the first embodiment of Figure 3 in which it can happen that a portion of the empty inside volume of the container 3 is immersed and needs to withstand hydrostatic pressure. Likewise, forces on the fastener elements no longer change direction as a function of the extent to which the FPSO is full, and it can be considered that the forces in the structure of the container and in its supports are substantially constant. In practice, regardless of the shape of the inside horizontal cross-section of the container, the outline of the float corresponds to said shape of the inside section of the container, it being understood that clearance, and preferably regular clearance, e.g. of a few centimeters, exists between said float and said inside wall of said container around the entire periphery of said float.

The drawback of this second embodiment of Figures 3A to 3C is that, where applicable, the available fraction of the inside volume of the container 3 tends to decrease as the storage tanks 2 are emptied. Under such circumstances, using second transfer means 8 or discharge means 3-6 is more particularly advantageous.

The float 6 is advantageously made in conventional manner out of syntactic foams, given their high level of mechanical strength and their excellent behavior at cryogenic temperatures (-165°C).

5 Because LNG presents a negative temperature at around -165°C, when it drops on the top surface 6a of the float, the ring of seawater situated between the periphery of the float 6 and the wall of the container freezes almost immediately and transforms into ice,
10 thereby blocking said float 6 against the cylindrical side wall 3a of the container and as a result sealing at the bottom of the container, thereby preventing said float from moving down below the level 11 of the sea under the effect of the weight of leakage liquid 2a' that
15 it is carrying.

 Also advantageously, the containers 3 are provided with a third opening 3-3 in the top portions of their cylindrical side walls 3a so as to enable an inert foaming agent to be inserted into the inside of the
20 container by means of a pipe element 3-7, the foaming agent coming from a foam generator (not shown). Thus, in the event of a leakage in the installation 1b, as soon as the container begins to fill, the foam generator is activated so as to confine the LNG and limit any
25 introduction of air, given that oxygen in the air runs the risk of explosion or fire when mixed with natural gas. The presence of this foam does not in any way hinder the vaporization of the LNG, nor does it hinder the evacuation of gas to the outside of the container, as
30 described above. Suitable foaming agents are foams of the firefighting type known to the person skilled in the art and sold by the supplier ANGUS FIRE (UK).

 It can be understood that said first, second, and third openings 3-1, 3-2, and 3-3 are advantageously
35 fitted with devices enabling them to be closed at will, such as valves.

The above described devices for transferring and collecting leakage liquids 2a' make it possible to collect the leakage liquid 2a' and to eliminate it quickly, where elimination may take place in controlled manner at will through the various above described transfer and discharge means in the form of a liquid or of a gas so as to avoid any risk of explosion or fire, and so as to enable the installations to be returned as quickly as possible to a configuration of maximum safety.

The volume of each of said containers is determined as a function of the volumes of LNG applicable to the areas covered by the collector devices connected to said container. Consideration is thus taken of the following:

- firstly the volumes of the vessels concerned (pipework, containers, pumps, ...) situated between the upstream and downstream valves; and
- secondly the production volume that is current during a period of time corresponding to the beginning of a leak incident and effective closure of all of the upstream and downstream valves involved, i.e. in general several minutes.

Thus, the volume of each of the containers is a function of its location relative to the installation, and may vary over a wide range, e.g. 50 m³ to 300 m³.

The description above relates to containers presenting respective covers on top through which there pass pipes for delivering LNG or foam, and also pipes for discharging gas; however, in a simplified version, said containers need not have covers. Under such circumstances, as soon as a leak occurs, it is essential to fill said containers with foam so as to confine the LNG, with the LNG then evaporating directly to the open air through the thickness of a layer of said foam.

CLAIMS

1. A support (1) installed at sea in grounded or floating manner, the support including both a processor installation (1b) on its deck (1a) for processing a first liquid (2a) that is dangerous and/or corrosive, preferably liquefied natural gas (LNG), and also at least one tank (2) for storing said first liquid (2a), preferably an LNG tank incorporated within the hull (1g) of said support under said deck (1a) the support being characterized in that: it includes at least one container (3) situated outside said support and situated at least in part, and preferably completely, below the deck (1a) of said support on which said installation is supported, said container being fastened to said support, preferably in reversible manner (5), said deck including or supporting first transfer means (4) suitable for transferring towards said container any leakage liquid (2a') flowing from at least a portion of said installation, in particular in the event of a leak.

2. A support according to claim 1, characterized in that said first transfer means for transferring leakage liquid comprise at least one collector device (4-1) for collecting said leakage liquid and extending from under a said portion at least of the installation (1b) to over a first upper orifice (3-1) of said container, said collector device being suitable for collecting said leakage liquid (2a') flowing from said portion of the installation and for directing it merely under gravity towards said first upper orifice of said container situated below said collector device.

3. A support according to claim 1 or claim 2, characterized in that said container is fastened in reversible manner against a side (1c, 1d) of said support.

4. A support according to any one of claims 1 to 3, characterized in that said first transfer means (4) for transferring leakage liquid comprise a liquid collector device comprising at least one decking element (4-1) fitted over said deck, said decking element comprising a sloping central plane structure (4a) preferably bordered laterally by lateral rims (4b), the angle of inclination (α_2) of said central plane portion (4a) of said decking element being greater than the angle of inclination (α_1) of said deck where applicable, preferably by an angle of inclination (α_2) lying in the range 1% to 5%, preferably in the range 2% to 4%.
5. A support according to claim 2, and according to any one of claims 2 to 4, characterized in that the walls or the surfaces of said collector device that might come into contact with said leakage liquid that it collects are constituted by or respectively covered in a layer of material that withstands cryogenic temperatures (4a-1), in particular a composite material.
6. A support according to claim 4 or claim 5, characterized in that it comprises:
- a plurality of elements of said decking (4-1), said decking elements together covering at least the entire surface of the portion of the deck that supports a said processor installation (1b); and
 - a plurality of containers (3), each said decking element (4-1) co-operating with a said container.
7. A support according to any one of claims 1 to 6, characterized in that it includes attachment means (5, 51-52) suitable for fastening a plurality of said containers along its sides (1c), and said containers have a volume of no more than 300 m³, and preferably lying in the range 50 m³ to 300 m³.

8. A support according to any one of claims 1 to 7,
characterized in that said container has an elongate
cylindrical shape with a vertical longitudinal axis (YY')
with only a portion of said container (3) being immersed
5 (13).

9. A support according to any one of claims 1 to 8,
characterized in that said container has a bottom (3b)
constituted by the top surface (6a) of a float (6) inside
10 the container and of a shape that fits against the
internal outline of the cylindrical side wall (3a) of
said container, the bottom surface of said cylindrical
side wall (3a) defining a bottom opening (3-4) in such a
manner that said cylindrical side wall (3a) is filled
15 with seawater (13) beneath said float and is suitable for
moving vertically relative to said float.

10. A support according to any one of claims 1 to 8,
characterized in that said container includes a leaktight
20 stationary bottom wall (3b) at the bottom end of its
cylindrical side wall (3a).

11. A support according to any one of claims 1 to 10,
characterized in that the walls of said container are
25 thermally insulated (3-5), and preferably insulated
internally.

12. A support according to any one of claims 1 to 11,
characterized in that said container comprises or co-
30 operates with second transfer means (8) comprising a pump
(8-1) and a second connection pipe (8-2) suitable for
transferring said leakage liquid contained in said
container to a tank, preferably a said tank (2) within
the hull of said support.

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13. A support according to any one of claims 1 to 12,
characterized in that said container further comprises

heater means (9) for heating said liquid contained in said container, said heater means preferably being joule effect heater means, said heater means more preferably being incorporated in or against said cylindrical side wall (3a) of the container or of its thermal insulation layer (3-5).

14. A support according to any one of claims 1 to 13, characterized in that said container further comprises a second upper orifice (3-2) for discharging gas, in the top portion of a side wall (3a) or in a cover-forming top wall (3c) of the container, and suitable for enabling the liquid contained in the container, once it has evaporated, to be discharged out from the container, preferably with the help of a third connection pipe (3-6), towards a burn-off flare (14), or towards the gas ceiling (2-1) of a said tank within the hull, or to the open air.

15. A support according to any one of claims 1 to 14, characterized in that said container includes or is suitable for co-operating with a device for injecting a foaming agent, preferably via a third upper orifice (3-3) in the top portion of a side wall (3a) or in a cover-forming top wall (3c) of the container.

16. A support according to any one of claims 1 to 7, characterized in that it is a floating support (10a) anchored at sea or resting on the sea bottom (12) and supporting a unit (1-2, 1-3) for liquefying LNG and/or for regasifying LNG and producing electricity, said liquid (2a) being LNG.