Large Bore Subsea Christmas Tree and Tubing Hanger System

Field of the invention

This invention concerns subsea completions and more particularly relates to a completion arrangement that may be used to provide a large bore, high pressure, conventional (i.e. non-horizontal), concentric Christmas tree and tubing hanger system.

Background of the Invention

For deep water developments it is now considered that conventional trees have advantages over horizontal trees. The horizontal tree concept has proven to be less advantageous than originally forecast in terms of installation times and design complexity. A demand has therefore arisen for a large bore conventional tree.

As the size of the production bore in a conventional Christmas tree and tubing hanger arrangement is increased, a large offset is often provided between the wellhead centre line and the fluid conducting bores at the tubing hanger / tree interface, primarily to avoid excessive enlargement of the tree block. In the case of parallel bore tubing hangers, this offset can arise in each of the production and tubing annulus bores. For concentric tubing hangers, there need be no offset in the production bore, but the tubing annulus offset is correspondingly larger. A very large offset in either the production bore or the tubing annulus bore will prevent wireline access.

During installation of parallel bore tubing hangers it is necessary to set wireline plugs in both bores. This requirement therefore restricts the permissible bore offsets. Tubing hangers are available which have a hydraulically operated annulus isolation valve rather than a plug. However it has usually been the practice to provide wireline access to this valve, for emergency operation in case of hydraulic actuator failure. Provision of such access and the consequent need to avoid dog legs at the tubing hanger/ tree interface makes the tubing hanger and tree design relatively bulky and incapable of accommodating large numbers of downhole service lines.

Providing full wireline accessibility in a large bore conventional completion therefore leads to a large and heavy Christmas tree and tubing hanger installation. The upper weight limit for the lifting gear used to transfer equipment between supply and installation vessels is approximately 35 tonnes. This limit is reached for a conventional Christmas tree for use with 5½ inch (140mm) tubing. We have realised that improved space utilisation and various consequential design improvements are possible, both in the tubing hanger and in the tree, if wireline accessibility for the annulus isolation valve is abandoned. By this means the tubing size can be increased to seven inches (178mm) or more whilst maintaining the tree weight within the 35 tonne limit and the tree dimensions likewise within acceptable limits.

Summary of the invention

One aspect of the present invention provides a tubing hanger comprising a substantially centrally located production bore, and a tubing hanger running tool; the running tool including a recess longitudinally engageable with a projection extending from the tubing hanger production bore, whereby the running tool may be orientated for engagement with the tubing hanger.

The various aspects and preferred features of the invention are described below with reference to illustrative embodiments shown in the drawings.

Brief Description of the Drawings

Figure 1 shows the interface between a tubing hanger embodying the invention and a Christmas tree;

Figure 2 shows the tubing hanger tubing annulus passage valve in more detail, in a closed position;

Figure 3 shows the valve of figure 2 in an open position;

Figure 4 shows a tubing hanger running tool engaged with the tubing hanger of figure 1;

Figure 5 shows a first embodiment of the Christmas tree of the invention;

Figure 6 is a fluid circuit diagram of the tree of figure 5;

Figure 7 shows a second embodiment of the Christmas tree of the invention;

Figure 7a shows a modification of the second embodiment; and

Figure 8 is a fluid circuit diagram of the tree of figures 7 and 7a.

Detailed Description of the Preferred Embodiments

Fig 1 shows the bottom of a Christmas tree 10 attached to a tubing hanger 12 landed in a wellhead housing 14. The tubing hanger 12 is supported by casing hangers 16 and held down by a lock down ring 18. It includes a concentric production flow bore 20 and a highly radially offset annulus flow passage 22 formed by a pair of intersecting drillings 24, 26. The upper end of the annulus flow passage 22 leads to an inlet port 28 of a pressure balanced integral shuttle valve 32, closeable for retaining annulus fluids below the tubing hanger. This valve has outlet ports 30 communicating with a void 34 formed between the top of the tubing hanger 12 and a seal stab assembly 36 of the Christmas tree 10. A circumferentially spaced series of drillings 38 in the seal stab assembly 36 (only one drilling 38 shown) communicate with an annulus flow conduit 40 in the tree 10 via an annular gap 42 formed between the seal stab assembly 36 and the tree body 44. The lower ends of the drillings 38 communicate with the void 34 thereby linking it with the Christmas tree annulus flow conduit 40.

As shown in Fig 1, there is ample space in the seal stab assembly 36 and tubing hanger 12 for service lines, circumferentially spaced about the production flow bore 20 at a similar radius from the hanger centre line in comparison to the annulus flow conduit/passage

22, 38, 40. One such line 46 is schematically indicated in dotted lines. With seven inch (178mm) production tubing 48, there is enough room for up to 8 circumferentially distributed service lines.

The void 34 provides space for service line couplers 35, which are bathed in the annulus fluid. The void 34 is sealed by an annular sealing ring 37 between the tubing hanger 12 and lock down ring 18, a further annular sealing ring 39 between the lock down ring 18 and the tree seal stab assembly 36 and a third annular sealing ring 41 between the tree seal stab assembly 36 and the tubing hanger 12.

The shuttle valve 32 is of similar construction to an annulus access valve disclosed in US Patent No 5769162, except that it is inverted so that instead of being provided at a lower end of the tubing hanger annulus flow passage, it is situated at the upper end of the flow passage 22, in the broadest part of the tubing hanger 12. This maximises the space available for the valve 32, besides maximising space in the lower part of the tubing hanger for the large diameter production flow bore 20. This results in a very compact tubing hanger design.

As shown in Fig 2, the valve 32 comprises an open-ended tubular shuttle 50 contained partly in a bore 52 formed in the tubing hanger 12, and partly in a housing 54 screw threaded into a counter bore 56 and sealed to the counter bore 56 by O-rings 58. A lower end of the shuttle 50 carriers a pair of sealing rings 60 which make a sliding seal between the shuttle and the bore 52. An upper end of the shuttle 50 carriers two pairs of sealing rings 62, 64 which similarly make a sliding seal with the housing 54. The shuttle 50 has an external circumferential collar 66 carrying a pair of O-rings 68 which make a sliding seal with a portion of the counter bore 56 between the lower end of the housing 54 and the bore 52. This portion of the counter bore thus forms a chamber 70 within which the collar 66 slides as a piston. Hydraulic fluid is supplied to and vented from the chamber 70 through ports 72, 74. In the position shown in Fig 2, the collar 66 lies at the upper end of the chamber 70, with the sealing rings 62, 64 lying to either side of the ports 30 to close the valve 32. In this position, supplying hydraulic fluid to the port 72 will cause the collar 66 and shuttle 50 to move downwardly, bringing the upper end of the shuttle 50 and the seals 64 below the ports 30, thus opening the valve 32. This position is shown in Fig 3, in which position supplying

hydraulic fluid to the port 74 will cause the shuttle to move upwardly, returning to the closed condition shown in Fig 2. With the valve closed, neither annulus pressure at the port 28 nor pressure in the void 34 will tend to cause movement of the shuttle 50. The valve 32 is therefore pressure balanced and reliable in operation. The size of the collar 66 and chamber 70 required for actuation of the shuttle is therefore small.

Fig 4 shows a running tool 76 engaged with the tubing hanger 12. A production flow bore seal stab 78 of the running tool 76 includes an orientation slot or keyway 80 longitudinally engageable over a key 82 projecting radially into the tubing hanger production bore 84. An optional orientation helix 86 is provided on the bottom of the seal stab 78, for coarse alignment of the running tool 76 to the tubing hanger 12. Provision of an orientation key and keyway at the interior surface of a concentric tubing hanger production bore provides simple and direct passive orientation between the tubing hanger and the running tool, without reliance on orientation components carried by a BOP.

Figs 5 and 6 show one possible layout of a Christmas tree 100 according to the invention. The Christmas tree production bore 88 is closed at its upper end by an internal tree cap 90, below which are positioned two crown plugs 92, 94 in series. Plug 94 replaces the conventional production master valve and plug 92 replaces the conventional production swab valve, thereby eliminating the bulk and weight of the associated valve actuators. The upper crown plug 92 together with the tree cap 90 maintains a permanent dual pressure barrier in the tree production bore.

A production outlet branch 96 is connected to the production bore 88 between the two plugs 92, 94. A $6^3/_8$ inch (162 mm) production wing valve 98, which may be a conventional gate valve, is provided in the outlet branch 96.

An annulus flow conduit 102 is provided in the tree, connected to the conduit 40 and void 34, fig. 1. This conduit 102 contains an annulus master valve 104 and annulus outlet valve 106. An annulus line 108 is branched off the annulus flow conduit 102 from between the valves 104, 106 and contains an annulus wing valve 110. The valves 104, 106,

110 may be conventional gate valves and together maintain the dual pressure barrier philosophy for the annulus conduit.

As shown more particularly in Fig 5, the annulus flow conduit 102 contains a deviated portion 112 which provides space in the tree block 114 for a crossover valve 116, which again may be an otherwise conventional gate valve. Crossover valve 116 is provided in a crossover conduit 118 formed in the tree block and extending between the deviated portion 112 of the annulus flow conduit 102 and the production flow bore 88. This eliminates the need for a separately formed external crossover conduit. All of the tree valves, except the annulus wing valve 110, are integrally formed with the tree block 114. Annulus wing valve 110 is located within a separate manifold 109, bolted and sealed to the tree block 114.

Figs. 7 and 8 show an alternative tree layout that is similar to the one of figs. 5 and 6, but which differs in that a production master valve 120 is provided upstream of the production wing valve 98 in the production outlet branch 96, replacing the crown plug 94. A second crown plug 122 is provided in the production flow bore 88 above the production outlet branch 96, in addition to the crown plug 92, to maintain a dual pressure barrier. As shown in Fig 7, the production wing valve 98 is situated in a separate valve block 124. A separately fabricated external flow loop 126 forming the crossover conduit connects the production outlet branch 96 in the valve block 124 with the annulus line 108 in the manifold 109, between the annulus wing valve 110 and the annulus line 108/annulus flow conduit 102 junction. A crossover valve 116 (not visible in Fig 7) is provided in the external flow loop 126.

The two crown plugs 92, 122 maintain the permanent dual pressure barrier in the tree production bore and the tree cap 90 is therefore optional in this embodiment. Where the tree cap 90 is not used, a debris plate (not shown) can be located above the upper plug 92 if desired, to ensure that stray objects falling onto the tree do not block access to the crown plugs.

Fig 7a shows a modification of Fig 7, in which the flow loop 126 is replaced by a crossover conduit formed in the tree block 114 by a pair of drillings 128, 130. These extend behind the plane of the drawing and intersect each other behind the production bore 88 as shown. Drilling 130 intersects the production outlet branch 96 at the junction between the production wing valve block 124 and the tree block 114. A crossover valve 116 is provided in a position accommodated by the deviated portion 112 of the annulus flow conduit 102, in like manner to Fig 5. The crossover conduit and crossover valve 116 of Fig 7a is represented in Fig 8 in dotted lines. However, because this internal crossover conduit is relatively difficult to manufacture, the external flow loop and crossover valve of Fig 7 may be more practical.

The invention in its preferred forms provides a large bore concentric tubing hanger with an integral, offset, pressure balanced annulus shuttle valve. The shuttle valve is located in such a way that it has minimal impact on the functionality and size of the tubing hanger and provides the primary means of retaining annulus fluids. The invention may be utilised in order to maximise the diameter of the production tubing and the number of downhole service lines. The invention advantageously provides a conventional concentric bore subsea Christmas tree system that can accommodate the largest possible diameter production bore. With such a system there need be no dog leg at the interface of the Christmas tree and tubing hanger production bores. Tree height and weight may be minimised by re-configuring the associated valves and adopting a tree pressure barrier philosophy similar to that of a horizontal subsea Christmas tree, using two plugs in the production bore, rather than valves. The system is of relatively simple configuration and may employ a riser and tooling similar to those used with horizontal tree systems. This offers some potential for standardisation between tree types. Compatibility with existing concentric subsea test trees and monobore riser technology is also provided, with the subsea test tree stackup achievable below the BOP shear rams. The tubing hanger and Christmas tree may be designed to retain 10,000 psi (68.9 MNm^{-2}) working pressure. Continuous monitoring of downhole electrical and hydraulic equipment is possible whilst the completion is being run or pulled, by virtue of the tubing hanger/running tool orientation system, which allows connection of downhole service lines to appropriate service couplers in the running tool. It also allows passive re-engagement of the tubing hanger running tool to the tubing hanger during retrieval or intervention operations.

CLAIMS:

1. A tubing hanger comprising a substantially centrally located production bore, and a tubing hanger running tool; the running tool including a recess longitudinally engageable with a projection extending from the tubing hanger production bore, whereby the running tool may be orientated for engagement with the tubing hanger.

2. A tubing hanger and running tool as defined in claim 1, including an orientation helix provided on the running tool to guide the projection into the recess.

3. A tubing hanger and running tool as defined in claim 1 or 2, comprising a recess or projection for longitudinal engagement with a complementary projection or recess on a Christmas tree to provide alignment between the tree and tubing hanger.

4. A tubing hanger as claimed in claim 1 and substantially as described with reference to or as shown in figure 4 of the drawings.

Abstract

Large Bore Subsea Christmas Tree and Tubing Hanger System

A concentric tubing hanger 12 includes a radially offset tubing annulus passage 22 closeable by a remotely operable valve, preferably a pressure balanced, hydraulically operated shuttle valve 32 at the upper end of the passage 22. The hanger 12 is of relatively compact design, accommodating a large diameter production bore and a large number of downhole service lines 46. Service line couplers 35 and outlet ports 30 of the valve 32 are housed in a void 34 defined between the tubing hanger and a seal stab assembly 36 of a subsea Christmas tree 10. The couplers 35 are bathed in annulus fluid. A tubing hanger running tool (76, fig. 4) includes a slot (80, fig. 4) and orientation helix (86, fig. 4) which co-operate with a key 82 projecting into the production bore 20 to provide passive orientation between the tool (76) and hanger 12. A subsea Christmas tree (100, fig.5) has an annulus conduit including a deviated portion (112, fig. 5) allowing room in the tree block for a bypass conduit and valve (118, 116 fig. 5). Two or more valves in the production flow path may be substituted by crown plugs to save tree bulk and weight.

Figure 1