

## Description

The invention relates to an optical scanning unit comprising a radiation source, an objective lens for focussing a radiation beam produced by the radiation source to form a scanning spot on a surface to be scanned, a translational-position and angular-position detection system for detecting the translational positions of the objective lens along and the angular positions of said lens about two orthogonal axes which both extend perpendicularly to the chief ray of the radiation beam, and an actuating device for translating and tilting the objective lens in response to the control signals supplied by the translational-position and angular-position detection system, the translational-position and angular-position detection system comprising a mirror which is fixed to the objective lens, and a radiation-sensitive detection system which is arranged in the path of the radiation reflected from the mirror and comprises two composed detectors. The invention also relates to apparatus for reading and/or recording information in an information surface of an optical record carrier.

The term "objective lens" must be interpreted in its widest sense. Such a lens may comprise a plurality of lens element but may alternatively comprise a single lens element having, for example, one or two aspheric surfaces. Alternatively, the objective lens may be, for example, a holographic lens or another lens whose operation is based on diffraction instead of refraction.

US-A 4 425 043 relating to the optical scanning unit as specified above describes an optical scanning unit for use in an apparatus for reading and/or inscribing an optical record carrier, in which scanning unit the objective lens with its holder is suspended in an electromagnetic system. This system ensures that the objective lens substantially follows the movements of the scanning unit, in other words, occupies a substantially fixed position in the scanning unit, without physical contact between this lens and the other elements of the scanning unit, i.e. the objective lens is floating. As a result of this, the position or the movement of the objective lens cannot be influenced by undesired resonances, which resonances do play a part if the objective lens is suspended in the scanning unit by means of, for example, mechanical or elastic means. Suspending or supporting the objective lens electromagnetically is very beneficial for the stability of the scanning spot formed by the objective lens.

When the objective lens is required to be capable of following movements or vibrations of the scanning unit steps must be taken to enable the translational position of the objective lens relative to the chief ray of the radiation beam and the angular position of the optical axis of this lens relative to the direction of the chief ray to be detected and these positions to be corrected.

European Patent Application no. 0,070,070, which has been laid open to public inspection, describes some examples of an electromagnetic suspension system for an objective lens in which the magnet coils of the systems are controlled by trans-

lational-position and angular-position signals in such a way that during operation of the apparatus the objective lens is not only kept floating but is also set to the correct translational position and angular position. In order to obtain the control signals necessary for this, a reflecting prism may be arranged on the circumference of the objective lens or its mounting in accordance with the above-mentioned United States Patent Specification no. 4,425,043. This prism forms part of a separate translational-position and angular-position detection system, which further comprises a radiation source and a radiation-sensitive detection system comprising at least for separate detections. The prism reflects the beam emitted by the radiation source to the detection system and splits this beam into two sub-beams which are each received by a separate set of at least two detectors. The radiation-distribution over the two sub-beams and hence the detector output signals are determined by the translational position and the angular position of the prism and, consequently, of the objective lens relative to the fixed position and orientation of the radiation beam.

The known translational-position and angular-position detection system requires some extra provisions such as an additional radiation source. Moreover, the system may exhibit cross-talk between the various detector signals and hence between the various control loops, which may render the entire translational-position and angular-position detection system unstable. Further, the known translational-position and angular-position detection system can be operative only for a specific position of the prism, viewed in a plane transverse to the optical axis of the objective lens. In the known system it is necessary either to ensure that the objective lens cannot rotate about its own axis or to provide an additional detector for detecting the rotation of the prism about the objective axis so as to enable the position of the prism to be corrected.

It is an object of the present invention to provide a translational-position and angular-position detection system which enables an independent measurement of the two translations and two pivotal movements of the object lens to be made, which requires only a small number of simple provisions in the scanning unit, and which is not influenced by a rotation of the objective lens about its axis. To this end the invention is characterized in that the mirror has a conical-ring form and is centered relative to the objective lens and that the two composed detectors are spaced by an intermediate ring and are each divided into four quadrantal sectors at the same central angles respectively, which receive an annular radiation pattern of the radiation reflected from the mirror (5), such that if the signals from the detectors are represented by S followed by the corresponding indices, the displacements along the X-axis and Y-axis and the pivotal movements about these axes may be represented by:

$$\begin{aligned} S_X &= (S_{14} + S_{15} + S_{18} + S_{19}) - (S_{13} + S_{16} + S_{17} + S_{20}) \\ S_Y &= (S_{13} + S_{14} + S_{17} + S_{18}) - (S_{15} + S_{16} + S_{19} + S_{20}) \\ S_\alpha &= (S_{13} + S_{14} + S_{19} + S_{20}) - (S_{17} + S_{18} + S_{15} + S_{16}) \\ S_\beta &= (S_{14} + S_{15} + S_{17} + S_{20}) - (S_{18} + S_{19} + S_{13} + S_{16}) \end{aligned}$$

For detecting the translational position and the angular position of the objective lens use is made of that part of the radiation from the radiation source of the apparatus which does not fall within the pupil of the objective lens and does not contribute to the scanning spot, so that it is not necessary to provide a separate radiation source for position-detection purposes. This radiation is reflected by the conical mirror to form an annular radiation spot whose average diameter is in conformity with that of the annular strip of the radiation-sensitive detection system. This system has a simple shape and can be integrated on one substrate. The tilts of the conical mirror and hence of the objective lens about the two axes transverse to the chief ray of the radiation beam and the displacement of the conical mirror along these axes each cause a different displacement of the intensity centre of the radiation distribution over the detection system, so that these displacements and tilts can be detected independently of one another. A rotation of the conical mirror about the chief ray of the beam has no effect on the detector signals because the conical mirror is ring-shaped.

An essential feature of the invention is that the conical-ring mirror has a fixed translational position and angular position relative to the objective lens. An embodiment of the optical scanning unit may be characterized further in that the conical-ring mirror is an element which is connected to the holder of the objective lens.

Another embodiment of the scanning unit is characterized in that the conical-ring mirror is constituted by a bevelled raised edge position of a lens element of the objective lens, which raised edge portion is provided with a reflecting layer. In this embodiment the raised edge portion of said lens element, which may be the sole element of the objective lens, may already be formed during the manufacture of this lens element, so that this raised edge portion merely has to be provided with a reflecting layer.

For reasons of weight and cost an objective lens of an optical scanning unit preferably comprises only one lens element. Such a lens is required to have one or two aspheric refracting surfaces. Manufacturing such a lens element in large quantities at acceptable costs is possible only if use is made of a lens die whose inner surface profile is the negative of the desired profile of the lens surface. By means of such dies it is possible to manufacture lens elements which are entirely made of a transparent plastics. However, it is preferred to use a glass preform on which a plastics in an adequately soft condition is deposited and which is given the required shape by means of a lens die, after which it is allowed to cure. This plastics may be an ultraviolet-curable synthetic resin.

A preferred embodiment of the optical scanning unit, in which the objective lens comprises one lens element in the form of a transparent body whose surface which faces the radiation source is provided with a plastics layer having an aspheric outer profile, is characterized further in that the raised edge portion consists of the said plastics.

The scanning unit may be characterized further in that the detectors of the radiation-sensitive detection system are annular. Since the surface areas of the detectors are now small, these detectors respond rapidly and the translational-position and angular-position detection system is more immune to spurious radiation as a result of, for example, undesired reflections in the scanning unit.

By the use of the translation-position and angular-position detection system in accordance with the invention it is possible to keep an objective lens which is suspended in the magnetic field accurately fixed in its translational and angular position if the scanning unit is provided with actuating means which convert the servo signals supplied by the translational-position and angular-position detection system into displacements and tilts of the objective lens.

Another aspect of the invention therefore relates to a combination of the translational-position and angular-position detection system with an electromagnetic actuating device specifically intended for this purpose. In accordance with this aspect, the scanning unit is characterized in that the actuating device comprises an annular permanent magnet which is fixedly connected to the objective lens and two sets of at least three stationary magnet coils each, the coils of the first set being arranged in a first plane transverse to the chief ray of the radiation beam and the coils of the second set being arranged in a second plane parallel to the first plane.

This actuating device also enables the axial position, i.e. the position along the chief ray of the radiation beam, and hence the focussing of the objective lens to be corrected. Such a correction is required when a disc-shaped record carrier is scanned and the axial distance between the scanning device and the point of the information surface being scanned can vary. The focussing-control signal is supplied by a focussing-error detection system which is already present in a conventional scanning unit, and not by the translational-position and angular-position detection system for the objective lens.

The variation in axial distance between the information surface and the scanning unit may be comparatively large, which means that corrections of the axial position of the objective lens should be possible over a comparatively wide range. A larger displacement of the objective system and the annular magnet out of the axial symmetrical position between the two sets of magnet coils may have the result that, when specific coils are energized in order to obtain a specific displacement of a specific tilt of the objective lens, in addition to the force in the desired direction undesired forces in other directions may occur, because the forces in the undesired directions produced by the magnet coils no longer cancel each other. This may give rise to crosstalk, referred to hereinafter as actuator cross-talk, which differs from the crosstalk between the detector signals mentioned at the beginning of the present description, referred to hereinafter as detector crosstalk.

In order to reduce actuator cross-talk the scanning unit in accordance with the invention may be

characterized further in that there is provided an axial-position detection system for detecting the position of the objective lens along the chief ray of the radiation beam and in that the signal supplied by said detection system is applied to the magnet coil. This ensures that the current through each magnet coil and hence the force generated by this coil, is corrected for, or weighted with, the actual axial position of the objective lens and the annular magnet relative to the axial centre position midway the two planes of the magnet coils.

A preferred embodiment of the scanning unit is characterized in that the axial-position detection system comprises a signal generator for supplying a first control signal to the first set of magnet coils and a second control signal to the second set of magnet coils, which signals have the same amplitude and frequency but are in phase opposition and cause the objective lens to be tilted periodically about one of the two axes transverse to the chief ray of the radiation beam, and in that the axial-position detection system further comprises the elements of the translational-position and angular-position detection system for converting the periodic tilting into a periodic signal whose amplitude and phase are representative of the magnitude and the direction of a displacement of the axial centre of the annular magnet out of a plane which is situated midway between the two planes in which the magnet coils are disposed.

The addition detection function is then obtained by means of a minimal number of additional elements and an optimum use is made of provisions which are already present in the scanning unit.

The optical scanning unit is very suitable for use in an apparatus for reading and/or recording information in an information surface of a round disc-shaped record carrier. Such an apparatus may be characterized in that a separating element is arranged between the objective lens and the radiation source for separating the radiation reflected by the conical ring mirror from the radiation emitted by the radiation source.

The radiation which emerges from the opening in the conical ring mirror may be used for the actual scanning of, for example, a disc-shaped record carrier. This record carrier may have a radiation-transmitting or a radiation-reflecting information surface. In the latter case the radiation reflected by the information surface can be directed to a radiation-sensitive information detector via said separating element. This information detector, which may comprise a plurality of sub-detectors, may be arranged at another location than the radiation-sensitive detection system of the translational-position and angular-position detection system. However, preferably a radiation-sensitive detector is arranged inside the annular inner detector of the translational-position and angular-position detection system, for converting the radiation reflected by the information surface into an electric signal. In addition to the information being read, this signal may contain information on the position of the scanning spot relative to an information track of the record carrier.

The invention will now be explained by describing, by way of example its use in an apparatus for reading and/or inscribing an optical record carrier. Reference is made to the drawings, in which:

Fig. 1 shows a read apparatus provided with a translational-position and angular-position detection system in accordance with the invention,

Fig. 2 shows the composite radiation-sensitive detector of this system,

Fig. 3 shows an electronic circuit for processing the signals from this detector,

Fig. 4 shows an objective lens with an integrated conical-ring mirror,

Fig. 5 is a plan view of an example of an electromagnetic suspension system,

Fig. 6 is a cross-sectional view of this system, and

Fig. 7 illustrates how an axial-position signal for the objective lens can be obtained.

The scanning unit shown in Fig. 1 comprises a radiation source 1, for example a diode laser, a collimator lens 2 and an objective lens 3, which is mounted in a holder 4. Both the collimator lens and the objective lens may comprise a plurality of lens elements, but preferably they comprise a single lens element having at least one aspheric refracting surface.

The diverging read beam *b* emitted by the radiation source is converted into a parallel beam by the collimator lens, which beam fills the aperture of the objective lens 3 in adequate manner. The objective lens focusses the read beam to form a diffraction-limited radiation spot *V* having a diameter of, for example, 1  $\mu\text{m}$  on the information surface 31 of a disc-shaped record carrier 30, of which a small part is shown in radial cross-section in Fig. 1. The information is arranged in concentric tracks 33 or quasi-concentric tracks which together constitute a spiral track. This information comprises a multitude of optically detectable information areas, not shown, which alternate with intermediate areas. Suitably, the information surface 31 is situated on the upper side of the record carrier, so that the read beam *b* traverses the transparent substrate 32 of the record carrier before it reaches the information surface. Further, the information surface is suitably radiation-reflecting, so that the read beam is reflected towards the radiation source.

As the record carrier is rotated relative to the scanning unit the beam which is reflected by the information source is time-modulated in conformity with the sequence of information areas and intermediate areas in an information track to be read. In order to separate the modulated beam from the beam which is emitted by the radiation source a separating element 6 is arranged in the radiation path, which element may be, for example, a semitransparent mirror or a beam-splitting prism, which may be polarization sensitive or not and whose interface 7 reflects at least a part of the radiation to the radiation-sensitive information detector 11. The information detector in the form of for example a photodiode, is suitably arranged in a plane 10 which coincides with the diode-laser exit face which is mirror-inverted rela-

tive to the interface 7. The information detector 11 converts the modulated read beam into an electric signal which is processed in known manner to form a signal which is suitable for being displayed, reproduced or processed in another manner depending on the type of information stored in the record carrier. The nature of the information and the processing of the signal from the information detector fall beyond the scope of the present invention and are not discussed in more detail.

In order to enable the objective lens 3 to follow the movements of the scanning unit without any physical contact between this lens and the other elements of the scanning unit the objective lens is suspended in an electromagnetic system which will be described in more detail with reference to Figs. 5 and 6. This requires the use of a translational-position and angular-position detection system for measuring deviations between the centre M of the objective lens and the chief ray L of the beam  $\underline{b}$  along an X-axis in the plane of the drawing and along an Y-axis perpendicular to the plane of the drawing and tilts of the objective lens about these two axes, so that such deviations from the translational position and the angular position can be eliminated by means of a control system.

The origin of the XYZ axial system shown in the right-hand part of Fig. 1 is in reality situated in the point M, so that the Z-axis coincides with the chief ray L. The direction along this axis may also be referred to as the axial direction. The tilt of the object lens about the X-axis may be represented by the tilting angle  $\alpha$  and that about the Y-axis by the tilting angle  $\beta$ . The X axis and the Y-axis extend, for example, in the information plane, parallel to the radial direction and the tangential direction respectively.

In accordance with the invention the translational-position and angular-position detection system comprises a ring mirror 5 which is fixedly connected to the objective lens which mirror is also conical, i.e. the reflecting surface is disposed at an angle which differs from 90° to the chief ray L, and a radiation-sensitive detection system 9 which is arranged in the plane 10 and which is shown in front view in Fig. 2, i.e. in a section taken on the line II-II' in Fig. 1. The conical ring mirror 5 reflects that part of the radiation beam  $\underline{b}$  which falls within the aperture 8 but outside the pupil of the objective lens to the separating element 6, which in its turn reflects a part of the radiation to the detection system 9. An annular radiation pattern is formed on this system. The radiation-sensitive detection system 9 comprises two detector rings which are spaced by an intermediate ring 12 and which each comprise four detectors 13, 14, 15, 16 and 17, 18, 19, 20 respectively. The annular radiation pattern is represented by the dashed circles 21 in Fig. 2. The average diameter of this radiation pattern is equal to that of the intermediate ring 12.

The radiation distribution of the pattern among the eight detectors depending on the translational position and the angular position of the conical-ring mirror 5 and, consequently, of the objective lens 3. A tilted position about the X-axis or the Y-axis results in the annular radiation pattern 21 being shifted in the direction indicated by the arrow 22 and the

arrow 23 respectively. A shift of the mirror 5 along the X-axis and Y-axis results in a change of the radiation distribution within the annular radiation pattern in such a way that in the case of a displacement along the X axis the left-hand part of the detection system will receive more radiation or less radiation than the right-hand part, because the portions of the two mirror halves which are situated within the beam, which is stopped down by the aperture 8, are no longer identical. Similarly, the upper part of the detection system will receive more radiation or less radiation than the lower part in the case of a movement along the Y-axis.

If the signals from the detectors 13 to 20 are represented by S followed by the corresponding indices, the displacements along the X-axis and Y-axis and the pivotal movements about these axes may be represented by:

$$S_x = (S_{14} + S_{15} + S_{18} + S_{19}) - (S_{13} + S_{16} + S_{17} + S_{20})$$

$$S_y = (S_{13} + S_{14} + S_{17} + S_{18}) - (S_{15} + S_{16} + S_{19} + S_{20})$$

$$S_\alpha = (S_{13} + S_{14} + S_{19} + S_{20}) - (S_{17} + S_{18} + S_{15} + S_{16})$$

$$S_\beta = (S_{14} + S_{15} + S_{17} + S_{20}) - (S_{18} + S_{19} + S_{13} + S_{16})$$

The individual detector signals can be processed to form composite signals  $S_x$ ,  $S_y$ ,  $S_\alpha$  and  $S_\beta$  by means of an electronic circuit, of which an example is shown in Fig. 3. The operation of the circuit, which comprises a number of adder circuits (40 to 47 and 50 to 57) and a number of subtractor circuits (48, 49, 58, 59), is evident from the Figure and requires no further explanation. The composite signals  $S_x$ ,  $S_y$ ,  $S_\alpha$  and  $S_\beta$  are independent of each other and exhibit no mutual crosstalk, so that the various displacements and tilting angles can be detected independently of each other. A rotation of the objective lens about the Z-axis does not cause a change of the annular radiation pattern 21 and consequently does not influence the detector signals. Displacements of the objective lens along the Z-axis also do not have any influence on the radiation pattern 21.

In the scanning unit the signals are employed for driving the magnet coils in an electromagnetic suspension system. In this way the translational position and the angular position of the objective lens are locked to the translational position and the angular position of the composite detector 13-20, which occupies a fixed position within the scanning unit, so that during operation of the read apparatus the objective lens is always controlled to assume the correct translational position and angular position within the scanning unit.

A requirement for this is that the conical ring mirror has a fixed translational position and angular position relative to the objective lens. For this purpose, as is shown in Fig. 1, the mirror 5 may form part of the objective holder on mounting 4, within which the objective lens is fixedly arranged. It is alternatively possible to use a separate element for this mirror, which element is secured to the exterior or interior of the objective holder. A very attractive possibility of accurately locking the translational position and the angular position of the annular mirror 5 to those of the objective lens 3 is obtained when this lens is manufactured in accordance with a

replica process. This possibility is illustrated in Fig. 4.

It has long been known that in the scanning unit described the objective lens comprising a plurality of elements may be replaced by an objective lens comprising only one lens element. However, instead of spherical refractive surfaces this lens element should have aspheric refractive surfaces in order to provide adequate correction for lens aberrations. In order to enable such single objective lenses with intricate surface profiles to be manufactured in large quantities at an acceptable price, it has already been proposed to employ a transparent body or preform 60 of, for example, glass, having for example two spherical refractive surfaces 61 and 62. A plastics material in an adequately soft condition is deposited on one of these surfaces or on both surfaces. This plastics material may be a thermosetting plastics, but alternatively it may be an ultraviolet-polymerisable synthetic resin. After the plastics material has been deposited on the surface a die whose surface profile is the negative of the desired lens profile is pressed into the material. Subsequently, the material is cured and the die is removed, so that a lens provided with a plastics layer 63 having an aspheric profile 64 is obtained. Such lenses need not be subjected to any further operation such as polishing.

In accordance with the invention the die by means of which the objective lens is manufactured can be adapted in such a way that along with the aspheric layer 63 a raised edge portion 65 with a bevelled surface 66 is formed. After the manufacture of the objective lens the surface 66 merely has to be provided with a reflecting coating 67, for example by vapour deposition, in order to obtain an objective lens with an integrated conical-ring mirror. The reflecting raised edge portion may be formed on the lens surface which is situated nearest the radiation source but alternatively it may be formed on the other lens surface.

Alternatively, the entire objective lens may be moulded from a transparent plastics by means of dies having the desired profile. The die used for manufacturing a lens surface may be formed with a recess at its edge so that the lens thus manufactured is formed with a raised edge portion with a bevelled inner surface. If a glass preform is used the first-mentioned replica lens has the advantage that it is more immune to temperature variations and other environmental influences, such as moisture.

It is obvious that the scanning unit may comprise an objective lens comprising a plurality of lens elements and that the surface of the last lens which faces the radiation source may have an aspheric surface and carry an integrated conical ring mirror. Alternatively, this mirror may be arranged on one of the other lens surfaces.

As is shown in Fig. 1 the information detector 11 may be arranged inside the composite detector of the translational-position and angular-position detection system and may be integrated on one substrate together with said system, using known and very accurate technologies for the manufacture of integrated circuits. The information detector may

comprise a single detector which only supplies the signal representing the information stored on the record carrier. Alternatively, the information detector may be divided into sub-detectors which in addition to the information signal also supply control signals, such as a tracking signal.

A tracking signal can be obtained by dividing the detector 11 into two sub-detectors 11a and 11b, as indicated by the broken line 45 in Fig. 2, which line corresponds to the tangential direction on the record carrier 30. The difference between the output signals of the sub-detectors 11a and 11b contain information on the magnitude and the direction of a deviation between the centre of the read spot V and the centre line of an information track to be read. The manner in which a tracking signal can be generated falls beyond the scope of the present invention and will not be described in more detail. By way of example reference is made to United States Patent Specification no. 4,425,043, where in addition to the said method of generating a tracking signal a method of generating a focussing error signal is described.

In the scanning unit in accordance with the invention it is possible, by analogy with the last-mentioned method to separate a part of the main-beam radiation reflected by the prism 6 from the main beam i.e. the beam which is incident on the detector 11, for example by means of a semitransparent mirror. By means of, for example, a roof prism the part thus separated can be divided into two sub-beams, which sub-beams are incident on three or four radiation-sensitive detectors which are arranged in line transversely of the roof edge of the prism. The focussing-error signal is given by the difference between the sum signal of the two outer detectors and the sum signal of the two inner detectors.

In order to keep the radiation spot V centred on an information track a read apparatus comprises a course control and a fine control. For coarse control purposes the scanning unit shown in Fig. 1 may be moved bodily in a radial direction relative to the record carrier. For this purpose the elements 1, 2, 3, 6, 9 and 11 may be arranged inside one tubular holder, which is radially movable by means of a pivotal arm or a rectilinearly movable slide. Fine control may be effected, for example, by means of a pivotal mirror, not shown in Fig. 1, or by moving the objective lens over small distances in the X-direction or the radial direction. As described in United States Patent Specification no. 4,423,496 this fine control results in the chief ray L of the read beam being displaced relative to the detectors 11a and 11b independently of the deviation between the centre of the radiation spot V and the centre line of a track being read. This introduces an error, referred to as offset, into the tracking signal. As is described in United States Patent Specification no. 4,423,496 this error can be eliminated by correcting the tracking signal obtained by means of the detectors 11a and 11b using a signal which is proportional to the radial position of the objective lens. In a scanning unit according to the invention this signal  $S_x$  is already supplied by the translational-position and angular position detection system, so that unlike apparatus-

es in accordance with United States Patent Specification no. 4,423,496 no separate system is required for this purpose.

When an optical record carrier having a radiation-reflecting information surface is read by means of a diode laser use can be made of the feedback effect of such a laser. The beam which is modulated by the information structure is then not separated from the beam emitted by the diode laser by the first-mentioned beam re-enters the diode laser and interferes with the radiation produced in the laser resonant cavity. As a result of this, the beam emitted by the diode laser is modulated in conformity with the information being read. This modulation can be detected by means of a radiation-sensitive detector arranged at the rear of the diode laser, from which radiation emerges which is correlated with the radiation emerging from the front of the diode laser. Another consequence of the feedback effect is that the electrical resistance of the diode laser varies in conformity with the information being read. Detecting this variation is another possibility of reading the information stored in the record carrier.

The translational-position and angular-position detection system in accordance with the invention may then be employed in scanning units using the feedback effect. Such a scanning unit differs from that shown in Fig. 1 in that the separating element 6 is dispensed with, the function of the information detector 11 is performed by the diode laser 1, and the radiation-sensitive detection system 9 for the translational-position and angular-position detection is arranged around the diode laser 1.

Moreover, the invention may be employed in apparatus for reading optical record carriers in transmission. In such apparatus the information detector is disposed on the other side of the record carrier remote from the radiation source, in an arrangement as shown in Fig. 1 on the upper side. This detector can then no longer be integrated with the detection system 9. This detection system may be arranged in the position shown in Fig. 1 or may again be arranged around the diode laser.

In order to maintain the objective lens in the correct X-position and Y-position and to maintain the objective axis parallel to the Z-axis, use may be made of an electromagnetic system comprising a plurality of coils, to which the signals  $S_x$ ,  $S_y$ ,  $S_\alpha$  and  $S_\beta$  from the translational-position and angular-position detection system are applied. European Patent Application no. 0,103,929 describes an electromagnetic system in which an objective lens for reading an optical record carrier is moved and tilted in such a way that the radiation spot formed by this objective lens is incident on the information surface at the correct radial and tangential position. In accordance with the invention a similar electromagnetic system may be employed for maintaining the objective lens in the correct translational-position and angular-positions relative to the radiation-sensitive detection system 8.

Fig. 5 is a plan view of the electromagnetic system and Fig. 6 is a sectional view of the system tak-

en on the line VI-VI'. In these Figures the numeral 3 denotes the objective lens and 4 its holder. A ring 70 of a permanent magnetic material is secured to this holder. This ring is situated in the magnetic-force field of at least six stationary magnet coils which are arranged in two axially shifted planes. Three magnet coils 71, 72 and 73 are visible in the plane view of Fig. 5. The magnet coils 74, 75 and 76 of the second set, which are situated underneath this first-mentioned set of magnet coils and which are therefore not visible, have the same shape. Suitably, the magnet coils have an arcuate shape in conformity with the three-dimensional field of the permanent magnet 70, so that the Lorentz forces are as large as possible. Instead of three it is possible to provide four magnet coils in each plane, i.e. eight magnet coils in total. For further details on the construction of the electro-magnetic system reference is made to European Patent Application no. 0,103,929. Said Application also describes how by applying specific control signals to specific coils displacements in the X-direction or Y-direction or tilts about the X-axis or Y-axis of the objective lens can be obtained and also how the objective lens can be moved in an axial direction. In the table in European Patent Application no. 0,103,929, which indicates through which coils and with the phase currents should be fed in order to obtain a specific displacement or pivotal movement of the objective lens, a current proportional to the signal  $S_x$ ,  $S_y$ ,  $S_\alpha$  or  $S_\beta$  should be inserted at the appropriate points of said table for each of the movements indicated therein. The current for the axial displacement of the objective lens is proportional to the focussing-error signal, which is supplied by a conventional focussing-error detection system, for example the system described in United States Patent Specification No. 4,425,043.

For each of the five possible movements at least two magnet coils are driven with signals in phase opposition, so that for a large travel only a small variation of the Lorentz forces occurs. In this electro-magnetic system the various drives are correctly isolated from one another which guarantees a higher stability of the five control systems.

When the scanning unit described herein is used for reading a rotating disc-shaped record carrier comparatively large variations in the axial distance between the objective lens and the information surface may occur. These variations may be caused by vibrations in the read apparatus, by obliquity of the record carrier or the axis of rotation, by an oblique position of the information surface in the record carrier, or in particular in the case of large record carriers, by sagging of the record carrier towards the edge. In the case of larger axial displacements of the objective lens in the scanning unit in order to provide correction for these variations, crosstalk may occur between the various actuators, referred to an actuator cross-talk. In accordance with a further aspect of the invention this cross-talk can be eliminated by detecting the axial position of the objective lens in the scanning unit and by correcting the control signals for the X and Y movements and

the  $\alpha$  and  $\beta$  tilts by means of the axial-position signal thus obtained.

This additional controller is illustrated in Fig. 7. In this Figure the block 79 contains all the elements of the scanning unit of Fig. 1, except for the objective lens 3 and the conical-ring mirror 5. Use is made of an oscillator 77 which supplies two 180° phase-shifted periodic signals  $S_w$  and  $S_w'$  in order to obtain a periodic pivotal movement of the objective lens. One of these signals is applied to the upper array of magnet coils and the second signal to the lower array of magnet coils. Within one magnet-coil array those magnet coils which are situated opposite one another relative to the pivotal axis are driven in phase opposition. These signals produce a periodic tilting, for example about the X-axis of the objective lens 3 with the conical-ring mirror 5, so that the translational-position and angular-position detection system supplies an additional signal  $S_{\alpha'}$ , which is a period signal of a specific phase. This phase indicates whether the upper or the lower magnet-coil array exerts the larger force on the annular magnet 70 and the objective lens 3 and consequently whether the objective lens has shifted upwards or downwards relative to the central position between the planes 80 and 81. The amplitude of the signal  $S_{\alpha'}$  is proportional to the magnitude of the deviation from the central position. By comparing the phase of the signal  $S_{\alpha'}$  with that of one of the signal  $S_w$ ,  $S_w'$  in the phase comparator 78 and axial-position signal  $S_z$  is obtained. This signal is superimposed on the signal  $S_x$ ,  $S_y$ ,  $S_{\alpha}$  and  $S_{\beta}$ , in order to correct the actuators to be energized by means of these signals with respect to the axial position of the objective lens and the annular magnet.

The fact that the invention is described for a read apparatus does not mean that the scope of the invention is limited thereto. Alternatively, the scanning unit in accordance with the invention may be employed in apparatuses for recording information in optical record carriers, which apparatuses in principle are of the same construction as the read apparatus but operate with a higher radiation intensity, which intensity is modulated in conformity with the information to be recorded. For this purpose a modulator, for example an acousto-optical modulator, may be arranged in the radiation path between the radiation source 1 and the separating element 6. If the radiation source is a diode laser the radiation emitted by this source may be modulated directly by modulating the electric current fed through the diode laser in conformity with the information to be recorded. Further, the invention may be employed in other optical scanning systems, such as a scanning microscope, and in general in imaging systems comprising small lenses and having a high imaging quality, in which the image field of the lenses may be limited.

## Claims

1. An optical scanning unit comprising a radiation source (1), an objective lens (3) for focussing a radiation beam (b) produced by the radiation source (1)

to form a scanning spot (v) on a surface (31) to be scanned, a translational-position and angular-position detection system for detecting the translational positions of the objective lens (3) along and the angular positions of said lens about two orthogonal axes (X, Y) which both extend perpendicularly to the chief ray (L) of the radiation beam (b), and an actuating device for translating and tilting the objective lens (3) in response to the control signals supplied by the translational-position and angular-position detection system, the translational-position and angular-position detection system comprising a mirror (5) which is fixed relative to the objective lens (3), and a radiation-sensitive detection system (9) which is arranged in the path of the radiation reflected from the mirror (5) and comprises two radiation sensitive detection means each being composed of a plurality of detectors, characterized in that the mirror (5) has a conical-ring form and is centered relative to the objective lens (3) and that the two radiation-sensitive detection means are spaced by an intermediate ring (12) and are each divided into four quadrantal sectors 13, 14, 15, 16 and 17, 18, 19, 20 at the same central angles respectively, which receive an annular radiation pattern (21) of the radiation reflected from the mirror (5), such that if the signals from the detectors 13 to 20 are represented by S followed by the corresponding indices, the displacements along the X-axis and Y-axis and the pivotal movements about these axes may be represented by:

$$S_x = (S_{14} + S_{15} + S_{18} + S_{19}) - (S_{13} + S_{16} + S_{17} + S_{20})$$

$$S_y = (S_{13} + S_{14} + S_{17} + S_{18}) - (S_{15} + S_{16} + S_{19} + S_{20})$$

$$S_{\alpha} = (S_{13} + S_{14} + S_{19} + S_{20}) - (S_{17} + S_{18} + S_{15} + S_{16})$$

$$S_{\beta} = (S_{14} + S_{15} + S_{17} + S_{20}) - (S_{18} + S_{19} + S_{13} + S_{16})$$

2. An optical scanning unit as claimed in Claim 1, characterized in that the conical-ring mirror is an element (5) which is connected to the holder (4) of the objective lens (3).

3. An optical scanning unit as claimed in Claim 1, characterized in that the conical-ring mirror is constituted by a bevelled raised edge portion (65) of a lens element (60) of the objective lens (3), which raised edge portion is provided with a reflecting layer (67).

4. An optical scanning unit as claimed in Claim 3, in which the objective lens (3) comprises one lens element in the form of a transparent body (60) whose surface (62) which faces the radiation source (1) is provided with a plastics layer (63) having an aspheric outer profile (64), characterized in that the raised edge portion (65) consists of the said plastics.

5. An optical scanning unit as claimed in Claim 1, 2, 3 or 4, characterized in that the detectors (13, 14, 15, 16, 17, 18, 19, 20) of the radiation-sensitive detection system (9) are annular.

6. An optical scanning unit as claimed in Claim 1, 2, 3, 4 or 5, characterized in that the actuating device comprises an annular permanent magnet (70) which is fixedly connected to the objective lens (3) and two sets of at least three stationary magnet coils each (71, 72, 73; 74, 75, 76), the coils (71, 72, 73) of the first set being arranged in a first plane

the  $\alpha$  and  $\beta$  tilts by means of the axial-position signal thus obtained.

This additional controller is illustrated in Fig. 7. In this Figure the block 79 contains all the elements of the scanning unit of Fig. 1, except for the objective lens 3 and the conical-ring mirror 5. Use is made of an oscillator 77 which supplies two 180° phase-shifted periodic signals  $S_w$  and  $S_w'$  in order to obtain a periodic pivotal movement of the objective lens. One of these signals is applied to the upper array of magnet coils and the second signal to the lower array of magnet coils. Within one magnet-coil array those magnet coils which are situated opposite one another relative to the pivotal axis are driven in phase opposition. These signals produce a periodic tilting, for example about the X-axis of the objective lens 3 with the conical-ring mirror 5, so that the translational-position and angular-position detection system supplies an additional signal  $S_{\alpha}'$ , which is a period signal of a specific phase. This phase indicates whether the upper or the lower magnet-coil array exerts the larger force on the annular magnet 70 and the objective lens 3 and consequently whether the objective lens has shifted upwards or downwards relative to the central position between the planes 80 and 81. The amplitude of the signal  $S_{\alpha}'$  is proportional to the magnitude of the deviation from the central position. By comparing the phase of the signal  $S_{\alpha}'$  with that of one of the signal  $S_w$ ,  $S_w'$  in the phase comparator 78 and axial-position signal  $S_z$  is obtained. This signal is superimposed on the signal  $S_x$ ,  $S_y$ ,  $S_{\alpha}$  and  $S_{\beta}$ , in order to correct the actuators to be energized by means of these signals with respect to the axial position of the objective lens and the annular magnet.

The fact that the invention is described for a read apparatus does not mean that the scope of the invention is limited thereto. Alternatively, the scanning unit in accordance with the invention may be employed in apparatuses for recording information in optical record carriers, which apparatuses in principle are of the same construction as the read apparatus but operate with a higher radiation intensity, which intensity is modulated in conformity with the information to be recorded. For this purpose a modulator, for example an acousto-optical modulator, may be arranged in the radiation path between the radiation source 1 and the separating element 6. If the radiation source is a diode laser the radiation emitted by this source may be modulated directly by modulating the electric current fed through the diode laser in conformity with the information to be recorded. Further, the invention may be employed in other optical scanning systems, such as a scanning microscope, and in general in imaging systems comprising small lenses and having a high imaging quality, in which the image field of the lenses may be limited.

## Claims

1. An optical scanning unit comprising a radiation source (1), an objective lens (3) for focussing a radiation beam (b) produced by the radiation source (1)

to form a scanning spot (v) on a surface (31) to be scanned, a translational-position and angular-position detection system for detecting the translational positions of the objective lens (3) along and the angular positions of said lens about two orthogonal axes (X, Y) which both extend perpendicularly to the chief ray (L) of the radiation beam (b), and an actuating device for translating and tilting the objective lens (3) in response to the control signals supplied by the translational-position and angular-position detection system, the translational-position and angular-position detection system comprising a mirror (5) which is fixed relative to the objective lens (3), and a radiation-sensitive detection system (9) which is arranged in the path of the radiation reflected from the mirror (5) and comprises two radiation sensitive detection means each being composed of a plurality of detectors, characterized in that the mirror (5) has a conical-ring form and is centered relative to the objective lens (3) and that the two radiation-sensitive detection means are spaced by an intermediate ring (12) and are each divided into four quadrantal sectors 13, 14, 15, 16 and 17, 18, 19, 20 at the same central angles respectively, which receive an annular radiation pattern (21) of the radiation reflected from the mirror (5), such that if the signals from the detectors 13 to 20 are represented by S followed by the corresponding indices, the displacements along the X-axis and Y-axis and the pivotal movements about these axes may be represented by:

$$S_x = (S_{14} + S_{15} + S_{18} + S_{19}) - (S_{13} + S_{16} + S_{17} + S_{20})$$

$$S_y = (S_{13} + S_{14} + S_{17} + S_{18}) - (S_{15} + S_{16} + S_{19} + S_{20})$$

$$S_{\alpha} = (S_{13} + S_{14} + S_{19} + S_{20}) - (S_{17} + S_{18} + S_{15} + S_{16})$$

$$S_{\beta} = (S_{14} + S_{15} + S_{17} + S_{20}) - (S_{18} + S_{19} + S_{13} + S_{16})$$

2. An optical scanning unit as claimed in Claim 1, characterized in that the conical-ring mirror is an element (5) which is connected to the holder (4) of the objective lens (3).

3. An optical scanning unit as claimed in Claim 1, characterized in that the conical-ring mirror is constituted by a bevelled raised edge portion (65) of a lens element (60) of the objective lens (3), which raised edge portion is provided with a reflecting layer (67).

4. An optical scanning unit as claimed in Claim 3, in which the objective lens (3) comprises one lens element in the form of a transparent body (60) whose surface (62) which faces the radiation source (1) is provided with a plastics layer (63) having an aspheric outer profile (64), characterized in that the raised edge portion (65) consists of the said plastics.

5. An optical scanning unit as claimed in Claim 1, 2, 3 or 4, characterized in that the detectors (13, 14, 15, 16, 17, 18, 19, 20) of the radiation-sensitive detection system (9) are annular.

6. An optical scanning unit as claimed in Claim 1, 2, 3, 4 or 5, characterized in that the actuating device comprises an annular permanent magnet (70) which is fixedly connected to the objective lens (3) and two sets of at least three stationary magnet coils each (71, 72, 73; 74, 75, 76), the coils (71, 72, 73) of the first set being arranged in a first plane



(80) transverse to the chief ray (L) of the radiation beam (b) and the coils (74, 75, 76) of the second set being arranged in a second plane (81) parallel to the first plane (80).

7. An optical scanning unit as claimed in any one of the preceding Claims, characterized in that there is provided an axial-position detection system for detecting the position of the objective lens (3) along the chief ray (L) of the radiation beam (b) and in that the signal supplied by said detection system is applied to the magnet coils (71, 72, 73; 74, 75, 76).

8. An optical scanning unit as claimed in Claim 7, characterized in that the axial-position detection system comprises a signal generator (77) for supplying a first control signal (S'w) to the first set of magnet coils (71, 72, 73) and a second control signal (Sw) to the second set of magnet coils (74, 75, 76), which signals have the same amplitude and frequency but are in phase opposition and cause the objective lens (3) to be tilted periodically about one of the two axes (X, Y) transverse to the chief ray (L) of the radiation beam (b) and in that the axial-position detection system further comprises the elements of the translational-position and angular-position detection system for converting the periodic tilting into a periodic signal (S'α) whose amplitude and phase are representative of the magnitude and the direction of a displacement of the axial centre of the annular magnet (70), out of a plane which is situated midway between the two planes (80, 81) in which the magnet coils (71, 72, 73; 74, 75, 76) are disposed.

9. An apparatus for reading and/or recording information in an information surface of a round disc-shaped record carrier (30), comprising an optical scanning unit as claimed in any one of the preceding Claims, characterized in that a separating element (7) is arranged between the objective lens (3) and the radiation source (1) for separating the radiation reflected by the conical-ring mirror from the radiation (b) emitted by the radiation source (1).

10. An apparatus as claimed in Claim 9, characterized in that a radiation-sensitive detector (11) is arranged inside the annular inner detector (17, 18, 19, 20) of the translational-position and angular-position detection system, for converting the radiation reflected by the information surface (31) into an electrical signal.

#### Patentansprüche

1. Optische Abtasteinheit mit einer Strahlungsquelle (1), einer Objektivlinse (3) zum Fokussieren eines Strahlungsbündels (b) aus der Strahlungsquelle (1) zur Bildung eines Strahlungsflecks (v) auf einer abzutastenden Oberfläche (31), einem System zum Detektieren der Schubpositionen der Objektivlinse (3) entlang zwei orthogonalen Achsen (X, Y) und der Winkelpositionen der Linse um diese beiden Achsen, die sich senkrecht zum Hauptstrahl (L) des Strahlungsbündels (b) erstrecken, und einer Aktuatoreinrichtung zum Translieren und Kippen der Objektivlinse (3) anhand der Steuersignale aus dem Schubpositions- und Winkelpositions-Detektorsystem, das einen in bezug auf die Objektivlinse (3) festgesetzten Spiegel (5) und eine strahlungs-

empfindliche Detektoranlage (9) enthält, die im Weg der am Spiegel reflektierten Strahlung angeordnet ist und zwei strahlungsempfindliche Detektormittel enthält, die aus je einer Anzahl von Detektoren bestehen, dadurch gekennzeichnet, daß der Spiegel (5) eine Konusringform besitzt und gegen die Objektivlinse (3) zentriert ist, und daß die zwei strahlungsempfindlichen Detektormittel durch einen Zwischenring (12) voneinander getrennt und in je vier Quadrantalsektoren 13, 14, 15, 16 und 17, 18, 19, 20 unter den gleichen zentralen Winkeln verteilt sind, die ein ringförmiges Strahlungsmuster (21) der vom Spiegel (5) herrührenden Strahlung derart empfangen, daß, wenn die Signale aus den Detektoren 13 bis 20 durch S, gefolgt von den entsprechenden Indizes dargestellt werden, wobei die Verschiebungen entlang der X-Achse und der Y-Achse und die Drehbewegungen um diese Achsen durch folgende Gleichungen dargestellt werden können:

$$S_X = (S_{14} + S_{15} + S_{18} + S_{19}) - (S_{13} + S_{16} + S_{17} + S_{20})$$

$$S_Y = (S_{13} + S_{14} + S_{17} + S_{18}) - (S_{15} + S_{16} + S_{19} + S_{20})$$

$$S_\alpha = (S_{13} + S_{14} + S_{19} + S_{20}) - (S_{17} + S_{18} + S_{15} + S_{16})$$

$$S_\beta = (S_{14} + S_{15} + S_{17} + S_{20}) - (S_{18} + S_{19} + S_{13} + S_{16})$$

2. Optische Abtasteinheit nach Anspruch 1, dadurch gekennzeichnet, daß der Konusringspiegel ein Element (5) ist, das an der Fassung (4) der Objektivlinse (3) befestigt ist.

3. Optische Abtasteinheit nach Anspruch 1, dadurch gekennzeichnet, daß der Konusringspiegel durch einen schrägen erhöhten Randteil (65) eines Linsenelements (60) der Objektivlinse (3) gebildet wird und dieser erhöhte Randteil ist mit einer Reflexionsschicht (67) versehen.

4. Optische Abtasteinheit nach Anspruch 3, in der die Objektivlinse (3) ein Linsenelement in Form eines transparenten Körpers (60) enthält, dessen der Strahlungsquelle (1) zugeordnete Oberfläche (62) mit einer Kunststoffschicht (63) mit asphärischem Außenprofil (64) überzogen ist, dadurch gekennzeichnet, daß der erhöhte Randteil (65) aus dem genannten Kunststoff besteht.

5. Optische Abtasteinheit nach Anspruch 1, 2, 3 oder 4, dadurch gekennzeichnet, daß die Detektoren (13, 14, 15, 16, 17, 18, 19, 20) der strahlungsempfindlichen Detektoranlage (9) ringförmig sind.

6. Optische Abtasteinheit nach Anspruch 1, 2, 3, 4 oder 5, dadurch gekennzeichnet, daß der Aktuator einen ringförmigen Dauermagneten (70), der auf der Objektivlinse (3) starr befestigt ist, und zwei Sätze von wenigstens je drei statischen Magnetspuln (71, 72, 73; 74, 75, 76) enthält, wobei die Spulen (71, 72, 73) des ersten Satzes in einer ersten Ebene (80) quer zum Hauptstrahl (L) des Strahlungsbündels (b) und die Spulen (74, 75, 76) des zweiten Satzes in einer zweiten Ebene (81) parallel zur ersten Ebene (80) angeordnet sind.

7. Optische Abtasteinheit nach einem oder mehreren der vorangehenden Ansprüche, dadurch gekennzeichnet, daß ein Achslagendetektorsystem zum Detektieren der Lage der Objektivlinse (3) entlang des Hauptstrahls (L) des Strahlungsbündels (b) vorgesehen ist, und daß das vom genannten Detektorsystem ausgegebene Signal an die Magnetspuln (71, 72, 73; 74, 75, 76) gelegt wird.



8. Optische Abtasteinheit nach Anspruch 7, dadurch gekennzeichnet, daß ein Achslagendetektorsystem einen Signalgenerator (77) zum Erzeugen eines ersten Steuersignals (S'w) zum ersten Satz der Magnetspulen (71, 72, 73) und eines zweiten Steuersignals (Sw) zum zweiten Satz der Magnetspulen (74, 75, 76) enthält, wobei diese Signale die gleiche Amplitude und Frequenz besitzen, jedoch gegenphasig sind und einen periodischen Kippvorgang der Objektivlinse (3) um eine oder beide Achsen (X, Y) quer zum Hauptstrahl (L) des Strahlungsbündels (b) auslöst, und daß das Achslagendetektorsystem außerdem die Elemente des Schubpositions- und Winkelpositionsdetektorsystems zum Umsetzen des periodischen Kippvorgangs in ein periodisches Signal (S'α) enthält, dessen Amplitude und Phase die Größe und Richtung einer Verschiebung der axialen Mitte des ringförmigen Magneten (70) aus einer Ebene darstellen, die sich halbwegs zwischen den zwei Ebenen (80, 81) befindet, in denen die Magnetspulen (71, 72, 73; 74, 75, 76) angeordnet sind.

9. Gerät zum Lesen und/oder Schreiben von Information auf einer Informationsoberfläche eines runden scheibenförmigen Aufzeichnungsträgers (30) mit einer optischen Abtasteinheit nach einem oder mehreren der vorangehenden Ansprüche, dadurch gekennzeichnet, daß ein Trennelement (7) zwischen der Objektivlinse (3) und der Strahlungsquelle (1) zum Trennen der vom Konusringspiegel reflektierten Strahlung von der Strahlung (b) aus der Strahlungsquelle (1) vorgesehen ist.

10. Gerät nach Anspruch 9, dadurch gekennzeichnet, daß ein strahlungsempfindlicher Detektor (11) im ringförmigen Innendetektor (17, 18, 19, 20) des Schubpositions- und Winkelpositionsdetektorsystems zum Umsetzen der von der Informationsfläche (31) reflektierten Strahlung in ein elektrisches Signal angeordnet ist.

#### Revendications

1. Dispositif de balayage optique comprenant une source de rayonnement (1), un objectif (3) pour focaliser un faisceau de rayonnement (b) produit par la source de rayonnement (1) en vue de former un spot de balayage (V) sur une surface à balayer (31), un système de détection de position de translation et de position angulaire destiné à détecter les positions de translation de l'objectif (3) le long, et les positions angulaires de cet objectif autour de deux axes orthogonaux (X, Y) qui s'étendent tous deux perpendiculairement au rayon principal (L) du faisceau de rayonnement (b), et un dispositif d'actionnement pour provoquer la translation et l'inclinaison de l'objectif (3) en réponse aux signaux de commande fournis par le système de détection de position de translation et de position angulaire, le système de détection de position de translation et de position angulaire comprenant un miroir (5) qui est fixé par rapport à l'objectif (3), et un système de détection sensible au rayonnement (9) qui est disposé dans le trajet du rayonnement réfléchi par le miroir (5) et qui comprend deux moyens de détection sensibles au rayonnement qui sont chacun composés de plusieurs détecteurs, caractérisé en ce que le miroir

(5) est de forme annulaire conique et est centré par rapport à l'objectif (3) et que les deux moyens sensibles au rayonnement sont espacés par un anneau intermédiaire et sont chacun divisés respectivement en quatre secteurs en forme de quadrants (13, 14, 15, 16 et 17, 18, 19, 20) présentant les mêmes angles au centre, qui reçoivent une répartition de rayonnement annulaire (21) du rayonnement réfléchi par le miroir (5), d'une manière telle que si les signaux des détecteurs (13 à 20) sont représentés par S suivi des indices correspondants, les déplacements le long de l'axe X et de l'axe Y et les mouvements de pivotement autour de ces axes peuvent être représentés par :

$$S_X = (S_{14} + S_{15} + S_{18} + S_{19}) - (S_{13} + S_{16} + S_{17} + S_{20})$$

$$S_Y = (S_{13} + S_{14} + S_{17} + S_{18}) - (S_{15} + S_{16} + S_{19} + S_{20})$$

$$S_\alpha = (S_{13} + S_{14} + S_{19} + S_{20}) - (S_{17} + S_{18} + S_{15} + S_{16})$$

$$S_\beta = (S_{14} + S_{15} + S_{17} + S_{20}) - (S_{18} + S_{19} + S_{13} + S_{16})$$

2. Dispositif de balayage optique suivant la revendication 1, caractérisé en ce que le miroir annulaire conique est un élément (5) qui est relié au porte-objectif (4) de l'objectif (3).

3. Dispositif de balayage optique suivant la revendication 1, caractérisé en ce que le miroir annulaire conique est constitué d'un bord saillant biseauté (65) d'une lentille (60) de l'objectif (3), ce bord saillant étant pourvu d'une couche réfléchissante (67).

4. Dispositif de balayage optique suivant la revendication 3, dans lequel l'objectif (3) comprend une lentille ayant la forme d'un corps transparent (60), dont la surface (62) qui est tournée vers la source de rayonnement (1) est pourvue d'une couche de matière plastique (63) présentant un profil extérieur asphérique (64), caractérisé en ce que le bord saillant (65) est constitué de la matière plastique.

5. Dispositif de balayage optique suivant la revendication 1, 2, 3 ou 4, caractérisé en ce que les détecteurs (13, 14, 15, 16, 17, 18, 19, 20) du système de détection sensible au rayonnement (9) sont annulaires.

6. Dispositif de balayage optique suivant la revendication 1, 2, 3, 4 ou 5, caractérisé en ce que le dispositif d'actionnement comprend un aimant permanent annulaire (70) qui est relié de manière fixe à l'objectif (9) et deux jeux de chaque fois au moins trois bobines d'excitation fixes (71, 72, 73, 74, 75, 76), les bobines (71, 72, 73) du premier jeu étant disposées dans un premier plan (80) transversal au rayon principal (L) du faisceau de rayonnement (b) et les bobines (74, 75, 76) du second jeu étant disposées dans un second plan (81) parallèle au premier plan (80).

7. Dispositif de balayage optique suivant l'une quelconque des revendications précédentes, caractérisé en ce qu'il est prévu un système de détection de position axiale pour la détection de la position de l'objectif (3) le long du rayon principal (L) du faisceau de rayonnement (b) et en ce que le signal fourni par le système de détection est appliqué aux bobines d'excitation (71, 72, 73; 74, 75, 76).

8. Dispositif de balayage optique suivant la revendication 7, caractérisé en ce que le système de détection de position axiale comprend un générateur



de signaux (77) destiné à fournir un premier signal de commande ( $S_w$ ) au premier jeu de bobines d'excitation (71, 72, 73) et un second signal de commande ( $S_w$ ) au second jeu de bobines d'excitation (74, 75, 76), ces signaux ayant la même amplitude et la même fréquence, mais étant en opposition de phase et forçant l'objectif (3) à s'incliner périodiquement autour d'un des deux axes (X, Y) transversaux au rayon principal (L) du faisceau de rayonnement (b) et en ce que le système de détection de position axiale comprend, en outre, les éléments du système de détection de position de translation et de position angulaire convertissant l'inclinaison périodique en un signal périodique ( $S_{\alpha'}$ ) dont l'amplitude et la phase sont représentatives de la grandeur et de la direction d'un déplacement du centre axial de l'aimant annulaire (70) hors du plan qui est situé à mi-distance entre les deux plans (80, 81) dans lesquels les bobines d'excitation (71, 72, 73; 74, 75, 76) sont disposées.

9. Appareil pour la lecture et/ou l'enregistrement d'information dans une surface d'information d'un support d'enregistrement en forme de disque rond (30) comprenant un dispositif de balayage optique suivant l'une quelconque des revendications précédentes, caractérisé en ce qu'un élément séparateur (7) est disposé entre l'objectif (3) et la source de rayonnement (1) pour séparer le rayonnement réfléchi par le miroir annulaire conique du rayonnement (b) émis par la source de rayonnement (1).

10. Appareil suivant la revendication 9, caractérisé en ce qu'un détecteur sensible au rayonnement (11) est disposé à l'intérieur du détecteur intérieur annulaire (17, 18, 19, 20) du système de détection de position de translation et de position angulaire pour convertir le rayonnement réfléchi par la surface d'information (31) en un signal électrique.

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