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APPARATUS FOR MEASURING THE THICKNESS OF THIN LAYERS

The invention relates to an apparatus according to the pre-characterizing clause of the main patent claim.

If it is desired to measure the thickness of thin layers on small articles, it is necessary to know, still more accurately, where the X-rays strike the small article, for it is certainly not intended to perform the measurement on the article as a whole. The typical size of the spot on which the measurement is performed varies between a few tenths of a millimeter, up to one millimeter. Small measurement-spots are necessary because knowledge is desired, for example, of the thickness of the layer, precisely at a specified point on the flank of a gearwheel tooth, or of the thickness of the layer in the contact region of a contact tongue, etc.

15 It is, of course, impossible to see where the X-ray beam strikes the layer.

Of one apparatus which is on the market, it is known, imprecisely, that the surface to be measured can

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somehow be observed, by means of a mirror, on the one hand, and that the mirror is then pushed away, to be replaced by the irradiating device.

The object of the invention is to indicate an apparatus which enables the measured spot to be analyzed with high precision, and in a simple manner.

This object is achieved, according to the invention, by means of the features which are evident from the characterizing clause of the main patent claim.

10 The through-bore is now visible, and this bore can be set precisely such that the center of the longitudinal geometrical axis passes through it, thus eliminating a first source of error. Furthermore, that point, on the layer, through which the longitudinal geometrical
15 axis passes, and which is the center of the measurement-spot, is visible. If the viewing microscope had two eyepieces, it would be possible to see the through-bore with one eye, and to see the layer with the other eye. However, it is also possible to work with a single eyepiece, and,
20 by shifting the optical elements in chronological succession, first to bring the through-bore into sharp focus, and then to bring the layer into sharp focus. The diaphragm device can be composed of an organic glass, or of an inorganic glass. Lead-doped organic glass is, for example,
25 available.

If silicate glass is used, the through-bores can, for example, be produced by ultrasonic machining. The cross-sectional shapes of the through-bores are congruent and always identical, and can be of any geometry which,

for example, is suited to the object to be measured.

The features of claim 2 permit the use of a glass which is widely available, and which, although an inorganic glass, is comparatively soft, and which, even in thicknesses of, for example, as little as 6 mm, does not permit the passage of enough X-ray radiation to influence the measuring effect by a significant amount, while, on the other hand, being sufficiently thin to permit viewing, in transmission, without any significant loss of light. Lead glass can also be polished to a very good finish, which is necessary in this application for a multiplicity of reasons.

The feature of claim 3 achieves essentially the same object as the feature of claim 2. However, while lead glass has a PbO content of 18 to 58%, flint glass contains, on average, a considerably higher proportion of PbO, namely 46 to 62%. This means that, for a given thickness, flint glass generally absorbs the X-ray radiation even more than lead glass, except for that proportion which passes through the through-bores.

The features of claims 4 to 6 enable the diaphragm device to be matched to the particular measurement problems, whereupon the calculations become simpler.

In tests, the geometries according to claims 7 to 9 have proved very successful, and, moreover, can be handled very well, from the technical point of view, when inorganic glasses are used.

The features of claim 10 simplify the construction, and the evaluation of the results of the measurements

also becomes easier. Moreover, the diaphragm device could, per se, also be shifted at an angle with respect to the longitudinal geometrical axis.

Once again, the features of claim 11 simplify the construction, and the required high precision can be achieved more easily. It is then possible, furthermore, to arrange the individual through-bores along a line, in the same way, if they are provided at fixed locations within the glass body.

10 The features of claim 12 endow the apparatus with small overall dimensions, despite a comparatively large number of through-bores, and the simple rotary movement can also be embodied in a precise manner, and at a cost, in technical terms, which can be justified.

15 The features of claim 13 enable the through-bores to be machined-in from the end-faces, without having to drill through the glass body, which, if not impossible, would nevertheless be very difficult.

The features of claim 14 enable the gap to be
20 allowed to run parallel to the longitudinal geometrical axis, which facilitates the manufacturing and assembly operations, as well as improving the ease with which these parts can be inspected, in addition to creating no disturbances when the layer is viewed through the monocular
25 microscope. Despite these advantages, this position of the gap does not falsify the result of the measurement.

The features of claim 15 render this gap negligibly small, both with regard to the X-rays and, moreover, with regard to the view, through the glass body, toward

the layer. In addition, the glass body then becomes a single piece which can be handled "en bloc", for when its two parts are wrung together, molecular adhesion forces most certainly occur, and it is then no longer possible to separate the two parts by hand.

In addition, the end-faces can also be welded together, by the action of heat, which is nowadays possible without altering the geometry, whereupon a glass body is obtained which is in fact a single piece.

10 As a result of the features of claim 16, the end-face of the other part-glass forms one of the boundary surfaces and is then straight in any case, to a high degree of precision. Furthermore, it is then necessary to machine the volume of the through-bore into only a single
15 part-glass, which is simpler than if, for example, half of each through-bore were to be machined into each of the two part-glasses. In the latter eventuality, the halves of the through-bore might no longer line up, following assembly, or they might possibly exhibit chips or
20 similar imperfections. This configuration is particularly suitable for cross-sectional geometries which are polygonal, such as, for example, triangles, quadrilaterals, squares, etc.

As a result of the features of claim 17, the
25 glass does not modify the color of the layer. In addition, visibility through the glass is good, and the light source can be kept less powerful.

The features of claim 18 permit viewing, through the glass body, without double-refraction, accompanied,

furthermore, by a minimal absorption loss.

The features of claim 19 ensure that the X-ray beam suffers virtually no attenuation, for organic glass has a very low order number, and the metal coating, for
5 producing the mirror effect, can be so thin that it can likewise be neglected in assessing the absorption.

The feature of claim 20 permits the production, using a known manufacturing technique, of a mirror which adds no color of its own, and which reflects very effi-
10 ciently.

In conjunction with the features of claim 20, the features of claim 21 enable the absorption to be reduced still further, since the order number of aluminum is considerably lower than that of silver.

15 In principle, the mirror could also be made, for example, of polished aluminum. However, if this polished aluminum is very thin, it could develop a wavy surface, and the mirror remains stiff if the supporting layer is composed of an organic glass.

20 As a result of the features of claim 22 influences on the X-ray beam are reduced to the absolute minimum.

The features of claim 23 also make it easy to estimate mentally, what peculiarities may be possessed by the layer, how large the measurement-spot is, the size of the
25 through-bore, etc., or to make a subjective assessment of these factors.

The feature of claim 24 results in a magnification which can be achieved by a monocular microscope without difficulty, and in the case of which the conversion cal-

ulation becomes particularly easy.

The features of claim 25 provide the possibility of positioning the longitudinal geometrical axis through the point at which the cross-hairs intersect. For an aiming device, it would, however, also be possible, per se, to use concentric circles, or wedge representations, or other similar reference marks.

In conjunction with a simple magnification factor, and graduations which are compatible with the millimeter system, the features of claim 26 permit easy calculation of the areas in question.

The features of claim 27 enable the monocular microscope arrangement to be kept simple. The monocular microscope is then focused sharply on the layer, without a collecting lens-element. The lower surface of the glass body can then be viewed, in sharp focus, using a lens-element located in the optical path. It is also possible, of course, to choose the equivalent method, focusing the monocular microscope sharply on the lower surface of the glass body, and then using a divergent lens-element in order to form a sharp image of the layer. With this latter arrangement, no operations for adjusting the sharpness are necessary, because all the distances involved - lower surface of layer/glass body/lens-element/monocular microscope - are precisely known, in advance.

In the case of substances possessing low order numbers, the probability of stimulation can be increased, by large increments, by means of the features of claim 28. If substances of this nature, possessing order numbers in the

range, for example, between 15 and 26, are considered, such as, for example, chromium or titanium, these substances exhibit an excitation energy of approximately 6 to 10 keV. If these substances are stimulated by means of high-energy X-rays, the probability of fluorescence (characteristic radiation) is much lower than when this bremsstrahlung spectrum contains more low-energy components. It is, of course, possible to stimulate the characteristic X-ray resonance, and thus the fluorescence radiation as well, only when the stimulating radiation is of higher energy than the characteristic radiation (fluorescence radiation). It is thus impossible to stimulate copper by means of 8 keV radiation, since its excitation energy is 9 keV. A stimulation voltage of 50 keV would reduce the probability considerably. The greater the voltage difference between the stimulating radiation and the stimulated radiation, the smaller is the probability of stimulation, according to a law involving, to a first approximation, the cube of the voltage difference.

20 According to the features of claim 29, the deflecting mirror of the first illustrative embodiment can still be used, this mirror being composed of glass, while despite this, low-energy X-rays can still pass through. The coating of the mirror, the means for holding it, and
25 its manufacture remain unchanged. The only effect of a hole of this nature is, on the one hand, a slight attenuation of the light, which can, on the other hand, easily be made good, while there is no reduction in the sharpness which is absolutely necessary for adjusting the apparatus.

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The features of claim 30 result in the cross-sectional area of the hole being equal to the effective cross-sectional area, meaning that a comparatively small hole can be made in the mirror. If other angles are used, the cross-section of the hole must then be enlarged, in order to ensure that the X-ray beam generator still "sees" the layer.

The dimensions according to claim 31 have proved successful in practice, and produce virtually no change in the optical properties of the mirror.

The features of claim 32 enable the generator, which is, in particular, an X-ray tube, to deliver very large amounts of low-energy radiation.

In its entirety, the invention also enables an accurate photographic record to be made of that spot on which the measurements have been performed. The same applies with regard to the shape of the through-bore, thus excluding the possibility of subsequent evaluation errors.

Two preferred illustrative embodiments of the invention are now described. In the drawing:
Figure 1 shows a perspective view of the entire apparatus,
Figure 2 shows a section, in perspective, on the plane 2-2 in Figure 1,
Figure 3 shows a diagrammatic section, perpendicular to the plane 2-2,
Figure 4 shows the plan view of a glass body,
Figure 5 shows the view according to the arrow A in Figure 4,

Figure 6 shows the view of a portion of the lower surface of a layer which is to be measured,

Figure 7 shows a diagrammatic plan view of a second type of diaphragm device,

5 Figure 8 shows a cross-section through a mirror which is a modified version of the mirror according to the second illustrative embodiment.

A measuring table 11 possesses a casing 12, of approximately rectangular, flat-sided form. In the front
10 region, an upward-pointed flange 14 projects vertically from its upper surface 13, this flange having a rectangular outline. A skirt 16 fits over this flange 14, this skirt being integral with a horizontal plate 17. In the center, the plate 17 merges into a smaller, rectangular working
15 plate 18 which projects upward, which, on its upper surface, is precisely horizontal, and which carries a network of rectangular coordinates. Equidistant ruled lines 19 run in the "X" direction, and equidistant ruled lines 21 run in the "Y" direction. An open through-hole 22 is
20 provided, extending downwards through the working plate 18 and the plate 17. An X/Y shifting drive 23 is provided, to the right of the assembly comprising the parts 16, 17 and 18, so that the working plate 18 can be moved, in the manner of a microscope stage, according to the arrows
25 24, 26. If the knurled screw 27 is turned in the directions indicated by the arrow 28, movement takes place along the double arrow 24, in accordance with the direction of rotation.

If the knurled screw 29 is turned in either of the directions indicated by the arrow 31, the working plate 18 moves in one of the directions indicated by the arrow 26. Simultaneous rotation of the knurled screws 27, 29 causes these movements to be superimposed. By this means, the through-hole 22 can be adjusted, in a precise manner, relative to a longitudinal geometrical axis 32, which stands vertically. Parts which span the through-hole 22 can be placed on the working plate 18, and these are then moved, in the same way, relative to the longitudinal geometrical axis 32. If the parts are small, and would fall through the through-hole 22, the latter can be covered with a suitable film, for example a mylar film, and the small parts are placed thereon, so that they likewise participate in the movement of the working plate 18. As before, the small parts can be viewed from the interior of the casing 12, since the film is 4 - 7 micrometers thick, and is perfectly transparent in the region of the wavelengths of the light.

For the sake of simplicity, this construction, which has been described in detail by reference to Figures 1 and 2, has been omitted from the more simple illustration in Figure 3.

The beam-generating system of an X-ray tube 33, which produces X-rays, is located in the casing 12, at the bottom. Insofar as these X-rays emerge along the longitudinal geometrical axis 32, they are permitted to pass through a through-hole 34 in a false bottom 36, this hole being coaxial with the longitudinal axis 32. All

other beams are held back by the false bottom 36, which is located above the X-ray tube 33. An extension piece 37 is seated on the false bottom 36 and, coaxially, on the through-hole 34, this extension piece 37 being composed of concentric, ring-shaped pieces of tubing. One of these ring-shaped pieces of tubing possesses a double bearing, in which a shaft 39, carrying a lead ball-plug 41, is mounted, in a manner such that its longitudinal geometrical axis intersects the longitudinal axis 32.

10 This ball-plug 41 possesses a through-bore 42, which, in the position drawn in Figure 3, is coaxial with the longitudinal axis 32, and hence allows the X-ray beam to pass through, in the upward direction. An operating lever 43 is attached to the shaft 39, externally with

15 respect to the casing 12, in a manner preventing rotation. When the operating lever 43 is in the position drawn in Figure 2, the through-bore 42 is aligned with the longitudinal axis 32, and permits the X-ray beam to pass through. In the position of the operating lever 43,

20 drawn in Figure 2' with a broken line, the shaft 39 has been rotated through 90° , according to the double arrow, and the through-bore 42 is located at rightangles to the axis 32, so that no X-rays emerge via the ball-plug 41.

As shown in Figure 2, the tubular piece 38 emerges, after

25 a reducing piece, into an upper tubular piece 44, which is coaxial with the longitudinal axis 32, is sliced-off, in its upper end region, at an angle of 45° , and there carries a mirror 46 which functions in the visible-light region. This mirror is composed of an acrylic glass

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disk 47, onto the rear of which an aluminum coating 48 has been vapor-deposited. The mirror 46 cannot move, is inclined at an angle of 45° , and the longitudinal axis 32 passes through its center. The mirror 46 is also inclined, at 45° , with respect to the longitudinal axis 32. The X-rays pass through the mirror 46, without being attenuated, and continue along the longitudinal axis 32. A diaphragm device is installed above the mirror 46, accurately horizontally and perpendicular to the longitudinal axis 32, of which device only one glass body 49 is illustrated, for the sake of simplicity. This glass body is composed of lead crystal. Its height is 6 mm, its width is 15 mm, and its length is 50 mm. It has a very high lead content. Its upper surface 51 is plane-parallel with respect to its lower surface 52, and these surfaces are perpendicular to the longitudinal axis 32. The upper surface and the lower surface, 51 and 52, are ground and polished. The glass itself is transparent, the attenuation of the visible light being negligible, and the view through the glass body 49 is not subject to distortion. The glass body 49 is composed of two flat-faced rectangular strips 53, 54. The end-face 56 of the strip 53 is wrung against the end-face 57 of the strip 54. A gap, which may under some circumstances form between the end-faces 56 and 57, has a width of less than 0.1 micrometer. Although X-rays may be able to pass through this gap, the proportion which does so is negligible.

Before the strips are wrung together, through-

bores 58, 59, 61, 62 have been ultrasonically machined into the end-face 56, these through-bores possessing, in the assembled condition, rectangular cross-sections of various sizes, and running precisely parallel to the longitudinal axis 32. Half of a through-bore 63, which has a circular cross-section, is machined into the strip 53, and its other half is machined into the strip 54. The spacing of the through-bores, 58 to 63, considerably exceeds the typical width of the X-ray beam which runs along the longitudinal axis 32 above the mirror 46. If, therefore, the longitudinal geometrical axis 32 runs through the through-bore 58, nothing passes through the through-bore 59, and the same holds good for the analogous positions.

At its periphery, the glass body 49 is seated in a holder, in a manner which is not illustrated, this holder being rigidly attached to a slide 64, which can be moved at rightangles to the longitudinal axis 32, as indicated by the double arrow 66. The slide 64 is guided on a bed 67, by means of a swallowtail. The bed 67 is rigidly attached to the casing. The slide 64 is driven by means of a micrometer drive, which is composed of a rotary knob 68, a shaft 69, a 90° angle-drive mechanism 71, and a shaft 72, the latter being connected to the slide 64. Depending on whether the rotary knob 68 is turned to the left, or to the right, the glass body 49 moves to the left, or to the right, as indicated by the double arrow which can be seen in Figure 2, and, depending on the extent to which it is rotated, one of the through-

bores, 58 to 63, can be brought into line with the longitudinal axis 32. The through-bores 58 to 63 are arranged on a line which, in fact, likewise passes through the longitudinal geometrical axis 32. The holder of the glass body 49 is rigidly attached to a Z-shaped angle-section 73, so that a perforated plate 74, which is connected to this angle-section, in a straight line, can also be moved with the glass body 49. This perforated plate 74 possesses as many lines 76 of holes as there are through-bores. A reader 77, which functions optically, is installed in a manner such that it cannot move with respect to the casing, this reader 77 possessing, on one side, lamps, and, on the other side, light-sensitive diodes. The lines 76 of holes are coded, thus permitting the reading-out of which of the through-bores, 58 to 63, is, at that particular moment, in line with the longitudinal axis 32.

Instead of the rotary knob 68, which can be operated without any further action, another embodiment incorporates a screw-head which can be operated by means of a special key, so that, once having been set, the glass body 49 cannot be repositioned without a further manipulation.

A monocular microscope arrangement 78 possesses an eyepiece 79. The associated housing contains a deflecting mirror 81, which sends the rays of light, which arrive horizontally, to the eyepiece 79, and to the eye of the observer. An objective 82 is installed in the horizontal tube portion of the monocular microscope.

arrangement 78, at the inner end of this tube portion.

If a collecting lens 83 is pushed in front of this objective 82, the lower surface 52 of the glass body 49 is seen in sharp focus. Cross-hairs 84 are also incorporated

5 into the monocular microscope arrangement 78, these cross-hairs 84 intersecting, at the point 86, in the center of the optical axis 87 of the monocular microscope arrangement 78. In its horizontal region, this optical axis 87 strikes the longitudinal geometrical axis 32.

10 Above the point at which the optical axis 87 strikes the mirror 46, the optical axis 87 runs precisely in the longitudinal geometrical axis 32. If, accordingly, the intersection point 86 of the cross-hairs 84 is located, as shown in Figure 4, at the center of the through-bore
15 61, the center of the bundle of X-rays is likewise located in the through-bore 61; and it is certain that X-rays are now passing through the entire cross-section of the through-bore 61.

The collecting lens 83 stands on a column 88,
20 which can be moved at rightangles to the optical axis 87, as indicated by the double arrow 91, in a guide 89 which is rigidly attached to the casing. In one of its positions, the collecting lens 83 is active, while it is inactive in its right-hand position according to Figure 2.

25 In its inactive position, the optical system of the monocular microscope arrangement 78 is such that the lower surface 92 of a layer 93, resting on the working plate 18, is now imaged, in sharp focus, for the eye of the observer. The distance between this layer 93 and the

glass body 49 is sufficiently large to prevent the through-bore in the glass body 49, which bore has been set, from being seen, and it is likewise no longer possible to see the end-faces 56, 57.

5 A light source 94 is employed for illuminating the lower surface 92, this light source 94 being installed, rigidly attached to the casing, and shining into the through-hole 22 from below, as shown in Figure 3.

Figure 6 now shows the cross-hairs 84 on the
10 lower surface. The intersection point 86 now indicates, once again, the position of the center of the X-ray beam. On the axes, the cross-hairs 84 have graduations 95, 90. Since the outline 96 of the through-bore 61 has previously been seen, it is also known, on observing the lower surface
15 92, that the outline of the X-ray beam accurately corresponds to the outline 96 shown in Figure 6. The dimensions of the region on which the X-rays are incident can be measured with the aid of the graduations 95, and, moreover, this region can be accurately defined.

20 The layer 93 reflects X-rays back again, which are received by a proportional-type counter tube 97, which is screened in the forward direction, with respect to the diaphragm device, by means of a screen 98.

Instead of providing the through-bores at fixed locations
25 within a glass body, it is also possible to use two diaphragm-halves, 99 and 101, which are likewise composed of a glass which is transparent to visible light, but which is opaque to X-rays. The diaphragm-half 101 is located above the diaphragm-half 99, and, in particular, with a

clearance which is small, but which is sufficient to ensure that, on being moved as indicated by the double arrows 102 and 103, the diaphragm-halves 99, 101 do not scrape against one another. On their mutually adjacent sides, the diaphragm-halves 99, 101 possess V-shaped cutouts, which appear antiparallel and are symmetrical with respect to a central plane 107. As a result of the antiparallel movement of the diaphragm halves 99, 101, the through-hole 108 now becomes larger or smaller, without the intersection point of the diagonals of the square outline of the through-hole 108 departing from the central plane 107.

In this manner, it is possible to produce regularly graded square outlines. If the V-shaped cutouts 104 and 106 are not right-angled, but are acute-angled or obtuse-angled cutouts, rhombic outlines can then be produced. If only one V-shaped cutout 104 is provided, and the cutout 106 is merely a straight end-face (180° "V" cutout), it is then possible to form triangles of different geometries, the central plane 107, through which the longitudinal geometrical axis 32 also passes, always being the principal plane.

The invention therefore achieves the object whereby merely very small masses need to be moved, and moved slowly, so that high accuracy is maintained, even over the long service life of the apparatus.

There are no stops which can wear away, no mechanical shocks, and no additional holding devices, springs, or the like.

In the case of the second illustrative embodiment, Figure 8 clearly shows that the mirror 46 is composed of a body 109 which is made of an inorganic glass, and onto which a coating 111, of silver or aluminum, has been vapor-deposited. A through-hole 112 which has a circular, cylindrical shape, is machined into the mirror 46, coaxially with the longitudinal geometrical axis 32, this hole 112 having a diameter of 1 mm. Since the mirror 46 is located at an angle of 45° with respect to the longitudinal geometrical axis 32, the through-hole 112 is, in turn, located at an angle of 45° with respect to the mirror 46. The center of the upper opening of the through-hole 112 is located at the point where the longitudinal geometrical axis 32 and the optical axis 87 intersect.

15 The through-hole 112 can also have an elliptical outline, or an polygonal outline. In order to ensure that sufficient low-energy radiation passes along the longitudinal geometrical axis 32, the X-ray tube 33 possesses a beryllium window 113.

20 Moreover, the through-hole 112 produces absolutely no scattering of the X-ray beam in this region. The second illustrative embodiment could also enable even smaller through-bores 58, 59, 61, 62, 63 to be achieved. The smallest of these bores could then even be, for
25 example, a 0.05 mm bore, which would then enable measurements to be performed even on tiny objects.



CLAIMS:—

1. Apparatus for measuring the thickness of thin layers according to the X-ray fluorescence principle, with an X-ray beam generator which emits an X-ray beam along a longitudinal geometrical axis, with a table device, as
5 the support for a layer which is to be measured, with a diaphragm device, composed essentially of a material which absorbs X-rays completely and possessing a through-aperture which can be brought along, into the longitudinal geometrical axis, with a light source for visible light
10 which can be directed onto the position for the layer which is to be measured, with a monocular microscope arrangement for viewing that region of the layer on which the X-ray beam falls, and with a deflecting mirror in the optical path between the monocular microscope arrangement
15 and the region of the layer, this measuring apparatus comprising the following features:
- a) the diaphragm device is composed of a glass which is transparent to visible light, and either possesses
20 several through-bores (58, 59, 61, 62, 63,), of different cross-sectional geometry, and can be moved in a manner such that one of the through-bores (58, 59, 61, 62, 63, 108) is, at all times, in line with the longitudinal geometrical axis (32) or has a through-bore (108) of variable size in
25 line with said axis (32),



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- b) the deflecting mirror (46) is composed of a material which, in practical terms, does not absorb X-rays, and the longitudinal geometrical axis (32) passes through it,
- 5c) the monocular microscope arrangement (78) forms sharp images of both the diaphragm device (49) and the region (92) of the layer (93),
- d) an aiming device (84) is provided in the monocular microscope arrangement, the aiming point (86) of this device intersecting the longitudinal geometrical axis (32), in the optical-path direction (87), that is to say at the point where the longitudinal geometrical axis (32) passes through the deflecting mirror (46).
- 10
- 15 2. Apparatus as claimed in claim 1, wherein the glass is lead glass.
3. Apparatus as claimed in claim 1, wherein the glass is flint glass.
4. Apparatus as claimed in claim 1, wherein the
- 20 cross-sectional geometry is rectangular, the sides being unequal.
5. Apparatus as claimed in claim 1, wherein the cross-sectional geometry is square.
6. Apparatus as claimed in claim 1, wherein the
- 25 cross-sectional geometry is circular.
7. Apparatus as claimed in claim 5, wherein the cross-sectional geometry is approximately 0.2 x 0.2 mm and/or 0.6 x 0.6 mm and/or 1.2 x 1.2 mm.
8. Apparatus as claimed in claim 4, wherein the



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cross-sectional geometry is 0.4 x 0.2 mm and/or 1 x 0.6 mm and/or 1.8 x 1.2 mm.

9. Apparatus as claimed in claim 6, wherein the cross-sectional geometry is 0.3 mm and/or 0.5 mm and/or 0.6 mm and/or 0.8 mm.

10. Apparatus as claimed in claim 1, wherein the diaphragm device (49) is guided in a manner permitting it to be shifted precisely perpendicular to the longitudinal geometrical axis (32).

10 11. Apparatus as claimed in claims 1 and 10, wherein the diaphragm device (49) is guided in a manner permitting it to be shifted in a straight line.

12. Apparatus as claimed in claims 1 and 10, wherein the diaphragm device (49) is guided in a manner permitting 15 rotation.

13. Apparatus as claimed in one or more of the preceding claims, wherein the diaphragm device (49) incorporates at least two part-glasses (53, 54), one end-face (56) of one part-glass (53) being adjacent to one end- 20 face (57) of the other part-glass (54), and wherein the through-bores (58, 59, 61, 62, 63) are machined, starting from at least one of these end-faces (56), into the part-glasses (53, 54).

14. Apparatus as claimed in claim 13, wherein the 25 end-faces (56, 57) are straight and flat-faced, and the gap present between the end-faces (56, 57) allows an amount of X-ray radiation to pass through which is smaller by at least one power of ten than the amount which can pass through the smallest through-bore (58).



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15. Apparatus as claimed in claim 14, wherein the end-faces (56, 57) are plane-polished to the extent required for wringing together.
16. Apparatus as claimed in claims 4, 5 and 14, wherein the through-bores (58, 59, 61, 62) are machined merely from the end-face (56) of one (54) of the part-glasses.
17. Apparatus as claimed in claim 1, wherein the glass is transparent to visible light, and is colorless.
- 10 18. Apparatus as claimed in claim 1, wherein the upper surface (51) and the lower surface (52) of the glass body (49), which is composed of this glass, are positioned so that they are perpendicular to the longitudinal geometric axis (32), and wherein the upper surface (51) and the lower surface (52) are polished to a mirror-finish.
- 15 19. Apparatus as claimed in claim 1, wherein the mirror (46) possesses a supporting layer (47) which is composed of an organic glass, and which is coated with a metal (48).
- 20 20. Apparatus as claimed in claim 19, wherein the metal (48) is silver.
21. Apparatus as claimed in claim 19, wherein the metal (48) is aluminum.
- 25 22. Apparatus as claimed in claim 19, wherein the coating (48) is applied by vacuum-evaporation.
23. Apparatus as claimed in claim 1, wherein the magnification factor of the monocular microscope (78) is a number which is preferred in the decimal system, exceed-



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ing 9 and less than 41. - 24 -

24. Apparatus as claimed in claim 23, wherein the number is 20.

25. Apparatus as claimed in claim 1, wherein the aiming device is a set of cross-hairs (84).

26. Apparatus as claimed in claim 25, wherein the axes of the cross-hairs (84) possess graduations (95, 97).

27. Apparatus as claimed in claim 1, wherein the monocular microscope (78) has a single eyepiece (79), and wherein a lens-element (83) can be brought into the optical path (87) of the microscope (78), according to choice.

28. Apparatus as claimed in claim 1, wherein the deflecting mirror (46) is transparent to the low-energy component of the X-ray radiation.

29. Apparatus as claimed in claim 1, wherein the deflecting mirror (46) is composed of glass, and contains a hole which is in line with the longitudinal geometrical axis (32).

30. Apparatus as claimed in claim 29, wherein the hole possesses a longitudinal geometrical axis which is positioned at 45° to the plane of the deflecting mirror (46).

31. Apparatus as claimed in claim 30, wherein the hole possesses a transverse measurement in the range 0.5 - 2 mm, preferably approximating to 1 mm.

32. Apparatus as claimed in claim 1 and one or more of claims 28 to 30, wherein the X-ray beam generator (33) has a beryllium window.



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33. Apparatus for measuring the thickness of thin layers according to the X-ray fluorescence principle, substantially as herein described with reference to the accompanying drawings.
