

Process for the manufacture of polypropylene

5 The present invention is directed to a new process for producing a propylene homopolymer as well as a new propylene homopolymer obtainable by this new process.

10 Polypropylene is used in many applications and is for instance the material of choice in the field of film capacitors as its chain lacks any kind of polar groups which orient under electrical field stress. As a result, polypropylene intrinsically possesses a low loss factor and high volume resistivity. These properties, combined with a relatively high dielectric constant and self-healing character in the capacitor as well as good mechanical properties, like high melting temperature and high stiffness, make polypropylene so valuable in this technical field. However in case a Ziegler-Natta catalyst has been employed during the manufacture of the polypropylene, typically the dielectric film made from such a polypropylene contains
15 considerable amounts of polar residues, like chlorine, aluminium, titanium, magnesium or silicon originating from the used Ziegler-Natta catalyst. These residues decrease the resistivity, i.e. increase the conductivity of the polymers, making the polymer unsuitable to be used as such in applications, where very low conductivity is needed, like in films for capacitors. Accordingly to make polypropylene commercially attractive in this technical
20 field it must be difficultly purified, typically washed in order to remove the undesired residues from the polymer material, a process which is time consuming and cost-intensive. Typically the purification of the polymer is carried out in an additional step after the last polymerisation step. Accordingly the polymer from the last polymerization step is conducted into a washing step, where the catalyst residues are dissolved out of the polymer material.
25 Washing liquid typically used comprises organic hydrocarbon solvents having polar groups, like hydroxyl groups, e.g. propanol. However due to the washing atactic and low molecular weight material which serves a lubricant during (BOPP) film processing is extracted and thus the processing properties of the polymer material are drastically deteriorated.

30 The high amount of residues is caused by several factors, wherein productivity plays a central role. In case the productivity of the used catalyst is high during the polymerization process, lower amounts of catalyst can be employed and thus the amount of undesired residues can be reduced.

35 Accordingly the object of the present invention is to provide a process which enables a skilled person to produce a propylene homopolymer with high productivity by keeping the

residue content in the propylene homopolymer low even without the need to apply a troublesome washing step. A further object is to provide a process which additionally enables a skilled artisan to produce a propylene homopolymer with broad molecular weight distribution.

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The finding of the present invention is to use a Ziegler Natta catalyst with a specifically selected internal donor and with a very balanced mol-ratio of co-catalyst (Co) to external donor (ED) [Co/ED] and of co-catalyst (Co) to transition metal (TM) [Co/TM], respectively.

- 10 Accordingly the present invention is directed to a process for the manufacture of propylene homopolymer (H-PP) in a sequential polymerization system comprising at least two polymerization reactors ((R1) and (R2)) or at least three polymerization reactors ((R1), (R2) and (R3)) connected in series, like in a sequential polymerization system consisting of two polymerization reactors (R1) and (R2) connected in series or consisting of three
- 15 polymerization reactors (R1), (R2) and (R3) connected in series, wherein the polymerization of propylene in the at least two polymerization reactors ((R1) and (R2)) or in the at least three polymerization reactors ((R1), (R2) and (R3)), like the two polymerization reactors (R1) and (R2) or the three polymerization reactors (R1), (R2) and (R3), takes place in the presence of
- 20 (a) a Ziegler-Natta catalyst (ZN-C) comprising a titanium compound (TC) having at least one titanium-halogen bond, and an internal donor (ID), both supported on a magnesium halide,
- (b) a co-catalyst (Co), and
- (c) an external donor (ED),
- 25 wherein
- (i) the internal donor (ID) comprises at least 80 wt.-% of a succinate;
- (ii) the molar-ratio of co-catalyst (Co) to external donor (ED) [Co/ED] is 10 to 45;
- (iii) the molar-ratio of co-catalyst (Co) to titanium compound (TC) [Co/TC] is 8 to 45; and
- 30 (iv) optionally the molar-ratio of external donor (ED) to titanium compound [ED/TC] is in the range of more than 0.5 to below 2.6, preferably in the range of 0.7 to 2.0.

Preferably at least one of the two polymerization reactors ((R1) and (R2)) is a gas phase reactor, more preferably one of the two polymerization reactors (R1) and (R2) is a loop reactor (LR) whereas as the other of the two polymerization reactors (R1) and (R2) is a gas phase reactor (GR1), still more preferably the first polymerization reactor (R1) is a loop reactor (LR) and the second polymerization reactor (R2) is a gas phase reactor (GPR1).
Accordingly in case the sequential polymerization system consists of two polymerization reactors (R1) and (R2) the first polymerization reactor (R1) is a loop reactor (LR) and the second polymerization reactor (R2) is a first gas phase reactor (GPR1)

10 In case the sequential polymerization system comprises, like consists of, three polymerization reactors (R1), (R2) and (R3), at least one, preferably at least two, of the three polymerization reactors ((R1), (R2) and (R2)) is/are (a) gas phase reactors, more preferably one of the three polymerization reactors (R1), (R2) and (R3) is a loop reactor (LR) whereas as the other two of the three polymerization reactors (R1), (R2) and (R3) are gas phase reactors (GR1) and
15 (GR2), still more preferably the first polymerization reactor (R1) is a loop reactor (LR), the second polymerization reactor is a first gas phase reactor (GPR1) and the third polymerization reactor (R2) is a second gas phase reactor (GPR2).

Preferably the operating temperature in the first polymerization reactor (R1) is in the range of 70 to 85 °C and/or the operating temperature in the second polymerization reactor (R2) and optional in the third reactor (R3) is in the range of 75 to 95 °C.

It has been surprisingly found out that a propylene homopolymer (H-PP) produced according to the inventive process has a low residue content. Further the productivity of the applied catalyst is very high. Additionally with the inventive process a high molecular weight distribution can be achieved.

In the following the invention will be described in more detail.

30 Polymerization process:

One requirement of the present invention is that the propylene homopolymer (H-PP) is produced in a sequential polymerization system comprising at least two reactors, preferably consists of two reactors (R1) and (R2). In another embodiment the propylene homopolymer (H-PP) is produced in a sequential polymerization system comprising at least three reactors (R1), (R2) and (R3), preferably consists of three reactors (R1), (R2) and (R3).

The term “sequential polymerization system” indicates that the propylene homopolymer (H-PP) is produced in at least two reactors connected in series. Accordingly the present polymerization system comprises at least a first polymerization reactor (R1) and a second polymerization reactor (R2), and optionally a third polymerization reactor (R3). The term “polymerization reactor” shall indicate that the main polymerization takes place. Thus in case the process consists of two polymerization reactors, this definition does not exclude the option that the overall system comprises for instance a pre-polymerization step in a pre-polymerization reactor. The term “consist of” is only a closing formulation in view of the main polymerization reactors.

Preferably at least one of the two polymerization reactors (R1) and (R2) is a gas phase reactor (GPR). Still more preferably the second polymerization reactor (R2) and the optional third polymerization reactor (R3) are gas phase reactors (GPRs), i.e a first gas phase reactor (GPR1) and a second gas phase reactor (GPR2). A gas phase reactor (GPR) according to this invention is preferably a fluidized bed reactor, a fast fluidized bed reactor or a settled bed reactor or any combination thereof.

Accordingly, the first polymerization reactor (R1) is preferably a slurry reactor (SR) and can be any continuous or simple stirred batch tank reactor or loop reactor operating in bulk or slurry. Bulk means a polymerization in a reaction medium that comprises of at least 60 % (w/w) monomer. According to the present invention the slurry reactor (SR) is preferably a (bulk) loop reactor (LR). Accordingly the average concentration of propylene homopolymer (H-PP), i.e. the first fraction (1st F) of the propylene homopolymer (H-PP) (i.e. the first propylene homopolymer fraction (H-PP1)), in the polymer slurry within the loop reactor (LR) is typically from 15 wt.-% to 55 wt.-%, based on the total weight of the polymer slurry within the loop reactor (LR). In one preferred embodiment of the present invention the

average concentration of the first propylene homopolymer fraction (H-PP1) in the polymer slurry within the loop reactor (LR) is from 20 wt.-% to 55 wt.-% and more preferably from 25 wt.-% to 52 wt.-%, based on the total weight of the polymer slurry within the loop reactor (LR).

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Preferably the propylene homopolymer of the first polymerization reactor (R1), i.e. the first propylene homopolymer fraction (H-PP1), more preferably the polymer slurry of the loop reactor (LR) containing the first propylene homopolymer fraction (H-PP1), is directly fed into the second polymerization reactor (R2), i.e. into the (first) gas phase reactor (GPR1),

10 without a flash step between the stages. This kind of direct feed is described in EP 887379 A, EP 887380 A, EP 887381 A and EP 991684 A. By "direct feed" is meant a process wherein the content of the first polymerization reactor (R1), i.e. of the loop reactor (LR), the polymer slurry comprising the the first propylene homopolymer fraction (H-PP1), is led directly to the next stage gas phase reactor.

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Alternatively, the propylene homopolymer of the first polymerization reactor (R1), i.e. the first propylene homopolymer fraction (H-PP1), more preferably polymer slurry of the loop reactor (LR) containing the first propylene homopolymer fraction (H-PP1), may be also

20 directed into a flash step or through a further concentration step before fed into the second polymerization reactor (R2), i.e. into the gas phase reactor (GPR). Accordingly, this "indirect feed" refers to a process wherein the content of the first polymerization reactor (R1), of the loop reactor (LR), i.e. the polymer slurry, is fed into the second polymerization reactor (R2), into the (first) gas phase reactor (GPR1), via a reaction medium separation unit and the reaction medium as a gas from the separation unit.

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More specifically, the second polymerization reactor (R2), and any subsequent reactor, for instance the third polymerization reactor (R3), are preferably gas phase reactors (GPRs).

Such gas phase reactors (GPR) can be any mechanically mixed or fluid bed reactors.

Preferably the gas phase reactors (GPRs) comprise a mechanically agitated fluid bed reactor
30 with gas velocities of at least 0.2 m/sec. Thus it is appreciated that the gas phase reactor is a fluidized bed type reactor preferably with a mechanical stirrer.

Thus in a preferred embodiment the first polymerization reactor (R1) is a slurry reactor (SR), like loop reactor (LR), whereas the second polymerization reactor (R2) and any optional subsequent reactor, like the third polymerization reactor (R3), are gas phase reactors (GPRs). Accordingly for the instant process at least two, preferably two polymerization reactors (R1) and (R2) or three polymerization reactors (R1), (R2) and (R3), namely a slurry reactor (SR), like loop reactor (LR) and a (first) gas phase reactor (GPR1) and optionally a second gas phase reactor (GPR2), connected in series are used. If needed prior to the slurry reactor (SR) a pre-polymerization reactor is placed.

10 The Ziegler-Natta catalyst (ZN-C) is fed into the first polymerization reactor (R1) and is transferred with the polymer (slurry) obtained in the first polymerization reactor (R1) into the subsequent reactors. If the process covers also a pre-polymerization step it is preferred that the Ziegler-Natta catalyst (ZN-C) is fed in the pre-polymerization reactor. Subsequently the pre-polymerization product containing the Ziegler-Natta catalyst (ZN-C) is transferred
15 into the first polymerization reactor (R1).

A preferred multistage process is a "loop-gas phase"-process, such as developed by Borealis A/S, Denmark (known as BORSTAR® technology) described e.g. in patent literature, such as in EP 0 887 379, WO 92/12182 WO 2004/000899, WO 2004/111095, WO 99/24478,
20 WO 99/24479 or in WO 00/68315.

A further suitable slurry-gas phase process is the Spheripol® process of Basell.

Especially good results are achieved in case the temperature in the reactors is carefully
25 chosen.

Accordingly it is preferred that the operating temperature in the first polymerization reactor (R1) is in the range of 70 to 85 °C, more preferably in the range of 75 to 85 °C, still more preferably in the range of 77 to 83 °C, like in the range of 78 to 82 °C, i.e. 80 °C.

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Alternatively or additionally to the previous paragraph it is preferred that the operating temperature in the second polymerization reactor (R2) and optional in the third reactor (R3) is in the range of 75 to 95 °C, more preferably in the range of 78 to 92 °C.

- 5 Preferably the operating temperature in the second polymerization reactor (R2) is equal or higher to the operating temperature in the first polymerization reactor (R1). Accordingly it is preferred that the operating temperature
- (a) in the first polymerization reactor (R1) is in the range of 70 to 85 °C, more preferably in the range of 75 to 85 °C, still more preferably in the range of 77 to 83 °C, like
- 10 in the range of 78 to 82 °C, i.e. 80 °C,
- and
- (b) in the second polymerization reactor (R2) is in the range of 75 to 95 °C, more preferably in the range of 78 to 92 °C, still more preferably in the range of 78 to 88 °C, with the proviso that the operating temperature in the in the second polymerization reactor
- 15 (R2) is equal or higher to the operating temperature in the first polymerization reactor (R1).

- Still more preferably the operating temperature of the third polymerization reactor (R3) – if present – is higher than the the operating temperature in the first polymerization reactor (R1). In one specific embodiment the operating temperature of the third polymerization reactor
- 20 (R3) – if present – is higher than the operating temperature in the first polymerization reactor (R1) and in the second polymerization reactor (R2). Accordingly it is preferred that the operating temperature
- (a) in the first polymerization reactor (R1) is in the range of 70 to 85 °C, more preferably in the range of 75 to 85 °C, still more preferably in the range of 77 to 83 °C, like
- 25 in the range of 78 to 82 °C, i.e. 80 °C,
- (b) in the second polymerization reactor (R2) is in the range of 75 to 95 °C, more preferably in the range of 78 to 92 °C, still more preferably in the range of 78 to 88 °C, and
- (c) in the third polymerization reactor (R3) – if present - is in the range of 75 to 95 °C,
- 30 more preferably in the range of 80 to 95 °C, still more preferably in the range of 85 to 92 °C, like in the range of 87 to 92 °C,

with the proviso that the operating temperature in the second polymerization reactor (R2) is equal or higher to the operating temperature in the first polymerization reactor (R1) and

with the proviso that the third polymerization reactor (R3) is higher than the operating
5 temperature in the first polymerization reactor (R1), preferably is higher than the operating temperature in the first polymerization reactor (R1) and in the second polymerization reactor (R2).

Typically the pressure in the first polymerization reactor (R1), preferably in the loop reactor
10 (LR), is in the range of from 20 to 80 bar, preferably 30 to 70 bar, like 35 to 65 bar, whereas the pressure in the second polymerization reactor (R2), i.e. in the (first) gas phase reactor (GPR1), and optionally in any subsequent reactor, like in the third polymerization reactor (R3), e.g. in the second gas phase reactor (GPR2), is in the range of from 5 to 50 bar, preferably 15 to 35 bar.

15 Preferably hydrogen is added in each polymerization reactor in order to control the molecular weight, i.e. the melt flow rate MFR_2 .

Accordingly it is preferred that the hydrogen to propylene feed ratio $[H_2/C_3]$ to the first
20 polymerization reactor (R1) is in the range of 2.5 to 5.0 mol/kmol, more preferably in the range of 2.8 to 4.5 mol/kmol, and/or the hydrogen to propylene feed ratio $[H_2/C_3]$ to the second polymerization reactor (R2) is in the range of 15.0 to 25.0 mol/kmol, more preferably in the range of 16.0 to 22.0 mol/kmol. In case a third polymerization reactor (R3) is present the hydrogen to propylene feed ratio $[H_2/C_3]$ to said reactor is in the range of 10.0 to 20.0
25 mol/kmol, more preferably in the range of 12.0 to 18.0 mol/kmol. It is especially preferred that the hydrogen and propylene feed are constant over the polymerization time.

Preferably the average residence time is rather long in the polymerization reactors (R1) and (R2). In general, the average residence time (τ) is defined as the ratio of the reaction volume
30 (V_R) to the volumetric outflow rate from the reactor (Q_o) (i.e. V_R/Q_o), i.e. $\tau = V_R/Q_o$ [$\tau = V_R/Q_o$]. In case of a loop reactor the reaction volume (V_R) equals to the reactor volume.

Accordingly the average residence time (τ) in the first polymerization reactor (R1) is preferably at least 20 min, more preferably in the range of 20 to 45 min, still more preferably in the range of 25 to 42 min, like in the range of 28 to 40 min, and/or the average residence time (τ) in the second polymerization reactor (R2) is preferably at least 90 min, more preferably in the range of 90 to 220 min, still more preferably in the range of 100 to 210 min, yet more preferably in the range of 105 to 200 min, like in the range of 105 to 190 min. Preferably the average residence time (τ) in the third polymerization reactor (R3) – if present – is preferably at least 30 min, more preferably in the range of 30 to 90 min, still more preferably in the range of 40 to 80 min, like in the range of 50 to 80 min.

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Further it is preferred that the average residence time (τ) in the total sequential polymerization system, more preferably that the average residence time (τ) in the first (R1) second polymerization reactors (R2) and optional third polymerization reactor (R3) together, is at least 160 min, more preferably at least 180 min, still more preferably in the range of 160 to 260 min, more preferably in the range of 180 to 240 min, still more preferably in the range of 190 to 230 min, yet more preferably in the range of 200 to 220 min.

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As mentioned above the instant process can comprises in addition to the (main) polymerization of the propylene homopolymer (H-PP) in the at least two polymerization reactors (R1, R3 and optional R3) prior thereto a pre-polymerization in a pre-polymerization reactor (PR) upstream to the first polymerization reactor (R1).

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In the pre-polymerization reactor (PR) a polypropylene (Pre-PP) is produced. The pre-polymerization is conducted in the presence of the Ziegler-Natta catalyst (ZN-C). According to this embodiment the Ziegler-Natta catalyst (ZN-C), the co-catalyst (Co), and the external donor (ED) are all introduced to the pre-polymerization step. However, this shall not exclude the option that at a later stage for instance further co-catalyst (Co) is added in the polymerization process, for instance in the first reactor (R1). In one embodiment the Ziegler-Natta catalyst (ZN-C), the co-catalyst (Co), and the external donor (ED) are only added in the pre-polymerization reactor (PR), if a pre-polymerization is applied.

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The pre-polymerization reaction is typically conducted at a temperature of 0 to 60 °C, preferably from 15 to 50 °C, and more preferably from 20 to 45 °C.

5 The pressure in the pre-polymerization reactor is not critical but must be sufficiently high to maintain the reaction mixture in liquid phase. Thus, the pressure may be from 20 to 100 bar, for example 30 to 70 bar.

In a preferred embodiment, the pre-polymerization is conducted as bulk slurry polymerization in liquid propylene, i.e. the liquid phase mainly comprises propylene, with
10 optionally inert components dissolved therein. Furthermore, according to the present invention, an ethylene feed is employed during pre-polymerization as mentioned above.

It is possible to add other components also to the pre-polymerization stage. Thus, hydrogen may be added into the pre-polymerization stage to control the molecular weight of the
15 polypropylene (Pre-PP) as is known in the art. Further, antistatic additive may be used to prevent the particles from adhering to each other or to the walls of the reactor.

The precise control of the pre-polymerization conditions and reaction parameters is within the skill of the art.
20

Due to the above defined process conditions in the pre-polymerization, preferably a mixture (MI) of the Ziegler-Natta catalyst (ZN-C) and the polypropylene (Pre-PP) produced in the pre-polymerization reactor (PR) is obtained. Preferably the Ziegler-Natta catalyst (ZN-C) is (finely) dispersed in the polypropylene (Pre-PP). In other words, the Ziegler-Natta catalyst
25 (ZN-C) particles introduced in the pre-polymerization reactor (PR) split into smaller fragments which are evenly distributed within the growing polypropylene (Pre-PP). The sizes of the introduced Ziegler-Natta catalyst (ZN-C) particles as well as of the obtained fragments are not of essential relevance for the instant invention and within the skilled knowledge.

30 As mentioned above, if a pre-polymerization is used, subsequent to said pre-polymerization, the mixture (MI) of the Ziegler-Natta catalyst (ZN-C) and the polypropylene (Pre-PP)

produced in the pre-polymerization reactor (PR) is transferred to the first reactor (R1). Typically the total amount of the polypropylene (Pre-PP) in the final propylene homopolymer (H-PP) is rather low and typically not more than 5.0 wt.-%, more preferably not more than 4.0 wt.-%, still more preferably in the range of 0.5 to 4.0 wt.-%, like in the
5 range 1.0 of to 3.0 wt.-%.

In case that pre-polymerization is not used propylene and the other ingredients such as the Ziegler-Natta catalyst (ZN-C) are directly introduced into the first polymerization reactor (R1).
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Accordingly the process according the instant invention comprises the following steps under the conditions set out above

- (a) in the first polymerization reactor (R1), i.e. in a loop reactor (LR), propylene is polymerized obtaining a first propylene homopolymer fraction (H-PP1) of the propylene
15 homopolymer (H-PP),
- (b) transferring said first propylene homopolymer fraction (H-PP1) to a second polymerization reactor (R2),
- (c) in the second polymerization reactor (R2) propylene is polymerized in the presence of the first propylene homopolymer fraction (H-PP1) obtaining a second propylene
20 homopolymer fraction (H-PP2) of the propylene homopolymer (H-PP), said first propylene homopolymer fraction (H-PP1) and said second propylene homopolymer fraction (H-PP2) form the propylene homopolymer (H-PP).

A pre-polymerization as described above can be accomplished prior to step (a).
25

Alternatively the process according the instant invention comprises the following steps under the conditions set out above

- (a) in the first polymerization reactor (R1), i.e. in a loop reactor (LR), propylene is polymerized obtaining a first propylene homopolymer fraction (H-PP1) of the propylene
30 homopolymer (H-PP),
- (b) transferring said first propylene homopolymer fraction (H-PP1) to a second polymerization reactor (R2),

- (c) in the second polymerization reactor (R2) propylene is polymerized in the presence of the first propylene homopolymer fraction (H-PP1) obtaining a second propylene homopolymer fraction (H-PP2) of the propylene homopolymer (H-PP), said first propylene homopolymer fraction (H-PP1) and said second propylene homopolymer fraction (H-PP2) form a first mixture (1st M),
- (d) transferring said first mixture (1st M) to the third polymerization reactor (R3), and
- (e) in the third polymerization reactor (R3) propylene is polymerized in the presence of the first mixture (1st M) obtaining a third propylene homopolymer fraction (H-PP3) of the propylene homopolymer (H-PP), said first mixture (1st M) and said propylene homopolymer fraction (H-PP3) form the propylene homopolymer (H-PP).

A pre-polymerization as described above can be accomplished prior to step (a).

- After step (c) and (e), respectively, the propylene homopolymer (H-PP) is preferably discharged without any washing step. Accordingly in one preferred embodiment the propylene homopolymer (H-PP) is not subjected to a washing step. In other words in a specific embodiment the propylene homopolymer (H-PP) is not subjected to a washing step and optionally converted to pellets. Accordingly it is preferred that the propylene homopolymer (H-PP) is used unwashed in application forming process, like in the process of film making, like in the process for making a biaxially oriented polypropylene film (BOPP-film).

The Ziegler-Natta Catalyst (ZN-C), the external donor (ED) and the co-catalyst (Co)

As pointed out above in the specific process for the preparation of the propylene homopolymer (H-PP) as defined above a Ziegler-Natta catalyst (ZN-C) must be used.

5 Accordingly the Ziegler-Natta catalyst (ZN-C) will be now described in more detail.

The Ziegler-Natta catalyst (ZN-C) comprises a titanium compound (TC), which has at least one titanium-halogen bond, and an internal donor (ID), both supported on magnesium halide, preferably in active form.

10

The internal donor (ID) used in the present invention comprises a succinate. The internal donor (ID) may in addition to the succinate comprise phthalate or a diether. The preferred internal donor (ID) is a succinate or a mixture of a succinate and a phthalate. It is especially preferred that the internal donor (ID) is a succinate only.

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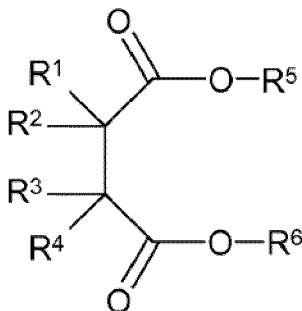
Accordingly it is preferred that the internal donor (ID) comprises succinate of at least 80 wt.-%, more preferably at least 90 wt.-%, still more preferably at least 95 wt.-% and even more preferably at least 99 wt.-%, of the total weight of the internal donor (ID). It is, however, preferred that the internal donor (ID) essentially consists, e.g. is, a succinate.

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The Ziegler-Natta catalyst comprising a succinate as defined above as internal donor (ID) can for example be obtained by reaction of an anhydrous magnesium halide with an alcohol, followed by titanation with a titanium halide and reaction with the respective succinate. Such a catalyst comprises 2 to 6 wt.-% of titanium, 10 to 20 wt.-% of magnesium and 5 to 30 wt.-% of internal donor (ID) with chlorine and solvent making up the remainder.

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Suitable succinates have the formula

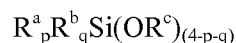


wherein R^1 to R^4 are equal to or different from one another and are hydrogen, or a C_1 to C_{20} linear or branched alkyl, alkenyl, cycloalkyl, aryl, arylalkyl or alkylaryl group, optionally containing heteroatoms, and R^1 to R^4 , being joined to the same carbon atom, can be linked together to form a cycle; and R^5 and R^6 are equal to or different from one another and are a linear or branched alkyl, alkenyl, cycloalkyl, aryl, arylalkyl or alkylaryl group, optionally containing heteroatoms.

Suitable phthalates are selected from the alkyl, cycloalkyl and aryl phthalates, such as for example diethyl phthalate, diisobutyl phthalate, di-n-butyl phthalate, dioctyl phthalate, diphenyl phthalate and benzylbutyl phthalate.

A Ziegler-Natta catalyst (ZN-C) comprising a succinate as internal donor (ID) is commercially available for example from Basell under the Avant ZN trade name. One particularly preferred Ziegler-Natta catalyst (ZN-C) is the catalyst ZN168M of Basell.

As further component in the instant polymerization process an external donor (ED) must be present. Suitable external donors (ED) include certain silanes, ethers, esters, amines, ketones, heterocyclic compounds and blends of these. It is especially preferred to use a silane. It is most preferred to use silanes of the general formula



wherein R^a , R^b and R^c denote a hydrocarbon radical, in particular an alkyl or cycloalkyl group, and wherein p and q are numbers ranging from 0 to 3 with their sum $p + q$ being equal to or less than 3. R^a , R^b and R^c can be chosen independently from one another and can be the same or different. Specific examples of such silanes are (tert-butyl)₂Si(OCH₃)₂,

(cyclohexyl)(methyl)Si(OCH₃)² (referred to as "C donor"), (phenyl)₂Si(OCH₃)₂ and (cyclopentyl)₂Si(OCH₃)₂ (referred to as "D donor").

The co-catalyst is preferably a compound of group 13 of the periodic table (IUPAC), e.g.

5 organo aluminum, such as an aluminum compound, like aluminum alkyl, aluminum halide or aluminum alkyl halide compound. Accordingly in one specific embodiment the co-catalyst (Co) is a trialkylaluminium, like triethylaluminium (TEAL), dialkyl aluminium chloride or alkyl aluminium sesquichloride. In one specific embodiment the co-catalyst (Co) is triethylaluminium (TEAL).

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Advantageously, the triethyl aluminium (TEAL) has a hydride content, expressed as AlH₃, of less than 1.0 wt% with respect to the triethyl aluminium (TEAL). More preferably, the hydride content is less than 0.5 wt%, and most preferably the hydride content is less than 0.1 wt%.

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Important aspect of the present invention is that the ratio between on the one hand of co-catalyst (Co) and the external donor (ED) [Co/ED] and on the other hand of the co-catalyst (Co) and the transition metal (TM) [Co/TM] have been carefully chosen.

20 Accordingly

(a) the mol-ratio of co-catalyst (Co) to external donor (ED) [Co/ED] must be in the range of 10 to 45, preferably is in the range of 12 to 45, more preferably is in the range of 15 to 43, still more preferably is in the range of 20 to 42; and

(b) the mol-ratio of co-catalyst (Co) to transition metal (TM) [Co/TM] must be in the
25 range of above 5 to 45, preferably is in the range of 8 to 45, more preferably is in the range of 8 to 43, still more preferably is in the range of 10 to 40, like 17 to 40.

It is especially preferred that the molar-ratio of external donor (ED) to titanium compound [ED/TC] is in the range of more than 0.5 to below 2.6, more preferably in the range of 0.7 to

30 2.0, still more preferably in the range of 0.8 to 1.8, like 0.8 to 1.5.

Therefore in one particular preferred embodiment

- (a) the mol-ratio of co-catalyst (Co) to external donor (ED) [Co/ED] must be in the range of 10 to 45, preferably is in the range of 12 to 45, more preferably is in the range of 15 to 43, still more preferably is in the range of 20 to 42;
- (b) the mol-ratio of co-catalyst (Co) to transition metal (TM) [Co/TM] must be in the range of above 8 to 45, preferably is in the range of 8 to 43, more preferably is in the range of 10 to 40, still more preferably is in the range of 17 to 40; and
- (c) the molar-ratio of external donor (ED) to titanium compound [ED/TC] is in the range of more than 0.5 to below 2.6, more preferably in the range of 0.7 to 2.0, still more preferably in the range of 0.8 to 1.8, like 0.8 to 1.5.

10

The propylene homopolymer (H-PP)

With the above described process including the specific defined Ziegler-Natta catalyst (ZN-C) a propylene homopolymer (H-PP) can be produced with high productivity. Accordingly, the propylene homopolymer (H-PP) is in particular featured by low ash content, in particular by low ash content without any purification, i.e. washing step. Accordingly the propylene homopolymer (H-PP) has an ash content of below 30 ppm, i.e. in the range of 8 to below 30 ppm, preferably of below 26 ppm, i.e. 10 to below 26 ppm, more preferably of below 25 ppm, i.e. in the range of 13 to below 25 ppm.

20

Additionally it is preferred that the magnesium content of the propylene homopolymer (H-PP) is at most 5.0 ppm, preferably at most 4.0 ppm, more preferably at most 3.5 ppm, still more preferably in the range of 0.5 to 3.5 ppm, yet more preferably in the range of 1.0 to 2.5 ppm.

25

Further it is preferred that the propylene homopolymer (H-PP) comprises at most 30 ppm of aluminum, preferably at most 15 ppm, more preferably in the range of 1.0 to 15 ppm, still more preferably in the range of 2.0 to 10 ppm, yet more preferably in the range of 3.0 to 8.0 ppm.

30

The propylene homopolymer (H-PP) of the present invention preferably comprises at most 10 ppm of chlorine, more preferably at most 6 ppm, still more preferably at most 5 ppm.

It is preferred that the propylene homopolymer (H-PP) according to this invention is featured by rather high cold xylene soluble (XCS) content, i.e. by a xylene cold soluble (XCS) of at least 2.5, like at least 2.8 wt.-%. Accordingly the propylene homopolymer (H-PP) has
5 preferably a xylene cold soluble content (XCS) in the range of 2.5 to 5.0 wt.-%, more preferably in the range of 2.8 to 4.5 wt.-%, still more preferably in the range of 2.9 to 3.8 wt.-%.

Accordingly the propylene homopolymer (H-PP) is preferably a crystalline. The term
10 "crystalline" indicates that the propylene homopolymer (H-PP) has a rather high melting temperature. Accordingly throughout the invention the propylene homopolymer (H-PP) is regarded as crystalline unless otherwise indicated. Therefore the propylene homopolymer (H-PP) has a melting temperature of more than 158 °C, i.e. of more than 158 to 168, more preferably of more than 160 °C, i.e. of more than 160 to 168 °C, still more preferably in the
15 range of 162 to 165 °C.

Preferably the propylene homopolymer (H-PP) is isotactic. Accordingly it is preferred that the propylene homopolymer (H-PP) has a rather high pentad concentration (mmmm%) i.e. more than 92.0 %, more preferably more than 93.5 %, like more than 93.5 to 97.0 %, still
20 more preferably at least 94.0 %, like in the range of 94.0 to 96.0 %.

A further characteristic of the propylene homopolymer (H-PP) is the low amount of misinsertions of propylene within the polymer chain, which indicates that the propylene homopolymer (H-PP) is produced in the presence of a catalyst as defined above, i.e. in the
25 presence of a Ziegler-Natta catalyst (ZN-C). Accordingly the propylene homopolymer (H-PP) is preferably featured by low amount of 2,1 erythro regio-defects, i.e. of equal or below 0.4 mol.-%, more preferably of equal or below than 0.2 mol.-%, like of not more than 0.1 mol.-%, determined by ¹³C-NMR spectroscopy. In an especially preferred embodiment no 2,1 erythro regio-defects are detectable.

30

Due to the low amounts of regio-defects the propylene homopolymer (H-PP) is additionally characterized by a high content of thick lamella. The specific combination of rather high

mmmm pentad concentration and low amount of regio-defects has also impact on the crystallization behaviour of the propylene homopolymer (H-PP). Thus, the propylene homopolymer (H-PP) of the instant invention is featured by long crystallisable sequences and thus by a rather high amount of thick lamellae. To identify such thick lamellae the
5 stepwise isothermal segregation technique (SIST) is the method of choice. Therefore, the propylene homopolymer (H-PP) can be additionally or alternatively defined by the weight ratio of the crystalline fractions melting in the temperature range of above 160 to 180 °C to the crystalline fractions melting in the temperature range of 90 to 160 [$(< 160-180) / (90-160)$], which is at least 1.20, more preferably in the range of 1.25 to 2.00, still more
10 preferably in the range of 1.30 to 1.80, wherein said fractions are determined by the stepwise isothermal segregation technique (SIST).

In one preferred embodiment of the present invention the propylene homopolymer (H-PP) has an MFR₂ (230 °C) of equal or below 10.0 g/10 min, more preferably in the range of 1.5
15 to 10.0 g/10min, yet more preferably in the range of 2.0 to 8.0 g/10min, still more preferably in the range of 2.5 to 6.0 g/10min.

Alternatively or additionally the propylene homopolymer (H-PP) is defined by its molecular weight distribution (Mw/Mn). Thus it is preferred that the propylene homopolymer (H-PP)
20 has a molecular weight distribution (Mw/Mn) of more than 9.0, more preferably of at least 10.0, still more preferably in the range of more than 9.0 to 15.0, yet more preferably in the range of at least 10.0 to 14.0, like in the range of 10.0 to 14.0 or in the range of 11.0 to 13.5.

According to the present invention the expression “polypropylene homopolymer (H-PP)”
25 relates to a polypropylene that consists substantially, i.e. of at least 99.0 wt.-%, more preferably of at least 99.5 wt.-%, of propylene units. In another embodiment no ethylene in the propylene homopolymer (H-PP) is detectable.

As mentioned in the section “polymerization process” the propylene homopolymer (H-PP) is
30 produced in at least two polymerization reactors (R1) and (R2), like in at least three polymerization reactors (R1), (R2) and (R3). Thus in one preferred embodiment the propylene homopolymer (H-PP) is produced in two polymerization reactors (R1) and (R2).

In another preferred embodiment the propylene homopolymer (H-PP) is produced in three polymerization reactors (R1); (R2) and (R3). Accordingly the propylene homopolymer (H-PP) comprises, preferably consists of, two fractions, namely a first propylene homopolymer fraction (H-PP1) and a second propylene homopolymer fraction (H-PP2). In another
5 embodiment the the propylene homopolymer (H-PP) comprises, preferably consists of, three fractions, namely a first propylene homopolymer fraction (H-PP1), a second propylene homopolymer fraction (H-PP2) and a third propylene homopolymer fraction (H-PP3).

Preferably the weight ratio between the first propylene homopolymer fraction (H-PP1) and
10 the second propylene homopolymer fraction (H-PP2) [(H-PP1):(H-PP2)] is 70:30 to 35:65, more preferably 60:40 to 40:60.

Preferably the weight ratio between the second propylene homopolymer fraction (H-PP2) and the third propylene homopolymer fraction (H-PP3) [(H-PP2):(H-PP3)] is 80:20 to 40:60,
15 more preferably 75:25 to 45:55.

In case the propylene homopolymer (H-PP) consists of the first propylene homopolymer fraction (H-PP1) and the second propylene homopolymer fraction (H-PP2), it is preferred that the weight ratio between the first propylene homopolymer fraction (H-PP1) and the
20 second propylene homopolymer fraction (H-PP2) [(H-PP1):(H-PP2)] is 70:30 to 40:60, more preferably 60:40 to 45:55, yet more preferably 55:45 to 50:50.

In case the propylene homopolymer (H-PP) consists of the first propylene homopolymer fraction (H-PP1), the second propylene homopolymer fraction (H-PP2) and the third
25 propylene homopolymer fraction (H-PP3), it is preferred that the weight ratio between the first propylene homopolymer fraction (H-PP1) and the second propylene homopolymer fraction (H-PP2) is 60:40 to 35:65, more preferably 55:45 to 40:60, yet more preferably 50:50 to 42:58 and the weight ratio between the second propylene homopolymer fraction (H-PP2) and the third propylene homopolymer fraction (H-PP3) [(H-PP2):(H-PP3)] is 80:20 to
30 40:60, more preferably 75:25 to 45:55., still more preferably 72:28 to 50:50.

Preferably the first propylene homopolymer fraction (H-PP1) has the same or lower melt flow rate MFR_2 (230 °C) than the second propylene homopolymer fraction (H-PP2).

Preferably the first propylene homopolymer fraction (H-PP1) has a lower melt flow rate MFR_2 (230 °C) than the second propylene homopolymer fraction (H-PP2). In case a third
5 propylene homopolymer fraction (H-PP3) is present, said fraction preferably has the same or higher melt flow rate MFR_2 (230 °C) than the second propylene homopolymer fraction (H-PP2).

Thus it is preferred that the first propylene homopolymer fraction (H-PP1) and the second
10 propylene homopolymer fraction (H-PP2) fulfill together the inequation (I), more preferably inequation (Ia),

$$4.0 \geq \frac{MFR(H-PP2)}{MFR(H-PP1)} \geq 1.0 \quad (I)$$

$$3.0 \geq \frac{MFR(H-PP2)}{MFR(H-PP1)} \geq 1.1 \quad (Ia)$$

wherein

15 $MFR(H-PP1)$ is the melt flow rate MFR_2 (230 °C) [g/10min] of the first propylene homopolymer fraction (H-PP1),

$MFR(H-PP2)$ is the melt flow rate MFR_2 (230 °C) [g/10min] of the second propylene homopolymer fraction (H-PP2).

20 The inequations (I) and (Ia) are in particular applicable in case the propylene homopolymer (H-PP) consists of the first propylene homopolymer fraction (H-PP1) and the second propylene homopolymer fraction (H-PP2).

Additionally it is preferred that the second propylene homopolymer fraction (H-PP2) and the
25 third propylene homopolymer fraction (H-PP3) fulfill together the inequation (II), more preferably inequation (IIa),

$$2.0 \geq \frac{MFR(H-PP3)}{MFR(H-PP2)} \geq 0.5 \quad (II)$$

$$1.7 \geq \frac{MFR(H-PP3)}{MFR(H-PP2)} \geq 0.7 \quad (IIa)$$

wherein

30 $MFR(H-PP2)$ is the melt flow rate MFR_2 (230 °C) [g/10min] of the second propylene homopolymer fraction (H-PP2),

MFR (H-PP3) is the melt flow rate MFR₂ (230 °C) [g/10min] of the third propylene homopolymer fraction (H-PP3).

5 The inequations (II) and (IIa) are in particular applicable in case the propylene homopolymer (H-PP) consists of the first propylene homopolymer fraction (H-PP1), the second propylene homopolymer fraction (H-PP2) and the third propylene homopolymer fraction (H-PP3).

10 Additionally or alternatively it is preferred that the first propylene homopolymer fraction (H-PP1) and the propylene homopolymer (H-PP) fulfill together the inequation (III), more preferably inequation (IIIa), still more preferably inequation (IIIb),

$$3.0 \geq \frac{MFR(H-PP)}{MFR(H-PP1)} \geq 1.0 \quad (III)$$

$$2.0 \geq \frac{MFR(H-PP)}{MFR(H-PP1)} \geq 1.1 \quad (IIIa)$$

$$1.8 \geq \frac{MFR(H-PP)}{MFR(H-PP1)} \geq 1.2 \quad (IIIb)$$

wherein

15 MFR (H-PP1) is the melt flow rate MFR₂ (230 °C) [g/10min] of the first propylene homopolymer fraction (H-PP1),

MFR (H-PP) is the melt flow rate MFR₂ (230 °C) [g/10min] of the propylene homopolymer (H-PP).

20 Preferably the first propylene homopolymer fraction (H-PP1) has a melt flow rate MFR₂ (230 °C) in the range of in the range of 1.5 to 8.0 g/10min, more preferably in the range 2.0 to 6.0 g/10min, still more preferably in the range of 2.0 to 5.0 g/10min.

25 Preferably the second propylene homopolymer fraction (H-PP2) has a melt flow rate MFR₂ (230 °C) in the range of in the range of 1.5 to 11.5 g/10min, more preferably in the range of more than 2.0 to 10.0 g/10min, more preferably in the range of 2.4 to 9.0 g/10min.

30 Preferably the third propylene homopolymer fraction (H-PP3) – if present – has a melt flow rate MFR₂ (230 °C) in the range of in the range of 1.5 to 11.5 g/10min, more preferably in the range of more than 2.0 to 8.0 g/10min, more preferably in the range of 2.4 to 7.0 g/10min.

Preferably the first propylene homopolymer fraction (H-PP1) is produced in the first polymerization reactor (R1) whereas the second propylene homopolymer fraction (H-PP2) is produced in the second polymerization reactor (R2). The third propylene homopolymer fraction (H-PP3) – if present – is preferably produced in the third polymerization reactor (R3).

The propylene homopolymer (H-PP) as defined in the instant invention may contain up to 5.0 wt.-% additives, like nucleating agents and antioxidants, as well as slip agents and antiblocking agents. Preferably the additive content is below 3.0 wt.-%, like below 1.0 wt.-%.

In a specific embodiment the present invention is directed to a propylene homopolymer (H-PP) having

- (a) a melt flow rate MFR_2 (230 °C) measured according to ISO 1133 in the range of 1.5 to 10.0 g/10min, preferably in the range of 2.0 to 8.0 g/10min, more preferably in the range of 2.5 to 6.0 g/10min;
- (b) a molecular weight distribution (MWD) of more than 9.0, preferably of at least 10.0, still more preferably in the range of more than 9.0 to 15.0, yet more preferably in the range of at least 10.0 to 14.0, like in the range of 11.0 to 13.5;
- (c) a xylene cold soluble content (XCS) determined according ISO 16152 (25 °C) of at least 2.8 wt.-%, preferably in the range of 2.5 to 5.0 wt.-%, more preferably in the range of 2.5 to 4.5 wt.-%, still more preferably in the range of 2.9 to 3.8 wt.-%.
- (d) a pentad isotacticity (mmmm) of more than 93.5 mol.-%, preferably in the range of more than 93.5 to 97.0 mol.-%, more preferably of at least 94.0 %, still more preferably in the range of 94.0 to 96.0 %; and
- (e) an ash content below 30 ppm, preferably below 25 ppm, more preferably in the range of 8 to below 30 ppm, still more preferably in the range of 10 to below 26 ppm, yet more preferably in the range of 13 to below 25 ppm.

Preferably the propylene homopolymer (H-PP) of the previous paragraph has a first propylene homopolymer fraction (H-PP1) and a second propylene homopolymer fraction (H-PP2), wherein optionally further

- (a) the first propylene homopolymer fraction (H-PP1) and the second propylene homopolymer fraction (H-PP2) fulfill together the inequation (I), preferably inequation (Ia),

$$4.0 \geq \frac{MFR(H-PP2)}{MFR(H-PP1)} \geq 1.0 \quad (I)$$

$$3.0 \geq \frac{MFR(H-PP2)}{MFR(H-PP1)} \geq 1.1 \quad (Ia)$$

wherein

- MFR (H-PP1) is the melt flow rate MFR₂ (230 °C) [g/10min] of the first propylene homopolymer fraction (H-PP1),

MFR (H-PP2) is the melt flow rate MFR₂ (230 °C) [g/10min] of the second propylene homopolymer fraction (H-PP2);

and/or

- (b) the first propylene homopolymer fraction (H-PP1) and the propylene homopolymer (H-PP) fulfill together the inequation (III), preferably inequation (IIIa), more preferably preferably inequation (IIIb),

$$3.0 \geq \frac{MFR(H-PP)}{MFR(H-PP1)} \geq 1.0 \quad (III)$$

$$2.0 \geq \frac{MFR(H-PP)}{MFR(H-PP1)} \geq 1.1 \quad (IIIa)$$

$$1.8 \geq \frac{MFR(H-PP)}{MFR(H-PP1)} \geq 1.2 \quad (IIIb)$$

- wherein

MFR (H-PP1) is the melt flow rate MFR₂ (230 °C) [g/10min] of the first propylene homopolymer fraction (H-PP1),

MFR (H-PP) is the melt flow rate MFR₂ (230 °C) [g/10min] of the propylene homopolymer (H-PP);

- and/or,

- (c) the weight ratio between the first propylene homopolymer fraction (H-PP1) and the second propylene homopolymer fraction (H-PP2) [(H-PP1):(H-PP2)] is 70:30 to 40:60, preferably 60:40 to 45:55, more preferably 55:45 to 50:50.

In another preferred embodiment of the propylene homopolymer (H-PP) described two paragraphs above, said propylene homopolymer (H-PP) has a first propylene homopolymer fraction (H-PP1) and a second propylene homopolymer fraction (H-PP2) and a third propylene homopolymer fraction (H-PP3), wherein optionally further

- 5 (a) the first propylene homopolymer fraction (H-PP1) and the second propylene homopolymer fraction (H-PP2) fulfill together the inequation (I), preferably inequation (Ia),

$$4.0 \geq \frac{MFR(H-PP2)}{MFR(H-PP1)} \geq 1.0 \quad (I)$$

$$3.0 \geq \frac{MFR(H-PP2)}{MFR(H-PP1)} \geq 1.1 \quad (Ia)$$

wherein

- 10 MFR (H-PP1) is the melt flow rate MFR₂ (230 °C) [g/10min] of the first propylene homopolymer fraction (H-PP1),

MFR (H-PP2) is the melt flow rate MFR₂ (230 °C) [g/10min] of the second propylene homopolymer fraction (H-PP2);

- (b) the second propylene homopolymer fraction (H-PP2) and the third propylene
15 homopolymer fraction (H-PP3) fulfill together the inequation (II), preferably inequation (IIa),

$$2.0 \geq \frac{MFR(H-PP3)}{MFR(H-PP2)} \geq 0.5 \quad (II)$$

$$1.7 \geq \frac{MFR(H-PP3)}{MFR(H-PP2)} \geq 0.7 \quad (IIa)$$

wherein

- MFR (H-PP2) is the melt flow rate MFR₂ (230 °C) [g/10min] of the second propylene
20 homopolymer fraction (H-PP2),

MFR (H-PP3) is the melt flow rate MFR₂ (230 °C) [g/10min] of the third propylene homopolymer fraction (H-PP3),

and/or

- (c) the first propylene homopolymer fraction (H-PP1) and the propylene homopolymer
25 (H-PP) fulfill together the inequation (III), preferably inequation (IIIa), more preferably preferably inequation (IIIb),

$$3.0 \geq \frac{MFR(H-PP)}{MFR(H-PP1)} \geq 1.0 \quad (III)$$

$$2.0 \geq \frac{MFR(H-PP)}{MFR(H-PP1)} \geq 1.1 \quad (IIIa)$$

$$1.8 \geq \frac{MFR(H-PP)}{MFR(H-PP1)} \geq 1.2 \quad (IIIb)$$

wherein

MFR (H-PP1) is the melt flow rate MFR_2 (230 °C) [g/10min] of the first propylene homopolymer fraction (H-PP1),

MFR (H-PP) is the melt flow rate MFR_2 (230 °C) [g/10min] of the propylene

5 homopolymer (H-PP);

and/or,

(d) the weight ratio between the first propylene homopolymer fraction (H-PP1) and the second propylene homopolymer fraction (H-PP2) is 60:40 to 35:65, more preferably 55:45 to 40:60, yet more preferably 50:50 to 42:58 and the weight ratio between the second propylene

10 homopolymer fraction (H-PP2) and the third propylene homopolymer fraction (H-PP3) [(H-PP2):(H-PP3)] is 80:20 to 40:60, more preferably 75:25 to 45:55., still more preferably 72:28 to 50:50.

Concerning 2,1 erythro regio-defects, melting temperature T_m and crystalline fractions of

15 the preferred propylene homopolymer (H-PP) of the present invention reference is made to the information provided above.

Further, all preferred embodiments of the described propylene homopolymer (H-PP) are also preferred products of the defined process of the instant invention.

20

Biaxially oriented film / Capacitor film

The propylene homopolymer (H-PP) as defined can be subjected to a film forming process obtaining thereby a capacitor film. Preferably the propylene homopolymer (H-PP) is the only polymer within the capacitor film. Accordingly the capacitor film may contain additives but preferably no other polymer. Thus the remaining part up to 100.0 wt.-% may be accomplished by additives known in the art, like antioxidants. However this remaining part shall be not more than 5.0 wt.-%, preferably not more than 2.0 wt.-%, like not more than 1.0 wt.-%, within the capacitor film. Accordingly the capacitor film preferably comprises more than 95.0 wt.-%, more preferably more 98.0 wt.-%, like more than 99.0 wt.-%, e.g. consists, of the propylene homopolymer (H-PP) as defined herein.

The thickness of the capacitor film can be up to 15.0 μm , however, typically the capacitor film has a thickness of not more than 12.0 μm , preferably not more than 10.0 μm , more preferably not more than 8.0 μm , yet more preferably in the range of 2.5 to 10 μm , like in the range of 3.0 to 8.0 μm .

Further it is preferred that the capacitor film is a biaxially oriented film, i.e. the propylene homopolymer (H-PP), as defined above or any mixtures (blends) comprising the propylene homopolymer (H-PP), has/have been subjected to a drawing process obtaining thereby a biaxially oriented polymer. As indicated above capacitor film preferably contains the propylene homopolymer (H-PP) as only polymer and thus it is preferably a biaxially oriented polypropylene (BOPP) made from said propylene homopolymer (H-PP).

Preferably the capacitor film, i.e. the biaxially oriented polypropylene (BOPP), has a draw ratio in machine direction of at least 3.0 and a draw ratio in transverse direction of at least 3.0. Such ratios are appreciated as commercial biaxially oriented polypropylene films must be stretchable at least to the above defined extent without breaking. The length of the sample increases during stretching in longitudinal direction and the draw ratio in longitudinal direction calculates from the ratio of current length over original sample length. Subsequently, the sample is stretched in transverse direction where the width of the sample is increasing. Hence, the draw ratio calculates from the current width of the sample over the

original width of the sample. Preferably the draw ratio in machine direction of the capacitor film, i.e. of the biaxially oriented polypropylene (BOPP), ranges from 3.5 to 8.0, more preferably from 4.5 to 6.5. The draw ratio in transverse direction of the capacitor film, i.e. of the biaxially polypropylene (BOPP), ranges preferably from 4.0 to 15.0, more preferably
5 from 6.0 to 10.0. Temperature range during stretching is in general 100 °C to 180 °C.

As the capacitor film, i.e. the biaxially oriented polypropylene (BOPP), preferably is produced from the propylene homopolymer (H-PP) as defined above, the properties given for the propylene homopolymer (H-PP) are equally applicable for the capacitor film if not
10 specified differently.

Preferably the propylene homopolymer (H-PP) is biaxially oriented.

After the preparation of the propylene homopolymer (H-PP) said polymer is subjected to a
15 film forming process. Any film forming processes which are suitable for the manufacture of a capacitor film can be used.

In a preferred embodiment the propylene homopolymer (H-PP) is not subjected to a washing step prior to the film forming process.

20

The capacitor film, i.e. the biaxially oriented polypropylene (BOPP), can be prepared by conventional drawing processes known in the art. Accordingly the process for the manufacture of a capacitor film, i.e. the biaxially oriented polypropylene (BOPP), according to this invention comprises the use of the propylene homopolymer (H-PP) as defined herein
25 and it's forming into a film preferably by the tenter method known in the art.

The tenter method is in particular a method in which the propylene homopolymer (H-PP) as defined herein is melt extruded from a slit die such as a T-die and cooled on a cooling drum obtaining an undrawn sheet. Said sheet is pre-heated for example with a heated metal roll
30 and then drawn in the length direction between a plurality of rolls over which a difference in peripheral speeds is established and then both edges are gripped with grippers and the sheet is drawn in the transverse direction in an oven by means of a tenter resulting in a biaxially

drawn film. The temperature of said stretched sheet during the longitudinal drawing is preferably controlled in such a way as to be within the temperature range of the melting point of the polypropylene as defined herein (machine direction: -20 to -10°C; transverse direction: -5 to +10°C). The uniformity of the film thickness on transverse drawing can be
5 evaluated with the method in which a fixed region on the film is masked after drawing in the length direction and measuring the actual drawing factor by measuring the spacing of the said masking after transverse drawing.

Subsequently, the capacitor film, i.e. the biaxially oriented film (BOPP), can be treated by
10 corona discharge in air, nitrogen, carbon dioxide gas or any of the mixtures on the surface to be metalized, to improve the adhesive strength to the metal to be deposited, and wound by a winder.

In the following the present invention is further illustrated by means of examples.
15

EXAMPLES

A. Measuring methods

The following definitions of terms and determination methods apply for the above general description of the invention including the claims as well as to the below examples unless
20 otherwise defined.

Quantification of microstructure by NMR spectroscopy

Quantitative nuclear-magnetic resonance (NMR) spectroscopy was used to quantify the isotacticity and regio-regularity of the polypropylene homopolymers.

Quantitative $^{13}\text{C}\{^1\text{H}\}$ NMR spectra were recorded in the solution-state using a Bruker
25 Advance III 400 NMR spectrometer operating at 400.15 and 100.62 MHz for ^1H and ^{13}C respectively. All spectra were recorded using a ^{13}C optimised 10 mm extended temperature probehead at 125°C using nitrogen gas for all pneumatics.

For polypropylene homopolymers approximately 200 mg of material was dissolved in 1,2-tetrachloroethane- d_2 (TCE- d_2). To ensure a homogenous solution, after initial sample
30 preparation in a heat block, the NMR tube was further heated in a rotatory oven for at least 1 hour. Upon insertion into the magnet the tube was spun at 10 Hz. This setup was chosen primarily for the high resolution needed for tacticity distribution quantification (Busico, V.,

- Cipullo, R., Prog. Polym. Sci. 26 (2001) 443; Busico, V.; Cipullo, R., Monaco, G., Vacatello, M., Segre, A.L., Macromolecules 30 (1997) 6251). Standard single-pulse excitation was employed utilising the NOE and bi-level WALTZ16 decoupling scheme (Zhou, Z., Kuemmerle, R., Qiu, X., Redwine, D., Cong, R., Taha, A., Baugh, D. Winniford, B., J. Mag. Reson. 187 (2007) 225; Busico, V., Carbonniere, P., Cipullo, R., Pellecchia, R., Severn, J., Talarico, G., Macromol. Rapid Commun. 2007, 28, 11289). A total of 8192 (8k) transients were acquired per spectra.
- Quantitative $^{13}\text{C}\{^1\text{H}\}$ NMR spectra were processed, integrated and relevant quantitative properties determined from the integrals using proprietary computer programs.
- 10 For polypropylene homopolymers all chemical shifts are internally referenced to the methyl isotactic pentad (mmmm) at 21.85 ppm.
- Characteristic signals corresponding to regio defects (Resconi, L., Cavallo, L., Fait, A., Piemontesi, F., Chem. Rev. 2000, 100, 1253;; Wang, W-J., Zhu, S., Macromolecules 33 (2000), 1157; Cheng, H. N., Macromolecules 17 (1984), 1950) or comonomer were
- 15 observed.
- The tacticity distribution was quantified through integration of the methyl region between 23.6-19.7 ppm correcting for any sites not related to the stereo sequences of interest (Busico, V., Cipullo, R., Prog. Polym. Sci. 26 (2001) 443; Busico, V., Cipullo, R., Monaco, G., Vacatello, M., Segre, A.L., Macromolecules 30 (1997) 6251).
- 20 Specifically the influence of regio-defects and comonomer on the quantification of the tacticity distribution was corrected for by subtraction of representative regio-defect and comonomer integrals from the specific integral regions of the stereo sequences.
- The isotacticity was determined at the pentad level and reported as the percentage of isotactic pentad (mmmm) sequences with respect to all pentad sequences:
- 25 $[\text{mmmm}] \% = 100 * (\text{mmmm} / \text{sum of all pentads})$
- The presence of 2,1 erythro regio-defects was indicated by the presence of the two methyl sites at 17.7 and 17.2 ppm and confirmed by other characteristic sites. Characteristic signals corresponding to other types of regio-defects were not observed (Resconi, L., Cavallo, L., Fait, A., Piemontesi, F., Chem. Rev. 2000, 100, 1253).
- 30 The amount of 2,1 erythro regio-defects was quantified using the average integral of the two characteristic methyl sites at 17.7 and 17.2 ppm:
- $$P_{21e} = (I_{e6} + I_{e8}) / 2$$

The amount of 1,2 primary inserted propene was quantified based on the methyl region with correction undertaken for sites included in this region not related to primary insertion and for primary insertion sites excluded from this region:

$$P_{12} = I_{CH3} + P_{12e}$$

- 5 The total amount of propene was quantified as the sum of primary inserted propene and all other present regio-defects:

$$P_{total} = P_{12} + P_{21e}$$

The mole percent of 2,1 erythro regio-defects was quantified with respect to all propene:

$$[21e] \text{ mol.-%} = 100 * (P_{21e} / P_{total})$$

- 10 **Calculation** of melt flow rate MFR_2 (230 °C) of the second propylene homopolymer fraction (H-PP2):

$$MFR(PP2) = 10^{\left[\frac{\log(MFR(PP)) - w(PP1) \times \log(MFR(PP1))}{w(PP2)} \right]} \quad (I)$$

wherein

w(PP1) is the weight fraction [in wt.-%] of the first propylene homopolymer fraction (H-PP1),

- 15 w(PP2) is the weight fraction [in wt.-%] of the second propylene homopolymer fraction (H-PP2),

MFR(PP1) is the melt flow rate MFR_2 (230 °C) [in g/10min] of the first propylene homopolymer fraction (H-PP1),

- 20 MFR(PP) is the melt flow rate MFR_2 (230 °C) [in g/10min] of the propylene homopolymer (H-PP),

MFR(PP2) is the calculated melt flow rate MFR_2 (230 °C) [in g/10min] of the second propylene homopolymer fraction (H-PP2).

Calculation of melt flow rate MFR_2 (230 °C) of the third propylene homopolymer fraction (H-PP3):

$$MFR(PP3) = 10^{\left[\frac{\log(MFR(PP)) - w(PP2) \times \log(MFR(PP2))}{w(PP3)} \right]} \quad (II)$$

- 25 wherein

w(PP2) is the weight fraction [in wt.-%] of the propylene homopolymer fractions (H-PP1) and (H-PP2) together,

w(PP3) is the weight fraction [in wt.-%] of the third propylene homopolymer fraction (H-PP3),

MFR(PP2) is the melt flow rate MFR₂ (230 °C) [in g/10min] of the mixture of the propylene homopolymer fractions (H-PP1) and (H-PP2) together, i.e. in the second polymerization reactor (R2)

5 MFR(PP) is the melt flow rate MFR₂ (230 °C) [in g/10min] of the propylene homopolymer (H-PP),

MFR(PP3) is the calculated melt flow rate MFR₂ (230 °C) [in g/10min] of the third propylene homopolymer fraction (H-PP3).

MFR₂ (230 °C) is measured according to ISO 1133 (230 °C, 2.16 kg load)

10 **Number average molecular weight (M_n), weight average molecular weight (M_w) and molecular weight distribution (MWD)**

Molecular weight averages (M_w, M_n), Molecular weight distribution (MWD) and its broadness, described by M_w/M_n (wherein M_n is the number average molecular weight and M_w is the weight average molecular weight) were determined by Gel Permeation Chromatography (GPC) according to ISO 16014-4:2003 and ASTM D 6474-99. A

15 PolymerChar GPC instrument, equipped with infrared (IR) detector was used with 3 x Olexis and 1x Olexis Guard columns from Polymer Laboratories and 1,2,4-trichlorobenzene (TCB, stabilized with 250 mg/L 2,6-Di tert butyl-4-methyl-phenol) as solvent at 160 °C and at a constant flow rate of 1 mL/min. 200 µL of sample solution were injected per analysis. The column set was calibrated using universal calibration (according to ISO 16014-2:2003) with
20 at least 15 narrow MWD polystyrene (PS) standards in the range of 0,5 kg/mol to 11 500 kg/mol. Mark Houwink constants for PS, PE and PP used are as described per ASTM D 6474-99. All samples were prepared by dissolving 5.0 – 9.0 mg of polymer in 8 mL (at 160 °C) of stabilized TCB (same as mobile phase) for 2.5 hours for PP or 3 hours for PE at max. 160°C under continuous gentle shaking in the autosampler of the GPC instrument.

25 **The xylene soluble fraction at room temperature (XS, wt.-%):** The amount of the polymer soluble in xylene is determined at 25 °C according to ISO 16152; first edition; 2005-07-01.

DSC analysis, melting temperature (T_m): measured with a TA Instrument Q200 differential scanning calorimetry (DSC) on 5 to 7 mg samples. DSC is run according to ISO
30 3146 / part 3 /method C2 in a heat / cool / heat cycle with a scan rate of 10 °C/min in the temperature range of -30 to +225°C. Crystallization temperature is determined from the cooling step, while melting temperature is determined from the second heating step.

The ash content is measured according to ISO 3451-1 (1997).

ICP (inductively coupled plasma) analysis

Inductively coupled plasma emission spectrometry (ICP) is an analytical technique used for the detection of trace metals. It is a type of emission spectroscopy that uses the inductively
5 coupled plasma (argon) to produce excited atoms and ions that emit electromagnetic radiation at wavelengths characteristic of a particular element. The intensity of this emission is indicative of the concentration of the element within the sample.

Apparatus used: Optima 2000DV from Perkin-Elmer

Titanium, aluminium and magnesium in pellets are determined with ICP. Acid standards are
10 used as reference.

Sample preparation

Samples (sample weight [g]) are first ashed following DIN EN ISO 3451-1 and the ash is dissolved in H_2SO_4 1N (sample conc. [mg/l])

Standards:

15 Standard Titanium solution (Merck): 1000 ppm Ti = stock solution A

Standard Aluminium solution (Merck): 1000 ppm Al = stock solution B

Standard Magnesium solution (Merck): 1000 ppm Mg = stock solution C

Standard 10 ppm Ti, Al, Mg

1 ml of the respective stock solution is diluted in a volumetric flask up to 100 ml with
20 distilled water

Acid standard 10 ppm Ti, 10 ppm Al and 10 ppm Mg

1 ml stock solutions A, B and C are put in a 100 ml volumetric flask. 2 g KHSO_4 and 25 ml H_2SO_4 1N are added and diluted up to 100 ml with distilled water = standard high concentration

25 Acid standard 1 ppm Ti, 1 ppm Al and 1 ppm Mg

10 ml of each standard 10 ppm Ti, AL, Mg are put in a 100 ml volumetric flask. 2 g KHSO_4 and 25 ml H_2SO_4 1N are added and dilute up to 100 ml with distilled water = standard low concentration

Blank sample for determination of Al, Ti and Mg

30 25 ml H_2SO_4 and 2 g KHSO_4 are put in a 100 ml volumetric flask and diluted up to 100 ml with distilled water = standard blank Al, Ti, Mg

The obtained results of the standard low concentration and standard high concentration are

inspected in the calibration summary. The “RSD value” (relative standard deviation value) of the standard should always be $\leq 10\%$. The obtained results must be close to the real value of the standards used. The calibration summary is checked. The correlation coefficient must be ≥ 0.997 .

- 5 The samples are analysed 3 times each. The obtained results are checked and ensured that the RSD $\leq 10\%$.

The average value of 3 determinations is reported.

Calculate the concentration of the element (ppm) as:

$$\frac{\text{Sample conc (mg/l)} \times 100}{\text{Sample weight used for calcinations (g)}}$$

Stepwise Isothermal Segregation Technique (SIST)

- 10 The isothermal crystallisation for SIST analysis was performed in a Mettler TA820 DSC on 3 ± 0.5 mg samples at decreasing temperatures between 200°C and 105°C.
 - (i) the samples were melted at 225 °C for 5 min.,
 - (ii) then cooled with 80 °C/min to 145 °C
 - (iii) held for 2 hours at 145 °C,
 - 15 (iv) then cooled with 80 °C/min to 135 °C
 - (v) held for 2 hours at 135 °C,
 - (vi) then cooled with 80 °C/min to 125 °C
 - (vii) held for 2 hours at 125 °C,
 - (viii) then cooled with 80 °C/min to 115 °C
 - 20 (ix) held for 2 hours at 115 °C,
 - (x) then cooled with 80 °C/min to 105 °C
 - (xi) held for 2 hours at 105 °C.

After the last step the sample was cooled down with 80 °C/min to -10 °C and the melting curve was obtained by heating the cooled sample at a heating rate of 10°C/min up to 200°C.

- 25 All measurements were performed in a nitrogen atmosphere. The melt enthalpy is recorded as function of temperature and evaluated through measuring the melt enthalpy of fractions melting within temperature intervals of

50 to 60 °C; 60 to 70 °C; 70 to 80 °C; 80 to 90 °C; 90 to 100 °C; 100 to 110 °C; 110 to 120 °C; 120 to 130 °C; 130 to 140 °C; 140 to 150 °C; 150 to 160 °C; 160 to 170 °C; 170 to

30 180 °C; 180 to 190 °C; 190 to 200 °C.

B. Examples

- The catalyst used in the polymerization process for the polypropylene of the inventive examples (IE1 to IE6) and the comparative examples (CE1 to CE4) was the commercial Ziegler-Natta catalyst ZN168M catalyst (succinate as internal donor, 2.5 wt% Ti) from
- 5 Lyondell-Basell was used along with triethyl-aluminium (TEAL) as co-catalyst and dicyclopentyl dimethoxy silane (D-donor) as donor.

The aluminium to donor ratio, the aluminium to titanium ratio and the polymerization conditions are indicated in table 1.

Table 1a: Preparation of inventive propylene homopolymers (H-PP)

		IE1	IE2	IE3	IE4	IE5	IE6
TEAL/Ti	[mol/mol]	40	19	25	35	35	17
TEAL/Donor	[mol/mol]	40	25	40	25	25	10
Donor/Ti	[mol/mol]	1.0	0.8	0.6	1.4	1.4	1.7
LOOP							
time	[min]	30	30	30	30	30	35
temp	[°C]	80	80	80	80	80	78
split	[wt.-%]	51	49	52	51	50	34.7
MFR ₂	[g/10']	4.0	4.0	4.0	4.0	4.0	2.1
H2/C3	[mol/kmol]	3.45	3.46	3.46	3.46	3.46	2.3
pressure	[bar]	37.3	37.3	37.3	37.3	37.3	
GPR1							
time	[min]	180	180	180	180	180	105
temp	[°C]	80	80	80	80	80	85
split	[wt.-%]	49	51	48	49	50	45.3
MFR ₂	[g/10']	6.9	8.5	9.6	8.2	7.0	2.4
H2/C3	mol/kmol	18.33	18.33	18.33	18.33	18.33	10.46
pressure	[bar]	22	22	22	22	22	21
GPR2							
time	[min]						65
temp	[°C]						90
split	[wt.-%]						20
MFR ₂	[g/10']						3.7
H2/C3	mol/kmol						14.0
pressure	[bar]						19
Final							
XCS	[wt%]	3.6	3.4	3.3	3.2	3.1	3.2
MFR ₂	[g/10']	5.2	5.9	6.1	5.7	5.3	2.5
Mw/Mn	[-]	12.7	-	12.2	-	12.2	10.2
Tm	[°C]	163	162	162	163	163	163
2,1 e	[%]	n.d.	n.d.	n.d.	n.d.	n.d.	n.d.
mmmm	[%]	94.6	94.1	94.6	94.1	95.3	94.8
Ash	[ppm]	16	18	23	25	29	15
Al	[ppm]	5.2	3.2	4.7	5.1	5.5	3.6
Mg	[ppm]	1.4	1.9	2.3	1.9	2.0	3.9
Cl	[ppm]	0	3.1	4.2	3.2	3.9	<1
Productivity	[kg/g]	92.8	66.9	73.4	79.3	77.3	135

n.d. = not detectable

Table 1b: Preparation of comparative propylene homopolymers (H-PP)

		CE1	CE2	CE3	CE4
TEAL/Ti	[mol/mol]	55	61	160	160
TEAL/Donor	[mol/mol]	10	25	40	10
Donor/Ti	[mol/mol]	5.5	2.4	4.0	16.0
LOOP					
time	[min]	30	30	30	30
temp	[°C]	80	80	80	80
split	[wt.-%]	54	52	57	59
MFR ₂	[g/10']	4.0	4.0	4.0	4.0
H2/C3	[mol/kmol]	3.46	3.46	3.46	3.46
pressure	[bar]	37.3	37.3	37.3	37.3
GPR					
time	[min]	180	180	180	180
temp	[°C]	80	80	80	80
split	[wt.-%]	46	48	43	41
MFR ₂	[g/10']	6.8	7.2	7.2	5.1
H2/C3	mol/kmol	18.33	18.33	18.33	18.33
pressure	[bar]	22	22	22	22
Final					
XCS	[wt%]	2.7	3.1	2.9	2.4
MFR ₂	[g/10']	5.1	5.3	5.2	4.4
Mw/Mn	[-]	-	11.4	10.4	12.8
Tm	[°C]	163	163	163	164
2,1 e	[%]	n.d.	n.d.	n.d.	n.d.
mmmm	[%]	95.4	94.6	95.4	96.2
Ash	[ppm]	30	36	55	78
Al	[ppm]	9.0	9.2	19.7	24.0
Mg	[ppm]	2.0	2.0	1.8	2.0
Cl	[ppm]	3.7	2.5	4.9	3.2
Productivity	[kg/g]	79.1	90.4	88.9	75.4

n.d. = not detectable

Table 2: SIST data of the examples

	IE1	IE2	IE3	IE4	IE5	IE6	CE1	CE2	CE3	CE4
Temp. Range/ °C	[wt%]	[wt%]	[wt%]	[wt%]	[wt%]	[wt%]	[wt%]	[wt%]	[wt%]	[wt%]
90-100	1.20	0.00	0.00	0.06	0.00	0	0.00	0.00	0.00	0.00
100-110	0.65	0.04	0.03	0.13	0.04	0	0.05	0.05	0.06	0.05
110-120	1.10	0.39	0.38	0.47	0.39	0.23	0.39	0.43	0.46	0.40
120-130	1.85	1.06	1.06	1.14	1.08	0.97	1.06	1.13	1.17	1.07
130-140	3.31	2.48	2.52	2.52	2.56	2.61	2.44	2.60	9.42	2.45
140-150	9.85	8.88	9.33	8.88	9.07	9.22	9.03	9.28	2.60	8.95
150-160	26.10	24.87	25.61	24.54	25.75	24.83	25.23	25.49	25.32	23.45
160-170	47.41	45.85	47.18	45.94	48.38	45	47.42	46.68	46.67	41.67
170-180	8.49	16.42	13.92	16.35	12.72	17.1	14.40	14.36	14.34	21.95
180-	0.00	0.00	0.00	0.00	0.00	0	0.00	0.00	0.00	0.00
SIST ratio	1.30	1.65	1.57	1.65	1.57	1.64	1.62	1.57	1.56	1.75

SIST ratio: the weight ratio of the crystalline fractions melting in the temperature range of above 160 to 180 °C to the crystalline fractions melting in the temperature range of 90 to 160

$$[(< 160-180) / (90-160)]$$

CLAIMS

1. Process for the manufacture of propylene homopolymer (H-PP) with a molecular weight distribution (M_w/M_n) of at least 10.0 in a sequential polymerization system comprising at least two polymerization reactors ((R1) and (R2)) connected in series, wherein the polymerization of propylene in the at least two polymerization reactors ((R1) and (R2)) takes place in the presence of
 - (a) a Ziegler-Natta catalyst (ZN-C) comprising a titanium compound (TC) having at least one titanium-halogen bond, and an internal donor (ID), both supported on a magnesium halide,
 - (b) a co-catalyst (Co), and
 - (c) an external donor (ED),wherein
 - (i) the internal donor (ID) comprises at least 80 wt.-% of a succinate;
 - (ii) the molar-ratio of co-catalyst (Co) to external donor (ED) [Co/ED] is 10 to 45;
 - (iii) the molar-ratio of co-catalyst (Co) to titanium compound (TC) [Co/TC] is 8 to 45; and
 - (iv) the molar-ratio of external donor (ED) to titanium compound (TC) [ED/TC] is 0.7 to 2.0.
2. Process for the manufacture of propylene homopolymer (H-PP) with a molecular weight distribution (M_w/M_n) of at least 10.0 in a sequential polymerization system comprising at least three polymerization reactors ((R1), (R2) and (R3)) connected in series, wherein the polymerization of propylene in the at least three polymerization reactors ((R1), (R2) and (R3)) takes place in the presence of
 - (a) a Ziegler-Natta catalyst (ZN-C) comprising a titanium compound (TC) having at least one titanium-halogen bond, and an internal donor (ID), both supported on a magnesium halide;
 - (b) a co-catalyst (Co), and
 - (c) an external donor (ED),wherein
 - (i) the internal donor (ID) comprises at least 80 wt.-% of a succinate;
 - (ii) the molar-ratio of co-catalyst (Co) to external donor (ED) [Co/ED] is 10 to 45;
 - (iii) the molar-ratio of co-catalyst (Co) to titanium compound (TC) [Co/TC] is 8 to 45; and

- (iv) the molar-ratio of external donor (ED) to titanium compound (TC) [ED/TC] is 0.7 to 2.0.
3. Process according to claim 1 or 2, wherein at least one of (a), (b), (c) and (d) below is satisfied:
- (a) the total average residence time is at least 160 min;
 - (b) the average residence time in the first polymerization reactor (R1) is at least 20 min;
 - (c) the average residence time in the second polymerization reactor (R2) is at least 90 min;
 - (d) the average residence time in the third polymerization reactor (R3) – if present – is at least 30 min.
4. Process according to claim 1 or 2, wherein at least one of the polymerization reactors is a gas phase reactor.
5. Process according to claim 1 or 2, wherein at least one of (a), (b) and (c) below is satisfied:
- (a) the operating temperature in the first polymerization reactor (R1) is in the range of 70 to 85 °C;
 - (b) the operating temperature in the second polymerization reactor (R2) is in the range of 75 to 95 °C;
 - (c) the operating temperature in the third polymerization reactor (R3) – if present – is in the range of 75 to 95 °C.
6. Process according to claim 1 or 2, wherein the propylene homopolymer (H-PP) is discharged from the polymerization system without any washing and optionally converted to pellets.
7. Process according to claim 1 or 2, wherein the internal donor (ID) is a succinate.
8. Process according to claim 1 or 2, wherein the propylene homopolymer (H-PP) comprises a first propylene homopolymer fraction (H-PP1), a second propylene homopolymer fraction (H-PP2) and optionally a third propylene homopolymer fraction (H-PP3).

9. Process according to claim 8, wherein at least one of (a) and (b) below is satisfied

- (a) the weight ratio between the first propylene homopolymer fraction (H-PP1) and the second propylene homopolymer fraction (H-PP2) [(H-PP1):(H-PP2)] is 70:30 to 35:65;
- (b) the first propylene homopolymer fraction (H-PP1) is produced in the first polymerization reactor (R1) whereas the second propylene homopolymer fraction (H-PP2) is produced in the second polymerization reactor (R2) and the optional third propylene homopolymer fraction (H-PP3) is produced in the third polymerization reactor (R3).

10. Process according to claim 8, wherein at least one of (a), (b) and (c) below is satisfied

- (a) the first propylene homopolymer fraction (H-PP1) and the second propylene homopolymer fraction (H-PP2) fulfill together the inequation (I)

$$4.0 \geq \frac{MFR(H-PP2)}{MFR(H-PP1)} \geq 1.0 \quad (I)$$

wherein

MFR(H-PP1) is the melt flow rate MFR₂ (230 °C) [g/10min] of the first propylene homopolymer fraction (H-PP1),

MFR(H-PP2) is the melt flow rate MFR₂ (230 °C) [g/10min] of the second propylene homopolymer fraction (H-PP2);

- (b) the second propylene homopolymer fraction (H-PP2) and the third propylene homopolymer fraction (H-PP3) fulfill together the inequation (I)

$$2.0 \geq \frac{MFR(H-PP3)}{MFR(H-PP2)} \geq 0.5 \quad (II)$$

wherein

MFR(H-PP2) is the melt flow rate MFR₂ (230 °C) [g/10min] of the second propylene homopolymer fraction (H-PP2),

MFR(H-PP3) is the melt flow rate MFR₂ (230 °C) [g/10min] of the third propylene homopolymer fraction (H-PP3);

- (c) the first propylene homopolymer fraction (H-PP1) and the propylene homopolymer (H-PP) fulfill together the inequation (III)

$$3.0 \geq \frac{MFR(H-PP)}{MFR(H-PP1)} \geq 1.0 \quad (III)$$

wherein

MFR(H-PP1) is the melt flow rate MFR₂ (230 °C) [g/10min] of the first propylene homopolymer fraction (H-PP1),

MFR (H-PP) is the melt flow rate MFR₂ (230 °C) [g/10min] of the propylene homopolymer (H-PP).

11. Process according to claim 1 or 2, wherein the propylene homopolymer (H-PP) satisfies at least one of (a) and (b) below:

- (a) a melt flow rate MFR₂ (230 °C) measured according to ISO 1133 in the range of 1.5 to 10.0 g/10min;
- (b) a xylene cold soluble content (XCS) determined according ISO 16152 (25 °C) of at least 2.8 wt.-%.

12. Process according to claim 1 or 2, wherein the propylene homopolymer (H-PP) satisfies at least one of (a), (b) and (c) below

- (a) 2,1 erythro regio-defects of equal or below 0.4 mol.-% determined by ¹³C-NMR spectroscopy;
- (b) a pentad isotacticity (mmmm) of more than 93.5 mol.-%;
- (c) an ash content below 30 ppm.

13. Process according to any one of the preceding claims wherein the propylene homopolymer (H-PP) satisfies at least one of (a) and (b) below:

- (a) a melting temperature T_m of more than 160 °C;
- (b) a weight ratio of the crystalline fractions melting in the temperature range of above 160 to 180 °C to the crystalline fractions melting in the temperature range of 90 to 160 [($< 160-180$) / ($90-160$)] of at least 1.20, wherein said fractions are determined by the stepwise isothermal segregation technique (SIST).

14. Propylene homopolymer (H-PP) having

- (a) a melt flow rate MFR₂ (230 °C) measured according to ISO 1133 in the range of 1.5 to 10.0 g/10min;
- (b) a molecular weight distribution (MWD) of more than 10;
- (c) a xylene cold soluble content (XCS) determined according ISO 16152 (25 °C) of at least 2.8 wt.-%;
- (d) a pentad isotacticity (mmmm) of more than 93.5 mol.-%, and
- (e) an ash content below 30 ppm, preferably below 25 ppm.

15. Propylene homopolymer according to claim 14, wherein said propylene homopolymer (H-PP) satisfies at least one of (a), (b) and (c) below

- (a) 2,1 erythro regio-defects of equal or below 0.4 mol.-% determined by ^{13}C -NMR spectroscopy,
- (b) a melting temperature T_m of more than 160 °C,
- (c) a weight ratio of the crystalline fractions melting in the temperature range of above 160 to 180 °C to the crystalline fractions melting in the temperature range of 90 to 160 [$(< 160-180) / (90-160)$] of at least 1.20, wherein said fractions are determined by the stepwise isothermal segregation technique (SIST).

16. Propylene homopolymer (H-PP) according to claim 14, wherein said propylene homopolymer (H-PP) has a first propylene homopolymer fraction (H-PP1), a second propylene homopolymer fraction (H-PP2) and optional a third propylene homopolymer fraction (H-PP3), wherein at least one of (a), (b), (c) and (d) below is satisfied:

- (a) the first propylene homopolymer fraction (H-PP1) and the second propylene homopolymer fraction (H-PP2) fulfill together the inequation (I)

$$4.0 \geq \frac{\text{MFR (H-PP2)}}{\text{MFR (H-PP1)}} \geq 1.0 \quad (\text{I})$$

wherein

MFR (H-PP1) is the melt flow rate MFR_2 (230 °C) [g/10min] of the first propylene homopolymer fraction (H-PP1),

MFR (H-PP2) is the melt flow rate MFR_2 (230 °C) [g/10min] of the second propylene homopolymer fraction (H-PP2);

- (b) the second propylene homopolymer fraction (H-PP2) and the third propylene homopolymer fraction (H-PP3) fulfill together the inequation (I)

$$2.0 \geq \frac{\text{MFR (H-PP3)}}{\text{MFR (H-PP2)}} \geq 0.5 \quad (\text{II})$$

wherein

MFR (H-PP2) is the melt flow rate MFR_2 (230 °C) [g/10min] of the second propylene homopolymer fraction (H-PP2),

MFR (H-PP3) is the melt flow rate MFR_2 (230 °C) [g/10min] of the third propylene homopolymer fraction (H-PP3);

- (c) the first propylene homopolymer fraction (H-PP1) and the propylene homopolymer (H-PP) fulfill together the inequation (III)

$$3.0 \geq \frac{\text{MFR (H-PP)}}{\text{MFR (H-PP1)}} \geq 1.0 \quad (\text{III})$$

wherein

MFR (H-PP1) is the melt flow rate MFR₂ (230 °C) [g/10min] of the first propylene homopolymer fraction (H-PP1),

MFR (H-PP) is the melt flow rate MFR₂ (230 °C) [g/10min] of the propylene homopolymer (H-PP);

- (d) the weight ratio between the first propylene homopolymer fraction (H-PP1) and the second propylene homopolymer fraction (H-PP2) [(H-PP1):(H-PP2)] is 70:30 to 35:65.

17. Propylene homopolymer (H-PP) according to any one of claim 14, wherein the propylene homopolymer (H-PP) has been produced according claim 1 or 2.

18. Biaxially oriented film comprising a propylene homopolymer (H-PP) according to one of the preceding claims 14 to 16.