

Description

The present invention relates to an oscillator circuit of the frequency locked loop type.

Recently, devices which perform speech synthesis using digital technology have been developed and used. In such a device, an impulse and a white noise are used as a sound source. The signal from the sound source is passed through several digital filters to obtain an audio signal. The conditions for the digital filters depend on the audio signal to be achieved. Furthermore, the conditions for the digital filters in the digital speech synthesizer are set by analyzing and recognizing an actual voice.

Fig. 1 is a conventional block diagram of a speech recognition circuit. In the figure, a mike amplifier 1 amplifies an analog signal from a microphone (not shown). The output from the mike amplifier 1 is supplied in parallel to, for example, four band-pass filters (BPF) 2A, 2B, 2C and 2D. The signals which pass through the four band-pass filters 2A, 2B, 2C and 2D are detected by four detectors, respectively. The detected four signals are supplied to four low-pass filter circuits 4A, 4B, 4C and 4D, respectively. The signals which pass through the low-pass filter circuits 4A, 4B, 4C and 4D are selectively supplied to an analog/digital converter (A/D) 6 through a multiplexer 5. The digital output from the analog/digital converter 6 results in a recognition result for the voice input through the microphone.

The employment of switched-capacitor filter technology introduces higher integration and higher accuracy to the recent speech recognition circuit. In other words, the mike amplifier 1, band-pass filter circuits 2A through 2D and low-pass filter circuits 4A through 4D all adopt the switched capacitor circuit. For the control of the switched capacitor circuit, any circuit which uses a switched capacitor circuit is required to include an oscillator and a clock generator which produces various clock pulses from the oscillator output.

When an accurate oscillating frequency is required, the actual oscillating frequency can be matched to the accurate oscillating frequency by knowing whether the actual oscillating frequency is greater or smaller than the accurate oscillating frequency, or the fluctuation or ratio between the actual oscillating frequency and the accurate oscillating frequency.

A PLL (phase locked loop) circuit has been known as a means for accurately detecting which frequency is greater or smaller, or the fluctuation or ratio between the actual and accurate frequencies.

However, the PLL circuit is not adapted to integration due to its complicated construction. Therefore, with prior art circuits with simplified constructions, an accurate oscillating frequency can not be obtained, thereby degrading the switched capacitor circuit which leads to a speech recognition circuit with poor accuracy.

Prior art document "IEEE Journal of Solid-State Circuits", Volume SC-17, No. 4, August 1982, pages 775 to 778, New York, US, discloses a switched-capacitor frequency control loop comprising a resistor in parallel with a switched capacitor network, DC supply means for supplying a current to the resistor and the switched capacitor network, an integrator for integrating the composite current from the resistor and the switched capacitor network and a voltage controlled oscillator receiving the integrator output signal through a filter and feeding a two phase clock generator which controls the switches of the switched capacitor network. The switched capacitor network removes a charge from the integrator input, contrary to the resistor through which a charge is supplied to the integrator input. The resistor can be replaced by a switched capacitor network clocked by a constant frequency and supplying a current to the integrator input, thus having a positive equivalent resistance, dependent on the constant frequency.

Further, prior art document GB-A-1 409 104 discloses an oscillator circuit of the voltage or current controlled oscillator type. Such voltage or current controlled oscillator is suitable to be used in a frequency controlled loop.

Prior art document FR-A-2 441 174 describes a phase and frequency comparator where in a frequency control loop a frequency divider is used in the feedback loop of the oscillator, the output of the frequency divider feeding one input of the frequency comparator.

Finally, prior art document Patents Abstract of Japan, Volume 7, No. 23 (P-171) (1168), January 29, 1983 (= JP-A-57175964) discloses a frequency detector in which a resistor and a capacitor are connected in parallel between the input and output terminals of an operational amplifier.

It is an object of the invention to provide an oscillator circuit using a frequency comparing circuit which can stably generate with high accuracy an arbitrary multiple of frequencies from the reference signal derived from an oscillating signal, which is supplied from an oscillator such as a crystal oscillator which stably oscillates.

To solve this object the present invention provides an oscillator circuit as specified in claim 1.

Other objects and features of the present invention will be apparent from the following description taken in connection with the accompanying drawings in which:

Fig. 1 is a block diagram showing a conventional construction of a speech recognition circuit;

Fig. 2 is a circuit diagram showing a frequency comparing circuit,

Fig. 3 is a circuit diagram showing another frequency comparing circuit;

Fig. 4 is a detailed circuit diagram of a switched capacitor circuit 10 used in the frequency comparing circuit of Figs. 2 and 3;

Fig. 5 is a detailed circuit diagram of a switched capacitor circuit 20 used in the frequency comparing circuit of Figs. 2 and 3;

Figs. 6A and 6B are timing charts of the switched capacitor circuit shown in Fig. 4 or 5;

Fig. 7 is a circuit diagram for application of the comparing circuit;

Fig. 8 is a circuit diagram showing another frequency comparing circuit;

Fig. 9 is a characteristic of the frequency comparing circuit shown in Fig. 8;

Fig. 10 is a circuit diagram for application of the frequency comparing circuit;

Figs. 11A and 11B are circuit diagrams showing an embodiment of an oscillator circuit;

Fig. 12 is a waveform explaining an operation of the Schmitt trigger shown in Figs. 11A and 11B;

Fig. 13 is a characteristic of an oscillating circuit shown in Figs. 11A and 11B;

Fig. 14 is a block diagram showing another embodiment of an oscillator circuit;

Fig. 15 is a detailed circuit diagram of an embodiment of a frequency divider shown in Fig. 14;

Fig. 16 is a block diagram showing an embodiment of the oscillator circuit of the invention;

Fig. 17 is a detailed circuit diagram of an embodiment of a synchronizing circuit shown in Fig. 16; and

Figs. 18A through 18H are timing charts of the circuitry in Fig. 17 in which: Fig. 18A shows the output signal of the Schmitt trigger; Fig. 18B, the output signal of the frequency divider 110; Fig. 18C, the output signal of the F/F 121 in Fig. 17; Fig. 18D, the output signal of F/F 122 in Fig. 17; Fig. 18E, the inverted output signal of F/F 121 in Fig. 17; Fig. 18F, the output signal of NOR gate 124 in Fig. 17; Fig. 18G, the inverted output signal of NAND gate 127 in Fig. 17; and Fig. 18H, the output of NOR gate 128 in Fig. 17.

Fig. 2 is a circuit diagram showing a frequency comparing circuit. The switched capacitor circuit 10 comprises a capacitor 11 and four switches 12 through 15. The circuit 10 has a negative equivalent resistance, and its value is determined corresponding to the frequency f_s of an oscillating signal S_s from an oscillator. One terminal of each switch 12 and 13 is connected to one terminal of the capacitor 11, and the other terminal of the switch 12 is grounded. The other terminal of the capacitor 11 is connected to one terminal of the switches 14 and 15, and the other terminal of the switch 14 is grounded.

Among the four switches 12 through 15, a pair of switches 12 and 15 and a pair of switches 13 and 14 are alternatively turned on in response to the Signal S_s . The switched capacitor circuit 20 comprises a capacitor 21 and four switches 22 through 25 and has a positive equivalent resistance, the value of which is determined corresponding to a reference signal S_c with frequency f_c . One terminal of the capacitor 21 is connected to one terminal of each switch 22 and 23, and the other terminal of the switch 23 is grounded. The other terminal of the capacitor 21 is connected to one terminal of each switch 24 and 25, and the other terminal of the switch 25 is grounded. A switch pair 22 and 24 and another switch pair 23 and 25 are alternatively turned on in response to a signal S_c .

The other terminal of the switch 13 in the switched capacitor circuit 10 and the other terminal of the switch 22 in the switched capacitor circuit 20 are connected at a common connection a. Furthermore, the positive electrode of a DC power source V is connected to the common connection a. The negative electrode of the DC power source V is grounded. Also, the other terminals of the switch 15 in the switched capacitor circuit 10 and the switch 24 in the switched capacitor circuit 20 are connected to a common connection b. Furthermore, an input terminal of an integrator 30 is connected to the common connection b. The integrator 30 is provided with a differential amplifier 31 having an inverted input terminal, a non-inverted input terminal and output terminal, and a capacitor 32. The capacitor 32 is connected between the inverted input terminal and output terminal, and the non-inverted input terminal of the differential amplifier 31 is grounded. The differential amplifier 31 operates at a voltage between a positive electrode voltage V_{DD} and a negative electrode voltage V_{SS} . The ground voltage is set at an intermediate potential between the positive and negative voltage, for example, at 0 V. The inverted input terminal of the differential amplifier 31 serves as the input terminal of the integrator 30. The integrator 30 produces on its output terminal a signal OUT corresponding to the magnitude relation between two frequencies f_s and f_c .

The equivalent resistance R_1 of the switched capacitor circuit 10 (hereafter referred to as SC circuit) is given by:

$$R_1 = - \frac{1}{C_1 \cdot f_s} \quad \dots (1)$$

wherein C_1 represents the capacitance of the capacitor 11. As well, the equivalent resistance R_2 of the SC circuit 20 is given by:

$$R_2 = \frac{1}{C_2 \cdot f_c} \quad \dots (2)$$

wherein C_2 represents the capacitance of the capacitor 21.

As the one terminal of each two SC circuits 10 and 20, namely, the other terminals of the switches 13 and 22 are connected through the connection a to the positive electrode of the DC power source V, the positive bias from the DC power source V is supplied to both SC circuits 10 and 20. Therefore, a predetermined DC current flows into the respective SC circuits 10 and 20. As the SC circuit 10 has negative equivalent resistance R_1 , the direction of the current I_1 is to the left in Fig. 2. Also, the SC circuit 20 has a positive equivalent resistance R_2 , and the direction of the current I_2 is to the right in Fig. 2. In other words, the directions of the currents I_1 and I_2 are opposite to each other. A composite current of I_1 and I_2 is supplied to the integrator 30. When the composite current is 0, the output signal OUT of the integrator 30 becomes ground voltage. When $I_1 > I_2$ and current corresponding to the difference between I_1 and I_2 flows from the integrator 30, the level of the output signal OUT of the integrator 30 becomes high (V_{DD} level). On the contrary, when $I_2 > I_1$ and current corresponding to the difference between I_1 and I_2 flows into the integrator 30, the level of the output signal OUT of the integrator 30 become low (V_{SS} level). Suppose that the capacitance C_1 of the capacitor 11 in the SC circuit 10 and the capacitance C_2 of the capacitor 21 in the SC circuit 20 are equally set. When the frequency f_s of the oscillating signal S_s coincides with the frequency f_c of the reference signal S_c , the output signal OUT of the integrator 30 becomes ground voltage. Furthermore, when the frequency f_s is greater than the frequency f_c , the level of the output signal OUT of the integrator 30 becomes high. On the other hand, when the frequency f_c is smaller than the frequency f_s , the level of the output signal OUT of the integrator 30 becomes low. In summary, the output signal OUT of the integrator 30 varies its level according to the cyclical relationship of the two frequencies f_s and f_c . Therefore, the comparison of the two frequencies can be performed by determining the output signal OUT. The equivalent resistances R_1 and R_2 of the SC circuits 10 and 20 are determined only by the frequencies f_s and f_c , provided that the capacitances C_1 and C_2 are constant as shown in the equations (1) and (2). Since the capacitances C_1 and C_2 can be set with a relatively higher accuracy than the resistances, the respective frequencies f_s and f_c can be converted into the resistances R_1 and R_2 with high accuracy. Furthermore, the integrator 30 achieves the signal OUT by integrating the composite values of flowing currents corresponding to the resistances R_1 and R_2 . Thus, the comparison between f_s and f_c can be performed with high accuracy even if the slew rate or gain of the differential amplifier 31 fluctuates.

As described above, the comparison and detection can be performed with high accuracy on the cyclical relationship between the frequency f_s of the oscillating signal S_s from the oscillator and the frequency f_c of the reference signal S_c . Therefore, the frequency f_s can be matched with the reference frequency f_c with high accuracy by using the output signal OUT.

Also in this comparing circuit, the apparent frequency of the reference signal S_c can be varied from the actual value f_c by changing the capacitances C_1 and C_2 of the capacitors 11 and 21 in the SC circuits 10 and 20. For example, by setting the values of the capacitors 11 and 21 to satisfy $C_1 = 2C_2$, the comparison and detection of the cyclical relationship between $2f_c$ and f_s can be performed.

Fig. 3 is a circuit diagram showing a construction of another frequency comparing circuit. The circuit in fig. 3 is same as that in Fig. 2 except that a resistor 33 is connected in parallel to the capacitor 32 in the integrator 30.

In this comparing circuit, as in the comparing circuit of Fig. 3, when the composite value of the output currents I_1 and I_2 in the SC circuits 10 and 20 is 0, the output signal OUT is set to ground voltage. However, when the composite value is not 0, the output signal OUT is set to less than the V_{DD} or V_{SS} level in accordance with the electrode of the composite current.

Figs. 4 and 5 show detailed circuits of the SC circuits 10 and 20 used in the above comparing circuit respectively. The same numerals as in Figs. 2 and 3 are used for the same parts in Figs. 4 and 5.

Furthermore, two signals S_{s1} and S_{s2} or S_{c1} and S_{c2} are used whose phases are different than each other as shown in the timing charts of Figs. 6A and 6B.

The switches 12 through 15 in the SC circuit 10 having negative resistance comprise, as shown in Fig. 4 CMOS switches 52 through 55 in which N channel MOSFETs 41 through 44 and P channel MOSFETs 45 through 48 are connected in parallel to each other. The signal S_{s1} in Fig. 6A is supplied to the gates of the N channel MOSFETs 41 and 44 and through a CMOS inverter 49 to the gates of the P channel MOSFETs 45 and 48. The signal S_{s2} in Fig. 6B is supplied to the gates of the N channel MOSFETs 42 and 43 and through a CMOS inverter 50 to the gates of the P channel MOSFETs 46 and 47.

Now the switching control of the CMOS switches 52 through 55 will be described in response to the signals S_{s1} and S_{s2} under the condition that the DC voltage V_1 is supplied to the other terminal of the CMOS switch 53 and the other terminal of the CMOS switch 55 is grounded. When the level of the signal S_{s2} is high, the CMOS switches 53 and 54 turn on. Then, the other terminal (point C in Fig. 4) of the capacitor 11 will be charged at $-C \cdot V_1$. When the level of the signal S_{s1} is high, the CMOS switches 52 and 55 turn on. At this time, the positive charge $+C_1 \cdot V_1$ from the ground is supplied through the CMOS switch 55 to the point C so as to cancel the negative charge at the point C. When such an operation is repeated f_c times per second and the direction of the current flowing through the CMOS switch 55 from the point C is positive, the value of the current I which flows in the SC circuit is given by:

$$-I = C_1 \cdot V_1 \cdot f_s \quad (3)$$

The equivalent resistance R in the SC circuit 10 is obtained by dividing the current I by the supply voltage V_1 . Thus, the equivalent resistance R is given by:

$$R = \frac{V_1}{-C_1 \cdot V_1 \cdot f_s} = - \frac{1}{C_1 \cdot f_s} \quad \dots (4)$$

The right side in the equation (4) is the same as the right side in equation (1). Therefore, the equation (4) reveals that the SC circuit 10 in Fig. 4 has the negative equivalent resistance corresponding to the frequency f_s .

The switches 22 through 25 in the SC circuit 20 comprise the CMOS switches 72 through 75 in which N channel MOSFETs 61 through 64 and P channel MOSFETs 65 through 68 are connected in parallel, respectively, as shown in Fig. 5. The signal S_{c1} in Fig. 6A is supplied to the gates of the N channel MOSFETs 61 and 63 and through the CMOS inverter 69 to the gates of the P channel MOSFETs 65 and 67. The signal S_{c2} in Fig. 6B is supplied to the gates of the N channel MOSFETs 62 and 64 and through a CMOS inverter 70 to the P channel MOSFETs 66 and 68.

Now a switching control will be described of the CMOS switches 72 through 75 in response to the signals S_{c1} and S_{c2} under the condition that the DC voltage V_2 is supplied to the other terminal of the CMOS switch 72 and the ground voltage is supplied to the other terminal of the CMOS switch 74. When the level of the signal S_{c1} is high, the CMOS switches 72 and 74 turn on. At this time, the capacitor 21 is charged to $C_2 \cdot V_2$. Then, when the level of the signal S_{c2} becomes high, the CMOS switches 73 and 75 turn on. Therefore, the charge stored in the capacitor 21 is discharged. When such an operation is repeated f_c times per second, and the direction of the current flowing from the other terminal of the capacitor 21 (point d in Fig. 5) through the CMOS switch 74 to the ground is positive, the current I which flows in the SC circuit 20 is given by:

$$I = C_2 \cdot V_2 \cdot f_c \quad (5)$$

The equivalent resistance R in the SC circuit is obtained by dividing the supply voltage V_2 by the current I . That is:

$$R = \frac{V_2}{C_2 \cdot V_2 \cdot f_c} = \frac{1}{C_2 \cdot f_c} \quad \dots (6)$$

The right side in equation (6) is the same as that in equation (2). Thus, the equation (6) reveals that the SC circuit 20 in Fig. 5 has a positive equivalent resistance corresponding to the frequency f_c .

Fig. 7 is a circuit diagram showing an applied construction of the comparing circuit. The circuit of this application comprises two frequency comparing circuits 100 and 200 constructed like those in Fig. 2 and an AND gate 300 which receives both the output signals OUT1 and OUT2. The SC circuit having the negative equivalent resistance (referred to by 10 in fig. 2) in one frequency comparing circuit 100 is controlled by a signal S_{ca} having a higher reference frequency f_{ca} . The SC circuit having a positive equivalent resistance (referred to by 20 in Fig. 2) is controlled by a signal S_s having a frequency f_s to be compared. The SC circuit having a negative equivalent resistance (referred by 10 in Fig. 2) in the frequency comparing circuit 200 is controlled by a signal S_{cb} having a lower frequency f_c and the SC circuit having a positive equivalent resistance is controlled by the signal S_s .

In this circuit, it is assumed that all the capacitances in the SC circuit are equally set. The level of the output signals OUT1 and OUT2 of the frequency comparing circuits 100 and 200 becomes high, thus the output level of the AND gate 300 becomes high only when the relation $f_{ca} > f_s > f_{cb}$ is satisfied between the frequencies f_{ca} , f_{cb} and f_s of the signals S_{ca} , S_{cb} and S_s , respectively. In other words, the circuit can detect whether the frequency f_s to be compared is between the higher reference frequency f_{ca} and the lower reference frequency signal f_{cb} .

In the comparing circuits in Figs. 2 and 3, a common DC power source V is used to flow DC current in the SC circuits 10 and 20. However, different DC power sources may be used for the SC circuits 10 and 20. When using different DC power sources, the apparent frequency of the reference signals S_c can be varied from the actual frequency f_c by using different DC power sources as changing values of the capacitors 11 and 21. In the above comparing circuits, one SC circuit 10 having a negative equivalent resistance is controlled by the signal S_s , and the other SC circuit 20 having a positive equivalent resistance is controlled by the signal S_c . However, the signals S_s and S_c are interchangeable.

Fig. 8 shows a frequency comparing circuit which can perform fluctuations between the two signal's frequencies with high accuracy. The same numerals are used for the same parts in Fig. 2 and the descriptions are omitted. In this frequency comparing circuit, two resistors 76 and 77 are connected in series between the positive electrode power source V_{DD} and the ground. The other terminal of the switch 13 in the switched capacitor circuit 10 is connected to a serial connection a1 between the resistors 76 and 77. Furthermore, two resistors 78 and 79 are serially connected between V_{DD} and the output point OUT of voltage V_0 . The other terminal of the switch 22 of the SC circuit 20 is connected at the serial connection a2 between the resistors 78 and 79. The differential amplifier 31 operates at a voltage between the positive electrode power source voltage V_{DD} and negative electrode power source voltage V_{SS} whose absolute value is equal that of V_{DD} . The ground potential is set between V_{DD} and V_{SS} , for example, to 0 V. In the integrator 30, the inverted input terminal of the differential amplifier 31 serves as the input terminal, and from the output terminal, voltage proportional to the fluctuation between the two frequencies f_s and f_c is provided.

In such a construction, a constant positive voltage V_1 , determined by the resistance ratio of the resistors 76 and 77, and the voltage V_{DD} is supplied to the connection a1 where the one terminal of the SC circuit 10, that is, the other terminal of the switch 13, is connected. The equivalent resistance R_1 of the SC circuit 10 becomes negative as in the equation (1) if the value of the capacitor 11 is C_1 . Thus, the direction of the current I_1 flowing into the SC circuit 10 is to the left in Fig. 8. Positive or negative voltage V_2 , determined by the resistance ratio of the resistors 78 and 79, voltage V_{DD} , and the output voltage V_0 from the integrator 30, is supplied to the connection a2 where one terminal of the SC circuit 20, that is, the other terminal of the switch 22, is connected. The equivalent resistance R_2 of the SC circuit 20 becomes positive as in the equation (2) if the value of the capacitor 21 is C_2 .

When the voltage V_2 is positive, the direction of the current I_2 flowing into the SC circuit 20 is to the right in Fig. 8. The integrator 30 integrates the composite current of I_1 and I_2 and reduces voltage V_0 .

Now supposed that the capacitance C_1 of the capacitor 11 in the SC circuit 10 is equal to the capacitance C_2 of the capacitor 21 in the SC circuit 20, all the resistors 76, 77, 78 and 79 have the same resistance, and the voltages V_1 and V_2 are equal. Under this condition, when the frequency f_s of the oscillating signal S_s coincides with the frequency f_c of the reference signal S_{c1} , current I_1 is equal to current I_2 , and their directions are opposite to each other as shown in Fig. 8. Therefore, the composite current of I_1 and I_2 become 0, and the output voltage of the integrator 30 becomes ground voltage. When the output voltage V_0 is ground voltage, the voltage V_2 at the connection a2 becomes $(V_{DD}-0)/2$ as the values of the resistors 78 and 79 are equal. Also, the voltage V_1 at the connection a1 becomes $(V_{DD}-0)/2$ as the values of the resistors 76 and 77 are equal. Therefore, voltage V_1 is equal to voltage V_2 . Thus, the output voltage V_0 of the integrator 30 becomes ground voltage (0 V) when the frequency f_s coincides with the frequency f_c . When the output voltage V_0 is equal to the ground voltage, the voltage V_2 at the connection a2 becomes

($V_{DD}-0$)/2 as the values of the resistors 78 and 79 are equal. Also, the voltage V_1 at the connection a1 becomes ($V_{DD}-0$)/2 as the values of the resistors 76 and 77 are equal. Therefore, voltage V_1 is equal to voltage V_2 . Thus, the output voltage V_0 of the integrator 30 is fixed at the ground level when the frequency f_s coincides with the frequency f_c . On the other hand, when the frequency f_s is lower than the frequency f_c , the equivalent resistance of the SC circuit 10 given by the equation (1) becomes greater. Since the value of voltage V_1 supplied to the SC circuit 10 is constant, the greater the resistance R_1 , the smaller the current value I_1 . As a result, the composite current of I_1 and I_2 becomes positive (in the direction of flowing into the integrator 30). The integrator 30 integrates the composite current and produces negative voltage V_0 proportional to the current. The voltage V_0 serves to lower the voltage V_2 at the connection a2, so that the value of the current flowing in the SC circuit 20 becomes smaller. When the current I_1 and I_2 are balanced, the output voltage V_0 of the integrator 30 becomes constant.

Now when the frequency f_s rises from the balance and becomes higher than the frequency f_c , the equivalent resistance R_1 of the SC circuit 10 becomes smaller. Thus, the value of the current I_1 flowing in the SC circuit 10 becomes greater. As a result, the composite current of I_1 and I_2 become negative (in the direction of flowing out of the integrator 30). At this time, the integrator 30 integrates the composite current and produces a positive voltage V_0 proportional to the current value. Thus produced voltage V_0 serves to raise the voltage V_2 at the connection a2. Therefore, the value of current I_2 flowing in the SC circuit 20 becomes greater. When the balance between the currents I_1 and I_2 is obtained, the output V_0 of the integrator 30 becomes constant.

Fig. 9 shows a characteristic of the frequency comparing circuit in Fig. 8 when $C_1 = C_2$. In the figure, the frequency f_s of the oscillating signal S_s is measured on the abscissa, and the output voltage V_0 of the integrator 30 is measured on the ordinate. As is shown, there is a proportional relation between the frequency f_s and the output voltage V_0 . Therefore, from the output voltage V_0 , the fluctuation between two frequencies f_s and f_c can be measured. That is, when the output voltage V_0 is 0, there is no fluctuation between the frequencies. When the voltage V_0 is positive, the frequency f_s fluctuates corresponding to a voltage higher than the frequency f_c , and when the voltage V_0 is negative, the frequency f_s fluctuates corresponding to a voltage lower than the frequency f_c . Furthermore, the equivalent resistances R_1 and R_2 in the SC circuits 10 and 20 depend, as is shown in the equations (1) and (2), only on the frequencies f_s and f_c if the values of C_1 and C_2 are constant, respectively. Therefore, the values of the capacitors C_1 and C_2 can be set with relatively higher accuracy compared to those of the resistors. Thus, the frequencies f_s and f_c can be converted into equivalent resistances R_1 and R_2 with higher accuracy.

Also, in this frequency comparing circuit, the apparent frequency of the reference signal S_c can be varied from the actual frequency f_c by setting values C_1 and C_2 of the capacitors 11 and 21 and values of resistors 76 and 79. For example, by setting the values of the capacitors 11 and 21 to satisfy $C_1 = 2C_2$, the gradient of the characteristic line in Fig. 9 will be doubled. In this case, V_0 becomes 0 at the point of $f_s = f_c/2$. Therefore, the output voltage V_0 corresponding to the fluctuation between the half-divided frequency of the frequency f_c and frequency f_s can be obtained. If the value of resistor 76 is set to be equal to that of resistor 77 and the value of resistor 78 is set to be greater than that of resistor 79, there is a relation of $V_1 > V_2$ at $V_0 = 0$. If the value of resistor 78 is set three times that of resistor 79, the relations are $V_1 = V_{DD}/2$ and $V_2 = (V_{DD} - V_0)/4$. Therefore, the gradient of the characteristic line in Fig. 9 will be doubled so that the same effect can be obtained as $C_1 = 2C_2$.

Using the circuit, the applicant has conducted an experiment where 100PF is selected for C_1 and C_2 , +7V for V_{DD} , -7V for V_{SS} and 2KHz, 4KHz and 8KHz for f_c , respectively. As a result of the experiment, the output voltage V_0 represents linear characteristic when the frequency f_s is in the range of $0.1f_c$ through 1.7 or $1.8f_c$.

Fig. 10 is a circuit diagram showing an applied construction of the frequency comparing circuit. The application circuit is constructed in such a way that the output voltage V_0 of a frequency comparing circuit 400, constructed as in Fig. 8, is supplied to an inverter 500, thereby to obtain a logic signal OUT with either a high or low level set according to the voltage V_0 .

Figs. 11A and 11B are circuit diagrams showing a construction of an embodiment of the oscillator circuit using the frequency comparing circuit device in Fig. 10. In the figures, the same numerals are used for the same parts in Fig. 2, thereby to omit the description thereof.

In the figure, the output of the integrator 30 is supplied through a voltage buffer circuit 80 to a Schmitt-type oscillator 83. The voltage buffer circuit 80 comprises a differential amplifier 81 with an inverted input terminal, non-inverted input terminal and output terminal. The inverted input terminal is connected to the output terminal. The inverted input terminal is supplied with the voltage V_0 .

The Schmitt-type oscillator 83 is provided with a differential amplifier 84 with a non-inverted input terminal, inverted input terminal and output terminal. A higher level threshold voltage V_H and lower-level

threshold voltage V_L are alternatively supplied to the non-inverted input terminal of the differential amplifier 84. The higher level threshold voltage V_H is obtained at the serial connection c of the two resistors 85 and 86 serially connected at the point between the positive power supply voltage V_{DD} and the output terminal of the voltage buffer circuit 80. The voltage V_H is input to the non-inverted input terminal of the differential amplifier 84 through a CMOS switch 89 which comprises the P-channel MOSFET 87 and N-channel MOSFET 88. The lower level threshold voltage V_L is obtained at the serial connection d of the resistors 90 and 91 serially connected between the point at which the positive power supply voltage V_{DD} is applied and the point at which the negative power supply voltage V_{SS} is applied. The voltage V_L is input to the non-inverted input terminal of the differential amplifier 84 through a CMOS switch 94 which comprises the P channel MOSFET 92 and N channel MOSFET 93. Furthermore, DC voltage V_{V1} is applied to the point a1 of the switched capacitor circuit 10, and variable DC voltage V_{V2} is applied to the point a2 of the switched capacitor circuit 20.

Two inverters 95 and 96 are cascade-connected to the output terminal of the differential amplifier 84, and a resistor 97 and a capacitor 98 are serially connected between the output terminal of the inverter 96 in the lower stream and the point at which the voltage V_{SS} is applied. The output signal of the inverter 96 is input in parallel to a gate of an N-channel MOSFET 88 which constitutes the CMOS switch 89 and a gate of a P-channel MOSFET 92 which constitutes the CMOS switch 94 as well as to two inverters 99 and 101.

The output signal of the inverter 99 is supplied in parallel to a gate of a P-channel MOSFET 87 which constitutes the CMOS switch 89 and a gate of an N-channel MOSFET 93 which constitutes the CMOS switch 94. Furthermore, a voltage at the point e where the resistor 97 and the capacitor 98 are serially connected is input to the inverted input terminal of the differential amplifier 84. The output signal of the inverter 101 is supplied to another circuit as the oscillating output signal S_s and is fed back to the SC circuit 10 through a line 102.

In this embodiment, the three differential amplifiers 31, 81 and 84 operate at a voltage between the positive power supply voltage V_{DD} and the negative power supply voltage whose absolute value is equal to V_{DD} . The voltage at the ground is set to 0 V which is intermediate between V_{DD} and V_{SS} .

Now the operation of the Schmitt-type oscillating circuit 83 in the embodiment will first be described. Suppose that the resistance ratio of the resistors 85 and 86 and the threshold voltage V_H obtained at the point c corresponding to the output voltage V_0 from the voltage buffer amplifier 80 are fixed, and that the voltage V_H is higher than the threshold voltage V_L obtained at the point d corresponding to the resistance ratio of the resistors 90 and 91. If the level of the output signal of the differential amplifier 84 is high (V_{DD} level), the level of the output signal of the inverter 96 becomes high, so that the capacitor 98 discharges through the resistor 97 at the time constant τ corresponding to the resistor 97 and the capacitor 98. Thus, the voltage at the point e raises gradually. On the other hand, when the level of the output signal of the inverter 96 is high, the CMOS switch 89 turns on. Therefore, a high level threshold voltage V_H is input to the non-inverted input terminal of the differential amplifier 84. The differential amplifier 84 compares the threshold voltage V_H and the voltage at the point e. When the voltage at the point e reaches the threshold voltage V_H , the output signal of the differential amplifier 84 is inverted from a high level to a low level (V_{SS} level). After the level inversion, the output signal of the inverter 96 is also inverted into two levels, and the capacitor 98 which has been charged now discharges with the time constant τ to the V_{SS} level through the resistance 97. Therefore, the voltage at the point e then lowers gradually. On the other hand, when the output signal of the inverter 96 is at a low level, the CMOS switch 94 turns on and the lower level threshold voltage V_L is input to the non-inverted input terminal of the differential amplifier 84 through the CMOS switch 94. Thus, the differential amplifier 84 compares the threshold value V_L with the voltage at the point e. As a result, the lowering voltage at the point e reaches the threshold value V_L , and the output signal of the differential amplifier 84 is again inverted to a high level. As described above, the differential amplifier 84 alternatively compares the voltage at the point e with the threshold voltage V_H and the threshold voltage V_L . Therefore, the output signal of the inverter 96 becomes an oscillating signal in which a high level and a low level are repeated alternatively. Furthermore, the output signal S_s of the inverter 101 is also the oscillating signal as it is the inverted signal through the inverter 96. The frequency f_s of the oscillating signal S_s of the Schmitt-type oscillator 83 is constant when the threshold voltages V_H and V_L are constant. The value f_s corresponds to the Schmitt width ($|V_H| + |V_L|$) determined by the threshold voltages V_H and V_L , and the time constant τ is determined by the resistor 97 and the capacitor 98.

Fig. 12 is a waveform showing the relation of the voltage V_e at the point e and the output voltage $\overline{S_s}$ of the inverter 96.

On the other hand, the equivalent resistance R_1 of the SC circuit 10, to which the oscillating signal S_s from the Schmitt-type oscillating circuit 83 is input, is given by the equation (1) when the value of the capacitor 11 is C_1 , as shown in Fig. 2.

Similarly, the equivalent resistance R_2 of the SC circuit 20, to which the signal S_c is input, is given by the equation (2) when the value of the capacitor 21 is C_2 .

As the positive voltage from the DC power supply V_1 or variable DC power supply V_2 is supplied to one terminal of the SC circuits 10 and 20, that is, the other terminal of the switch 13 in the SC circuit 10 and the other terminal of the switch 22 in the SC circuit 20, direct current flows in the SC circuits 10 and 20, respectively. On the other hand, as the SC circuit 10 has a negative equivalent resistance R_1 , the direction of the current I_1 flowing in the SC circuit 10 is to the left (negative direction) in Figs. 11A and 11B. And as other SC circuit 20 has a positive equivalent resistance R_2 , the direction of the current I_2 flowing in the SC circuit 20 is to the right (positive direction) in Figs. 11A and 11B. In other words, the directions of I_1 and I_2 are opposite to each other. The composite current of I_1 and I_2 is supplied to the integrator 30. When the composite current is negative, that is, the current I_1 is greater than the current I_2 , the output voltage V_o of the integrator 30 rises gradually to the positive power supply voltage V_{DD} .

On the contrary, when the composite current of I_1 and I_2 is positive, that is, the current I_2 is greater than the current I_1 , the output voltage V_o of the integrator 30 lowers gradually toward the negative power supply voltage. When the output currents I_1 and I_2 of the SC circuits 10 and 20 are balanced and their composite current becomes 0 during rising and lowering of the output voltage V_o of the integrator 30, the change of the output voltage V_o is ceased and can never be changed thereafter.

Supposed that the value of the DC power supply V_1 and the value of the variable DC power supply V_2 are equally set, and the values C_1 and C_2 of the capacitors 11 and 12 in the SC circuits 10 and 20 are equally set. Then, in the SC circuits 10 and 20 the composite current of I_1 and I_2 becomes 0, and the output voltage V_o of the integrator 30 is fixed to some value when the coincidence between the frequencies f_s and f_c of the signals S_s and S_c is achieved. When value V_o is fixed, the higher threshold voltage V_H formed in the Schmitt-type oscillator 83 is fixed, thereby fixing the Schmitt width ($|V_H| + |V_L|$) and frequency f_s of the oscillating signal S_s .

Now suppose the frequency f_s lowers from the balance between the two frequencies f_s and f_c . When the frequency f_s lowers, the equivalent resistance R_1 of the SC circuit 10 given by the equation (1) becomes greater than before, and thus the absolute value of the current I_1 becomes smaller. The composite current of I_1 and I_2 becomes positive, and the output voltage V_o of the integrator 30 lowers towards V_{SS} . Then, the voltage V_H obtained at the point c in the Schmitt-type oscillator lowers. Therefore, the Schmitt width ($|V_H| + |V_L|$) is narrower, thereby raising the frequency f_s of the oscillating signal S_s in the Schmitt-type oscillating circuit 83. When frequency f_s rises, the equivalent resistance R_1 of the SC circuit 10 becomes smaller and the absolute value of the current I_1 gradually becomes greater. As a result, the composite current of I_1 and I_2 decreases and becomes 0 when the frequency f_s coinciding with the frequency f_c lowers, and the output voltage V_o of the integrator 30 rises toward V_{DD} until f_s equals f_c . When the output voltage V_o returns to its original value, the rise of the voltage is ceased, and the rise of frequency f_s is also ceased when the frequency f_s of the oscillating signal S_s coincides with the frequency f_c .

Now suppose the frequency f_s rises under the condition that the frequency f_s coincides with the frequency f_c . When the frequency f_s rises, the equivalent resistance R_1 of the SC circuit 10 given by the equation (1) becomes lower, and the absolute value of the current I_1 becomes greater. The composite current of I_1 becomes greater. The composite current of I_1 and I_2 becomes negative, and the output voltage V_o of the integrator 30 rises toward V_{DD} . When the voltage V_o rises, the higher threshold voltage V_H becomes higher than before, and the Schmitt width ($|V_H| + |V_L|$) becomes wider than before. Therefore, the frequency f_s of the oscillating output signal S_s in the Schmitt-type oscillating circuit 83 lowers. When the frequency f_s lowers, the equivalent resistance R_1 of the SC circuit 10 becomes greater, and the absolute value of the current I_1 gradually becomes smaller.

The composite value of the current I_1 and I_2 increases toward 0 from negative and becomes 0 when f_s coincides with f_c . Thus, when the frequency rises, the output voltage V_o of the integrator 30 lowers toward V_{SS} until f_s coincides with f_c . When the output voltage V_o becomes its original value, the lowering of the voltage ceases. And lowering of the frequency f_s is also ceased when the frequency f_s of the oscillating output signal S_s coincides with f_c .

In other words, in this embodiment, the frequency f_s of the oscillating output signal S_s is controlled so as to coincide with the frequency f_c of the signal S_c .

Now the setting of the variable DC power supply V_2 will be explained. When the voltage V_2 is set higher than V_1 , the output current I_2 of the SC circuit 20 becomes greater than before since the equivalent resistance R_2 of the SC circuit 20 is constant. In order to balance the currents I_1 and I_2 and to make the composite current 0, the absolute value of the output current I_1 of the SC circuit 10 must be greater than before.

When the current I_2 becomes greater, the output voltage V_o of the integrator 30 lowers towards V_{SS} , and

thereafter, the frequency f_s of the oscillating output signal of the Schmitt-type oscillator 83 rises. The rise in the frequency f_s continues until the absolute value of the output current I_1 of the SC circuit 10 coincides with the absolute value of the current I_2 . When the voltage V_2 is set higher than the voltage V_1 , the frequency f_s of the oscillating output signal S_s is controlled to be constant at a point higher than the frequency f_c .

When the voltage V_2 is set lower than the voltage V_1 , the output current I_2 of the SC circuit 20 becomes smaller than before. In order to balance the currents I_1 and I_2 and to make the composite current 0, the absolute value of the output current I_1 of the SC circuit 10 must be smaller than before.

When the current I_2 becomes smaller, the output voltage V_0 of the integrator 30 rises toward V_{DD} and, therefore the frequency f_s of the oscillating output signals S_s lowers. The lowering of the frequency f_s continues until the absolute value of output current I_1 of the SC circuit 10 coincides with the absolute value of I_2 . In other words, when V_2 is set lower than V_1 , the frequency f_s of the oscillating output signal S_s is controlled to be lower than f_c .

In this embodiment, the condition where the oscillating frequency f_s becomes stabilized is when the composite current I_1 and I_2 of the SC circuits 10 and 20 becomes 0. Thus, the stabilizing condition is given by:

$$I_1 + I_2 = 0 \quad (7)$$

By substituting the relation of R_1 and R_2 given in the equations (1) and (2) for equation (7), the following equation is obtained:

$$-C_1 \cdot f_s \cdot V_1 + C_2 \cdot f_c \cdot V_2 = 0 \quad (8)$$

From the equation (8), the following equation is obtained:

$$f_s = \frac{C_2}{C_1} \cdot \frac{V_2}{V_1} \cdot f_c \quad \dots (9)$$

As it is assumed that $C_1 = C_2$, f_s equals f_c times V_2/V_1 . Therefore, the signal S_s having the frequency f_s equal an arbitrary multiple of the frequency f_c .

Fig. 13 shows a characteristic of the above embodiment when $C_1 = C_2$. In the figure, the frequency f_s of the oscillating signal S_s is measured on the abscissa and the value of the variable power supply V_2 is measured on the ordinate. As is shown, f_s is related to V_2 linearly.

The equivalent resistances R_1 and R_2 in the SC circuits 10 and 20 are determined only by the frequencies f_s and f_c if $C_1 = C_2$, as shown in the equations (1) and (2). Since the values C_1 and C_2 of the capacitors 11 and 21 can be set with relatively higher accuracy than the resistances, the frequencies f_s and f_c can be converted into resistances R_1 and R_2 with high accuracy. The difference between the resistances R_1 and R_2 is converted into current and then converted into voltage. The oscillating frequency f_s of the Schmitt-type oscillator 83 can be adjusted corresponding to the above voltage. Thus, the frequency f_s can be stably adjusted with high accuracy.

In the above embodiment, the adjustment of the oscillating frequency f_s is performed by varying the value of the variable DC power supply V_2 . That is, as is apparent from the equation (8), the values C_1 and C_2 of the capacitors 11 and 21 in the SC circuits 10 and 20 are changed, and a multiple frequency corresponding to the ratio of C_1 and C_2 is produced. For example, by setting the C_1 and C_2 as $n \cdot C_1 = C_2$, the frequency f_s can be adjusted to be a frequency n times as much as the frequency f_c . Furthermore, the n must not be an integer but may be a real number including a decimal. This applies to when the adjustment of the frequency f_s is performed by changing the variable DC power supply V_2 . Furthermore, V_1 may be a variable power supply instead of V_2 .

Fig. 14 is a block diagram showing another embodiment of the oscillator circuit. In the embodiment, a frequency divider 110 is added to the embodiment of Figs. 11A and 11B. The frequency divider 110 divides the oscillating output signal S_s of the Schmitt-type oscillator 83 into $1/n$. The SC circuit 10 is controlled by the $1/n$ divided signal S'_s in stead of the oscillating signal S_s .

According to the above construction, the frequency f_s of the oscillating output signal S_s is controlled to be constant at a frequency n times as much as the frequency f_s in the embodiment of Figs. 11A and 11B.

Fig. 15 is a circuit diagram showing an example of the frequency divider 110 in Fig. 14 in detail. The

frequency divider 110 in this embodiment frequency divides the oscillating output signal by 1/8. The divider 110 is a known circuit and comprises three D-type flip-flops 111 through 113. Each data input terminal D of the flip-flops 111 through 113 is connected to the respective first output terminal $\bar{Q}$, and each second output terminal Q in the previous stage is connected to each clock input terminal cp in the next stage. The oscillating output signal S_s from the Schmitt-type oscillator 83 is supplied to the clock input terminal of the flip-flop 111 in the first stage and, the 1/8 frequency-divided signal S'_s is output from the second output terminal of the flip-flop 113 in the final stage. The division ratio can be modified by adjusting the number of flip-flops.

Fig. 16 is a block diagram showing an embodiment of the present invention. This embodiment further comprises the frequency divider 110 in Fig. 14 and two synchronizing circuits 120A and 120B. The frequency divider 110 is constructed the same as that in Fig. 15 and frequency divides the oscillating signal S_s by 1/8 to produce the signal S'_s . The synchronizing circuit 120A synchronizes the 1/8 frequency-divided signal S'_s with the signal S_s , which is not frequency divided. The SC circuit 10 is controlled by the output signal S'_{so} of the synchronizing circuit 120A. The synchronizing circuit 120B synchronises the reference signal S_c with the oscillating signal S_s of the Schmitt-type oscillator 83. The SC circuit 20 is controlled by the output signal S_{co} of the synchronizing circuit 120B.

Fig. 17 shows the synchronizing circuits 120A and 120B in Fig. 16 in detail. The synchronizing circuits 120A and 120B are the same in construction but different in their input signals. The oscillating signal S_s from the Schmitt-type oscillator 83 is supplied to the clock input terminals (cp) of the synchronized D-type flip-flops 121 and 122. The frequency-divided signal S'_s from the frequency divider 110 is supplied to the data input terminal D of the synchronizing circuit 120A, and the signal S_c is supplied to the input terminal D of the synchronizing circuit 120B. The signal Q_1 of the output terminal Q of the one flip-flop 121 is supplied to the data input terminal of the other flip-flop 122 and to the inverter 123. The output signal $\bar{Q}_1$ of the inverter 123 is supplied in parallel together with the signal Q_2 from the other flip-flop 122 to a NOR gate 124. The output signal X of the NOR gate 124 is supplied to a NAND gate 127 and a NOR gate 128 through two cascade-connected inverters 125 and 126. The output signal of the inverter 126 is supplied to the NAND gate 127 and NOR gate 128 through four cascade-connected inverters 129 through 132. Furthermore, the output signal of the NAND gate 127 is supplied to the inverter 133. The output signal of the inverter 133 is supplied to the SC circuit 10 as the signal to control the switches 13 and 14 in the SC circuit 10 when the signal to be supplied to the flip-flop 121 is S'_s , and is supplied to the SC circuit 20 as the signal to control the switches 23 and 25 in the S_c circuit 20 when the signal to be supplied to the flip-flop 121 is S_c . The output signal of the NOR gate 128 is supplied to the SC circuit 10 as the signal to control the switches 12 and 15 in the SC circuit 10 when the signal to be supplied to the flip-flop 121 is S'_s and is supplied to the SC circuit as the signal to control the switches 22 and 24 in the SC circuit 20 when the control S_c to be supplied to the flip-flop 121 is S_c .

The synchronizing circuits 120A and 120B as shown in Fig. 17 operate as follows. Suppose that the signal S'_s has the phase distortion as shown in Fig. 18B against the oscillating output signal S_s (Fig. 18A) from the Schmitt-type oscillator 83. The flip-flops 121 and 122 set the levels of the output signal Q_1 and Q_2 in Figs. 18C and 18D to those of the input signals in synchronism with the leading edge of the clock input signal, that is, the signal S_s , and holds the previous output level at the trailing edge of the signal S_s . Therefore, the output signals Q_1 and Q_2 vary as shown in Figs. 18C and 18D. Thus, the pulse signal is obtained as the output signal X (Fig. 18F) of the NOR gate 124, which is synchronized with the signal S_s and is at a high level during one period of the signal S_s . Using the delayed time obtained by the inverters 129 through 132. The circuit which comprises the inverters 129 through 132 to which the signal X is supplied (the inverter 133, NAND gate 127 and NOR gate 128) forms from the signal X a pair of signals S'_{so1} and S'_{so2} , as shown in Figs. 18G and 18H, corresponding to the two phase signals S_{s1} and S_{s2} , as shown in Figs. 6A and 6B, with high level durations which do not overlay each other. The switches 12 and 15 in the S_c circuit 10 controlled by the signal S'_{so1} turn on for nearly one cycle of the signal S_s . In other words, the duration the positive charge flows into the SC circuit 10 is set to the duration corresponding to nearly one cycle of the signal S_s . Also in the synchronizing circuit 120B to which the signal S_c is supplied as the input signal, a pulse signal is obtained which is in synchronism with the signal S_s and is at a high level during one cycle of the signal S_s as the output signal X of the NOR gate 124. Furthermore, a pair of signals S_{co1} and S_{co2} are formed corresponding to the two-phase signals S_{c1} and S_{c2} as shown in Figs. 6A and 6B.

The switches 22 and 24 in the SC circuit 20 controlled by the signal corresponding to the signal S'_{so1} in Fig. 18G turn on for nearly one cycle of the signal S_s . That is, the duration for the positive charge flowing out from the SC circuit 20 is set to nearly one cycle of the signal S_s as in the case of the SC circuit 10. Therefore, the embodiment of Fig. 16 satisfies the equation (8), thereby preventing the generation of an

oscillating frequency error when the oscillating frequency is relatively large. As shown in Figs. 18G and 18H, the high level durations of the signal S'_{so1} and S'_{so2} (or S'_{co1} and S'_{co2}) are not overlaid. Therefore, the switches 12 and 15 and the switches 13 and 14 are not simultaneously turned on, and a difference between an ideal value and a measured value of the current I_1 is not generated. This applies also to the SC circuit 20.

The present invention is not limited to the above embodiments but various modifications can be performed. For example, in the embodiments of Figs. 11A, 11B, 14 and 16, the oscillating circuit in which the oscillating frequency is controlled by the composite current of the output currents of the SC circuits 10 and 20 is a Schmitt-type oscillating circuit 83. However, any type of oscillating circuits having the same function may be used. Further in the above embodiment, the SC circuit 10 having negative equivalent resistance is controlled by the signal S_a , and the SC circuit 20 having positive equivalent resistance is controlled by the signal S_c . However, these signals are interchangeable.

Claims

1. An oscillator circuit, comprising:

first means (10) comprised of a switched capacitor circuit and having negative equivalent resistance, the value of which is determined according to the frequency of a first signal;

second means (20) comprised of a further switched capacitor circuit and having positive equivalent resistance, the value of which is determined according to the frequency of a second signal;

third means (VV1, VV2) for supplying DC voltages to said first and second means (10, 20);

fourth means (30) for integrating composite current of the output currents of said first and second means (10, 20), and

fifth means (83) for producing an oscillating signal whose frequency is adjusted according to the integrated composite current value produced from said fourth means (30), said fifth means (83) comprising a voltage controlled oscillator whose one input terminal is supplied sequentially with first and second threshold voltages, one of the threshold voltages being dependent on the integrated composite current value produced from said fourth means (30), so that the oscillating frequency of said voltage controlled oscillator is dependent on the values of the first and second threshold voltages;

characterized by

sixth means (110) for frequency-dividing the oscillating signal; seventh means (120A) for synchronizing the frequency-divided signal with the oscillating signal, for controlling a pulse duration of the frequency-divided signal, and for supplying the synchronized and pulse-duration controlled signal to said first or second means (10, 20) as the first or the second signal, respectively; and

eighth means (120B) for synchronizing the second signal with the oscillating signal, for controlling a pulse duration of the second signal, and for supplying the synchronized and pulse-duration controlled second signal to said second or first means (20, 10).

2. An oscillator circuit according to claim 1, characterized in that said fourth means comprises (30) a differential amplifier (31) and a capacitor (32) for integration connected to the input and output terminals of said differential amplifier (31).

3. An oscillator circuit according to claim 1 or 2, characterized in that said third means comprises: a DC voltage supply (VV1) for supplying a DC voltage to one of said first and second means (10, 20), and a variable DC power supply (VV2) for supplying a DC voltage to the other of said first and second means (10, 20) for adjusting the frequency of the oscillating signal produced from said fifth means (83).

4. An oscillator circuit according to claim 1, characterized in that said sixth means (102) includes a frequency divider (110) for frequency-dividing the oscillating signal and for feeding the frequency-divided signal to said first or second means (10, 20) as the first signal.

Patentansprüche

1. Oszillatorschaltung mit:

einer ersten Einrichtung (10), die aus einer geschalteten Kondensatorschaltung besteht und einen negativen Ersatzwiderstand hat, dessen Wert gemäß der Frequenz eines ersten Signals bestimmt ist;

einer zweiten Einrichtung (20), die aus einer weiteren Schaltkondensatorschaltung besteht und einen positiven Ersatzwiderstand hat, dessen Wert gemäß der Frequenz eines zweiten Signals be-



oscillating frequency error when the oscillating frequency is relatively large. As shown in Figs. 18G and 18H, the high level durations of the signal S'_{so1} and S'_{so2} (or S'_{co1} and S'_{co2}) are not overlaid. Therefore, the switches 12 and 15 and the switches 13 and 14 are not simultaneously turned on, and a difference between an ideal value and a measured value of the current I_1 is not generated. This applies also to the SC circuit 20.

The present invention is not limited to the above embodiments but various modifications can be performed. For example, in the embodiments of Figs. 11A, 11B, 14 and 16, the oscillating circuit in which the oscillating frequency is controlled by the composite current of the output currents of the SC circuits 10 and 20 is a Schmitt-type oscillating circuit 83. However, any type of oscillating circuits having the same function may be used. Further in the above embodiment, the SC circuit 10 having negative equivalent resistance is controlled by the signal S_s , and the SC circuit 20 having positive equivalent resistance is controlled by the signal S_c . However, these signals are interchangeable.

Claims

1. An oscillator circuit, comprising:

first means (10) comprised of a switched capacitor circuit and having negative equivalent resistance, the value of which is determined according to the frequency of a first signal:

second means (20) comprised of a further switched capacitor circuit and having positive equivalent resistance, the value of which is determined according to the frequency of a second signal;

third means (VV1, VV2) for supplying DC voltages to said first and second means (10, 20);

fourth means (30) for integrating composite current of the output currents of said first and second means (10, 20), and

fifth means (83) for producing an oscillating signal whose frequency is adjusted according to the integrated composite current value produced from said fourth means (30), said fifth means (83) comprising a voltage controlled oscillator whose one input terminal is supplied sequentially with first and second threshold voltages, one of the threshold voltages being dependent on the integrated composite current value produced from said fourth means (30), so that the oscillating frequency of said voltage controlled oscillator is dependent on the values of the first and second threshold voltages;

characterized by

sixth means (110) for frequency-dividing the oscillating signal; seventh means (120A) for synchronizing the frequency-divided signal with the oscillating signal, for controlling a pulse duration of the frequency-divided signal, and for supplying the synchronized and pulse-duration controlled signal to said first or second means (10, 20) as the first or the second signal, respectively; and

eighth means (120B) for synchronizing the second signal with the oscillating signal, for controlling a pulse duration of the second signal, and for supplying the synchronized and pulse-duration controlled second signal to said second or first means (20, 10).

2. An oscillator circuit according to claim 1, characterized in that said fourth means comprises (30) a differential amplifier (31) and a capacitor (32) for integration connected to the input and output terminals of said differential amplifier (31).

3. An oscillator circuit according to claim 1 or 2, characterized in that said third means comprises: a DC voltage supply (VV1) for supplying a DC voltage to one of said first and second means (10, 20), and a variable DC power supply (VV2) for supplying a DC voltage to the other of said first and second means (10, 20) for adjusting the frequency of the oscillating signal produced from said fifth means (83).

4. An oscillator circuit according to claim 1, characterized in that said sixth means (102) includes a frequency divider (110) for frequency-dividing the oscillating signal and for feeding the frequency-divided signal to said first or second means (10, 20) as the first signal.

Patentansprüche

1. Oszillatorschaltung mit:

einer ersten Einrichtung (10), die aus einer geschalteten Kondensatorschaltung besteht und einen negativen Ersatzwiderstand hat, dessen Wert gemäß der Frequenz eines ersten Signals bestimmt ist;

einer zweiten Einrichtung (20), die aus einer weiteren Schaltkondensatorschaltung besteht und einen positiven Ersatzwiderstand hat, dessen Wert gemäß der Frequenz eines zweiten Signals be-



stimmt ist;

einer dritten Einrichtung (VV1, VV2) zum Liefern von Gleichspannungen an die erwähnte erste und zweite Einrichtung (10, 20);

einer vierten Einrichtung (30) zum Integrieren des zusammengesetzten Stroms aus den Ausgangsströmen der erwähnten ersten und zweiten Einrichtung (10, 20), und

einer fünften Einrichtung (83) zum Erzeugen eines Schwingensignals, dessen Frequenz gemäß dem Wert des integrierten zusammengesetzten Stroms eingestellt ist, der von der erwähnten fünften Einrichtung (83) erzeugt wird, die einen spannungsgesteuerten Oszillator aufweist, an dessen eine Eingangsklemme sequentiell erste und zweite Schwellenspannungen angelegt werden, wobei eine der Schwellenspannungen vom Wert des integrierten zusammengesetzten Stroms abhängig ist, der von der erwähnten vierten Einrichtung (30) erzeugt wird, so daß die Schwingfrequenz des erwähnten spannungsgesteuerten Oszillators von den Werten der ersten und zweiten Schwellenspannungen abhängt;

gekennzeichnet durch

eine sechste Einrichtung (110) zur Frequenzteilung des Schwingensignals;

eine siebte Einrichtung (120A) zum Synchronisieren des frequenzgeteilten Signals mit dem Schwingensignal zum Steuern einer Impulsdauer des frequenzgeteilten Signals und zum Liefern des synchronisierten und impulsdauer gesteuerten Signals an die erste oder zweite Einrichtung (10, 20) als das erste bzw. das zweite Signal; und

eine achte Einrichtung (120B) zum Synchronisieren des zweiten Signals mit dem Schwingensignal zum Steuern einer Impulsdauer des zweiten Signals und zum Liefern des synchronisierten und impulsdauer gesteuerten zweiten Signals an die erwähnte zweite oder erste Einrichtung (20, 10).

2. Oszillatorschaltung nach Anspruch 1, dadurch gekennzeichnet, daß die erwähnte vierte Einrichtung (30) aus einem Differenzverstärker (31) und einem Kondensator (32) zum Integrieren besteht, der mit der Eingangs- und der Ausgangsklemme des erwähnten Differenzverstärkers (31) verbunden ist.

3. Oszillatorschaltung nach Anspruch 1 oder 2, dadurch gekennzeichnet, daß die erwähnte dritte Einrichtung aufweist;

eine Gleichspannungsversorgung (VV1) zum Liefern einer Gleichspannung an eine der erwähnten ersten und zweiten Einrichtung (10, 20), und

eine veränderliche Gleichstromversorgung (VV2) zum Liefern einer Gleichspannung an die andere der erwähnten ersten und zweiten Einrichtung (10, 20) zum Einstellen der Frequenz des Schwingensignals, das von der erwähnten fünften Einrichtung (83) erzeugt wird.

4. Oszillatorschaltung nach Anspruch 1, dadurch gekennzeichnet, daß die erwähnte sechste Einrichtung (102) einen Frequenzteiler (110) zur Teilung der Frequenz des Schwingensignals und zum Zuführen des frequenzgeteilten Signals an die erwähnte erste oder zweite Einrichtung (10, 20) als erstes Signal enthält.

Revendications

1. Un circuit oscillateur, comprenant :

des premiers moyens (10) constitués par un circuit à capacités commutées et ayant une résistance équivalente négative dont la valeur est déterminée conformément à la fréquence d'un premier signal;

des seconds moyens (20) constitués par un circuit à capacités commutées supplémentaire, et ayant une résistance équivalente négative dont la valeur est déterminée conformément à la fréquence d'un second signal;

des troisièmes moyens (VV1, VV2) qui sont destinés à appliquer des tensions continues aux premiers et seconds moyens (10, 20);

des quatrièmes moyens (30) qui sont destinés à intégrer un courant composite formé par les courants de sortie des premiers et seconds moyens (10, 20), et

des cinquièmes moyens (83) destinés à produire un signal oscillant dont la fréquence est réglée conformément à la valeur du courant composite intégré que produisent les quatrièmes moyens (30), ces cinquièmes moyens (83) comprenant un oscillateur commandé par tension dont une borne d'entrée reçoit séquentiellement des première et seconde tensions de seuil, l'une des tensions de seuil dépendant de la valeur du courant composite intégré que produisent les quatrièmes moyens (30), de façon que la fréquence d'oscillation de l'oscillateur commandé par tension dépende des valeurs des première et seconde tensions de seuil;



caractérisé par

des sixièmes moyens (110) destinés à effectuer une division de fréquence du signal oscillant;

des septièmes moyens (120A) destinés à synchroniser le signal à fréquence divisée avec le signal oscillant, pour commander une durée d'impulsion du signal à fréquence divisée, et pour appliquer aux premiers ou seconds moyens (10, 20) le signal synchronisé et à durée d'impulsion commandée, respectivement sous la forme du premier ou du second signal; et

des huitièmes moyens (120B) qui sont destinés à synchroniser le second signal avec le signal oscillant, pour commander une durée d'impulsion du second signal, et pour appliquer aux seconds ou premiers moyens (20, 10) le second signal synchronisé et à durée d'impulsion commandée.

2. Un circuit oscillateur selon la revendication 1, caractérisé en ce que les quatrièmes moyens (30) comprennent un amplificateur différentiel (31) et un condensateur (32) pour l'intégration, connecté aux bornes d'entrée et de sortie de l'amplificateur différentiel (31).

3. Un circuit oscillateur selon la revendication 1 ou 2, caractérisé en ce que les troisièmes moyens comprennent :

une source de tension continue (VV1) qui est destinée à appliquer une tension continue aux premiers moyens ou aux seconds moyens (10, 20), et

une source de tension continue variable (VV2) qui est destinée à appliquer une tension continue aux autres moyens parmi les premiers et les seconds moyens (10, 20), pour régler la fréquence du signal oscillant que produisent les cinquièmes moyens (83).

4. Un circuit oscillateur selon la revendication 1, caractérisé en ce que les sixièmes moyens (102) comprennent un diviseur de fréquence (110) qui est destiné à diviser la fréquence du signal oscillant et à appliquer le signal à fréquence divisée aux premiers ou aux seconds moyens (10, 20), sous la forme du premier signal.