

Description

This invention relates to systems for optimizing the performance of a plurality of steam turbines.

Typically, optimization of the performance of a plurality of energy conversion devices, such as steam turbines, is achieved only through the use of computers and extensive computer programs. Such computer systems have some inherent disadvantages. For example, the computer programs usually use a "high level" language which requires expensive hardware and software to implement. Such a "high level" language usually results in a relatively long processing time for determining operation optimization. In addition, such computer systems typically require highly trained personnel to program and operate same. Thus, the computer system that is required for the optimization calculations is very costly to install and operate, and may not react to changes in the operation of the turbines as rapidly as desired.

Because of the foregoing, it has become desirable to develop a system for optimizing the operation of a plurality of steam turbines without the use of a computer system.

International (PCT) Patent Application Publication No. WO 82/03133 discloses control apparatus for use in multiple steam generator multiple hot water generator installations. To maximise the efficiency of the installation in the case of a particular load demand, the number of generators that are on line is minimized and the load requirement is then allocated among the generators that remain on line such that maximum efficiency is achieved.

According to the present invention there is provided a system for optimizing the performance of a plurality of multi-stage steam turbines, the system comprising:

means for measuring the steam output flow from the multi-stages of the steam turbines and establishing a plurality of steam output signals;

means for measuring the steam input flow to the steam turbines and establishing a plurality of steam input signals;

means for measuring the output power produced by the steam turbines and establishing a plurality of output power signals;

limit setting means responsive to the plurality of output power signals, the plurality of steam input signals and the plurality of steam output signals for establishing steam output logic signals, steam input logic signals and output power logic signals that are representative of whether or not the steam output signals, the steam input signals and the output power signals, respectively, are within preset limits;

limit sequencing means responsive to said logic signals established by the limit setting means for establishing for each turbine stage, further logic signals whose values vary in accordance with the values of associated ones of the logic signals established by the limit setting means;

means for measuring the efficiency of each of the multi-stages of the steam turbines and establishing a plurality of efficiency signals;

means for establishing a load increase limit signal in response to the signals established by the efficiency measuring means and the limit sequencing means;

pressure measuring means for measuring the pressure of the outputs of the turbines and establishing a signal indicative thereof; and

load allocation means responsive to the signals established by the pressure measuring means and the load increase limit establishing means for assigning a decrease in load demand to the lowest efficiency turbine and an increase in load demand to the highest efficiency turbine.

A preferred embodiment of the present invention described hereinbelow solves or at least alleviates the aforementioned problems associated with the prior art by utilizing function blocks having fixed functional relations to provide calculating features, which are generally only available through the use of computers, to determine the manner in which the steam turbines should be loaded to effect optimization of the overall system. Measurements of fluid flow into and out of the turbines, the power produced by the turbines, and the efficiencies of the turbine stages are processed through the use of function blocks to determine the efficiencies of the extraction flows. When there is a decrease in load demand, the load is assigned to the extraction flow with the lowest overall efficiency, whereas when there is an increase in load demand, the load is assigned to the extraction flow with the highest efficiency. In this manner, the efficiency of the overall system is optimized.

The invention will now be further described, by way of illustrative and non-limiting example, with reference to the accompanying drawings, in which:

Figure 1 is a schematic diagram of a system comprising two turbines whose operation are to be optimized;

Figure 2 is a schematic diagram of logic utilized by a system embodying the invention to effect optimization of the system illustrated in Figure 1;

Figure 3 is a schematic diagram of function blocks which comprise a limit setting module of Figure 2;

Figure 4 is a plurality of graphs illustrating the output of function generators illustrated in Figure 3;

Figure 5 is a schematic diagram of function block which comprise a limit sequence module of Figure 2;

Figure 6 is a schematic diagram of function blocks which comprise a load limit module of Figure 2;

Figure 7 is a schematic diagram of function blocks which comprise low and high selectors and a load allocation module of Figure 2;

Figure 8 is a schematic drawing of function blocks which comprise an optimum loading module of Figure 7; and

Figure 9 is a graph illustrating the output of the function generator illustrated in Figure 8.

Referring now to the drawings, Figure 1 is a schematic diagram of a pair of multi-stage turbines 10, 12 showing their respective connections to an input steam supply conduit 14, extraction flow conduits 16, 18, and steam condenser conduit 20. By-pass valves 22, 24 are provided between the supply conduit 14 and extraction flow conduit 16, and between the extraction flow conduits 16 and 18, respectively. In one instance the objective is to optimize performance of the turbines 10, 12 based upon steam demand. In this case, the demands of the extraction flows X_m and X_1 of conduits 16 and 18 are specified and the power outputs W_1 and W_2 of the respective turbines 10, 12 are optimized so as to achieve the maximum output power ($W=W_1+W_2$) therefrom. In this instance, during normal operating conditions the extraction flow X_e through conduit 20 and the steam flows X_{pm} and X_{p1} through valves 22 and 24, respectively, should be zero. When the extraction flows from the turbines 10, 12 reach their limits, any additional steam demands are met by the opening of the by-pass valves 22 and 24. In another instance, the objective is to optimize performance of the turbines 10, 12 based upon megawatt demand. In this case, the megawatt demand $W=W_1+W_2$ is specified and the overall steam usage is minimized while the steam needs of X_m and X_1 of conduits 16 and 18 are satisfied. In this instance, during normal operating conditions the steam flows X_{pm} and X_{p1} through valves 22 and 24, respectively, should be zero. Here again, when the extraction flows from the turbines 10, 12, reach their limits, any additional steam demands are satisfied by the opening of the valves 22 and 24.

Referring now to Figure 2, which is a schematic diagram of the logic utilized to effect optimization of the operation of the turbines, measurements of steam flow X and power output W are used as inputs to a limit setting module 26. The function blocks comprising this module 26 are shown in Figure 3. In this Figure, flow transmitters 28 are provided to measure the output flows X_{1m} , X_{2m} ... from each stage of the turbines 10, 12 and power transmitters 30 are provided to measure the respective output power W_1 , W_2 produced by each of these turbines. In addition, flow transmitters 32 and 34 are provided to measure the flow into the turbines and through the by-pass valves, respectively. Considering only the turbine 10, the output flow from the first stage thereof, i.e., output flow X_{1m} , as measured by flow transmitter 28, is applied to the negative input to a subtraction function block 36. The other input to the subtraction function block 36, which is applied to the positive input thereto, is a preset maximum limit for output flow from this turbine stage. The output of this subtraction function block 36 is used as the input to a function generator 38 which produces an output signal $\hat{F}_{1m}(\Delta)$, as shown in Figure 4, equal to zero when the output of the subtraction function block 36 is negative, thus indicating that the output flow from the first turbine stage is above the preset maximum limit, and produces an output signal $\hat{F}_{1m}(\Delta)$ equal to positive one when the output of the function block 36 is positive, this indicating that the output flow from the first turbine stage is below the preset maximum limit.

The output flow from the first stage of turbine 10, i.e., output flow X_{1m} , as measured by flow transmitter 28, is also applied to the positive input to a subtraction function block 40. The other input to this function block 40 is a preset minimum limit for output flow from this turbine stage, and this minimum limit is applied to the negative input to this function block 40. The output of this function block is used as the input to a function generator 42 which produces an output signal $\hat{F}_{1m}(\Delta)$, as shown in Figure 4, equal to a large positive number G when the output of the subtraction function block 40 is negative, this indicating that the output flow from the first turbine stage is below the preset minimum limit, and produces an output signal $\hat{F}_{1m}(\Delta)$ equal to positive one when the output of the function block 40 is positive, thus indicating that the output flow from the first turbine stage is above the preset minimum limit.

Again considering only turbine 10, the input flow thereto, i.e., X_{1i} , as measured by the flow transmitter 32, is applied to the negative input to a subtraction function block 44. The other input to this function block 44, which is applied to the positive input thereto, is a preset maximum limit for input flow into this turbine. The output of this function block 44 is used as the input to a function generator 46 which produces an output signal $\hat{F}_{1i}(\Delta)$, as shown in Figure 4, equal to zero when the output of the subtraction function block 44 is negative, thus indicating that the input flow into the turbine 10 is above the preset maximum limit, and produces an output signal $\hat{F}_{1i}(\Delta)$ equal to positive one when the output of the function block 44 is positive, thus indicating that the input flow to the turbine 10 is below the preset maximum limit.

The input flow to the turbine 10, i.e. X_{1i} , as measured by the flow transmitter 32, is also applied to the positive input to a subtraction function block 48. The other input to this function block 48 is a preset minimum limit for input flow to this turbine 10, and this minimum limit is applied to the negative input to this function block 48. The output of this function block 48 is used as the input to a function generator 50 which produces an output signal $\hat{F}_{1i}(\Delta)$, as shown in Figure 4, equal to a large positive number G when the output of the subtraction function block 48 is negative, thus indicating that the input flow into the turbine 10 is below the preset minimum limit, and produces an output signal $\hat{F}_{1i}(\Delta)$ equal to positive one when the output of the function block 48 is positive, thus indicating that the input flow into the turbine is above the preset minimum limit.

As noted in Figure 3, the foregoing approach can be used to find $\hat{F}_{2m}(\Delta)$ and $\hat{F}_{2m}(\Delta)$ for the output flow from the first stage of turbine 12, $\hat{F}_{2i}(\Delta)$ and $\hat{F}_{2i}(\Delta)$ for the input flow to turbine 12, $\hat{F}_{pm}(\Delta)$ and $\hat{F}_{pm}(\Delta)$ for the flow through by-pass valve 22, $\hat{F}_{w1}(\Delta)$ and $\hat{F}_{w1}(\Delta)$ for the power produced by turbine 10, and $\hat{F}_{w2}(\Delta)$ and

$\hat{F}_{w2}(\Delta)$ for the power produced by turbine 12. In each case, if the parameters are within the preset limits, the foregoing output signals are equal to positive one.

Referring to Figure 2, the foregoing output signals produced by the limit setting module 26 are applied as inputs to a limit sequence module 52. The function blocks comprising this limit sequence module 52 are shown in Figure 5. As shown in this Figure, the output signal $\hat{F}_{1m}(\Delta)$ produced by the function generator 42 is used as an input to a multiplication function block 54 whose other input is the output signal $\hat{F}_{1t}(\Delta)$ produced by the function generator 50. The output signal produced by the multiplication function block 54 is used as an input to a multiplication function block 56 whose other input is the signal $\hat{F}_{w1}(\Delta)$ which represents the low limit for the power produced by the turbine 10. Similarly, the output signal $\hat{F}_{1m}(\Delta)$ produced by the function generator 38 is used as an input to a multiplication function block 58 whose other input is the output signal $\hat{F}_{1t}(\Delta)$ produced by the function generator 46. The output signal produced by the multiplication function block 58 is used as an input to a multiplication function block 60 whose other input is the signal $\hat{F}_{w1}(\Delta)$ which represents the high limit for the power produced by the turbine 10.

Assuming that the input flow to the turbine and the power produced by the turbine are within the preset maximum and minimum limits, i.e., input signals $\hat{F}_{1t}(\Delta)$, $\hat{F}_{1t}(\Delta)$, $\hat{F}_{w1}(\Delta)$ and $\hat{F}_{w1}(\Delta)$ are all equal to a positive one, then the output signals produced by multiplication function blocks 56 and 60 are as follows:

	Output of function block 56 [$\hat{F}_{1m}(\Delta)$]	Output of function Block 60 [$\hat{F}_{1m}(\Delta)$]	Condition
20	G	1	$X_{1m} \leq \bar{X}_{1m}$
	1	1	$\bar{X}_{1m} < X_{1m} < \hat{X}_{1m}$
25	1	0	$X_{1m} \geq \hat{X}_{1m}$

It should be noted that the foregoing analysis, with similar results, can be obtained for $\hat{F}_{2m}(\Delta)$ and $\hat{F}_{2m}(\Delta)$ for the output flow from the first stage of the turbine 12.

As shown in Figure 2, the foregoing output signals produced by the limit sequence module 52 are used as inputs to a load limit module 62. The function blocks comprising this load limit module 62 are shown in Figure 6. As shown in this Figure, the output signal $\hat{F}_{1m}(\Delta)$ produced by the multiplication function block 56 is used as an input to a multiplication function block 64 whose other input is the efficiency η_{t1m} of the first stage of the turbine 10 causing a signal η'_{t1m} to be produced at the output thereof. Similarly, the output signal $\hat{F}_{2m}(\Delta)$ is used as an input to a multiplication function block 66 whose other input is the efficiency η_{t2m} of the first stage of the turbine causing a signal η'_{t2m} to be produced at the output thereof. And, lastly, the signal $\hat{F}_{pm}(\Delta)$ is used as an input to a multiplication function block 68 whose other input is the efficiency η_{pm} of the by-pass valve 22 causing a signal η'_{pm} to be produced at the output thereof. The foregoing output signals η'_{t1m} , η'_{t2m} , and η'_{pm} represent load decrease limiters on demand decrease.

The first stage efficiency η_{t1m} of the turbine 10 is also used as an input to a multiplication function block 70 whose other input is the output signal $\hat{F}_{1m}(\Delta)$ produced by the multiplication function block 60 causing a signal η''_{t1m} to be produced at the output thereof. Similarly, the first stage efficiency η_{t2m} of the turbine 12 is also used as an input to a multiplication function block 72 whose other input is the signal $\hat{F}_{2m}(\Delta)$ causing a signal η''_{t2m} to be produced at the output thereof. And, lastly, the efficiency η_{pm} of the by-pass valve 22 is also used as an input to a multiplication function block 74 whose other input is the signal $\hat{F}_{pm}(\Delta)$ causing a signal η''_{pm} to be produced at the output thereof. The foregoing output signals η'_{t1m} , η'_{t2m} and η'_{pm} represent load increase limiters on demand increase.

Again referring to Figure 2, the foregoing output signals produced by the load limit module 62 are used as inputs to a low and high selector and load allocation module 76. The function blocks comprising this low and high selector and load allocation module 76 are shown in Figure 7. As illustrated in this figure, the output signals η'_{t1m} , η'_{t2m} and η'_{pm} produced by multiplication function blocks 64, 66 and 68, respectively, are used as inputs to a low limit function block 78 which produces an output signal equal to the smallest of the foregoing input signals. This output signal is then applied to the negative inputs to subtraction function blocks 80, 82 and 84 whose positive inputs are connected to the outputs of multiplication function blocks 64, 66 and 68, respectively. In this manner, the value of the smallest of the foregoing input signals, η'_{t1m} , η'_{t2m} and η'_{pm} , is subtracted from each of these input signals to produce a signal $1_m'$, $2_m'$ and pm' at the output of subtraction function blocks 80, 82 and 84, respectively. Inasmuch as the value of the smallest input signal is subtracted from each of the input signals, one of the output signals, $1_m'$, $2_m'$ and pm' , will be zero, while the other two output signals will be positive. The output signal which is zero will be associated with the turbine stage or by-pass valve having the lowest efficiency. Similarly, the output signals η''_{t1m} , η''_{t2m} and η''_{pm} produced by multiplication function blocks 70, 72 and 74, respectively are used as inputs to a high limit function block 86 which produces an output signal equal to the largest of the foregoing input signals. This output signal is then applied to the positive inputs to subtraction function blocks 88, 90 and 92 whose negative inputs are connected to the outputs of multiplication function blocks 70, 72 and 74, respectively. In this manner, each of the input signals, η'_{t1m} , η'_{t2m} and η'_{pm} , is subtracted from the largest of these signals to produce a signal $1_m''$, $2_m''$ and pm'' at the output of subtraction function blocks 88, 90 and 92, respectively.

Inasmuch as each of the input signals is subtracted from the largest of the input signals, one of the output signals, $1m''$, $2m''$ or pm'' , will be zero while the other two output signals will be positive. The output signal which is zero will be associated with the turbine stage or by-pass valve having the highest efficiency.

The low and high selector and load allocation module 76 also includes an optimum loading module 94, and the foregoing output signals, $1m'$, $2m'$, pm' , $1m''$, $2m''$ and pm'' are used as inputs thereto. The function blocks comprising this optimum loading module 94 are shown in Figure 8. As shown in this figure, each of the foregoing input signals is used as an input to a separate function generator 96 which produces an output as shown in Figure 9. If the input signal into the generator 96 is zero, the generator produces a positive one output signal. However, if the input signal is positive, the generator produces a zero output signal. Thus, because of the previous logic employed, the smallest of the input signals $1m'$, $2m'$ and pm' , will cause a positive one to be produced at the output of the respective function generator 96 while the remaining input signals will cause a zero to be produced at the output of the respective function generator 96. Similarly, because of the logic employed, the largest of the input signals, $1m''$, $2m''$ and pm'' , will cause a positive one to be produced at the output of the respective function generator 96 while the remaining two input signals will cause a zero to be produced at the output of the respective function generators 96.

Referring again to Figure 7, a pressure transmitter 98 is provided to measure the pressure of the extraction flow conduit 16. The output of the pressure transmitter 98 is connected to the negative input to a subtraction function block 100 whose positive input is connected to a preset desired pressure. The output (Δp) of the function block 100 becomes positive on a steam demand increase and negative on a steam demand decrease. This output (Δp) of block 100 is connected to the input to the high and low limiters 102 and 104, shown in Figure 8. High and low limiter 102 permits the input Δp as output for a negative Δp and limits the output to zero for other values of Δp input representing a steam demand decrease. In contrast, high and low limiter 104 permits the input Δp as output for a positive Δp input and limits the output to zero for other values of input Δp representing a steam demand increase. The output of limiter 102 is connected to the inputs to multiplication function blocks 106, 108 and 110 which are connected to the function generators 96 for the input signals $1m'$, $2m'$ and pm' . Similarly, the output of limiter 104 is connected to the inputs to multiplication function blocks 112, 114 and 116 which are connected to the function generators 96 for the input signals $1m''$, $2m''$, and pm'' . In this manner, the smallest of the input signals $1m'$, $2m'$ and pm' , will cause a positive Δp to be produced at the output of the multiplication function block (106, 108 or 110) to which it is the input while a zero is produced at the output of the two remaining function blocks. Similarly, the smallest of the input signals $1m''$, $2m''$ and pm'' , will cause a positive Δp to be produced at the output of the multiplication function block (112, 114 or 116) to which it is the input while a zero is produced at the output of the two remaining function blocks. As shown in Figure 7, output signals $1m'$ and $1m''$ produced by multiplication function blocks 106 and 112, respectively, are used as inputs to a summation function block 118 which produces a signal $1m$ at its output; output signals $2m'$ and $2m''$ produced by multiplication function blocks 108 and 114, respectively, are used as inputs to a summation function block 120 which produces a signal $2m$ at its output; and output signals pm' and pm'' produced by multiplication function blocks 110 and 116, respectively, are used as inputs to a summation function block 122 which produces a signal pm at its output. The foregoing output signals, $1m$, $2m$ and pm , are subsequently used as biases for the extraction flows from the turbines 10 and 12 and through the by-pass valve 22. From the foregoing, it is apparent, that in the case of a decrease in load demand, the load is assigned to the extraction flow with the lowest overall efficiency, whereas in the case of an increase in load demand, the load is assigned to the extraction flow with the highest efficiency. The foregoing analysis was based on optimization on steam demand. However, a similar analysis can be undertaken based on megawatt demand with analogous results other than the resulting bias signals will be used to regulate the flow of fluid through the condenser.

Claims

1. A system for optimizing the performance of a plurality of multi-stage steam turbines (10, 12), the system comprising:
 - means (28) for measuring the steam output flow from the multi-stages of the steam turbines (10, 12) and establishing a plurality of steam output signals (X_{1m} , X_{2m} ...);
 - means (32) for measuring the steam input flow to the steam turbines (10, 12) and establishing a plurality of steam input signals (X_{1i} , X_{2i} ...);
 - means (30) for measuring the output power produced by the steam turbines (10, 12) and establishing a plurality of output power signals (W_1 , W_2);
 - limit setting means (26—Figure 3) responsive to the plurality of output power signals (W_1 , W_2), the plurality of steam input signals (X_{1i} , X_{2i}) and the plurality of steam output signals (X_{1m} , X_{2m}) for establishing steam output logic signals ($\hat{F}_{1m}(\Delta)$, $\hat{F}_{1m}'(\Delta)$), steam input logic signals ($\hat{F}_{1i}(\Delta)$, $\hat{F}_{1i}'(\Delta)$) and output power logic signals ($\hat{F}_{w1}(\Delta)$, $\hat{F}_{w1}'(\Delta)$) that are representative of whether or not the steam output signals, the steam input signals and the output power signals, respectively, are within preset limits;
 - limit sequencing means (52—Fig. 5) responsive to said logic signals established by the limit setting means (26) for establishing, for each turbine stage, further logic signals (e.g. $\hat{F}_{1m}''(\Delta)$, $\hat{F}_{1m}'''(\Delta)$) whose values vary in accordance with the values of associated ones of the logic signals established by the limit setting means (26);



(12)

Inasmuch as each of the input signals is subtracted from the largest of the input signals, one of the output signals, $1m''$, $2m''$ or pm'' , will be zero while the other two output signals will be positive. The output signal which is zero will be associated with the turbine stage or by-pass valve having the highest efficiency.

The low and high selector and load allocation module 76 also includes an optimum loading module 94, and the foregoing output signals, $1m'$, $2m'$, pm' , $1m''$, $2m''$ and pm'' are used as inputs thereto. The function blocks comprising this optimum loading module 94 are shown in Figure 8. As shown in this figure, each of the foregoing input signals is used as an input to a separate function generator 96 which produces an output as shown in Figure 9. If the input signal into the generator 96 is zero, the generator produces a positive one output signal. However, if the input signal is positive, the generator produces a zero output signal. Thus, because of the previous logic employed, the smallest of the input signals $1m'$, $2m'$ and pm' , will cause a positive one to be produced at the output of the respective function generator 96 while the remaining input signals will cause a zero to be produced at the output of the respective function generator 96. Similarly, because of the logic employed, the largest of the input signals, $1m''$, $2m''$ and pm'' , will cause a positive one to be produced at the output of the respective function generator 96 while the remaining two input signals will cause a zero to be produced at the output of the respective function generators 96.

Referring again to Figure 7, a pressure transmitter 98 is provided to measure the pressure of the extraction flow conduit 16. The output of the pressure transmitter 98 is connected to the negative input to a subtraction function block 100 whose positive input is connected to a preset desired pressure. The output (Δp) of the function block 100 becomes positive on a steam demand increase and negative on a steam demand decrease. This output (Δp) of block 100 is connected to the input to the high and low limiters 102 and 104, shown in Figure 8. High and low limiter 102 permits the input Δp as output for a negative Δp and limits the output to zero for other values of Δp input representing a steam demand decrease. In contrast, high and low limiter 104 permits the input Δp as output for a positive Δp input and limits the output to zero for other values of input Δp representing a steam demand increase. The output of limiter 102 is connected to the inputs to multiplication function blocks 106, 108 and 110 which are connected to the function generators 96 for the input signals $1m'$, $2m'$ and pm' . Similarly, the output of limiter 104 is connected to the inputs to multiplication function blocks 112, 114 and 116 which are connected to the function generators 96 for the input signals $1m''$, $2m''$, and pm'' . In this manner, the smallest of the input signals $1m'$, $2m'$ and pm' , will cause a positive Δp to be produced at the output of the multiplication function block (106, 108 or 110) to which it is the input while a zero is produced at the output of the two remaining function blocks. Similarly, the smallest of the input signals $1m''$, $2m''$ and pm'' , will cause a positive Δp to be produced at the output of the multiplication function block (112, 114 or 116) to which it is the input while a zero is produced at the output of the two remaining function blocks. As shown in Figure 7, output signals $1m'$ and $1m''$ produced by multiplication function blocks 106 and 112, respectively, are used as inputs to a summation function block 118 which produces a signal $1m$ at its output; output signals $2m'$ and $2m''$ produced by multiplication function blocks 108 and 114, respectively, are used as inputs to a summation function block 120 which produces a signal $2m$ at its output; and output signals pm' and pm'' produced by multiplication function blocks 110 and 116, respectively, are used as inputs to a summation function block 122 which produces a signal pm at its output. The foregoing output signals, $1m$, $2m$ and pm , are subsequently used as biases for the extraction flows from the turbines 10 and 12 and through the by-pass valve 22. From the foregoing, it is apparent, that in the case of a decrease in load demand, the load is assigned to the extraction flow with the lowest overall efficiency, whereas in the case of an increase in load demand, the load is assigned to the extraction flow with the highest efficiency. The foregoing analysis was based on optimization on steam demand. However, a similar analysis can be undertaken based on megawatt demand with analogous results other than the resulting bias signals will be used to regulate the flow of fluid through the condenser.

Claims

1. A system for optimizing the performance of a plurality of multi-stage steam turbines (10, 12), the system comprising:
 - means (28) for measuring the steam output flow from the multi-stages of the steam turbines (10, 12) and establishing a plurality of steam output signals (X_{1m} , X_{2m} ...);
 - means (32) for measuring the steam input flow to the steam turbines (10, 12) and establishing a plurality of steam input signals (X_{1i} , X_{2i} ...);
 - means (30) for measuring the output power produced by the steam turbines (10, 12) and establishing a plurality of output power signals (W_1 , W_2);
 - limit setting means (26—Figure 3) responsive to the plurality of output power signals (W_1 , W_2), the plurality of steam input signals (X_{1i} , X_{2i}) and the plurality of steam output signals (X_{1m} , X_{2m}) for establishing steam output logic signals ($\bar{F}_{1m}(\Delta)$, $\bar{F}_{1m}(\Delta)$), steam input logic signals ($\bar{F}_{1i}(\Delta)$, $\bar{F}_{1i}(\Delta)$) and output power logic signals ($\bar{F}_{w1}(\Delta)$, $\bar{F}_{w1}(\Delta)$) that are representative of whether or not the steam output signals, the steam input signals and the output power signals, respectively, are within preset limits;
 - limit sequencing means (52—Fig. 5) responsive to said logic signals established by the limit setting means (26) for establishing, for each turbine stage, further logic signals (e.g. $\bar{F}_{1m}'(\Delta)$, $\bar{F}_{1m}'(\Delta)$) whose values vary in accordance with the values of associated ones of the logic signals established by the limit setting means (26);



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means for measuring the efficiency of each of the multi-stages of the steam turbines (10, 12) and establishing a plurality of efficiency signals (η_{11m} , η_{12m});

means (62—Figure 6) for establishing a load increase limit signal in response to the signals established by the efficiency measuring means and the limit sequencing means (52);

5 pressure measuring means (98) for measuring the pressure of the outputs of the turbines (10, 12) and establishing a signal indicative thereof; and

load allocation means (76—Figure 7) responsive to the signals established by the pressure measuring means (98) and the load increase limit establishing means (62) for assigning a decrease in load demand to the lowest efficiency turbine and an increase in load demand to the highest efficiency turbine.

10 2. A system according to Claim 1, wherein a decrease in load demand involving a decrease in steam output demand for the system is applied to the turbine output stage having the lowest efficiency of all of the output stages and an increase in load demand involving an increase in steam output demand for the system is applied to the turbine output stage having the highest efficiency of all of the output stages.

3. A system according to Claim 1, wherein said change in load demand involves a change in electrical
15 output demand for the system.

4. A system according to any one of the preceding claims, wherein the load allocation means (76) comprises one or more function blocks arranged in a logic configuration.

Patentansprüche

20 1. System für die Optimierung der Wirksamkeit einer Mehrzahl von mehrstufigen Dampfturbinen (10, 12) mit:

Mitteln (28) zum Messen des Dampfausstoßflusses aus den Mehrfachstufen der Dampfturbinen (10, 12) und Bereitstellen einer Mehrzahl von Dampfausstoßsignalen (X_{1m} , X_{2m} ...); Mitteln (32) zum Messen des
25 Dampfzufuhrflusses zu den Dampfturbinen (10, 12) und Bereitstellen einer Mehrzahl von Dampfeinlaßsignalen (X_{1v} , X_{2v} ...);

Mitteln (30) zum Messen der Leistungsabgabe, welche von den Dampfturbinen (10, 12) erzeugt wird, und Bereitstellen einer Mehrzahl von Leistungsabgabesignalen (W_1 , W_2);

Grenzwerteinstellmitteln (26—Figure 3), welche auf die Mehrzahl von Leistungsabgabesignalen (W_1 , W_2), die Mehrzahl von Dampfeinlaßsignalen (X_{1v} , X_{2v}) und die Mehrzahl von Dampfausstoßsignalen (X_{1m} , X_{2m}) ansprechen, zum Bereitstellen von Logiksignalen für den Dampfausstoß ($\dot{F}_{1m}(\Delta)$, $\dot{F}_{1m}(\Delta)$), Logiksignalen
30 für den Dampfeinlaß ($\dot{F}_{1v}(\Delta)$, $\dot{F}_{1v}(\Delta)$) und Logiksignalen für die Leistungsabgabe ($\dot{F}_{w1}(\Delta)$, $\dot{F}_{w1}(\Delta)$), welche eine Anzeige dafür sind, ob die Dampfausstoßsignale, die Dampfeinlaßsignale bzw. die Leistungsabgabesignale innerhalb der vorher eingestellten Grenzen liegen oder nicht;

Grenzwerteinreihmitteln (52—Figur 5), welche auf die von den Grenzwerteinstellmitteln (26) bereitgestellten Logiksignale ansprechen, um für jede Turbinenstufe weitere Logiksignale (z.B. $\dot{F}_{1m}'(\Delta)$, $\dot{F}_{1m}'(\Delta)$) bereitzustellen, deren Werte entsprechend den Werten der zugehörigen Logiksignale variieren, welche durch die Grenzwerteinstellmittel (26) bereitgestellt werden;

Mitteln zum Messen der Wirksamkeit jeder der Vielfachstufen der Dampfturbinen (10, 12) und
40 Bereitstellen einer Mehrzahl von Effektivitätssignalen (η_{11m} , η_{12m});

Mitteln (62—Figur 6) zum Bereitstellen eines Begrenzungssignals für Belastungsanstieg unter Ansprechen auf die von den Wirksamkeitsmeßmitteln und den Grenzwerteinreihmitteln (52) bereitgestellten Signale;

Druckmeßmitteln (98) zum Messen des Druckes am Ausgangs der Turbinen (10, 12) und Bereitstellen
45 eines Signales, welches diesen anzeigt; und

Belastungszuordnungsmitteln (76—Figur 7), welche auf die Signale ansprechen, welche durch die Druckmeßmittel (98) und die Mittel (62) zur Bereitstellung eines Grenzwertes für den Lastanstieg bereitgestellt werden, um einen Abfall in der Lastanforderung der Turbine mit der geringsten Wirksamkeit und einen Anstieg in der Lastanforderung der Turbine mit der höchsten Wirksamkeit zuzuordnen.

50 2. System nach Anspruch 1, wobei ein Abfall in der Lastanforderung, der eine Abnahme der Anforderung für den Dampfausstoß des Systems beinhaltet, der Turbinenausgangsstufe zugeführt wird, welche die geringste Wirksamkeit von allen Ausgangsstufen hat, und wobei ein Anstieg in der Lastanforderung, der einen Anstieg der Anforderung an den Dampfausstoß des Systems beinhaltet, der Turbinenausgangsstufe zugeführt wird, welche die höchste Wirksamkeit von allen Ausgangsstufen hat.

3. System nach Anspruch 1, wobei die Änderung der Lastanforderung eine Änderung der Anforderung der elektrischen (Energie-) Abgabe für das System beinhaltet.

4. System nach einem der vorstehenden Ansprüche, wobei die Lastzuordnungsmittel (76) einen oder mehrere Funktionsblocks aufweisen, welche in einem logischen Aufbau angeordnet sind.

60 Revendications

1. Un système pour optimiser le fonctionnement d'un ensemble de turbines à vapeur à étages multiples (10, 12), ce système comprenant:

des moyens (28) pour mesurer le débit de sortie de vapeur des étages multiples des turbines à vapeur
65 (10, 12), et pour établir un ensemble de signaux de sortie de vapeur (X_{1m} , X_{2m} ...);



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des moyens (32) pour mesurer le débit d'entrée de vapeur des turbines à vapeur (10, 12) et pour établir un ensemble de signaux d'entrée de vapeur (X_{1n} , X_{2n} ...);

des moyens (30) pour mesurer la puissance de sortie qui est produite par les turbines à vapeur (10, 12) et pour établir un ensemble de signaux de puissance de sortie (W_1 , W_2);

5 des moyens de fixation de limites (26, Figure 3) qui fonctionnent sous la dépendance de l'ensemble de signaux de puissance de sortie (W_1 , W_2), et l'ensemble de signaux d'entrée de vapeur (X_{1n} , X_{2n}) et de l'ensemble de signaux de sortie de vapeur (X_{1m} , X_{2m}), pour établir des signaux logiques de sortie de vapeur ($\bar{F}_{1m}(\Delta)$, $\bar{F}_{1m}(\Delta)$), des signaux logiques d'entrée de vapeur ($\bar{F}_{1n}(\Delta)$, $\bar{F}_{1n}(\Delta)$) et des signaux logiques de puissance de sortie ($\bar{F}_{w1}(\Delta)$, $\bar{F}_{w1}(\Delta)$), qui indiquent respectivement si les signaux de sortie de vapeur, les
10 signaux d'entrée de vapeur et les signaux de puissance de vapeur sont compris ou non entre des limites préétablies;

des moyens de génération de séquence de limites (52, figure 5) qui fonctionnent sous la dépendance des signaux logiques qui sont établis par les moyens de fixation de limites (26) pour établir, pour chaque étant de turbine, des signaux logiques supplémentaires, (par exemple $\bar{F}'_{1m}(\Delta)$, $\bar{F}'_{1m}(\Delta)$) dont les valeurs
15 varient conformément aux valeurs de signaux associés parmi les signaux logiques qui sont établis par les moyens de fixation de limites (26);

des moyens pour mesurer le rendement de chacun des étages multiples des turbines à vapeur (10, 12) et pour établir un ensemble de signaux de rendement (η_{11m} , η_{12m});

des moyens (62, Figure 6) pour établir un signal de limite d'augmentation de charge sous la
20 dépendance des signaux qui sont établis par les moyens de mesure de rendement et par les moyens de génération de séquence de limites (52);

des moyens de mesure de pression (98) pour mesurer la pression aux sorties des turbines (10, 12) et pour établir un signal représentatif de cette pression; et

des moyens d'affectation de charge (76, figure 7) qui fonctionnent sous la dépendance des signaux
25 établis par les moyens de mesure de pression (98) et les moyens d'établissement de limite d'augmentation de charge (62), de façon à affecter une diminution de la demande de charge à la turbine ayant le plus faible rendement, et une augmentation de la demande de charge à la turbine ayant le rendement le plus élevé.

2. Un système selon la revendication 1, dans lequel une diminution de la demande de charge faisant intervenir une diminution de la demande de sortie de vapeur pour le système est appliquée à l'étage de
30 sortie de turbine ayant le plus faible rendement parmi tous les étages de sortie, et une augmentation de la demande de charge faisant intervenir une augmentation de la demande de sortie de vapeur pour le système est appliquée, à l'étage de sortie de turbine ayant le rendement le plus élevé de tous les étages de sortie.

3. Un système selon la revendication 1, dans lequel le changement de la demande de charge fait
35 intervenir un changement de la demande de puissance de sortie électrique pour le système.

4. Un système selon l'une quelconque des revendications précédentes, dans lequel les moyens d'affectation de charge (76) comprennent un ou plusieurs blocs de fonction arrangés en une configuration logique.

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