

METHOD FOR TRANSMISSION LINE ANALYSIS

TECHNICAL FIELD OF THE INVENTION

5 The present invention relates to the field of transmission line analysis.

BACKGROUND

10 In DSL(Digital Subscriber Line) technology, such as VDSL2, the use of the spectrum available for the service is governed by a band plan, which is usually part of the standard. The plan specifies, for each end of the loop, which bands (frequency intervals) are intended to be used for transmission (pass bands) and which may not (stop
15 bands). A PSD (Power Spectral Density) mask specifies the permitted transmit power for the bands.

Normally, some bands, upstream bands, are reserved for transmission by the CPE (Customer Premises Equipment),
20 whereas other bands, downstream bands, are reserved for transmission by the DSLAM (Digital Subscriber Line Access Multiplexer) at the central office. Thus, a band which is a passband in the band plan for one end of the loop will be a stop band in the band plan for the other end of the loop.

25

There may be bands which are not intended for transmission at all (e.g. they are stop bands in the band plan for the central office end as well as being stop bands also in the band plan for the customer end). This may be to prevent
30 interference with other systems.

Different band plans may be used depending on the setting, i.e. the circumstances and the location on the loop where transmission takes place. E.g. the PSD masks are
5 (naturally) different for the customer and central office ends of the loop, but may also be different for different applications, such as fiber-fed cabinets near the customer end as opposed to copper connection all the way between customer and central office. Band plans and PSD masks may
10 also differ between different markets or operators depending on regulatory requirements designed to limit interference to/from other equipment.

In general, it is not possible to design a transmitter to be absolutely quiet (i.e. to transmit no power at all) in some
15 frequency bands while transmitting at normal power in others. In particular, when transmitting in a pass band at normal transmit power there will always be side lobes and intermodulation products in the adjacent stop bands, i.e. a leakage of power into the bands not intended for
20 transmission. For this reason, the PSD masks allow a certain small transmit power also in the stop bands.

Single Ended Line Testing, SELT, is a method for testing a transmission line (loop) which requires actions at one end of the line only. Typically a signal of some kind is sent
25 to the line and a resulting signal, such as an echo is received. From the relationship between the sent and the received signal, information about the line and its properties may be deduced.

30 In TDR (Time Domain Reflectometry) SELT, a brief pulse is sent to the line. The resulting echo as a function of time is recorded. Defects in the line may be seen as peaks in the

echo curve, and the position in time on the curve gives information about where on the line the defect is located.

FDR (Frequency Domain Reflectometry) SELT is a method wherein a more or less stationary signal covering many
5 frequencies is applied to the line for a certain time. The resulting reflected signal as a function of frequency, is recorded (i.e. amplitude and phase as a function of frequency).

The received signal as a function of frequency is then
10 divided by the sent signal as a function of frequency, to get an echo frequency response. Various adjustments and other manipulations can be made in order to represent different line properties. By use of the inverse Fourier transform, the impulse response of the line may be generated
15 mathematically.

When making a measurement, there is often a desire for greater accuracy, to be able to better resolve the location and other characteristics of faults and other line artifacts.

20

EP 1 111 808 A1 describes a TDR (Time Domain Reflectometry) method wherein specially designed edge regions of TDR pulses makes it possible to add the corresponding time domain echoes to produce a wideband impulse response measurement.
25 This allegedly solves the problem of how to detect more than just the first defect on a line.

ITU-T standards G.993.2 and G.992.5 describe the VDSL2 and ADSL2+ standards respectively.

30

SUMMARY OF THE INVENTION

When making a FDR SELT measurement on a DSL line intended for a technology such as VDSL2, a signal may be sent in one
5 of the pass bands and the resulting signal received.

For better accuracy, it is desirable to make the measurement with a strong signal and a large bandwidth. However, the transmit bandwidth and signal power are limited by the band plan and associated PSD masks.

10 Certain advantages may be achieved by transmitting in the bands not intended for transmission (the stop bands), contrary to the intention of the standard, while still keeping the transmit PSD in accordance or substantially in accordance with the standard.

15 The PSD being substantially according to the standard in this context means that the power may exceed the PSD mask limit somewhat, but is still low enough as not to cause unacceptable interference to e.g. other systems, and still very much lower than the PSD levels allowed in pass bands
20 and used for regular transmission.

In some band plans, there may be a stop band which is significantly wider than any of the pass bands. For example, in some VDSL2 band plans, the spectrum from 8 to 30 MHz is intended neither for downstream nor upstream transmission,
25 in order to protect against unacceptable interference to other systems.

By transmitting the FDR SELT test signal in such a band, using a PSD that complies or at least substantially complies with the PSD mask, a measurement can be made which has a
30 greater bandwidth than if a pass band had been used while still not creating unacceptable interference. A greater bandwidth gives improved resolution when line properties in the time domain are to be estimated.

Since the signal (and hence the echo) is quite weak, the Signal to Noise Ratio (SNR) will not be as good as when transmitting a stronger signal in a pass band, where much stronger signals are allowed according to the PSD mask.

5 This disadvantage may be at least in part compensated for by sending the signal during a longer time (and averaging the echo in order to improve SNR).

The signal is preferably as strong as the PSD mask allows to get as good SNR as possible, but if other circumstances

10 require it, a weaker signal may of course be used.

Combining measurements in different bands is a further way to improve resolution in the time domain. However, simply transmitting with the maximum allowed PSD in all pass bands and then combining these measurement results will give rise

15 to side lobes in the time domain because of the gaps in the measurement caused by the stop bands. A measurement over a contiguous frequency band would have been desired.

Instead of a normal contiguous measurement over a wide range of frequencies (which would either be all low power, or else

20 violate the PSD mask of the stop band parts of the range), measurements may be made in the different bands preferably using the maximum allowed PSDs of the particular bands, and those results then concatenated in the frequency domain.

At least a measurement in a stop band and a measurement in

25 an adjacent pass band are desired, the results of which may be concatenated.

Compared to a measurement on only one pass band, or concatenated measurements in several pass bands (i.e. non-contiguous), such a measurement has a higher noise level,

30 but much better time resolution.

The result of a measurement in a band is usually expressed as an echo function in the frequency domain, i.e. the quotient between the received and the sent signal as a function of frequency. In principle, the quotient is not
5 affected by the used PSD, and hence results may be combined directly.

If the AGC level of the receiver is not precisely known, the measurement results from different bands may not fit perfectly to each other at the band edges, which may give
10 rise to side lobes that may decrease the time resolution of the combined measurement.

This may be addressed by various adjustment techniques. For example, the measurement signal for a stop band may be made a little wider than the band, so as to extend a little into
15 the respective pass bands. The measurements may then be scaled, to achieve best fit in the region of overlap. The pass band measurement result and the stop band measurement result in the region of overlap may then be further adapted to fit precisely to each other.

20 Another approach is to make a measurement over a wide frequency range (e.g. the entire range supported by the transceiver) at low power (e.g. stop band levels), then make high power measurements in the pass bands. Each of the pass band measurement results can then be scaled so as to achieve
25 a best fit to the wideband measurement results for frequencies that they have in common. A combined result can then be made from the high power pass band results and the stop band parts of the wideband result.

30 It is an advantage of the invention that increased time and/or spatial resolution may be achieved.

A further advantage is that higher resolution measurements may be made without serious interference with other systems or lines.

Another advantage is that higher resolution measurements can
5 be made without violating standards requirements.

Yet another advantage is that except for the PSD limits of the applicable PSD mask, there are no special requirements on the shape of the PSD curve of the sent signal, at band edges or otherwise.

10 Still an advantage is that the sent signal can be a more or less stationary signal and noise reduction by averaging over time is easily implemented.

A further advantage is that measurements can be made by a standard DSL transceiver. Metallic access for special test
15 equipment is not needed.

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 shows the PSD mask of a VDSL2 band plan.

20 Figure 2 shows an example of PSDs of echo measurements in non-overlapping but adjacent bands (one stopband and one passband).

Figure 3 shows a setup to simulate a SELT measurement on a 500 meter long cable with a bad splice (2 ohm series
25 resistance) at 50 meter from the xTU. The figure also shows a signal graph showing the transmitted signal (T) and some of the received reflections (R_i).

Figure 4 shows a graph of echo vs. distance using only band DS1.

Figure 5 shows a graph of echo vs. distance using the whole 17 MHz band including measurements in receive bands.

Figure 6 shows a graph of echo vs. distance using all transmit bands and setting $S_{11}(f)$ to zero in the receive
5 bands.

Figure 7 shows a graph of echo vs. distance using the whole 17 MHz band including measurements on receive bands but with AGC errors in some receive bands.

Figure 8 shows a graph of a measured frequency domain echo
10 with a step at the edge between two bands.

Figure 9 shows a graph which displays how the step of figure 8 was corrected.

Figures 10 and 11 show flow charts of measurement methods.

DETAILED DESCRIPTION OF EMBODIMENTS

15 Single Ended Line Test (SELT) tools utilizing noise and echo measurements can be very powerful in diagnosing problems that prohibit or severely disturb communication in a telecommunication system. High-resolution results require a wide measurement bandwidth and in order to achieve good
20 Signal-to-Noise Ratio, a high transmit Power Spectral Density (PSD) is desired in order to keep measurement time down. However, SELT tools in principle need to comply with the same band plans and PSD masks as used for normal operation of the systems.

25 Usually, regional regulatory PSD masks also exist in addition to the DSL band plans, in order to ensure compatibility between multiple communication standards (e.g. both ADSL2 Annex A and M) present in the same access network. No system is allowed to violate the regulatory
30 limits while one system can violate another system's

standard band plan and PSD mask if allowed by the regulatory limits.

These PSD masks are needed to:

- 5 -- limit Far-End Crosstalk (FEXT) levels, thus protecting communication on neighbor lines (e.g. same or other DSL flavors, POTS, ISDN)
- limit Near-End Crosstalk (NEXT) levels when transmit and receive bands are overlapping (common problem with echo-
- 10 cancelled systems and when different systems are mixed in the same cable binder)
- limit out-of-band emissions such as sidelobes and intermodulation products from the transmit band leaking into the receive band (primarily for frequency division duplexing
- 15 systems)

For DSL technologies, the PSD limit mask specifies the maximum PSD both for the transmit bands and for the receive bands (spectral leakage). This mask is separate for xTU-R and xTU-O side. Existing ADSL SELT tools are intended for

20 Central Office (CO) deployment and typically use a flat PSD at about -40 dBm/Hz since a flat PSD simplifies the measurement and analysis.

Such a signal violates the CO-side ADSL PSD limit mask regarding the upstream (stopband) and may cause bit errors

25 on upstream of neighbor lines. It may however still be allowed according to regulatory limits since there are other systems that use this spectrum but this approach is not always feasible and definitely not for higher frequencies, e.g. for VDSL2 upstream bands other than US0.

30 Since the dynamic range of a communication receiver is limited by the effective number of bits in the Analog-to-

Digital converter, an Automatic Gain Control (AGC) is often used to adapt the input signal to a level which best utilizes the dynamic range.

Time resolution is inversely proportional to the measurement
5 bandwidth, which implies that, in order to achieve high resolution, measurements should be performed over a large bandwidth. However, when using a wideband signal for time-domain analysis, it is important not to have gaps in the frequency domain, i.e. non-measured frequencies within the
10 band. These gaps can be seen like multiplication with a rectangular window which in time-domain translates to convolution with a sinc function ($\text{sinc}(x) \equiv \sin(\pi x)/(\pi x)$). Such a convolution causes excessive "ringing" due to the high sidelobe level of the sinc function and sidelobes from
15 a strong echo can hide the main lobe of a weaker echo. Apart from gaps, any type of step or rapid change of slope in the frequency domain will cause similar effects.

A problem in e.g. VDSL2 is that the transmission band is split into multiple bands separated by receive bands
20 (transmission gaps). Although typical VDSL2 transceivers are capable of 17 or 30 MHz bandwidth, limiting e.g. FDR Single-Ended-Line-Test (SELT) to only the first downstream band (DS1) in a VDSL2 DSLAM would usually mean a measurement bandwidth of less than 3 MHz, i.e. not much more than the
25 2.2 MHz available for ADSL2+. The achieved resolution will in this case be less than 20% ($3 \text{ MHz} / 17 \text{ MHz}$) of the attainable resolution. Using another downstream band (e.g. DS2, DS3) instead of DS1 can give slightly better time resolution if the used band is wider but the improvement is
30 marginal and the attenuation will increase due to the higher frequency, leading to reduced SNR. Using multiple downstream bands together in a time domain analysis of a FDR measurement result is also not trivial due to the frequency gaps mentioned above.

(However, a frequency domain approach could still be used, e.g. adapting parameters in a model of a transmission line (with/without faults) to the measurement results of the measured frequency bands.)

5 A further problem is that when a wideband FDR echo measurement is performed by concatenating multiple measurements, different AGC settings may apply in the receiver, leading to discontinuities in the concatenated signal if the AGC gain steps are not perfectly known. This
10 will create effects similar to the frequency domain gaps albeit usually not as severe.

The problems can be solved by performing multiple FDR echo measurements, even on bands not intended for transmission, using different (overlapping or adjacent) parts of the
15 available spectrum and using PSD levels that do not violate applicable PSD limits. These measurements are then scaled properly, to ensure a continuous echo at band edges, and concatenated to form a wideband echo measurement with high resolution and low sidelobe levels in the time domain. If
20 necessary, repeated measurements are performed and averaged in order to improve the SNR.

Although a modem is not supposed to transmit on the receive bands or other bands outside the intended transmission bands, a certain transmit PSD level must be allowed in those
25 bands (stopbands) due to spectral leakage from the transmit bands (passbands) as mentioned in above. If the transmit PSD is kept below the limit, it should be possible to transmit in the receive bands without disturbing neighbor lines. Of course, the SNR will typically be much lower than for
30 transmit bands.

PSD limits outside the intended transmission bands in VDSL2 are typically about -100 dBm/Hz and sometimes even lower but

with sufficiently long measurement time, a useful echo can still be acquired.

As an example, figure 1 shows VDSL2 band plan B7-9 [G.993.2, Amendment 1].

- 5 It has three downstream bands (DS1 - DS3) and four upstream bands (US0 - US3) where the lowest (US0: 25 - 138 kHz) is not visible in the figure since it is too narrow for the used frequency scale.

10 The widest transmission band is DS1, which is about 3 MHz wide.

Some ADSL SELT implementations already today transmit on the ADSL upstream frequencies with the same flat PSD as for downstream frequencies (e.g. -40 dBm/Hz). This means that they actually violate the ADSL downstream PSD mask but this
15 is possible in some telecommunication networks since operators usually have other systems like ISDN and SHDSL generating crosstalk at these frequencies and crosstalk coupling is low. However, this approach is not always feasible and definitely not for higher frequencies, e.g. for
20 VDSL2 upstream bands other than US0.

In this invention, gaps in frequency when performing normal FDR echo measurements on transmit bands can be mitigated by also performing echo measurements on the receive bands, using the PSD limits intended for spectral leakage. In
25 principle, transmit and receive bands could be measured simultaneously (e.g. with a single test signal where the power is much higher in the pass bands than in the stop bands, for example several orders of magnitude higher), however in order to best utilize the dynamic range of the
30 transceiver (and not to violate receive band PSD masks due to the combination of transmitted signal and spectral leakage from neighbor bands), receive and transmit band measurements are preferably performed separately. Also, with

simultaneous measurement, spectral leakage from the stronger passband signal will interfere with the weaker signal in the stopband, reducing the already low SNR further.

5 An example of this is shown in figure 2 which shows echo measurements in non-overlapping but adjacent bands. Here, one stopband and one passband is measured. In the shown example, it would also be possible to measure over all frequencies with a PSD of -100 dBm/Hz and then measure again with a higher PSD in the passbands.

10

In order to illustrate the enhanced resolution achieved with the current invention, a simulation was performed with a FDR SELT measurement on a 500 meter long ETSI 0.5 mm cable with a bad cable splice (2 ohm series resistance) at 50 meters
15 from the xTU, as shown in figure 3.

Figure 3 also shows a signal graph showing the transmitted signal (T) and some of the received reflections (R_i).

A frequency domain echo $U(f)$ is calculated as:

$$U(f) = \frac{R(f)}{T(f)}, R(f) = \sum_i R_i(f)$$

20 where $R(f)$ is the received signal and $T(f)$ is the transmitted signal. By dividing the received signal $R(f)$ with the transmitted signal $T(f)$, the echo will in principle not be affected by the used PSD and hence the large PSD difference in figure 2 is compensated for automatically. As shown in
25 figure 3, the received signal is a sum of several different components $R_i(f)$ with different delays depending on the traveled path from transmitter to receiver. Further, since $T(f)$ contains the transmit PSD level, the resulting echo should ideally be independent of the used PSD curve apart
30 from SNR, which will be proportional to the PSD. The

uncalibrated echo frequency response $U(f)$ is then corrected for any (linear) distortion in the transceiver in order to get a calibrated echo response or input return loss $S_{11}(f)$. This calibration procedure is already described in WO 2004/100512 A1 (US-7,069,165 , EP-1625735) and will not be repeated here. Further, in order to get a time-domain echo response, $s_{11}(t)$, the return loss $S_{11}(f)$ is filtered, e.g. by multiplication with a suitable window function such as a Kaiser window, and then an inverse Discrete Fourier Transform is applied. By performing the substitution

$$t = \frac{2d}{v}, \quad d = \text{distance and } v = \text{velocity of propagation}$$

we get an approximation for an echo vs. distance function

$$s'_{11}(d) = s_{11}\left(\frac{2d}{v}\right).$$

Using an echo measurement in band DS1 with the PSD shown in figure 1 when performing an echo measurement gives an $s'_{11}(d)$ result which does not reveal the existence of the bad splice since the reflection is drowned by the stronger echo from the impedance discontinuity between the DSLAM and the cable. This is displayed in figure 4 which shows Echo vs. distance using only band DS1 (approx 3 MHz). The bad splice at 50 meter distance cannot be resolved due to the mainlobe width of the near-end echo.

However, when performing echo measurement with the full 17 MHz band and the PSD levels from figure 1, the bad splice at 50 meter distance is seen clearly as displayed in figure 5. The figure shows echo vs. distance using the whole 17 MHz band including measurements on receive bands.

The far-end echo at 500 meter has become much weaker due to the strong attenuation of the wideband signal. Also, the noise floor has increased dramatically due to the much lower SNR in the receive bands. Still, the multiband signal is
5 very useful to detect problems close to the transmitter. Also, the noise floor in the multiband method could be lowered to some extent by filtering. This filtering does not have to be applied to all bands; it can be beneficial for the wanted signal to only filter the noisiest bands, which
10 typically would be the receive bands. This would allow reducing noise while still keeping most of the increased resolution.

To show that the receive band echo measurement really improves the result, we also tried to fill the gaps between
15 the transmit bands with a constant value, e.g. set the echo to zero in those bands. This will keep noise levels low but instead, sidelobe levels will increase dramatically as seen in figure 6. The figure shows echo vs. distance using all transmit bands and setting $S_{11}(f)$ to zero in the receive
20 bands. The bad splice at 50 meter distance cannot be seen due to the high sidelobe level of the near-end echo at 0 meter.

The results so far assume either an ideal AGC or some method to properly scale echoes measured in different bands in
25 order to form a continuous echo when concatenating the measured bands. If this is not the case, we can get results similar to figure 7 where all bands were measured but the echoes in two of the receive bands were multiplied by a random number corresponding to that AGC gains were not
30 perfectly known. Here, the sidelobes will make it difficult to see the bad splice. Figure 7 shows echo vs. distance using the whole 17 MHz band including measurements on receive bands but with AGC errors in some receive bands. The bad splice at 50 meter cannot be differentiated from the
35 sidelobes.

Although the problem with AGC error was exaggerated in the example above, this problem is not unlikely given the large span of PSD levels between transmit and receive bands as shown in figure 1. Some solutions to this include:

- 5 -- Measure without overlap (adjacent bands) and make sure that the measured echo response is continuous by proper scaling of the different bands
- Measure without overlap (adjacent bands) and use a polynomial or other data model to fit the measured data at
10 the band edges and extrapolate towards the neighbor band to create an artificial overlap between bands at one or more frequencies.
- Make sure that the measured bands always overlap at least slightly and use this overlap to adjust scaling of the
15 measurements with e.g. a least squares fitting
- Calibration of the different AGC levels in the receiver in order to improve the error between selected AGC level and actual AGC level..
- Using the same AGC setting for all measurements that
20 should be concatenated to a single result (may result in bad utilization of the dynamic range of the receiver).

An example of how the problem looks in frequency domain is shown in figure 8 with a large step at 14 MHz where DS3 and
25 US3 meet. The step was caused by insufficient calibration of the AGC.

The result when US3 measurements are adjusted so that the Uncalibrated echo response ($UER(f)$) becomes continuous can be seen in figure 9, which shows the step corrected by
30 adjusting the level of the echo response in the last band in

order to get a smooth transition between bands, i.e. continuous UER(f).

A variant of measuring with overlap is to make a first measurement covering the whole range that the transceiver
5 is capable of measuring, e.g. the full 17 or 30 MHz. (A smaller range is possible, but it should at least partly cover one stop band and one pass band)

The first measurement is preferably made with a flat PSD level which is the maximum allowed PSD in the band which has
10 the lowest allowed PSD. I.e. the measurement uses the stop band allowed PSD, typically -100 dBm/Hz.

Further measurements are then made in the pass bands, using PSDs allowed in those bands.

Each of the further measurements are then scaled so as to
15 produce a best fit between the further measurement result and the first measurement results for at least some, but preferably all of the frequencies that are present in both measurements.

Best fit may be by least squares or some other method.

20 A single concatenated echo frequency response result for the whole covered frequency range may be generated by simply discarding the parts of the low-power (e.g. low SNR) results that are within the region of overlap, and then concatenating the remaining data.

25 A more elaborate method is that the results of the first and second measurements for frequencies that are present in both measurements are combined using a weighted average, preferably with a high weight for the results with a high SNR, e.g. the pass band measurements, so as to create a
30 single, concatenated echo frequency response result for the whole covered frequency range. This will reduce the influence of noise.

Further, in order to prevent discontinuities (e.g. caused by noise) at the edges of the region of overlap, the weights of the weighted average may be selected differently near the edges of the overlap region. At the edges to the low power measurement, the weight for that measurement is set to 1 (and the weight for the high power measurement is thus set to zero), and then the weights are gradually (for example linearly with frequency) changed into an SNR-based weighting when moving into the region of overlap.

10 In a variant where the high power measurements are not completely overlapped by low power measurements (e.g. the case where each stop band measurement covers the stop band and a little bit of each adjacent pass band), the region of overlap will have an edge to a low power measurement on one side and an edge to a high power measurement on the other side. In this case, the weight is preferably set to 1 for the low power measurement at the edge towards that measurement, and set to 1 for the high power measurement at the edge towards that measurement. In both cases, the weights are gradually changed into an SNR-based weighting when moving into the region of overlap.

In a variant, the weighting is changed linearly with frequency from 1-0 to 0-1 from edge to edge for the low-power and high-power results respectively. I.e. at the edge to the low-power measurement that measurement is used, and at the edge to the high-power measurement that measurement is used, and in between there is a gradual change from one to the other.

When an echo frequency response has been so obtained it may then be further used, for example to generate the line impulse response by inverse Fourier transform, as explained above.

Figures 10 and 11 provide a further illustration of the measurement methods disclosed above.

In figure 10, in a step 100, a first FDR SELT measurement is made in a stop band. In a step 104, a line property is
5 estimated from the measurement result. The line property may be the echo frequency response, or some other property such as the line impulse response or the position of a fault.

In figure 11, in a step 110, a first measurement is made in
10 a stop band, as in step 100 of figure 10. In a step 111, one or more further measurements are made (which may or may not be in stop bands). In an optional step 112, measurement results are adjusted and/or scaled to fit smoothly to each other. In a step 113, measurement results are concatenated
15 to form a single result. In a step 114, a line property is estimated from the single result.

Results

The multi-band technique can improve time resolution for a
20 VDSL2 FDR SELT application about 5 - 10 times depending on the used band plan, provided that echoes from the different bands are properly scaled before concatenation. Typical resolution improvement will be 5 - 6 times while a resolution improvement of 10 would apply when using 30 MHz
25 capable hardware on a 17 MHz bandplan with DS1 width of about 3 MHz. The improved resolution allows much more detailed information on problems on the transmission line, especially for problems close to the xTU performing the SELT. This is important since there is often a connector or
30 cable splice within tens of meters from the DSLAM in the CO. If this connection degrades, the problem will be visible much earlier with this invention.

The importance of the invention will be even higher for SELT in street cabinets and other remote locations due to the Downstream Power Back Off (DPBO) function that has to be applied in these locations. DPBO is needed to protect xDSL
5 lines originating in the CO from excessive crosstalk generated by equipment in remote locations. The PSD shaping applied in DPBO will effectively narrow the transmit bands thus decreasing resolution but this can be mitigated by the current invention. Further, the invention is not limited to
10 SELT in an xTU-O but can also be used in e.g. xTU-R SELT (CPE SELT).

Such a CPE SELT could be utilized to examine whether or not a POTS/DSL splitter is present and, if there is no splitter, also to characterize the telephone lines (home wiring)
15 inside the customer premises.

Abbreviations

ADSL Asymmetric Digital Subscriber Line

AGC Automatic Gain Control

20 CO Central Office

CPE Customer Premises Equipment

DPBO Downstream Power Back Off

FEXT Far-End Crosstalk

NEXT Near-End Crosstalk

25 PSD Power Spectral Density

FDR Frequency Domain Reflectometry

SELT Single Ended Line Test

SNR Signal-to-Noise Ratio

VDSL2 Very High Speed Digital Subscriber Line

xTU xDSL Transceiver Unit

xTU-OxTU at operator end of the loop (CO, cabinet etc.)

5 xTU-RxTU at remote end of the loop (subscriber side)

CLAIMS

1. A method for estimating a transmission property of a telecommunications transmission line comprising the step of
5 Making a first frequency domain reflectometry SELT measurement which comprises the steps of
- sending a first signal to the line;
- receiving a resulting, second signal from the line, and;
- 10 estimating a property of the line in dependence of the relationship between the first signal and the second signal, characterized in that the first SELT measurement is made in a first stop band and in accordance or substantially in accordance with the PSD mask, meaning that
- 15 the first signal is sent in a first stop band of a DSL band plan, the first signal having a PSD in accordance, or substantially in accordance with a PSD mask associated with the band plan and applicable to a particular setting where the sending of the first signal takes place,
- 20 2. A method according to claim 1, comprising the further step of
- making a second frequency domain reflectometry SELT measurement in a first pass band adjacent to the first stop band, the measurement comprising sending a signal to the
25 line.
3. A method according to claim 2, wherein the results of the first and second SELT measurements are concatenated to form a single measurement result over a contiguous frequency range comprising the whole, or at least parts of the
30 frequency ranges of the first and second measurements.

4. A method according to claim 2 or 3 wherein the power of the signal sent for the second SELT measurement is several orders of magnitude greater than the power of the signal sent for the first SELT measurement.
- 5 5. A method according to claim 3 or 4 wherein the PSD of the signal sent for the second measurement is the maximum allowed for the band in which it is sent, according to the PSD mask of the band plan, or it is the maximum according to regulatory limits which specify a lower PSD than the PSD
- 10 mask of the band plan.
6. A method according to claim 3, 4 or 5 wherein edge regions of individual measurement results are adapted to corresponding edge regions of adjacent measurement results to create a continuous concatenated measurement.
- 15 7. A method according to claim 6 wherein the adaption is made using least squares fitting.
8. A method according to any of claims 3-5 wherein each individual SELT measurement result is scaled so as to fit smoothly to each adjacent measurement result.
- 20 9. A method according to claim 8 wherein the set of scaling factors for the individual SELT measurements is selected using a least squares fitting.
10. A method according to any of claims 1-9 wherein SELT measurements are made in several stop bands and several pass
- 25 bands, and the measurement results concatenated to form a single measurement result.
11. A method according to any of claims 1-10 wherein several SELT measurements are made and concatenated so as to cover substantially the whole of the frequency range of which a
- 30 transmitter used for sending the signals is capable of covering.

12. A method according to any of claims 1-11 which is used in VDSL2 bands other than US0.

13. A method according to any of the claims 1-12 wherein the first SELT measurement covers a frequency range which partly
5 or wholly covers at least one stop band and at least one pass band,

14. A method according to claim 13 wherein one or more further SELT measurements are made in the at least one pass band

10 and wherein each one of the further SELT measurement results is scaled so as to achieve a best fit between the further measurement result and the first measurement result for frequencies which are present in the measurement results of both measurements.

15 15. A method according to claim 13, wherein the power of the part of the signal sent in the pass band is several orders of magnitude greater than the power of the part of the signal sent in the stop band.

16. A method according to claim 2, wherein the measurement
20 according to claim 1 is made simultaneously with the measurement of claim 2.