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More recently, electronic components have been incorporated into a contact lens. Some components can include semiconductor devices. However, physical constraints including the size, shape and control aspects of a liquid meniscus lens have precluded their use in an ophthalmic lens. Generally the cylindrical shape, sometimes referred to as the “hockey puck” shape of liquid meniscus lenses, has not been conducive to something that can work in a human eye.

In addition, a curved liquid meniscus lens includes physical challenges that are not necessarily present in a traditional design of a liquid meniscus lens with parallel sidewalls.

SUMMARY

Accordingly, the present invention provides a liquid meniscus lens. Some preferred embodiments include an arcuate front curve lens and an arcuate back curve lens. The present invention provides for a meniscus wall with physical features conducive for one or both of attraction and repulsion of a liquid contained within the lens and forming a meniscus with another liquid.

According to the present invention, a first optic is proximate to a second optic with a cavity formed therebetween. Preferred embodiments include a first arcuate shaped optic proximate to a second arcuate shaped optic with a cavity formed therebetween. A saline solution and an oil are maintained within the cavity. Application of an electrical charge to a meniscus wall generally located in a perimeter area of one or both of the first optic and the second optic changes the physical shape of a meniscus formed between the saline solution and oil maintained within the cavity.

The present invention includes a meniscus wall formed into a shape essentially including a segment of a torus. According to the present invention a cross section of the torus-segment includes a convex shaped wall. The present invention additionally teaches unique operation of a liquid meniscus lens including a convex formation of the meniscus wall imparts

DESCRIPTION OF THE DRAWINGS

Fig. 1A illustrates a prior art example of a cylindrical liquid meniscus lens in a first state.

5 Fig. 1B illustrates the prior art example of a cylindrical liquid meniscus lens in a second state.

Fig. 2 illustrates a profile sliced cut away of an exemplary liquid meniscus lens according to some embodiments of the present invention.

10 Fig. 3 illustrates a cross section of a portion of an exemplary arcuate liquid meniscus lens, according to some embodiments of the present invention.

Fig. 4 illustrates additional exemplary aspects of an arcuate liquid meniscus lens.

Fig. 5 illustrates meniscus wall elements within an arcuate liquid meniscus lens, according to some embodiments of the present invention.

15 Fig. 6A illustrates a convex meniscus wall within a liquid meniscus lens, showing a liquid meniscus boundary in its unpowered state.

Fig. 6B illustrates a convex meniscus wall within a liquid meniscus lens, showing a liquid meniscus boundary in its powered state.

20 Fig. 6C illustrates a convex meniscus wall within a liquid meniscus lens, showing powered and unpowered states of the liquid meniscus boundary in a single diagram for comparison.

Fig. 7 illustrates a convex torus-segment, which is the shape of a convex meniscus wall when viewed separately from the rest of an arcuate liquid meniscus lens.

DETAILED DESCRIPTION OF THE INVENTION

25 The present invention provides for a liquid meniscus lens with at least one of a front curve lens and a back curve lens defining a meniscus cavity of the liquid meniscus lens.

GLOSSARY

In this description and claims directed to the presented invention, various terms may be used for which the following definitions will apply:

Contact Angle: The angle at which the oil/saline solution interface, also referred to as the liquid meniscus boundary, meets the meniscus wall. In the case of a linear meniscus wall, the contact angle is measured as the angle between the meniscus wall and the line tangent to the liquid meniscus boundary at the point where the liquid meniscus boundary meets the meniscus wall. In the case of a curved meniscus wall, the contact angle is measured as the angle between the lines tangent to the meniscus wall and the liquid meniscus boundary at the point where they meet.

Liquid Meniscus Boundary: The arcuate surface interface between the saline solution and the oil. Generally, the surface will form a lens that is concave on one side and convex on the other.

Meniscus Cavity: The space in an arcuate liquid meniscus lens between the front curve lens and the back curve lens in which oil and saline solution are maintained.

Meniscus Wall: A specific area on the interior of the front curve lens, such that it is within the meniscus cavity, along which the liquid meniscus boundary moves.

Optical Zone: as used herein refers to an area of an ophthalmic lens through which a wearer of the ophthalmic lens sees.

Sharp: A geometric feature of an internal surface of either a front curve or back curve lens piece sufficient to contain the location of a contact line of two predefined fluids on the optic. The sharp is usually an outside corner rather than an inside corner. From a fluid standpoint it is an angle greater than 180 degrees.

Referring now to Fig. 1A, a cut away view of a prior art lens 100 is illustrated with an oil 101 and a saline solution 102 contained within cylinder 110. The cylinder 110 includes two plates of optical material 106. Each plate 106 includes a flat interior surface 113-114. The cylinder 110 includes an interior surface that is essentially rotationally symmetric. In some prior art embodiments, one or more surfaces may include a hydrophobic coating. Electrodes 105 are also included on or about the perimeter of the cylinder. An electrical insulator may also be used proximate to the electrodes 105.

According to the prior art, each of the interior surfaces 113-114 is essentially flat or planar. An interface surface 112A is defined between the saline solution 102A and the oil 101. As illustrated in Fig. 1A, the shape of the interface 112A is combined with the refractive index properties of the saline solution 102A and the oil 101 to receive incident light 108 through a first interior surface 113 and provide divergent light 109 through a second interior surface 113. The shape of the interface surface between the oil 101 and the saline solution 102 may be altered with the application of an electrical current to the electrodes 105.

Fig. 100A illustrates a perspective view of the prior art lens illustrated at 100.

Referring now to Fig. 1B, the prior art lens 100 is illustrated in an energized state. The energized state is accomplished by applying voltage 114 across the electrodes 115. The shape of the interface surface 112B between the oil 101 and the saline solution 102 is altered with the application of an electrical current to the electrodes 115. As illustrated in Fig. 1B, incident light 108B passing through the oil 101 and the saline solution 102B is focused into a convergent light pattern 111.

Referring now to Fig. 2, a cut away view of a liquid meniscus lens 200 with a front curve lens 201 and a back curve lens 202. The front curve lens 201 and the back curve lens 202 are positioned proximate to each other and form a cavity 210 therebetween. The front curve lens includes a concave arcuate interior lens surface 203 and a convex arcuate exterior lens surface 204. The concave arcuate lens surface 203 may have one or more coatings (not illustrated in Fig. 2). Coatings may include, for example, one or more of electrically conductive materials or electrically insulating materials, hydrophobic materials or hydrophilic materials. One or both of the concave arcuate lens surface 203 and the coatings are in liquid and optical communication with an oil 208 contained within the cavity 210.

The back curve lens 202 includes a convex arcuate interior lens surface 205 and a concave arcuate exterior lens surface 206. The convex arcuate lens surface 205 may have one or more coatings (not illustrated in Fig. 2). Coatings may include, for example, one or more of electrically conductive materials or electrically insulating materials, hydrophobic materials or hydrophilic materials. At least one of the convex arcuate lens surface 205 and the coatings are in liquid and optical communication with a saline solution 207 contained

within the cavity 210. The saline solution 207 includes one or more salts or other components which are electrically conductive and as such may be either attracted to or repulsed by an electric charge.

According to the present invention, an electrically conductive coating 209 is located along at least a portion of a periphery of one or both of the front curve lens 201 and the back curve lens 202. The electrically conductive coating 209 may include gold or silver and is preferably biocompatible. Application of an electrical charge to the electrically conductive coating 209 creates either an attraction or a repulsion of the electrically conductive salts or other components in the saline solution.

The front curve lens 201 has an optical power in relation to light passing through the concave arcuate interior lens surface 203 and a convex arcuate exterior lens surface 204. The optical power may be 0 or may be a plus or minus power. In some preferred embodiments, the optical power is a power typically found in corrective contact lenses, such as, by way of non-limiting example, a power between -8.0 and +8.0 diopters.

The back curve lens 202 has an optical power in relation to light passing through the convex arcuate interior lens surface 205 and a concave arcuate exterior lens surface 206. The optical power may be 0 or may be a plus or minus power. In some embodiments, the optical power is a power typically found in corrective contact lenses, such as, by way of non-limiting example, a power between -8.0 and +8.0 diopters.

Various embodiments may also include a change in optical power associated with a change in shape of a liquid meniscus 211 formed between the saline solution 207 and the oil. In some embodiments, a change in optical power may be relatively small, such as, for example, a change of between 0 to 2.0 diopters of change. In other embodiments, a change in optical power associated with a change in shape of a liquid meniscus may be up to about 30 or more diopters of change. Generally, a higher change in optical power associated with a change in shape of a liquid meniscus 211 is associated with a relatively thicker lens thickness 210.

According to some embodiments of the present invention, such as those embodiments that may be included in an ophthalmic lens, such as a contact lens, a cross cut lens thickness 210 of an arcuate liquid meniscus lens 200 will be up to about 1,000 microns

thick. An exemplary lens thickness 210 of a relatively thinner lens 200 may be up to about 200 microns thick. Preferred embodiments may include a liquid meniscus lens 200 with a lens thickness 210 of about 600 microns thick. Generally a cross cut thickness of front curve lens 201 may be between about 35 microns to about 200 microns and a cross cut thickness of a back curve lens 202 may also be between about 35 microns and 200 microns.

According to the present invention, an aggregate optical power is an aggregate of optical powers of the front curve lens 201 the back curve lens 202 and a liquid meniscus 211 formed between the oil 208 and the saline solution 207. In some embodiments, an optical power of the lens 200 will also include a difference in refractive index as between one or more of the front curve lens 201, the back curve lens 202, oil 208 and the saline solution 207.

In those embodiments that include an arcuate liquid meniscus lens 200 incorporated into a contact lens, it is additionally desirable for the saline 207 and oil 208 to remain stable in their relative positions within the curved liquid meniscus lens 200 as a contact wearer moves. Generally, it is preferred to prevent the oil 208 from floating and moving relative to the saline 207 when the wearer moves, accordingly, an oil 208 and saline solution 207 combination is preferably selected with a same or similar density. Additionally, an oil 208 and a saline solution 207 preferably have relatively low immiscibility so that the saline 207 and oil 208 will not mix.

In some preferred embodiments, a volume of saline solution contained within the cavity is greater than the volume of oil contained within the cavity. Additionally, some preferred embodiments include the saline solution 207 in contact with essentially an entirety of an interior surface 205 of the back curve lens 200. Some embodiments may include a volume of oil 208 that is about 66% or more by volume as compared to an amount of saline solution 207. Some additional embodiments may include an arcuate liquid meniscus lens wherein a volume of oil 208 that is about 90% or less by volume as compared to an amount of saline solution 207.

Referring now to Figure 3, a cutaway of an edge portion arcuate liquid meniscus lens 300 is illustrated. As discussed above, an arcuate liquid meniscus lens 300 includes combined front curve lens 301 and back curve lens 302 components. The front curve lens

301 and back curve lens 302 may be formed with one or more materials that are at least partially transparent. In some embodiments, one or both of the front curve lens 301 and the back curve lens 302 include generally optically clear plastic, such as for example, one or more of: PMMA, Zeonor and TPX.

5 One or both of the front curve lens 301 and the back curve lens 302 may be fashioned, for example via processes such as one or more of: single point diamond turning lathing; injection molding; digital mirror device free forming.

One or both of the front curve lens 301 and the back curve lens 302 may include a conductive coating 303, as illustrated, the conductive coating 303 extending along a
10 perimeter portion from 309 to 310. In some preferred embodiments, a conductive coating 303 includes gold. The gold may be applied via a sputter process, vapor deposition or other known process. Alternative conductive coating 303 may include, by way of non-limiting example, aluminum, nickel, and indium tin oxide. Generally, the conductive coating 303 will be applied to perimeter areas of one or both of the front curve lens 301 and the back
15 curve lens 302.

In some embodiments, of the present invention, a back curve lens 302 has a conductive coating 304 applied to specific areas. For example, portions about the perimeter of the back curve lens 302 may be coated from a first boundary 304-1 to a second boundary 304-2. The gold coatings may be applied for example via a sputter process or a vapor
20 deposition. In some embodiments, a mask may be used to apply the gold or other conductive material in a predetermined pattern around one or more perimeter portions of a front curve lens 301 or a back curve lens 302. Alternative conductive materials may be applied using various methods and covering varying areas of the back curve lens 302.

In some embodiments, a conductive pass through, such as, for example one or more
25 holes or slots in a back curve lens 302 may be filled with a conductive filler material, such as, for example, a conductive epoxy. The conductive filler may provide electrical communication to a conductive coating on an interior surface of one or both of the front curve lens 301 and the back curve lens 302.

In another aspect of the present invention, one or both of the front curve lens 301
30 and the back curve lens 302 may be created from multiple different materials wherein an

optical zone generally in a central area of the front curve lens 301 and the back curve lens 302 (not illustrated) may include an optically transparent material and a peripheral zone may include an optically opaque area that includes an electrically conductive material. The optically opaque area may also include one or more of control circuitry and energy sources.

5 In still another aspect, in some embodiments, an insulator coating 305 is applied to a front curve lens 301. By way of non-limiting example, the insulator coating 305 may be applied in an area from a first region 305-1 and extend to a second region 305-2. Insulators may include, for example, Parylene C™, Teflon AF or other materials with various electrical and mechanical characteristics and electrical resistance.

10 In some specific embodiments, an insulator coating 305 creates a boundary area to maintain separation between the conductive coating 303 and a saline solution 306 contained in a cavity between the front curve lens 301 and the back curve lens 302. Some embodiments accordingly include an insulator coating 305 patterned and positioned in an one or more areas of one or both of the front curve lens 301 and the back curve lens 302 to
15 prevent a positively charged conductor 303 and negatively charged saline solution 306 from coming into contact, wherein contact of a conductor 303 and a saline solution 306 will result in an electrical short. Embodiments may include a positively charged saline solution 306 and a negatively charged conductor 303.

 Still other embodiments may allow for a short between a conductor 303 and a saline
20 solution 306 as a reset function of circuitry associated with the operation of the lens 300. For example, a short condition may interrupt power source to the lens and cause the saline solution 306 and the oil 307 to revert to a default position.

 Some preferred embodiments include a conductor 303 that extends from an area 309 on the interior of the cavity 311 to an area 310 external to the cavity 311. Other
25 embodiments may include a channel 312 through the front curve lens or the back curve lens which may be filled with a conductive material 313, such as, for example, a waterproof conductive epoxy. The conductive material 313 may form or be connected to an electrical terminal external to the cavity. An electrical charge may be applied to the terminal and conducted to the coating via the conductive material 313 in the channel 312.

The thickness of the insulator coating 305 may be varied as a parameter of lens performance. According to the present invention, charged components, including the saline solution 306 and the conductor 303, are generally maintained on either side of the insulator coating 305. The present invention provides for an indirect relationship between the
5 thickness of the insulator coating 305 and an electrical field between the saline solution 306 and the conductor 303, wherein the farther apart the saline solution 306 and the conductor 303 are maintained, the weaker the electrical field will be.

Generally, the present invention provides that electrical field strength may fall off dramatically as insulator coating 305 thickness increases. The closer together the fields are,
10 the more energy that will generally be available to move a spherical liquid meniscus boundary 308. As a distance between the saline solution 306 and conductor 303 increases, the farther apart electrical fields of the saline solution 306 and the conductor coating 303 will be and therefore the harder it is to get the spherical meniscus boundary 308 to move. Inversely, the thinner the insulator coating 305, the more sensitive movement of the
15 spherical liquid meniscus 308 is to defects in an insulator coating 305. Generally, even a relatively small hole in the insulator coating 305 will short a lens 300 out.

In some embodiments, it is desirable to include a saline solution 306 with density that is generally the same density of an oil 307 also contained within the lens 300. For example, a saline solution 306 may preferably include a density that is within 10% of a
20 density of an oil 307 and more preferably the saline solution 306 will include a density within 5% of a density of an oil and most preferably within about 1%. In some embodiments, a concentration of salts or other components within the saline solution 306 may be adjusted to adjust the density of the saline solution 306.

According to the present invention, an arcuate liquid meniscus lens 300 will provide
25 a more stable optical quality by limiting movement of the oil 307 in relation to the front curve lens 301 and the back curve lens 302. One method of maintaining stability of movement of the oil 307 in relation to one or both of the arcuate front curve lens 301 and the back curve lens 302 is to maintain a relatively congruent density in the oil 307 and the saline solution 306. In addition, due to the curve design of the interior surfaces of both the
30 front curve lens 301 and the back curve lens 302, the relative depth or thickness of a layer of

saline solution 306 is diminished as compared to a traditional cylindrical lens design. Accordingly, stability of a position of oil within the lens 300 becomes more in order to avoid movement of the oil and possible breaking of the meniscus between the oil 306 and the saline solution 307.

5 In some preferred embodiments, the saline solution 306 provides a low refractive index as compared to the oil 307 which provides a relatively high refractive index. However, in some embodiments it is possible to include a saline solution 306 with a higher refractive index as compared to the oil 307 which in such cases provides a relatively lower refractive index.

10 An adhesive 308 may be used to secure the front curve lens 301 and back curve lens 302 in place proximate to each other thereby retaining the oil 307 and saline solution 306 therebetween. The adhesive 308 acts as a seal so that there is no leakage of saline 306 or oil 307 from the curved liquid meniscus lens 300.

Referring now to Figure 4, a curved liquid meniscus lens 400 is illustrated with a
15 liquid meniscus boundary 401 between the saline solution 406 and oil 407. According to some preferred embodiments, a meniscus wall 405 is defined in the front curve lens 404 by a first angular break in an arcuate wall extending between 402 and 403. The liquid meniscus boundary 401 will move up and down the meniscus wall 405 as charge is applied and removed along one or more conductive coatings or conductive materials 408.

20 In some preferred embodiments, a conductive coating 403 will extend from an area internal to the cavity 409 holding the saline solution 406 and the oil 407 to an area external to the cavity 409 containing the saline solution 406 and oil 407. In such embodiments, the conductive coating 403 may be a conduit of an electrical charge applied to the conductive coating 403 at a point external to the cavity 409 to an area of the conductive coating within
25 the cavity and in contact with the saline solution 406.

Referring now to Figure 5, a cut away view of an edge portion of an arcuate liquid meniscus lens 500 is shown with a front curve lens 501 and a back curve lens 502. The arcuate liquid meniscus lens 500 may be used to contain saline solution 503 and oil 504. A geometry of the arcuate liquid meniscus lens 500 and the characteristics of the saline

solution 503 and oil 504 facilitate formation of a liquid meniscus boundary 505 between the saline solution 503 and oil 504.

Generally, a liquid meniscus lens may be viewed as a capacitor with one or more of: conductive coatings, insulator coatings, pathways, and materials are present on or through the front curve lens 501 and back curve lens 502. According to the present invention, a shape of a liquid meniscus boundary 505 and therefore a contact angle between the liquid meniscus boundary 505 and the front curve lens 501 change in response to an electrical charge applied to a surface of at least a portion of one or both of the front curve lens 501 and the back curve lens 502.

According to the present invention, a change in an electrical current applied to the saline solution via the conductive coatings or materials changes a position of the liquid meniscus boundary 505 along a meniscus wall 506. The movement takes place between a first sharp 506-1 and a second sharp 506-2.

In preferred embodiments, the liquid meniscus boundary 505 will be at or near the first sharp 506-1 when a first magnitude of electrical current is applied to the lens, such as, for example, a voltage and current correlating with an unpowered or rest state.

Application of a second magnitude of electrical current, sometimes referred to as a powered state, may correlate with a movement of the liquid meniscus boundary 505 along the meniscus wall 506 generally in the direction of the second sharp 506-2, causing the shape of the liquid meniscus boundary to change.

In some embodiments, the meniscus wall 506 will be a smooth surface in relation to the thickness of the insulator coating. A smooth meniscus wall 506 surface may minimize defects in the insulator coating. Additionally, because random irregularities in surface texture may result in uneven fluid motion and therefore cause uneven or unpredictable meniscus motion when energizing or de-energizing the lens, a smooth meniscus wall 506 is preferred.

In another aspect, in some embodiments, it is desirable for the meniscus wall 506 to be hydrophobic, in which case a defined texture, such as a nano-textured surface, may be incorporated in the design of the arcuate liquid meniscus lens.

In still another aspect, in some embodiments, the meniscus wall 506 may be angled relative to an optical axis of the lens. The angle can range from 0° , or parallel to the optical axis, to at or near 90° , or perpendicular to the optical axis. As illustrated, and in some preferred embodiments, the meniscus wall 506 angle is generally between about 30° and 50° in order for the arcuate liquid meniscus lens to function given the current contact angle between the liquid meniscus boundary 505 and the insulator-coated meniscus wall 506. With the use of different materials or with different optical objectives, such as telescopic vision, the angle of the meniscus wall 506 may be closer to 0° or 90° .

According to the present invention, an angle of a meniscus wall 506 may be designed to accommodate a magnitude of movement along a meniscus wall 506 upon application of a specified electrical voltage and current. In some embodiments, as meniscus wall 506 angle increases, the ability to change lens power generally decreases within given lens size and voltage parameters. Additionally, if the meniscus wall 506 is at or near 0° relative to the optical axis, the liquid meniscus boundary 505 will be steered nearly straight onto the front optic. Meniscus wall angle is one of several parameters that can be tailored to provide various outcomes in lens performance.

In some preferred embodiments, the meniscus wall 506 is approximately 0.265 mm in length. However, the angle of the meniscus wall 506 together with the size of the overall lens will naturally affect meniscus wall 506 length in various designs.

It may generally be considered that an arcuate liquid meniscus lens 500 will fail if the oil 504 contacts the back curve lens 502. Therefore, in preferred embodiments, the meniscus wall 506 is designed to allow a minimum clearance of 50 microns between the first sharp 506-1 and the back curve lens 502 at its nearest point. In other embodiments, the minimum clearance may be less than 50 microns, although the risk of lens failure increases as the clearance is reduced. In yet other embodiments, the clearance may be increased to mitigate the risk of lens failure, but the overall lens thickness will also increase which may be undesirable.

In still another aspect of some preferred embodiments of the present invention, the behavior of a liquid meniscus boundary 505 as it travels along a meniscus wall 506 may be extrapolated using Young's Equation. Although Young's Equation defines the balance of forces caused by a wet drop on a dry surface and assumes a perfectly flat surface, the

fundamental properties can be applied to the electrowetted lens environment created within the arcuate liquid meniscus lens 500.

When a first magnitude of electrical energy is applied to the lens, such as, for example, when the lens is in an unpowered state, there will be achieved a balance of
5 interfacial energies between the oil 504 and saline solution 503, herein referred to as the liquid meniscus boundary 505, the oil 504 and meniscus wall 506, and the saline solution 503 and meniscus wall 506, resulting in an equilibrium contact angle between the liquid meniscus boundary 505 and the meniscus wall 506. When a change in magnitude of voltage
10 is applied to the arcuate liquid meniscus lens 500, the balance of interfacial energies will change, resulting in a corresponding change in contact angle between the liquid meniscus boundary 505 and the meniscus wall 506.

The contact angle of the liquid meniscus boundary 505 with the insulator-coated meniscus wall 506 is an important element in the design and function of the arcuate liquid meniscus lens 500 not only due to its role in the Young's Equation in movement of the
15 liquid meniscus boundary 505, but also because the contact angle is used in conjunction with other features of the arcuate liquid meniscus lens 500 to limit meniscus movement.

Discontinuities, such as sharps 506-1 506-2, at both ends of the meniscus wall 506 act as boundaries for liquid meniscus 505 movement because it would require a significant change in voltage to effect a large enough change in liquid meniscus contact angle to move
20 the liquid meniscus boundary 505 past one of the sharps. By way of non-limiting example, in some embodiments, a contact angle of the liquid meniscus boundary 505 with the meniscus wall 506 is in the range of 15 to 40° whereas the contact angle of the liquid meniscus boundary 505 with the step 507 below the second sharp 506-2 is perhaps in the range of 90 to 130° and in some preferred embodiments about 110°.

25 A voltage applied to the lens may result in movement of the liquid meniscus boundary 505 along the meniscus wall 506 toward the second sharp 506-2. The natural contact angle of the liquid meniscus boundary 505 with the insulator-coated meniscus wall 506 will cause the liquid meniscus boundary 505 to stop at the second sharp 506-2 unless significantly more voltage is supplied.

30 At one end of the meniscus wall 506, a first sharp 506-1 generally defines one limit beyond which the liquid meniscus boundary 505 will not typically move. In some

embodiments, the first sharp 506-1 is constructed as a sharp edge. In other preferred embodiments, the first sharp 506-1 has a defined small radial surface which can be created with less possibility of defect. Conductive, insulator, and other possible desired coatings may not deposit evenly and predictably on a sharp edge, whereas a defined radius edge of the radial surface can be coated more reliably.

In some embodiments, the first sharp 506-1 is constructed at about a 90° angle with a defined radius of about 10 microns. The sharp may also be created with less than a 90° angle. In some embodiments, a sharp with a larger angle than 90° may be used to increase the sturdiness of the sharp, but the design would then take up more lens space.

In various embodiments, a defined radius of a sharp 506-1 506-2 may be in the range of 5 microns to 25 microns. A larger defined radius may be used to improve the reliability of the coatings, but at the cost of using more space within the tight tolerances of the lens design. In this, as in many other areas of lens design, tradeoffs exist between ease of construction, optimization of lens functions, and minimizing size. A functional, reliable arcuate liquid meniscus lens 500 may be made using a wide range of variables.

A second sharp 506-2, includes a feature designed to limit oil movement when voltage is applied to the arcuate liquid meniscus lens 500. The second sharp 506-2 may also include, in some embodiments a sharp, or in other embodiments, the second sharp 506-2 may include a defined radius of between 5 and 25 microns, most preferred 10 microns. A 10 micron radius performs well as a sharp and can be created using single point diamond turning lathe or injection molding processes.

A vertical, or nearly vertical step 507, extending to a start of the optical area 508 of the front curve lens 501 may be included on a side of the second sharp 506-2 opposing the meniscus wall 506. In some embodiments, the step 507 is 120 microns in height, although it could be in the range of 50 to 200 microns.

In some embodiments, the step 507 may be angled at about 5° from optical axis. In other embodiments, the step 507 angle may be as little as 1° or 2° or may be angled more than 5° . A step 507 that is less angled from optical axis will generally act as a more effective limiter of meniscus movement because it would require a greater change in the contact angle of the liquid meniscus boundary 505 to move off of the meniscus wall 506 and onto the step 507. The transition from the step 507 to the start of the optical area 508 is a 25

micron radius. A larger radius would unnecessarily consume more space within the lens design. A smaller radius is possible and may be implemented if necessary to gain space. The decision to use a defined radius rather than a theoretical sharp in this area as well as others in the lens is based, in part, on the potential move to an injection molding process for lens elements. A curve between the step 507 and the start of the optical area 508 will improve plastic flow during the injection molding process and result in a lens with optimal strength and stress-handling characteristics.

Referring now to Figs. 6A-6C, several modeled examples are illustrated. The model assumes an 8.45 mm front curve lens and an 8.05 mm back curve lens. The lens curves may be changed in other embodiments without affecting the general conclusions about the function of the arcuate liquid meniscus lens.

Referring now to Figure 6A, in one of multiple possible embodiments, an exemplary convex meniscus wall 601 is depicted. The convex meniscus wall 601 component of the arcuate liquid meniscus lens, if viewed separately from the rest of the arcuate liquid meniscus lens, includes at least a portion of the meniscus wall 701 that includes a segment of a torus (shown as a perspective view in Figure 7). As further depicted in Figure 7, in these embodiments a meniscus wall 701 is convex toward the optical axis and of a consistent length between the first sharp 702-1 and the second sharp 702-2 around the entire lens.

Figure 6A depicts exemplary embodiments in which a meniscus wall 601, convex toward the optical axis with a radius of 0.25 mm, is placed approximately at a 45° angle from optical axis in an arcuate liquid meniscus lens containing approximately 4.5 µl of oil 602. A saline solution 603 fills a remainder of a meniscus cavity bordered by the meniscus wall 601. The liquid meniscus boundary 604A contacts the meniscus wall 601 at an angle of approximately 20° (606A) when unpowered. The contact point 605A is at the end of the meniscus wall 601 closest to the first sharp 608.

Referring now to Fig. 6B, application of a voltage moves the liquid meniscus boundary moves about 0.025 mm to 605B along the meniscus wall 601 generally toward the front curve lens 607, resulting in a contact angle of approximately 30° (606B) between the liquid meniscus boundary 604B and the meniscus wall 601. This meniscus change, shown

in Figure 6C from 605A to 605B, results in an add power of about 0.854 diopters when the lens power changes from +0.046 to +0.926.

According to the present invention, a liquid meniscus lens with a meniscus wall, including at least a portion with a convex meniscus wall placed at a given angle relative to the optical axis, as shown in Figure 6C, will exhibit less change in lens power for a given amount of applied voltage than a liquid meniscus lens with a linear meniscus wall placed at a similar angle relative to the optical axis. A liquid meniscus lens with a linear meniscus wall is more fully described in U.S. Patent Application Serial Number 61/359,548, entitled “LENS WITH CONICAL FRUSTUM MENISCUS WALL” and filed on June 29, 2010. A specific change in applied voltage causes a change in the balance of interfacial energies and is therefore expected to cause a corresponding change in contact angle between the liquid meniscus boundary and the meniscus wall. On a linear meniscus wall, the change in contact angle results in a relatively more significant movement of the liquid meniscus boundary along the meniscus wall, whereas the movement is expected to be relatively less significant on a convex meniscus wall, Figure 6C.

While the invention has been described with reference to particular embodiments, it will be understood by those skilled in the art that various changes may be made and equivalents may be substituted for elements thereof without departing from the scope of the invention. In addition, many modifications may be made to adapt a particular situation or material to the teachings of the invention without departing from the scope of the invention.

Therefore, it is intended that the invention not be limited to the particular embodiments disclosed as the best mode contemplated for carrying out this invention, but that the invention will include all embodiments falling within the scope and spirit of the appended claims.

CLAIMS

1. An optical lens comprising:

5 a front curve lens comprising a front curve lens exterior surface and a front curve lens interior surface, wherein both said front curve lens exterior surface and said front curve lens interior surface comprise an arcuate shape;

a back curve lens comprising a back curve lens interior surface and a back curve lens exterior surface, wherein both said back curve lens interior surface and
10 the back curve lens exterior surface comprise an arcuate shape, said back curve lens positioned proximate to said front curve lens such that said front curve lens interior surface and said back curve lens interior surface form a cavity therebetween;

a volume of saline solution and oil contained within the cavity formed between said front curve lens interior surface and said back curve lens interior
15 surface, said volume of saline solution and oil comprising a meniscus therebetween; and

a meniscus wall comprising a general shape of a conical frustum with at least a portion of the conical frustum convex toward the optical axis.

20 2. The optical lens of claim 1 additionally comprising a conductive coating on at least a portion of said meniscus wall.

3. The optical lens of claim 2 wherein the volume of oil is less than the volume of
25 saline solution contained within the cavity.

4. The optical lens of claim 3 wherein the volume of oil comprises about 66% or more by volume as compared to an amount of saline solution.

5. The optical lens of claim 3 wherein the volume of oil comprises about 90% or less by volume as compared to an amount of saline solution.
- 5 6. The optical lens of claim 2 wherein the volume of oil comprises a density about equal to a density of the saline solution.
7. The optical lens of claim 2 wherein the volume of oil comprises density within about 10% of a density of the saline solution.
- 10 8. The optical lens of claim 2 wherein the volume of oil comprises density within about 5% of a density of the saline solution.
9. The optical lens of claim 2 wherein the conductive coating extends from an area interior to the cavity to an area external to the cavity.
- 15 10. The optical lens of claim 9, wherein the area of conductive coating external to the cavity forms an electrical terminal for providing an electrical charge to the liquid meniscus lens.
- 20 11. The optical lens of claim 9 wherein the saline solution and the oil form a meniscus and an application of an electrical charge to the area of conductive coating external to the cavity causes a change in position of contact of the meniscus along the meniscus wall.
- 25 12. The optical lens of claim 9 wherein the electrical charge comprises a direct current.
13. The optical lens of claim 9 wherein the electrical charge comprises about 20.0 volts.

14. The optical lens of claim 9 wherein the electrical charge comprises between about 18.0 volts to 22.0 volts.
- 5 15. The optical lens of claim 9 wherein the electrical charge comprises about 5.0 volts.
16. The optical lens of claim 9 wherein the electrical charge comprises between about 3.5 volts to about 7.5 volts.
- 10 17. The optical lens of claim 3 wherein the front curve lens exterior surface comprises an optical power other than about 0.
18. The optical lens of claim 3 wherein the front curve lens interior surface comprises an optical power other than about 0.
- 15 19. The optical lens of claim 3 wherein the back curve lens exterior surface comprises an optical power other than about 0.
- 20 20. The optical lens of claim 3 wherein the back curve lens interior surface comprises an optical power other than about 0.
21. The optical lens of claim 3 additionally comprising a channel through one or both of the front curve lens and the back curve lens and a conductive material filling the channel.
- 25 22. The optical lens of claim 21 additionally comprising a terminal in electrical communication with the conductive material filling the channel.

23. The optical lens of claim 22 wherein application of an electrical charge to the terminal causes a change in the shape of the meniscus.
- 5 24. The optical lens of claim 3 additionally comprising an insulator coating along at least a portion of the interior surface of the front curve lens, wherein the insulator coating comprises an electrical insulator.
- 10 25. The optical lens of claim 24, wherein the insulator comprises one of Parylene C and Teflon AF.
26. The optical lens of claim 24 wherein the insulator comprises a boundary area to maintain separation between the conductive coating and a saline solution contained in the cavity between the front curve lens and the back curve lens.
- 15 27. The optical lens of claim 3 wherein an angle of the conical frustum with at least a portion of the conical frustum convex toward the optical axis comprises between about 30° and 50°.
- 20 28. The optical lens of claim 27 additionally comprising a meniscus sharp adjacent to the meniscus wall, said sharp comprising an angular feature for containing the volume of saline solution and oil.
29. The optical lens of claim 27 wherein the sharp comprises a radial surface portion.
- 25 30. The optical lens of claim 28 wherein the radial surface portion comprises a radius in the range of 5 microns to 25 microns.
- 30 31. The optical lens of claim 1 wherein the meniscus wall is formed in one or both of the front curve lens and back curve lens and bordering the meniscus formed between the saline solution and oil.