

Description

This invention relates to a heterojunction bipolar transistor.

There is continuing and increasing interest in improving the operating speed of bipolar transistors in microcircuits, particularly in the context of VLSI circuits for high-speed and ultra high-speed logic applications.

One route to such speed improvements, which has been relentlessly pursued to the practical limits of existing technology, is the reduction in feature size of the devices. In connection with this, new self-aligned processes, which remove the need to provide for alignment tolerances, continue to be developed.

An alternative route to achieving higher operating speeds is to use gallium arsenide (GaAs) or other related III-V compound semiconductors in place of silicon, since the electron mobility and saturation velocity are higher in GaAs and the other III-Vs than in silicon. Unfortunately, although at first sight it appears possible to achieve a respectable speed increase by producing GaAs versions of bipolar transistors which are conventionally made of silicon, such an approach does not in fact give rise to any significant improvement in performance. The problem is that, in such devices, it is necessary to keep the base width small, and use only low levels of base doping, with the result that the base resistance tends to be high. In order to keep the base resistance acceptably low, high hole mobility is needed. Unfortunately, although electron mobility in GaAs is high (which is useful for giving short emitter-collector transit times), hole mobility is less than half that of silicon, resulting in excessive base resistance.

An approach to making high speed bipolar devices in GaAs which gets round the limitation of poor hole mobility is to produce the device as a heterojunction bipolar transistor (HBT) using aluminium gallium arsenide (AlGaAs) and gallium arsenide (GaAs).

In an HBT, the emitter is formed of a material having a larger energy gap than the base, whereby injection of holes from the base into the emitter is prevented and it becomes possible to use heavy base doping, and hence very thin (100nm) base widths, without excessive base resistance.

Unfortunately, although HBTs theoretically offer quite exceptional performance (for more details of which see the review paper by Herbert Kroemer in PROC.IEEE, Vol.70, No. 1, January 1982), they have proved exceedingly difficult to make.

The bulk of the work done on HBTs has involved the use of AlGaAs and GaAs, in part because of the superior electronic properties of GaAs, but also because it is possible to make very high

quality AlGaAs-GaAs heterojunctions. Unfortunately, fabrication of GaAs HBTs is very complex because of the difficulties inherent in GaAs processing. In particular, the absence of a native oxide means that processing is limited to etching and non-selective deposition, which in turn means that GaAs devices are essentially non-planar. It can be seen, therefore, that there are appreciable costs associated with the speed advantages offered by GaAs. It is to the reduction of these costs, while realising the benefits of improved speed, that work on HBTs has been directed in recent years.

The comparative ease with which silicon can be processed and the ubiquitous nature of silicon processing together provide a strong incentive for the development of an HBT which is compatible with existing silicon technology. A few silicon based wide-gap emitter transistors have been reported. For example, gallium phosphide-silicon has been tried with disappointing results; and, with a heavily-doped "semi-insulating polycrystalline" silicon emitter on a silicon base (the polycrystalline/amorphous silicon having a wider band gap than that of the single crystal silicon of the base), the results achieved have been better, but are still a long way short of those obtained with AlGaAs/GaAs. Consequently, research on HBTs continues to be centred on the use of GaAs. US4529455 relates to the growth of SiGe/Si heterostructures in which the alloy layer is undoped and an associated wide band gap material is heavily doped. The growth of SiGe on Si substrates is considered in the Journal of Electronics Materials Vol. 12 No. 4 1983 H M Manasevit et al entitled "The Properties of Si/Si_{1-x}Ge_x films grown on Si substrates by chemical vapour deposition", the films of SiGe being in the form of superlattices.

The aim of the invention is to provide an HBT which is largely compatible with known silicon processing techniques.

The present invention provides a heterojunction bipolar npn transistor having an emitter which comprises an epitaxial layer of silicon grown on a non-superlatticed base layer having a strained lattice of a silicon and germanium alloy, the lattice strain being such as to produce a predetermined valence band offset at the emitter/base junction, the alloy being epitaxially and commensurately grown on a {100} plane of silicon, the base being heavily p-doped, and wherein the emitter zone within 0.15 micrometers of the interface between the emitter and the base is less heavily doped than the base.

Advantageously, the lattice strain is such as to enhance the effective mobility of electrons in the base. Preferably, the lattice strain is tailored throughout the base depth such that the energy separation between the low mobility and high mobility conduction bands is increased towards the

collector.

In a preferred embodiment, the germanium content of the silicon and germanium base layer lies within the range of from 12% to 20%, and is preferably at least 15%.

Using a silicon germanium alloy base, it is possible to produce devices which, apart from the growth of the heterolayers, are made using conventional silicon processing steps. The heterolayers may be grown using molecular beam epitaxy (MBE).

Embodiments of the invention will now be described with reference to the accompanying drawings in which:

Figure 1 shows six-fold degeneracy of the silicon conduction band;

Figure 2a shows the four-fold degeneracy of the conduction band of strained {100} Si-Ge layers;

Figure 2b shows the two-fold degeneracy of the conduction band of strained silicon;

Figure 3 shows the band discontinuity in {100} Si:Si-Ge;

Figure 4 shows the band structure of a conventional silicon bipolar transistor;

Figure 5 shows the doping levels of the same conventional silicon transistor;

Figure 6 shows the band structure of an HBT using Si:Si-Ge;

Figure 7 shows the doping levels for a HBT with 15% germanium content in the base; and

Figure 8 shows a simple mesa etched HBT.

Since silicon and germanium have different lattice constants, it is possible to tailor lattice strains by adjusting the relative proportions of silicon and germanium in the alloy layers. In this way, it is possible to engineer band structures and band offsets, so that charge carrier transport can be modified. However, layer thickness is limited, since dislocations result from excessive thickness, the critical thickness being dependent upon the germanium content.

In unstrained SiGe, the conduction band remains Si-like until the molar Ge content exceeds about 85%. It has a six-fold degeneracy with a conduction band minimum lying in each of the {100} directions (see Fig. 1). Thus, for an electron travelling in a given direction, the effective mass is averaged over all six minima since these are approximately equally occupied. In the {100} direction, this requires averaging over two heavy longitudinal masses ($0.98 m_0$) and four light transverse masses ($0.19 m_0$), and gives $0.45 m_0$, where m_0 is the stationary electron mass. But, for SiGe grown on a {100} Si plane, the unit cell is distorted from the cubic system into the orthorhombic, by forcing the atoms closer together in the plane. This breaks the six-fold conduction band degeneracy, and forces two minima up in energy (by about 150-170

meV when the Ge content is 20%) and four down (see Fig. 2). Thus, the lowest conduction band consists only of the four lobes which lie in the plane, and an electron traversing this layer experiences mainly the light transverse electron mass. The effective mass is, therefore, lowered to that of the transverse mass which is similar to that of silicon. Thus, in the strained layer, the electron's effective mass is reduced, and its mobility increased over that of unstrained alloys of the same composition. However, the mobility will not scale directly with effective mass.

If the heterostructure were to be grown on a {111} plane, the distortion would be from the cubic into the hexagonal system. As the six-fold symmetry of the resulting crystal would remain, the degeneracy of the conduction band would not be split, and the effective mass of the electron would not be significantly altered.

In addition to the mobility changes associated with the heterostructure, the layers of differing composition have different band-gaps and offsets. If SiGe layer is grown on a {100} Si substrate, there is a small discontinuity in the conduction band, but a major discontinuity in the valence band. Following growth on a SiGe substrate (which may simply be a thick SiGe buffer layer grown on Si), there is a discontinuity in both bands, as shown in Figure 3. This discontinuity varies with both strain and composition.

In the {111} direction, valence band offsets are similar to those in the {100} direction, but the conduction band in the Si is lower than in the SiGe for all substrates.

Figure 4 shows a schematic band structure of a conventional npn silicon transistor under normal bias conditions. Because the emitter has to be very heavily doped, it suffers bandgap narrowing, and there is a smaller barrier to holes than to electrons at the base-emitter junction. As the current gain in a well-designed transistor is given largely by the ratio of electrons and holes crossing this junction, the base must have a much lower doping than the emitter. This also prevents breakdown. For high frequency operation, the base must be narrow, because the electrons drift across this (with a low effective acceleration voltage of kT/q , where k is Boltzmann's constant, T is the thermodynamic temperature, and q is the charge). Consequently the collector must have a low doping, so that the depletion layer is in the collector rather than in the base, otherwise the base would punch through at too low a collector voltage. This gives a large depletion region, and a large contribution to the transit time, even though the electrons traverse it at saturated drift velocity. A compromise is usually made between punch-through voltage, collector transit time and collector capacitance, whereby the

collector doping is increased deeper into the transistor. A typical doping regime is shown in Figure 5.

As well as the time taken for the electrons to traverse the base and the collector, there is a component of transit time given by the product of the emitter resistance and the sum of base-emitter and base-collector capacitance. As the emitter resistance is the slope resistance of the diode, its value falls as emitter current increases. The transistor must, therefore, be operated at the highest possible value of current density to get the best speed. However, when the density of electrons injected into the base from the emitter becomes too large, the base-collector junction is pushed into the collector (the Kirk effect), and the time taken for electrons to drift across the base increases sharply. Thus, there is a natural maximum operating current which is related to the base doping.

The effects of these individual time constants are summed into one figure of merit, the transit frequency f_t , which is inversely proportional to the sum of the transit times. Clearly, the larger this parameter is, the faster circuits can operate. However, when a real transistor is made, the circuit is also slowed down by the time constant of the base resistance and the collector-base capacitor. A second figure of merit f_{max} is applied which takes account of this effect. As the base is low-doped, the base resistance is high, and only by using very fine dimensions (particular layer-layer tolerances) can f_{max} be made reasonably large. Self-aligned bipolar transistors are under development, and these promise very large values of f_{max} , such that f_t once again becomes the limiting factor. Values of f_t in excess of 10-15 GHz are extremely difficult to achieve with a conventional device.

Because there is an energy barrier preventing hole injection into the emitter, the wide-gap emitter HBT allows gain to be high, even for a heavily-doped base. Thus base resistance can be very low. More importantly, the base does not widen (as a result of the Kirk effect) until a much higher injection level, and the transistor may be operated at a significantly higher current density, thus reducing the emitter charging time. Also, the collector doping can be increased, without pushing the depletion region into the base, and the collector transit time is also reduced. Since the base width is less sensitive to operating voltage, it can be made somewhat smaller, to reduce its transit time. Finally, if a strained SiGe {100} layer is used for the base, the predicted mobility will reduce the base transit time even further.

Thus the silicon-germanium HBT offers a way to increase f_t substantially above the values available with silicon bipolar transistors. A value of 20 GHz should be feasible for a 0.15-0.2 μm base width, with further improvement possible at even

narrower dimensions.

The foregoing theory suggests the use of a Si emitter with a SiGe base grown commensurately on {100} Si. Figure 6 shows the band structure of a suitable layer arrangement.

An example of a Si-Ge HBT of a very simple construction is shown in Figure 8. The relevant doping profiles are shown in Figure 7. This simple structure is readily formed using molecular beam epitaxy (MBE) and mesa etching.

At a base width of between 0.15 and 0.2 μm , the germanium content in the SiGe layer can be up to 20%, giving a bandgap discontinuity in the valence band of about 150 meV, whilst maintaining commensurate growth of the SiGe layer on the Si substrate. Preferably, the germanium content of the SiGe layer is at least 15%, though useful results are obtained with a lower germanium content. Assuming equal Gummel numbers in the base and the emitter, a germanium content of 20% would give a gain of ~ 300 , and this allows the base Gummel number to exceed that of the emitter. With a high base doping of $1\text{E}19$, and an emitter doping of around $1\text{E}18$, a gain of ~ 100 is obtained. This is an ideal value to give the required 3-5 V emitter-base breakdown voltage. To make contact to the emitter, this doping level is inadequate, but it can safely be increased at the surface, at a distance of at least 0.15-0.2 μm from the base. The collector can be doped at $1\text{E}16$ to $2\text{E}16$ to give a fairly short transit time, and ample breakdown voltage, but should rise to a buried layer of $1\text{E}19$ at a distance of about 0.2-0.5 μm . With this doping profile, the collector must be silicon to ensure that the bandgap difference at the emitter junction appears in the valence band rather than the conduction band. The band discontinuity at the collector junction has little effect, as it is swamped by the applied bias.

For a simple structure, such as that shown in Figure 8, the collector contact can be made to the back of the wafer, and the emitter area can be defined by a mesa etching technique. Mesa etching right through the base layer, to reduce the base/collector contact area may be beneficial, but this etch need not be controlled accurately. Figure 8 shows the structure formed in this manner, and Figure 7 shows the required doping profiles.

For integrated devices, it is of course necessary to deposit dielectric and metal layers. This can be done using the techniques used in silicon processing. For high performance devices, selective epitaxy offers a method of reducing base area and also permits the introduction of heteroepitaxy after initial processing. This avoids problems with temperature cycling of strained materials.



Claims

1. A heterojunction bipolar npn transistor having an emitter which comprises an epitaxial layer of silicon grown on a non-superlatticed base layer having a strained lattice of a silicon and germanium alloy, the lattice strain being such as to produce a predetermined valence band offset at the emitter/base junction, the alloy being epitaxially and commensurately grown on a {100} plane of silicon, the base being heavily p-doped, and

wherein the emitter zone within 0.15 micrometers of the interface between the emitter and the base is less heavily doped than the base.

2. A bipolar transistor as claimed in Claim 1, wherein the emitter is doped to about $1E18$ within 0.15 micrometers of its interface with the base and the base is doped to $1E19$.

3. A bipolar transistor as claimed in any one of the preceding claims, wherein the lattice strain is such as to enhance the effective mobility of electrons in the base, above that of unstrained material of the same composition.

4. A bipolar transistor as claimed in any one of the preceding claims, wherein the lattice strain is tailored throughout the base depth such that the energy separation between the two-fold and four-fold degenerate conduction bands is increased towards the collector.

5. A bipolar transistor as claimed in any one of the preceding claims, wherein the germanium content of the silicon and germanium base layer lies within the range of from 12% to 20%.

6. A bipolar transistor as claimed in Claim 5, wherein the germanium content of the base is at least 15%.

7. A bipolar transistor as claimed in any one of the preceding claims, wherein the transistor is fabricated by selective epitaxy.

Patentansprüche

1. Bipolarer npn-Transistor mit Heteroübergang, mit einem Emittor, der eine auf eine übergritterlose Basisschicht mit einer verspannten Schicht aus einer Legierung von Silicium und Germanium aufgewachsene epitaktische Siliciumschicht umfaßt, wobei die Gitterspannung beschaffen ist, um eine vorgegebene Valenz-

bandverschiebung am Emittor-Basis-Übergang zu erzeugen, die Legierung im richtigen Verhältnis (commensurately) epitaktisch auf einer Silicium-100-Ebene aufgewachsen ist, die Basis stark p-dotiert ist und wobei der Emittorbereich innerhalb eines Abstands von $0,15 \mu m$ von der Grenzschicht zwischen Emittor und Basis weniger stark dotiert ist als die Basis.

2. Bipolartransistor nach Anspruch 1, bei dem der Emittor innerhalb eines Abstands von $0,15 \mu m$ von seiner Grenzschicht zur Basis mit ca. $1 \cdot 10^{18}$ und die Basis mit $1 \cdot 10^{19}$ dotiert ist.

3. Bipolartransistor nach einem der vorhergehenden Ansprüche, bei dem die Gitterspannung beschaffen ist, um die effektive Beweglichkeit von Elektronen in der Basis gegenüber unverspanntem Material derselben Zusammensetzung zu erhöhen.

4. Bipolartransistor nach einem der vorhergehenden Ansprüche, bei dem die Gitterspannung über die Tiefe der Basis so bemessen ist, daß der Energieabstand zwischen den zweifach und vierfach degenerierten Leitungsbändern zum Kollektor hin zunimmt.

5. Bipolartransistor nach einem der vorhergehenden Ansprüche, bei dem der Germaniumgehalt der Basisschicht aus Silicium und Germanium im Bereich von 12 % bis 20 % liegt.

6. Bipolartransistor nach Anspruch 5, bei dem der Germaniumgehalt der Basis wenigstens 15 % beträgt.

7. Bipolartransistor nach einem der vorhergehenden Ansprüche, hergestellt durch selektive Epitaxie.

Revendications

1. Transistor npn bipolaire à hétérojonction ayant un émetteur qui comprend une couche épitaxiale de silicium qui croît sur une couche de base non surstructurée ayant un réseau déformé d'un alliage de silicium et de germanium, la déformation du réseau étant telle qu'elle peut produire une compensation de la bande de valence prédéterminée à la jonction émetteur/base, l'alliage croissant de manière épitaxiale et proportionnée sur un plan {100} de silicium, la base étant fortement dopée en p, et dans lequel la zone de l'émetteur à l'intérieur de 0.15 micromètres de l'interface entre l'émetteur et la base est moins fortement dopée que la base.



2. Transistor bipolaire selon la revendication 1, dans lequel l'émetteur est dopé à environ $1E18$ à l'intérieur de 0.15 micromètres de son interface avec la base et la base est dopée à $1E19$. 5
3. Transistor bipolaire selon l'une des revendications précédentes, dans lequel la déformation du réseau est telle qu'elle augmente la mobilité effective des électrons de la base au-delà de celle d'un matériau non déformé de même composition. 10
4. Transistor bipolaire selon l'une des revendications précédentes, dans lequel la déformation du réseau est adaptée sur toute la profondeur de la base de sorte que la séparation d'énergie entre les bandes de conduction dégénérées double ou quadruple est augmentée vers le collecteur. 15 20
5. Transistor bipolaire selon l'une des revendications précédentes, dans lequel la teneur en germanium de la couche de base de silicium et de germanium est comprise entre 12% et 20 %. 25
6. Transistor bipolaire selon la revendication 5, dans lequel la teneur en germanium de la base est d'au moins 15 %. 30
7. Transistor bipolaire selon l'une des revendications précédentes, dans lequel le transistor est fabriqué par épitaxie sélective. 35

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