

DESCRIPTION

PROCESS FOR THE PREPARATION OF SILANE POLYSULFIDES

Technical Field

The invention is directed to the preparation of sulfur-containing organosilicon compounds useful as coupling agents in vulcanizable rubbers to enhance products made from them. In its preferred form, the invention
5 improves the preparation of Ω,Ω' -bis (trialkoxysilylalkyl) polysulfides.

Sulfur-containing organosilicon compounds have found widespread use in a variety of rubber products in the last two decades. Uses include tire walls and bodies, rubber hoses, rubber belts, and numerous other rubber products. Depending on the formulation, selected properties of the
10 rubber can be modified.

Since the early 1980's, automobile manufacturers have been encouraging the production of low-rolling-resistance tires. A number of sulfur-containing organosilicon compounds have been identified as useful in this regard. The improvements obtainable could be helpful in meeting federal
15 fuel economy standards without sacrificing wet traction and wear. Silane polysulfide coupling agents, such as 3,3'-bis (triethoxysilylpropyl) tetrasulfide, have been proposed for use in low-rolling-resistance tires.

To achieve optimum effect, it has been found that each low-rolling-resistance tire should contain several ounces of this or another suitable silane.

5 There is a need for new processes to produce organosilane polysulfides effective for use in low-rolling-resistance tires, and other uses, in good yield to permit economical production of large quantities with controllable safety and environmental impact.

Background Art

10 The art of manufacturing organosilane polysulfides is well established, with the art offering a variety of processing strategies.

Meyer-Simon, Schwarze, Thurn, and Michel disclose the reaction of a metal polysulfide with an Ω -chloroalkyltrialkoxysilane in U.S. Patent 3,842,111. Example 2 shows the preparation of 3,3'-bis (triethoxysilylpropyl) tetrasulfide by reacting Na_2S_4 with 3-
15 chloropropyltriethoxysilane in absolute ethanol. The procedure for preparing the metal polysulfide is not exemplified, and the examples imply that this starting material is an isolated compound.

In U.S. Patent 4,072,701, Pletka describes the preparation of sulfur-containing organosilicon compounds by first heating 3-
20 chloropropyltrichlorosilane (Example 1) with ethanol, and then adding both sulfur and NaSH in the presence of alcohol. The reaction developed gaseous hydrogen sulfide *in situ*, but some of the sulfur therein was not recoverable (see, U.S. Patent 4,129,585, col. 1, lines 32-34, in this regard). Therefore, the yields based on added sulfur tended to be low. Also, the
25 use of NaSH is problematic due to its deliquescent nature and its tendency

to oxidize to sulfate. The deliquescence is troublesome from the standpoint that it increases the risk that water will enter the reaction and cause hydrolysis of the alkoxide reactants.

After describing the above two patents in U.S. Patent 4,129,585,
5 Buder, Pletka, Michel, Schwarz and Düsing, describe a procedure for making the noted compounds without the production of gaseous hydrogen sulfide. The process entails reacting a suitable alkali metal alcoholate, *e.g.*, sodium ethoxide, in preferably alcoholic solution with a desired Ω -chloroalkyltrialkoxysilane, a suitable metal hydrogen sulfide, and sulfur. The
10 resulting product was purified by separating the salt formed and distilling off the alcohol. Again, the use of the metal hydrogen sulfide can be a source of water entering the system unless precautions are taken. French and Lee also disclosed a process that employed an alkali metal hydrogen sulfide such as NaSH in a separate step (U.S. Patent 5,399,739).

15 In U.S. Patent 4,507,490, Panster, Michel, Kleinschmidt and Deschler, first prepare Na_2S . Again, they employ a metal hydrogen sulfide but react it with an alkali metal, such as sodium, in a polar solvent, such as ethanol. This reaction is highly exothermic and evolves hydrogen gas. The process is said to eliminate the use of an alkali metal alcoholate solution,
20 noting that its production requires such a great deal of time as to be industrially improbable. The Na_2S is reacted with additional sulfur to form a desired polysulfide, preferably Na_2S_4 . The polysulfide is then reacted with a desired Ω -chloroalkyl trialkoxysilane, *e.g.*, $\text{Cl}(\text{CH}_2)_3\text{Si}(\text{OC}_2\text{H}_5)_3$, to form the desired Ω, Ω' -bis (trialkoxysilylalkyl) polysulfide.

25 Janssen and Steffen, in U.S. Patent 3,946,059, offer a distinct approach and criticize procedures of the type described above. They eliminate the production, and therefore separation, of salts formed in the above reactions by contacting a bis (alkylalkoxysilyl) disulfide with sulfur at

a temperature between 100° and 200°C. This procedure, however, adds the difficulty of the high temperature processing and requires the initial preparation of bis-silyl disulfides by the reaction of sulfuryl chloride with silyl mercaptans. Parker, *et al.*, also disclosed a somewhat complicated process involving a phase transfer catalyst and an aqueous phase (U.S. Patent 5,405,985).

While the possibility might appear to exist that commercial forms of alkali metal sulfides, *e.g.*, sodium tetrasulfide, could be employed, this would not be practical. The commercial forms of sodium tetrasulfide include water which must be completely removed prior to contact with the alkoxylates. If water is present, the alkoxide is hydrolyzed and a polysiloxane polymer is formed. And, while Bittner, *et al.* teach in U.S. Patent 4,640,832, the reaction of sodium salts with hydrogen sulfide, this route has certain economic and practical limitations. Reaction temperatures are high; for formation of Na_2S_3 or Na_2S_4 , for example, the reaction is preferably run at 340° to 360°C. At these temperatures, the polysulfides are corrosive so that choosing an appropriate reaction vessel is imperative; costly alloys of aluminum and magnesium are suggested, as is the use of glassy carbon.

Thus, the prior art has typically found the use of hydrogen sulfide gas, the separation of sodium chloride and the preparation of metal alkoxylates to be problematic in the preparation of sulfur-containing organosilicon compounds, and did not recognize that there was possible a reaction scheme which efficiently and effectively combines all of them. The invention provides a process which combines these and still obtains high yields based on sulfur.

Summary of the Invention

It is an object of the invention to provide improved processes for preparing sulfur-containing organosilicon compounds useful as coupling agents in vulcanizable rubbers.

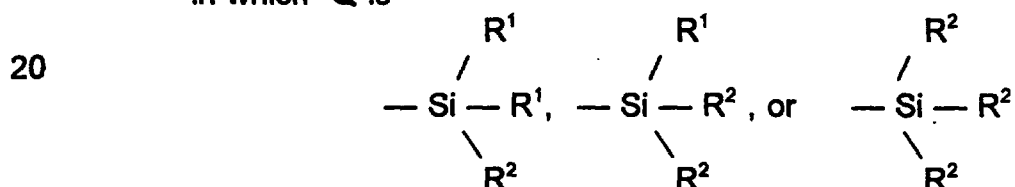
- 5 It is a further object of a preferred aspect of the invention to provide improved processes for preparing Ω, Ω' -bis (trialkoxysilylalkyl) polysulfides useful in the preparation of a variety of rubber products, specifically including low-rolling-resistance tires.

- 10 It is a further and more specific object of the invention to prepare 3,3'-bis (triethoxysilylpropyl)tetrasulfide economically in high yield.

These and other objects are achieved by the invention which provides a process for preparing silane polysulfides, comprising:

- (a) contacting hydrogen sulfide gas with an active metal alkoxide solution;
- 15 (b) reacting elemental sulfur with the product of step (a); and
- (c) reacting the product of step (B) with a halohydrocarbylalkoxysilane of the formula $Q - R - X$

in which Q is



and in which

- 25 R^1 is an alkyl group of 1 to 4 carbon atoms or phenyl, and R^2 is an alkoxy group with 1 to 8, preferably 1 to 4, carbon atoms,

a cycloalkoxy group including 5 to 8 carbon atoms, or a straight or branched chain alkylmercapto group with 1 to 8 carbon atoms,

wherein the various R^1 and R^2 groups can be the same or different,

R is a divalent hydrocarbyl group including 1 to 18 carbon atoms, and

X is a halogen,

to produce a compound of the formula $Q - R - S_n - R - Q$

in which Q and R are as defined above, and n is an integer of from 2 to 9, preferably from 3 to 5. The reaction mixture can contain a number of compounds meeting this formula, and the average can be a fractional number.

In an alternate embodiment, the process combines steps (b) and (c) and comprises reacting the product of step (a) with a slurried mixture of elemental sulfur and a halohydrocarbylalkoxysilane of the formula $Q - R - X$ to obtain the product $Q - R - S_n - R - Q$, where Q, R, X and n are as defined above.

In a preferred embodiment, the product is 3,3'-bis (triethoxysilylpropyl) tetrasulfide, represented by the formula



and is prepared by: (a) contacting an ethanol solution of sodium ethoxylate with hydrogen sulfide gas to produce a solution of Na_2S , (b) adding elemental sulfur to the solution of Na_2S in an amount sufficient to form Na_2S_4 , and adding $Cl(CH_2)_3Si(OC_2H_5)_3$ to the resulting reacting mixture and carrying the reaction to completion. Alternatively, it is prepared by contacting an ethanol solution of sodium ethoxylate with hydrogen sulfide gas to produce a solution of sodium sulfide, and then reacting the intermediate product so produced in a slurry with elemental sulfur and

$\text{Cl}(\text{CH}_2)_3\text{Si}(\text{OC}_2\text{H}_5)_3$ and carrying the reaction to completion. By the use of either embodiment of the invention, silane polysulfides of high quality are prepared efficiently and in good yield.

- 5 All parts and percentages in this description are on a weight basis and are based on the weight of the composition at the referenced stage of processing.

Detailed Description

- 10 The invention, which relates to the preparation of sulfur-containing organosilicon compounds useful for a variety of purposes, especially as coupling agents in vulcanizable rubbers, will be described with special reference to the preparation of a preferred class of compounds, the Ω,Ω' -bis (trialkoxysilylalkyl) polysulfides.

- 15 Among this class of compounds are a large number of materials, including the various polysulfides listed below wherein the term polysulfide includes all of the di, tri, tetra, penta, hexa, hepta, octa, and nona-sulfides according to the following formulae:

- 20 bis (trimethoxysilylmethyl) polysulfides, bis (triethoxysilylmethyl) polysulfides, bis (dimethylethoxysilylmethyl) polysulfides, bis (tripropoxysilylmethyl) polysulfides, bis (tributoxysilylmethyl) polysulfides, bis (tripentoxysilylmethyl) polysulfides, bis (trihexoxysilylmethyl) polysulfides, bis (triheptoxysilylmethyl) polysulfides, and bis (trioctyloxysilylmethyl) polysulfides;

- 25 3,3'-bis (trimethoxysilylpropyl) polysulfides, 3,3'-bis (triethoxysilylpropyl) polysulfides, 3,3'-bis (dimethylethoxysilylpropyl) polysulfides, 3,3'-bis (tripropoxysilylpropyl) polysulfides, 3,3'-bis (tributoxysilylpropyl) polysulfides, 3,3'-bis (tripentoxysilylpropyl) polysulfides,

3,3'-bis (trihexoxysilylpropyl) polysulfides, 3,3'-bis (triheptoxysilylpropyl) polysulfides, 3,3'-bis (trioctyloxysilylpropyl) polysulfides, and 3,3'-bis (methyldiethoxysilylpropyl) polysulfides;

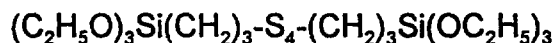
- 4,4'-bis (trimethoxysilylbutyl) polysulfides, 4,4'-bis (triethoxysilylbutyl) polysulfides, 4,4'-bis (dimethylethoxysilylbutyl) polysulfides, 4,4'-bis (tripropoxy-silylbutyl) polysulfides, 4,4'-bis (tributoxysilylbutyl) polysulfides, 4,4'-bis (tripentoxysilylbutyl) polysulfides, 4,4'-bis (trihexoxysilylbutyl) polysulfides, 4,4'-bis (triheptoxysilylbutyl) polysulfides, and 4,4'-bis (trioctyloxysilylbutyl) polysulfides;
- 5,5'-bis (trimethoxysilylpentyl) polysulfides, 5,5'-bis (triethoxysilylpentyl) polysulfides, 5,5'-bis (dimethylethoxysilylpentyl) polysulfides, 5,5'-bis (tripropoxy-silylpentyl) polysulfides, 5,5'-bis (tripentoxysilylpentyl) polysulfides, 5,5'-bis (trihexoxysilylpentyl) polysulfides; and
- 5,5'-bis (triheptoxysilylpentyl) polysulfides, and 5,5'-bis (trioctyloxysilylpentyl) polysulfides.

Similarly, the 6,6'-bis (trialkoxysilylhexyl) polysulfides; the 7,7'-bis (trialkoxysilylheptyl) polysulfides; the 8,8'-bis (trialkoxysilyloctyl) polysulfides; the 9,9'-bis (trialkoxysilylnonyl) polysulfides; the 10,10'-bis (trialkoxysilyldecyl) polysulfides; and the isomers of these are included. Indeed, this disclosure is meant to include, each of the individual compounds comprised of combinations of the various groups encompassed by the generic formula



wherein, Q, R and n are as defined above. As used herein, where n is defined as an integer, e.g., 4, because of the method of preparation the formula typically describes mixtures of distinct polysulfides wherein n has a range of values which average to 4.

This description illustrates the production of the preferred compound, 3,3'-bis (triethoxysilylpropyl) tetrasulfide:



by either embodiment of the process described above. At times in the following description, Et is used to designate an ethyl group and Me is used to designate a methyl group.

Preparation of the Active Metal Alkoxide

As noted above, the process can be used to prepare a large number of end products. For each of these it is necessary to start with an active metal alkoxide solution, which is typically derived by prereacting a active metal with an alcohol. The active metal alkoxide will have the formula M-R^2 , wherein M represents an active metal and R^2 is as defined above. Among the preferred active metals are those of the alkali metal group, especially sodium and potassium. The most preferred is sodium. However, among the other metals useful are lithium, rubidium and cesium. Among the preferred alkoxides are those containing methoxy, ethoxy, *n*-propoxy, *i*-propoxy, *n*-butoxy, *i*-butoxy, 2-methoxyethoxy or 2-ethoxyethoxy groups.

The prereaction, if performed, is carried out in a suitable organic solvent compatible with the alkoxide. In principle, any polar organic solvent can be employed that reacts with neither the alkali or other metal nor with the organic silicon compounds to form an undesired byproduct.

Preferably, the organic solvent is a linear or branched alcohol having 1 to 5 carbon atoms, e.g., methyl, ethyl, propyl, butyl or pentyl alcohol, as well as *iso*-propyl alcohol, *iso*-butyl alcohol and 2-methoxyethanol. Also suitable are cycloalkyl alcohols having 5 to 8 carbon atoms, e.g., cyclopentyl alcohol, cyclohexyl alcohol, cyclooctyl alcohol, phenyl or benzyl alcohol. It is useful to employ the alcohol which in each case corresponds

to the R^2 group. In a given case, advantageously there can also be used a mixture of these alcohols, e.g., when different R^2 groups are used in a compound. Particularly preferred are methanol and ethanol, preferably in absolute form. In one preferred process, sodium metal is reacted with
 5 ethanol to form an ethanolic solution of sodium ethoxylate.

The reaction of active metal, e.g., sodium metal, and a suitable alcohol, e.g., ethanol, is preferably conducted with an excess of alcohol to produce a metal alkoxide, e.g., sodium ethoxide, solution. The following equation summarizes the reaction:



The sodium or other metal should be maintained free of contact with moisture. The manufacture of sodium methoxide has been described by Arend (Arend, A. G., *Perfumery Essent. Oil Record*, 28, 372-75, 1947). The preferred sodium ethoxide reaction is similar to, but slower than, the
 15 sodium methoxide reaction.

The concentration of the sodium ethoxide solution may be as low as about 10 wt % and as high as its solubility limit, which is about 25 wt % at 25°C. A high concentration of sodium ethoxide is desirable, since better product yields for given reactor size are obtained. The typical concentration
 20 for commercially-available sodium ethoxide is about 21 wt %.

The H_2S -Active Metal Alkoxide Reaction

H_2S (hydrogen sulfide) gas is reacted with the active metal alkoxide (e.g., sodium ethoxide) in a suitable solvent (e.g., ethanol) to produce a suitable active metal sulfide, e.g., Na_2S :



This reaction can be performed in production quantities of from about 50 to about 5,000 pound batches. Continuous and semi-continuous processes can also be employed. Preferably, the reaction is carried out with an excess of ethanol, typically charging the preferred sodium ethoxide
5 raw material as a 21 wt % solution in ethanol. The preferred reaction between hydrogen sulfide gas and sodium ethoxide employs a molar feed ratio of the hydrogen sulfide to the sodium ethoxide of 1:2.

The reaction is conveniently conducted in a semi-batch mode. First, all of the metal alkoxide is added to the reactor. Then, the reactor
10 contents are heated to a temperature effective for reaction, in the preferred case discussed, within the range of from about 40° to about 50°C, e.g., about 50°C. The hydrogen sulfide gas is then fed to the reactor. The hydrogen sulfide feed rate is not critical, typically it will be of the order of one hour, but will vary with equipment and batch size. At the end of the
15 reaction, most of the active metal sulfide is in solution. However, some solid active metal sulfide particles may be present. In general, it is desirable to keep the system agitated until the next step.

Preferably, the reactor is maintained at a temperature between about 40° and about 60°C during the hydrogen sulfide addition to avoid discolor-
20 ation. The reaction necessitates some degree of cooling. After the hydrogen sulfide addition is completed, it is desirable to purge out the feed conduit with nitrogen to prevent draw back of liquid. After the purge, the kettle is preferably cooled, e.g., to about 25°C, and then vented to atmospheric pressure through a reflux condenser to trap out any ethanol
25 vapors while maintaining the kettle blanketed with nitrogen gas.

The system is preferably equipped with a scrubber or absorber for capturing hydrogen sulfide emissions. Strong sodium hydroxide is a good scrubbing medium. The reaction is preferably conducted in a mechanically-

agitated kettle to assure good gas-liquid mixing to facilitate the reaction of the hydrogen sulfide with the active metal alkoxide. The hydrogen sulfide gas is desirably fed subnatantly via a diptube or gas sparger located near or preferably below the agitator.

- 5 Stoichiometry is important. The desired ratio is one mole of hydrogen sulfide per two moles of active metal alkoxide, with a preferred accuracy of hydrogen sulfide addition being about $\pm 3\%$.

Sulfur Addition and Reaction

- In one embodiment, after the hydrogen sulfide reaction is completed,
 10 the reaction mixture is cooled, e.g., to about 25° , then sulfur, preferably in powdered form, is added to the reactor in an amount sufficient to form the desired active metal polysulfide. When the sulfur addition is complete the reactor is reheated, e.g., to about 45°C . During this period, the system is preferably maintained at atmospheric pressure under a nitrogen blanket.
 15 For the preparation of sodium tetrasulfide from sodium sulfide, the molar feed ratio of sulfur to sodium sulfide is 3:1, but can be varied as needed to obtain polysulfides having 2 to 9 sulfur atoms. During the heating, the following reaction preferably occurs in this embodiment of the process:



- 20 It is preferred to maintain agitation in the reactor after the sulfur addition, sufficient to insure solubilization and reaction. It is also preferred, during and after the sulfur addition, to keep air out of the kettle to avoid oxidation which may contribute to a darkening of product color.

Halohydrocarbyltrialkoxysilane

Both embodiments of the process of the invention employ a halohydrocarbyltrialkoxysilane. These compounds meet the general formula $Q - R - X$ in which Q and R are as defined above and X is a halogen, typically chlorine, but bromine, iodine and fluorine compounds can be effective. In this formula, and therefore also in the final product, the hydrocarbyl group R signifies methylene as well as preferably *n*-propylene, *i*-butylene, or *n*-butylene, but can also be *n*-pentylene, 2-methylbutylene, 3-methylbutylene, 1,3-dimethylpropylene, *n*-hexylene, or *n*-decylene.

Illustrative compounds within formula $Q - R - X$ are 3-chloropropyl-triethoxysilane, 3-bromopropyltriethoxysilane, chloromethyltrimethoxysilane, 3-chloropropyltrimethoxysilane, 3-chloropropyldiethoxymethylsilane, 3-chloro-propylcyclohexoxydimethylsilane, 4-bromobutyldiethoxybenzylsilane, 4-chloro-butyltrimethoxysilane, 5-chloropentyldimethoxyphenylsilane, 3-bromo-*i*-butyl-triethoxysilane, 3-chloropropyldimethoxy-*p*-ethylphenylsilane, 3-chloropropylethoxymethylethylsilane, 5-chloro-*n*-pentyldiethoxycyclopentylsilane, 3-bromo-propyldimethoxycyclopentoxysilane, 3-bromo-2-methylpropyldimethoxy-cyclooctylsilane, 3-chloropropyldiethoxy-2-methoxyethoxy-silane, 3-chloropropyl-dibutoxymethylsilane, 3-bromopropylphenyloxydimethoxysilane, 3-chloropropyl-di-*i*-butoxy-2-methylphenylsilane, 4-chlorobutyldimethoxybenzyloxysilane, 3-chloropropyltributoxysilane, 3-chloropropyldiethoxyamylsilane, and 3-chloropropyldiethoxy-*p*-methylphenylsilane.

Again here, as in the case of the inclusion of compounds meeting the definition of the formula for the end products, this disclosure is meant to include each of the individual compounds comprised of combinations of the

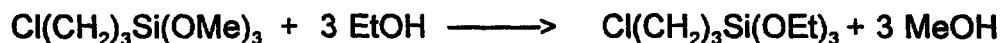
various groups encompassed by the generic formula $Q - R - X$ in which Q, R and X are as defined above.

In the first embodiment of the invention, a halohydrocarbyltrialkoxysilane is reacted with the sodium polysulfide formed as described above. In a preferred form of this embodiment, a
 5 chloroalkylalkoxysilane is reacted with the sodium polysulfide. The chloroalkylsilane can be purchased or prepared according to any of the techniques available to those of ordinary skill in the art. One preferred practice is to prepare it by transesterification of $Cl(CH_2)_3Si(OMe)_3$.

10

Alternatively, the methoxy ester can be employed to form 3,3'-bis (trimethoxyalkoxysilane) polysulfide, and this product can then be converted to the ethyl or higher ester by transesterification *in situ*.

Using this procedure, $Cl(CH_2)_3Si(OEt)_3$ can be prepared by the
 15 following transesterification reaction, typically at a temperature of from about 70° to about 100°C and atmospheric pressure using about 2000 ppm para-toluenesulfonic acid:

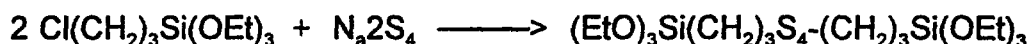


This reaction is preferably run by continuously feeding ethanol while
 20 removing by-product methanol from the system to drive the equilibrium toward chloropropyltriethoxysilane. The reaction can conveniently begin at atmospheric pressure and reflux temperatures, *i.e.*, a pot temperature of from about 80° to about 100°C. At the end of the reaction, the excess ethanol can be stripped off using vacuum and a somewhat higher
 25 temperature. A typical final condition for the ethanol strip would be a temperature of about 120°C and a pressure of about 100 mm Hg.

Reaction of Active Metal Polysulfide with Halohydrocarbyltrialkoxysilane

In the first embodiment, the active metal polysulfide formed by reacting the sodium sulfide with sulfur is reacted with the

- 5 halohydrocarbyltrialkoxysilane. The feed of halohydrocarbyltrialkoxysilane (preferably, chloroalkyltrialkoxysilane) to the reactor is preferably started as soon as a temperature of about 45°C is reached after the sulfur addition as described above. The preferred reaction is:



10 Sulfur and Halohydrocarbyltrialkoxysilane Addition and Reaction

- In an alternate process of the invention, a halohydrocarbyltrialkoxysilane described above is reacted with sulfur and the H₂S-active metal alkoxide prepared above in one step. The active metal sulfide solution is added to a slurry of elemental sulfur in the
- 15 halohydrocarbylalkoxysilane. After the hydrogen sulfide addition and reaction is completed, the reaction mixture is cooled, *e.g.*, to about 25°C, and the solution is added to a slurry of S/Cl(CH₂)₃Si(OEt)₃ at around 40° to 45°C, until addition is complete, at a rate commensurate with the heat removal capability of the reactor. In laboratory glassware, this may require
- 20 from about 1 to 3 hours. When the addition is complete, the reactor is preferably heated to about 80°C and held at reflux for a suitable time, *i.e.*, from about 1 to 3 hours, typically about 1.5 hours. It is preferred to maintain agitation in the reactor to insure solubilization and reaction, and to maintain in suspension the salt particles formed during the reaction. During
- 25 this period, the system is preferably maintained at atmospheric pressure under a nitrogen blanket, to keep air out of the kettle to avoid oxidation which may contribute to a darkening of product color. After this reflux period, the reactor is immediately cooled, *i.e.*, to about 25°C.

For the preferred product, the desired reaction is:



Salt Removal

5 The reactions employed in either embodiment produce the desired product and also produce salt. In the preferred reactions, sodium chloride salt produced in the sulfur and chloropropyl-triethoxysilane addition step can be removed by filtering or centrifuging. If filtration is used, the media pore size should be about 5μ . Typically, no filter aid is necessary since the
10 average particle size is fairly large, but one can be employed if needed. If centrifuging is employed, a basket or continuous scroll-type device can be employed.

The resulting filtercake will contain residual liquid product and can be washed, e.g., with ethanol to improve overall product yield.

15

Solvent Strip

The process preferably includes a step of stripping off detrimental levels of solvent, preferably reducing the solvent concentration to less than about 5% by weight. In the preferred process embodiments as described above, assuming an ethanol wash has not been used, the crude product
20 contains about 60 wt % ethanol. Stripping, preferably in a single stage, can be employed to yield a product containing less than about 2 wt % ethanol. One suitable stripping technique is batch stripping of the crude material in a reactor, e.g., to a final condition of 100°C and 50 mm Hg absolute pressure. A small quantity of salt may precipitate out during the ethanol strip, and it is
25 preferred to subject the product to a final filtration as necessary to remove this.

EXAMPLES

The following examples are presented for the purpose of further illustrating and explaining the invention, and are not to be taken as limiting in any regard. Unless otherwise indicated, all parts and percentages are based on the weight of the components at the indicated stage of processing.

Example 1

This example describes the preparation of the preferred end product, 3,3'- bis (triethoxysilylpropyl) tetrasulfide. To accomplish this result, sodium ethoxide was prepared fresh, as was sodium tetrasulfide.

Preparation of Sodium Ethoxide

To a 500 ml glass reactor equipped with a feed funnel, a reflux column, a fritted glass sparge tube and thermometer, 17.0 grams of dry sodium chunks were added. Then, the reactor and the column were purged with N₂ for >5 minutes. Then, 227.4 grams of ethanol were charged into the feed funnel. During this step, the ethanol was added slowly enough to prevent the sodium from melting. After 85 minutes, all of the sodium was dissolved and the reactor was cooled from about 80°C to about 40°C for the next step.

H₂S Reaction with Sodium Ethoxide

Addition of hydrogen sulfide gas was started through a fritted glass sparge tube. The reaction was run with vigorous agitation during sparge.

During a feed time of about 54 minutes, 10.31 grams of hydrogen sulfide gas was fed to the reactor.

Preparation of Na_2S_4

Following the above reaction, the reactor was cooled to 25°C. The
5 reactor contents were water white. Some undissolved Na_2S were present.

To this reaction mixture was added 29.12 grams of sublimed sulfur. The reactor temperature was 25°C. After sulfur addition, the reactor contents turned dark in color. The reactor was sparged with N_2 for 6 minutes to remove any entrained air. The reactor was then heated to
10 reflux, i.e., 78-82°C. Heat up time from 25° to 82°C was 13 minutes.

Preparation of Chloropropyltriethoxysilane

Chloropropyltrimethoxysilane was separately transesterified to the ethyl ester, chloropropyltriethoxysilane, in a 1 liter glass reactor equipped with a heating mantle, thermometer, ethanol addition funnel and a 5 tray, 1
15 inch diameter glass Oldershaw column. This column should have at least about 3 theoretical trays.

The reactor was initially charged with 527.15 grams of chloropropyltrimethoxysilane, 1.05 grams of *p*-toluenesulfonic acid (2000 ppm), and 130 grams of ethanol. During the first part of the reaction the reactor
20 temperature was run in the range 80°-90°C. Then the ethanol feedrate was cut back and the reactor was run at 98°-115°C, to help drive MeOH out of the reactor. A reflux ratio of about 8:1 was used for the entire run. The ethanol usage was 2.3 times the theoretical amount. The reaction was run for about 8.9 hours, over a two day period. High temperature (111°C) at
25 the end of the run helped assure a relatively low residual ethanol

concentration, *i.e.*, 6.7%. This material could be vacuum stripped to reduce the ethanol further.

PRODUCT ANALYSIS BY GAS CHROMATOGRAPHY

	Ethanol	6.7 area %
5	Chloropropylmethoxydiethoxysilane	1.02 area %
	Chloropropyltriethoxysilane	90.7 area %

Chloropropyltriethoxysile Reaction with Na_2S_4

The chloropropyltriethoxysilane made from transesterification of the corresponding methyl ester was used as the raw material to make 3,3'-
10 bis(trialkoxysilylpropyl)tetrasulfide. A charge of 145.97 grams of the chloropropyltriethoxysilane prepared above was added to the addition funnel. Chloropropyltriethoxysilane addition was begun when the reactor started to reflux. This reaction was conducted over a period of 46 minutes.

Recovery of Product

15 At the end of the reaction, the material in the reactor was red with orange suspended solids. The system was held at reflux for 1.5 hours. The reactor was cooled to 25°C and held overnight for filtration. The reactor contents were filtered through a pressure filter equipped with a 0.25 μ filter pad. The filter cake was washed with 635 grams of acetone and
20 dried overnight. The product was then ethanol stripped by charging 318.54 of filtrate to the reactor, and applying a vacuum to 100 mm Hg.

Finally, the reactor contents from the strip step were filtered through a 0.25 μ filter pad to yield 143.39 grams of product. The product was analyzed by gas chromatography (GC) for % sulfur, solvent pH, sodium
25 concentration, and color (GVS), with the following results:

GC Analysis of Product Sample

	Component	Area%
	EtOH	0.46
	Chloropropyltriethoxysilane	0.45
5	3-Mercaptopropyltriethoxysilane	1.3
	3-Sulfur Product	26
	4-Sulfur Product	68.6

The product contained 22.4% sulfur and 0.26 ppm sodium. The solvent pH was 6.3 and the color (GVS) was rated 10-11.

10

Example 2

This example illustrates an alternate preparation of the preferred end product, 3,3'- bis (triethoxysilylpropyl) tetrasulfide.

H₂S Reaction with Sodium Ethoxide

15 Sodium ethoxide was prepared fresh as described in Example 1 above. Addition of hydrogen sulfide gas was started through a fritted glass sparge tube as described above. During a feed time of just under an hour, 12.7 grams of hydrogen sulfide gas was fed to the reactor. The solution was added to an addition funnel for later use.

Reaction of Na₂S Solution with Sulfur/Chloropropyltriethoxysilane

20 The chloropropyltriethoxysilane made from transesterification of the corresponding methyl ester as described in Example 1 was used as the raw material to make 3,3'-bis (trialkoxysilylpropyl) tetrasulfide.

To a second glass reactor were added 184.6 grams chloropropyltriethoxysilane and 36.0 grams of ground sulfur. The reactor was equipped with a heating mantle, reflux column, agitator and thermometer. The silane-sulfur slurry was heated to 45°C. Then the Na₂S solution (contained in the addition funnel) was continuously added over a 2.3 hour period, during which the reaction temperature was maintained between 39°C and 49°C. After the Na₂S addition was completed, the reaction was held at 45°C for 1 hour, and then held at 75°C for 1.5 hours.

Recovery of Product

The reactor was then cooled to room temperature. Its contents were filtered to remove NaCl solids formed in the reaction. Next the filtrate from the above step was stripped to 100°C and 50 mm Hg to remove ethanol. Finally the stripped product was filtered through a 0.25 micron filter.

The final product had a weight of 190.6 grams. It was analyzed by gas chromatography (GC) and for % sulfur and shown to contain about 70% 3,3'-bis(triethoxysilylpropyl)tetrasulfide and about 25% 3,3'-bis(triethoxysilylpropyl) trisulfide at 22.4% contained sulfur. Less than 1% chloropropyltriethoxysilane was present. The gas chromatographic analysis was virtually identical to commercially available product and that produced by the process described above in Example 1.

Example 3

This example illustrates the surprising results applicants achieve using the process of their invention as well as the importance of the ordered addition of reactants in applicants' claimed process.

Reaction of Na₂S/Chloropropyltriethoxysilane Product with Sulfur

In equipment analogous to that used above, a solution of Na₂S in ethanol was prepared as above from 260.7 grams of 21% sodium ethoxide in ethanol and 12.6 grams of H₂S gas. The solution was heated to reflux
5 and 182.4 grams of chloropropyltriethoxysilane were added over a 1 hour period. After cooling to 25°C, 35.6 grams of sulfur were added, and heat applied to reflux within 30 minutes, followed by heating at reflux for 90 minutes. After filtration, gas chromatographic analysis of the unstripped product showed the major non-solvent component to be monosulfide,
10 (EtO)₃Si(CH₂)₃S-(CH₂)₃Si(OEt)₃, with significant unreacted chloropropyltriethoxysilane. The unfiltered reaction mixture contained unreacted sulfur as well as the expected salt.

The above description is for the purpose of teaching the person of ordinary skill in the art how to practice the present invention and it is not
15 intended to detail all of those obvious modifications and variations of it which will become apparent to the skilled worker upon reading the description. It is intended, however, that all such obvious modifications and variations be included within the scope of the present invention which is defined by the following claims. The claims cover the indicated components
20 and steps in all arrangements and sequences which are effective to meet the objectives intended for the invention, unless the context specifically indicates the contrary.

CLAIMS

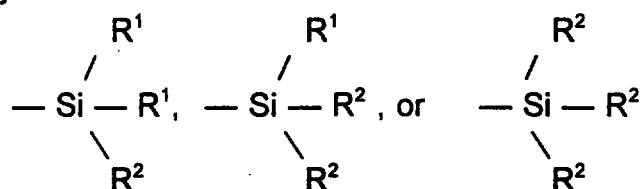
1. A process for the preparation of silane polysulfides comprising:

(a) contacting hydrogen sulfide gas with an active metal alkoxide solution,

(b) reacting elemental sulfur with the product of step (a), and

(c) reacting the product of step (b) with a halohydrocarbylalkoxysilane of the formula $Q - R - X$

in which Q is



and in which

R^1 is an alkyl group of 1 to 4 carbon atoms or phenyl, and

R^2 is an alkoxy group with 1 to 8, preferably 1 to 4, carbon atoms,

a cycloalkoxy group including 5 to 8 carbon atoms, or a straight or branched chain alkylmercapto group with 1 to 8 carbon atoms,

wherein the various R^1 and R^2 groups can be the same or different,

R is a divalent hydrocarbyl group including 1 to 18 carbon atoms, and

X is a halogen,

to produce a compound of the formula $Q - R - S_n - R - Q$

in which Q and R are as defined above, and n is an integer of from 2 to 9.

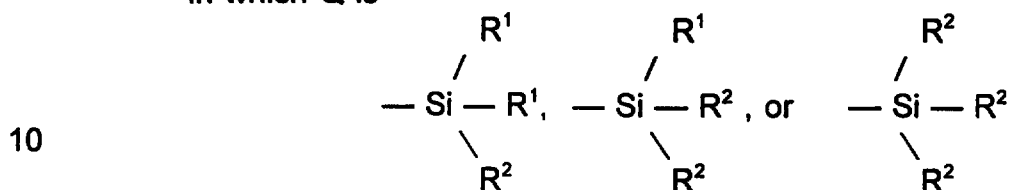


2. A process for the preparation of silane polysulfides comprising:

(a) contacting hydrogen sulfide gas with an active metal alkoxide solution, and

(b) reacting elemental sulfur and a halohydrocarbylalkoxysilane of the formula $Q - R - X$ with the product of step (a)

in which Q is



and in which

R^1 is an alkyl group of 1 to 4 carbon atoms or phenyl, and
 R^2 is an alkoxy group with 1 to 8, preferably 1 to 4, carbon atoms,

a cycloalkoxy group including 5 to 8 carbon atoms, or a straight or branched chain alkylmercapto group with 1 to 8 carbon atoms,

wherein the various R^1 and R^2 groups can be the same or different,

R is a divalent hydrocarbyl group including 1 to 18 carbon atoms, and

X is a halogen,

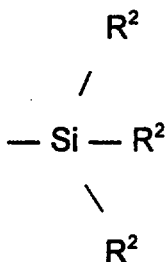
to produce a compound of the formula $Q - R - S_n - R - Q$

in which Q and R are as defined above, and n is an integer of from 2 to 9.

3. A process according to claims 1 or 2 wherein n is within the range of from 3 to 5.



4. A process according to claims 1 or 2 wherein Q is



5

5. A process according to claims 1 or 2 wherein R² is ethoxy.
6. A process according to claims 1 or 2 wherein the active metal alkoxide is sodium ethoxylate.
7. A process according to claims 1 or 2 wherein the halogen is chlorine.
8. A process according to claims 1 or 2 wherein R is 1,3-propylene.
9. A process according to claims 1 or 2 wherein the products of the last reaction step are methoxy derivatives, and said methoxysilane derivatives are converted to silane derivatives containing higher alkoxy groups.
10. A process for the preparation of (C₂H₅O)₃Si(CH₂)₃-S₄-(CH₂)₃Si(OC₂H₅)₃, selected from the group consisting of: (a) contacting an ethanol solution of sodium ethoxylate with hydrogen sulfide gas to produce a solution of Na₂S, adding elemental sulfur to the solution of Na₂S in an amount sufficient to form polysulfides, and adding Cl(CH₂)₃Si(C₂H₅O)₃ to the resulting reaction mixture and reacting to completion; and
- (b) contacting an ethanol solution of sodium ethoxylate with hydrogen sulfide gas to produce a solution of Na₂S, and adding the solution of Na₂S to a slurry of elemental sulfur and Cl(CH₂)₃Si(C₂H₅O)₃ and reacting to completion.

10

ABSTRACT**PROCESS FOR THE PREPARATION OF
SILANE POLYSULFIDES**

Sulfur-containing organosilicon compounds useful as coupling agents in vulcanizable rubbers to enhance various properties, including low rolling resistance for automobile tires, are prepared. Preferred compounds include Ω , Ω' -bis (trialkoxysilylalkyl) polysulfides. In one embodiment, preferred compounds are prepared by reacting sodium ethoxylate with hydrogen sulfide gas to yield a sodium sulfide solution, and then reacting this product with a slurried mixture of elemental sulfur and chloropropyltriethoxysilane to form the compound 3,3'-bis (triethoxysilylpropyl) tetrasulfide. Alternatively, the compounds are prepared by reacting the sodium sulfide solution with sulfur to form tetrasulfide, and then reacting this product with chloropropyltriethoxysilane. The use of hydrogen sulfide gas and sodium metal alcoholates provides an efficient and economical process.