

Steel band with good forming properties and a procedure for its production

This invention relates to a procedure for the production of steel band for the manufacture of parts fabricated by draw and ironing process, during which a hot rolled steel band is cold formed, in one or multiple stages, with a cold-rolling coefficient of at least 86%, where at least one side of the band material is coated with a galvanic layer containing Ni, Co, Cu, Fe, In, Pd, Bi and/or their alloys, or with a roll-bonded cladding containing Cu and/or brass and/or their alloys.

Cold rolled steel band is used for the fabrication of rotationally symmetrical cold-formed parts such as battery shells. The procedures applied during the cold forming are deep drawing and ironing, where the latter procedure is also called DI procedure (for drawing and ironing).

Due to rising requirements as for the application and use properties of such steel band material, the industry seeks constantly improving mechanical properties and especially better forming properties. Good plasticity is characterized by high r values for anisotropy characterizing the deep-drawing quality, and by n values characterizing drawing and ironing properties, as well as by high stretching values. It is also advantageous if the forming properties are the same lengthwise, crosswise and diagonally, i.e., if they are isotropic. The advantage of isotropic properties of the steel sheet are substantially reflected in the uniformity of the material flow during cold drawing or drawing and ironing so that no or very little earing occurs which results in a reduction of metal sheet waste.

In order to achieve an almost isotropic forming, steel sheet with very small permissible thickness variations in a texture-free and homogeneous rolled band or sheet is used.

The undesirable earing and its causes are explained in detail in the magazine "Blech, Rohre, Profile" [Metal Sheet, Tubes, Profiles], 9/1977 issue, on pages 341 through 346. The same article also describes that an earing-free material can normally be produced only by normalizing (annealing for relieving stresses) in a continuous annealing furnace at a temperature of about 1000°C. However, the operation of a continuous annealing furnace at such a high temperature requires high investment and operation costs.

DE-38 03 064 C1 reveals that low values for anisotropy and therefore a low tendency to form earing is achieved for globular-type steels that the steel has a higher content of titanium of up to 0.04 % using a cold rolling coefficient over 80%. However, such high rolling coefficients reach the stretching limit of steel of over 250 N/mm². In addition, steels stabilized by an ingredient of titanium are known to require high recrystallization temperatures, which would lead to a high tendency of individual band layers to stick together if such a steel band should be annealed in coiled state. However, the resulting damage of the steel sheet surface is very undesirable for high-value products and thus would result in a high rate of rejected products.

The application of a continuously operated band annealing furnace for the production of steel sheet designed for the fabrication of parts manufactured by drawing and ironing is also revealed in the publications US-5,078,809, WO 98/06881 and EP 0 822 266 A1. The latter document describes steel with a low content of carbon, whose steel analysis further contains boron with a content between 0.0005 and 0.0015 weight %. The aforementioned lower limit is based on the

requirement to increase the resistance of the steel sheet to corrosion by adding boron to the steel melting charge. The document EP 0 822 266 A1 justifies the upper limit of 0.0015 weight % by the circumstance that a higher boron content would cause forming defects in cylindric parts.

Finally, the document DE-195 47 181 C1 describes a type of steel with content of titanium, vanadium, or niobium, where a sort of a mixed-grain steel material is achieved based on certain hot rolling conditions under the gamma range of the iron-carbon diagram and based on a high reeling temperature in the hot band. With rolling coefficients between 50 and 85 %, this mixed grain leads to a lower tendency to form earing; however it also leads to the formation of coarse, band-shaped cementite, which causes undesirable structures on the steel sheet surface during the drawing of thin parts with high surface requirements, and, therefore, causes a high rate of defective products.

The task of this invention is to develop a general procedure leading to material properties, as for its anisotropy, very close to those of materials produced by normal annealing, while allowing relatively low operation costs with as few production steps as possible. The annealing process is supposed to produce a globular grain material; furthermore, the steel band produced by the invented procedure must show no disadvantages based on ageing or higher mechanical values due to high rolling coefficients.

According to this invention, the procedure of the aforementioned type suggests that the procedure steps performed after hot rolling include:

- pickling
- one- or multiple-stage cold rolling
- annealing of the band in coiled state (coil annealing)
- possibly also temper rolling of the band.

The warm band preferably contains boron in a portion between 0.0013 and 0.006 weight %, where the weight ratio of boron to carbon is from 0.5 to 2.5. The preferred goal should be to achieve a content of boron between 0.0013 and 0.003 weight %.

In order to achieve a uniform structure of the band material, hot rolling procedure is applied, preferably with the rolling temperature of over 870°C and a reeling temperature under 710°C.

In order to achieve a very small earing formation during the deep drawing or drawing and ironing, and especially a relative earing of a maximum of 2.5 %, the value of the vertical anisotropy Δr of the band after coil annealing should not amount to more than ± 0.12 .

Finally, this invention proposes a steel band capable to be processed by a deep drawing or drawing and ironing process, which is produced in a procedure according to at least one of the patent claims.

The procedure that is the subject of this invention as well as the steel band capable to be processed by a deep drawing or drawing and ironing process that is produced in a procedure according to this invention are explained in further text by means of an example.

The base material is a hot band with a starting thickness of 1.2 to 8 mm, preferably of 2.0 to 2.5 mm. The steel analysis of the used hot band is, in the first version, as follows:

	Weight percentage - minimum	Weight percentage - minimum
C	0.010	0.065
Mn	0.100	0.275
P		0.040
S		0.040
Si		0.050
N		0.0040
Al (acid-soluble)		0.070
B ppm	0.0013	0.0060
Cu		0.100
Sn		0.100
Cr		0.100
Ni		0.100
Mo		0.030
Fe		rest
B/N (ratio)	0.5	2.5

According to the second version, which is especially preferred, the steel composition is as follows:

	Weight percentage - minimum	Weight percentage - minimum
C	0.010	0.040
Mn	0.140	0.200
P		0.020
S		0.020
Si		0.030
N		0.0025
Al (acid-soluble)		0.035
B ppm	0.0013	0.0030
Cu		0.040
Sn		0.010
Cr		0.040
Ni		0.040
Mo		0.010
Fe		rest
B/N (ratio)	0.8	0.8

The hot rolling of the band occurs at an end rolling temperature of over 870°C and a reeling temperature under 710°C in order to achieve an especially uniform structure of the steel band. During experiments we were able to determine that the stretching limit values of the edge and of the band middle differ by less than 15 N/mm².

A boron content higher than indicated above requires significantly bigger hot rolling forces. On the contrary, a boron content of less than 0.0060 weight per cent allows working with moderate hot rolling forces. This then leads also to a reduction of thickness tolerances throughout the width of the steel sheet due to a significantly lower deflection of the rolls.

The hot-rolled band is subsequently pickled and then subjected to a one- or two-stage cold rolling process. The cold-rolling coefficient is 86 % or more. In this manner, the starting material of a thickness of 1.2 to 8 mm can be cold rolled to an end thickness of 0.1 to 1.0 mm. The cold rolling is followed by a recrystallization annealing in coil, i.e. annealing of the band in coiled state). The effects of such a recrystallization annealing are very similar to those of normal annealing usually performed in continuous furnaces with the band spread out. The coil annealing is then followed by temper rolling of the band in order to improve its surface and to fix specific mechanical and technical values.

The steel band is coated, on at least one of its two surfaces, with a galvanically produced layer. This coating may contain Ni, Co, Cu, Fe, Sn, In, Pd, Bi and/or their alloys. Within the scope of the entire process, the electrolytic processing can follow the first stage or the second stage of the cold rolling, and only then follows the annealing in coil as well as the temper rolling of the band. An additional annealing step between the two stages of cold rolling is also possible.

Besides the described galvanization process, another method of applying a coating on at least one side of the steel sheet is roll-bonding of a metal foil. In this case, the hot rolling and pickling of the steel band is followed first by roll-bonding and then by coil annealing. Another version is that a new cold rolling and a second annealing in coil can follow the first annealing in coil, before the steel band is finally subjected to temper rolling to improve its surface.

Layers of copper and/or brass and/or their alloys are especially suitable for the roll-bonding. Finally, the steel band with a coating applied by galvanization process or by roll-bonding can be further improved by another non-metal layer or a galvanic layer in order to achieve special effects and properties.

If a galvanization process is used, the thickness of the entire galvanic coating on one or both sides of the steel band should be between 0.1 µm and 8 µm. If roll-bonding is used, the sum of the one-side or two-side layers of bonded metal should be up to 50 % of the entire thickness of the steel band.

In order to achieve a very low tendency of the steel band to form earing, the parameters of the cold rolling must be set up in such a manner as to achieve a vertical anisotropy of Δr of a maximum of ± 0.12 after the first annealing in coil, which corresponds with a relative earing value of 2.5 %. Another advantage is that the result is also a material of globular grain suitable for the subsequent deep drawing and/or drawing and ironing process.



Patent claims

1. A procedure for the production of steel band designed for the manufacture of parts fabricated by a deep drawing or a drawing and ironing process, where a hot band is cold rolled, in one or several steps, with a cold rolling coefficient of at least 86 %, and at least one side of the band material is coated with a galvanic layer containing Ni, Co, Cu, Fe, Sn, In, Pd, Bi and/or their alloys, or, by roll-bonding, with a layer containing Cu and/or brass and/or their alloys. characterized in that the procedure steps after the hot rolling include pickling, cold rolling in one or two steps, annealing of the band in coiled state (coil annealing) and possibly also temper rolling of the steel band.
2. A procedure according to claim 1, characterized in that the hot band contains between 0.0013 and 0.0060 weight per cent of boron, and that the weight ration of boron to nitrogen is 0.5 to 2.5.
3. A procedure according to claim 2 characterized in that the boron content is between 0.0013 and 0.0030 weight per cent.
4. A procedure according to one of claims 1 to 3 characterized in that hot rolling occurs at a rolling temperature of over 870°C and a reeling temperature of under 710°C.
5. A procedure according to one of claims 1 to 4 characterized in that the value of the vertical anisotropy Δr of the band after coil annealing amounts to no more than ± 0.12 .
6. A procedure according to one of the preceding claims characterized by the following weight content in the hot band:

	Weight percentage - minimum	Weight percentage - minimum
C	0.010	0.065
Mn	0.100	0.275
P		0.050
S		0.050
Si		0.060
N		0.0060
B ppm	0.0013	0.0030

7. A procedure according to one of the preceding claims characterized in that the hot band is 1.2 mm to 8 mm thick before the cold rolling.
8. Steel band capable to be processed by deep drawing or by drawing and ironing characterized in that it is produced in a procedure according to one of claims 1 to 7.