

MANUAL HOIST AND TRACTION MACHINE

The present invention relates to a manual hoist and traction machine, and more particularly to a manual hoist and traction machine which is provided with a manual driving member mainly comprising a handwheel and with a mechanical brake operated by the manual driving member so that the manual driving member operates to rotatably drive a load sheave to hoist, haul, or lower a load, or to release traction thereof.

The conventional manual chain block, one of the manual hoist and traction machines, has been well-known as disclosed in, for example, the Japanese Utility Model Publication Gazette No. Sho 54-39231.

The manual chain block disclosed in the above Gazette is so constructed that a driving shaft is supported between side plates through a pair of bearings, a load sheave in association with the driving shaft through a reduction gear mechanism is rotatably supported to the driving shaft, a driven member having at one side thereof a driven disc is coupled with the driving shaft, a boss of a handwheel is screwably mounted thereto, and a braking ratchet wheel engageable with a braking pawl and a pair of lining plates positioned sandwiching therebetween the braking ratchet wheel, are supported at the outer periphery of a cylindrical

NO.	DESCRIPTION	DATE	INITIALS
✓	1. Design of the machine	1/1/78	SG
✓	2. Design of the machine	1/1/78	SG
✓	3. Design of the machine	1/1/78	SG
✓	4. Design of the machine	1/1/78	SG

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portion of the driven member, so that these members constitute a mechanical brake. A hand chain engaging with the handwheel is adapted to operate for rotatably driving the driving shaft through the mechanical brake and drive the load sheave to hoist a load or release the mechanical brake to lower the hoisted load.

The manual chain block constructed as the above-mentioned, however, uses a usual lining plate commercially available as a brake lining for a bicycle or the like for the lining plate to be used in the mechanical brake. Therefore, a diameter of the lining plate is made approximately equal to that of the handwheel at the handwheel and opposite to the side surface of the wheel.

The brake lining generally used for industrial machines, even when it is the most superior in property, may have a coefficient of friction of 0.20 or more at a friction surface temperature of 200 °C in consideration its function, and compressive strength may be 1000 (kg/cm²) at the largest and the maximum strain about 8 (10⁻³ mm/mm), which will comply with the provisions of Japanese Industrial Standard. When the usually commercial product is used for the mechanical brake at the manual chain block, in consideration of performance and quality, the lining plate is made larger in diameter, the friction surface of the wheel opposite to the lining plate increases in area and decreases in surface



pressure, so tat the mechanical brake is adapted to operate corresponding to a hoist load without hindrance.

Meanwhile, the manual chain block has recently been required to be small-sized from simplicity in handling, which is realized by improving the quality of material of each component to raise its durability. However, the handwheel is limited to its diameter from a limit to a diameter of the lining plate, thereby being restricted in its miniaturization. Also, the axial position of the handwheel needs to be set at the axially outside of the mechanical brake so that the axial size of the handwheel also is limited in the miniaturization thereof. When the handwheel is axially outwardly positioned, a distance between the mounting portions of the handwheel and bearing for supporting the driving shaft to the side plates, so that, when the handwheel is driven by the hand chain, the driving shaft is easy to deflect due to a load acting on the handwheel. Hence, in some cases where the hand-chain is forcibly operated, the problem is created in that the driving shaft is deformed. Also, in the no-load state where a hook at the load chain engaged with the load sheave hangs no load and the load sheave is not affected by the load, the body of chain block, as shown by the two-dot chain line in Fig. 7 which illustrates a prior art arrangement, is slanted due to weight of the hand chain engageable with the handwheel, whereby, when the hand chain 100 is operated to rotate the handwheel 101, not only the hand chain 100 comes

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into contact with a wheel cover 103 at the chain block body 102 so as to generate noises, but also resistance is generated against the operation of hand chain 100. Hence, there is no inertia resistance of handwheel 101 caused by the operation of hand chain 100, so that the hand chain 100 cannot quickly rotate the hand wheel 101, thereby creating the problem in that the hook of the load chain cannot be lifted rapidly.

An object of the present invention is that in the manual chain block mainly having the handwheel, the number of pockets thereof can be minimized and also the wheel of the handwheel is lapped on the mechanical brake so that the handwheel can be axially positioned in proximity to a side of the side plate for supporting the load sheave and moreover a diameter of the wheel can be small so as to enable the chain block to be miniaturized.

Another object of the present invention is that in the manual hoist and traction machine including the above-mentioned manual chain block, the friction surface of the mechanical brake or an overload prevention device is improved to stabilize the performance thereof.

In order to attain the above-mentioned objects, a manual hoist and traction machine which is provided with first and second side plates, a load sheave supported therebetween through a pair of bearings, a driving shaft for



driving the load sheave, a driven member coupled with the driving shaft and having the friction surface, and a driving member screwably mounted on the driving shaft and having a friction surface opposite to that of the driven member, and which is also provided between the driven member and the driving member with a mechanical brake having at both axial sides thereof the friction surfaces and the outer peripheral portion with which a braking pawl is engageable, and first and second lining plates interposed between the friction surfaces of the driven member and braking ratchet wheel and between the friction surfaces of the braking ratchet wheel and driving member respectively, is characterized in that the lining plates each are formed of a lining raw material comprising heat-resistant fiber, a friction regulating agent and a bonding agent, and having the performance such that, when the mechanical brake operates due to forward screw movement of the driving member, the raw material having a friction coefficient of 0.35 or more at a temperature of 200°C of the respective friction surfaces, compressive strength of 15 (kgf/mm²) at hardness (HRS) of 90 to 120, and the maximum strain of 12 (10⁻³ mm/mm) or more.

The present invention is further characterized in that at the manual chain block in which the driving member comprises a handwheel provided with a wheel and a boss screwably mounted to the driving shaft and with a hand chain



engageable with the wheel of the handwheel, a friction surface is provided at the side surface of the boss at the mechanical brake side ; the wheel has pockets in the minimum number for receiving therein horizontal links of the hand chain and is provided at the inside surface with an inside swollen portion swollen from the friction surface toward the first side plate, and furthermore, an outer diameter of the first lining plate is smaller than an inner diameter of the inside swollen portion at the wheel, the braking ratchet wheel is provided with a cylindrical portion extending from the outer periphery thereof toward the first side plate, the cylindrical portion is provided at the outer periphery thereof with teeth engageable with the braking pawl, and the teeth are displaced toward the first side plate with respect to the inside swollen portion of the wheel, and furthermore outer diameters of the second lining plate and driven member with the friction surface are made smaller than the inner diameter of the cylindrical portion at the braking ratchet wheel.

The cylindrical portion at the braking ratchet wheel is preferable to be overlapped on the outer periphery of the bearing supporting the load sheave to the first side plate. Also, it is preferable that, among the friction surfaces with which the first and second lining plates come into frictional contact because they are axially biased by

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forward screw movement of the handwheel, the friction surfaces provided on at least the driven member and braking ratchet wheel are each provided with a friction control layer plated and heat-treated.

Furthermore, the present invention is still further characterized in that in the manual chain block wherein the the driving member comprises a brake holder screwably mounted to the driving shaft and having a flange having at the inside surface a friction surface and a cylindrical portion, a handwheel having a boss having at both axially side surfaces the friction surfaces and an inside swollen portion and rotatably supported to the cylindrical portion at the brake holder, and a hand chain engageable with the handwheel; a load setting and adjusting member is screwably mounted to the cylindrical portion of the brake holder, a first friction plate is interposed between the flange of the brake holder and the boss of the handwheel, a second friction plate is interposed between the boss and the load setting and adjusting member, and a holding plate and an elastic member are interposed between the second friction plate and the load setting and adjusting member to thereby form an overload prevention device, and also the respective outer diameters of the flange at the brake holder and first and second friction plates are made smaller than the inner diameter of the inside swollen portion at the handwheel.

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It is preferable that in the overload prevention device , the respective outer diameters of the elastic member, holding plate and load setting and adjusting member are made smaller than the inner diameter of the axially outside swollen portion at the handwheel and the overload prevention device is adapted to be contained in a plane of projection of both the axially side surfaces at the wheel of the handwheel.

Also, it is preferable that, in the manual hoist and traction machine provided with the overload prevention device, at the friction surfaces of at least the flange at the brake holder and of the holding plate among the friction surfaces with which the first and second friction plates come into frictional contact is provided a friction control layer formed of a heat-treated plated layer.

The present invention is yet further characterized in that in a lever type hoist and traction machine, the driving member comprises a brake holder screwably mounted to the driving shaft and having a flange having at the inside surface the friction surface and a cylindrical portion, a driving gear having a boss having at both axial side surfaces friction surfaces and teeth positioned at the outer periphery, and an operating lever having a driving pawl engageable with the teeth at the driving gear, an overload setting and adjusting member is screwably mounted to the cylindrical portion at the brake holder, a first friction

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plate is interposed between the flange of the brake holder and the boss of the driving gear, a second friction plate is interposed between the boss of the driving gear and the load setting and adjusting member, and a holding plate having the friction surface and an elastic member are interposed between the second friction plate and the load setting and adjusting member to thereby form an overload prevention device, and also the respective friction surfaces of the flange at the brake holder, driving gear and holding plate are provided a friction control layers each formed of a heat-treated plated layer.

Also, it is preferable that in the aforesaid lever type hoist and traction machine, the plated layer at the friction control surface is formed of nickel phosphorus, nickel chromium, or chromium, and that the heat-treatment temperature of the plated layer is set to an austenite transformation point temperature at the respective raw materials of the brake holder, driving gear and holding plate provided with the layer and the plated layer being diffused onto the surface of each raw material.

Therefore, according to the invention as set forth in claim 1, the first and second lining plates of the mechanical brake are formed of the above-mentioned lining raw material, whereby an outer diameter of the respective lining plates can be smaller.

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Accordingly, when the present invention is applied to the manual chain block having a handwheel according to a first example, the handwheel can be smaller in diameter thereof to thereby enable the chain block to be miniaturized as a whole.

Also, according to the invention as set forth in claim 2, in the manual chain block provided with the handwheel, a friction surface is provided at the side surface of the boss of the handwheel at the mechanical brake side, the number of pockets at the wheel at the handwheel made minimum, at the inside thereof, that is, at the side surface at a side of the first side plate is provided an inside swollen portion swollen beyond the friction surface toward the first side plate, an outer diameter of the first lining plate is made smaller than an inner diameter of the inside swollen portion, the cylindrical portion is provided at the braking ratchet wheel, the teeth are provided at the cylindrical portion and displaced from the inside swollen portion toward the first side plate, and the outer diameters of the second lining plate and driven member which is provided with the friction surface are made smaller than the inner diameter of the cylindrical portion, whereby while enabling the handwheel to be smaller in diameter, the handwheel can be axially displaced toward the load sheave, in other words, the side plate supported to the load sheave.



Accordingly, the handwheel can be made smaller in the size not only radially but also axially, thereby enabling the chain block to be miniaturized and also the driving shaft to be less deflected, and the entire chain block when no-loaded can be less slanted and the handwheel is inertial-rotatable, whereby the hand chain can be operated smoothly, rapidly, and without noises.

Accordingly to the invention as set forth in claim 3, the cylindrical portion of the braking ratchet wheel is overlapped on the outer periphery of the bearing for supporting therethrough the load sheave to the second side plate, whereby the braking pawl engageable with the teeth at the cylindrical portion can be displaced toward the side plate so that the handwheel also can be displaced toward the same to that extent, thereby enabling the chain block to be further reduced in axial length and the driving shaft to be reduced in deflection when the handwheel is driven, and the chain block as a whole can be less slanted during the no loading.

According to the invention as set forth in claim 4, the friction control layer is provided at the friction surface, whereby, while forming the lining plate and of the lining raw material, the attack resistance of the friction surface is improvable and the coefficient of friction is controllable, whereby, even in long use, the

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coefficient of friction of the friction surface can be stabilized and the braking property can be prevented from being varied after long use, thereby enabling stable use to be performed for long use.

Furthermore, according to the invention as set forth in claim 5, in the chain block assembling therein the overload prevention device since the outer diameter of the flange and those of the friction plates and at the brake holder are made smaller than the inner diameter of the inside swollen portion at the wheel of the handwheel, the friction plates can be contained in the plane of projection of the wheel at the handwheel whereby, while providing the overload prevention device the handwheel can further be reduced in axial length and miniaturized as the whole.

According to the invention as set forth in claim 6, the outer diameter of the elastic member, holding plate and load setting and adjusting member at the overload prevention device are made smaller than the inner diameter of the wheel and the overload prevention device is contained in the plane of projection at the wheel, whereby, while providing the overload prevention device, the chain block can effectively be prevented from increasing in axial length due to the overload prevention device.

According to the invention as set forth in claims

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8 and 9, the manual chain block and lever-type hoist and tracation machine each are provided at the friction surface of the overload prevention device with the friction control layer 39, whereby the coefficient of friction of the friction surface is controllable to be a desired value, a transmitting torque by the load setting and adjusting member can accurately be set, variation between the products is eliminated, and the surface condition of the friction surface is never changed by attack of friction plates. Also the hoist and tracation machine is not affected by rust, thereby enabling the set value of transmitting torque to be held to a proper value for a long time. Hence, the load sheave is ensured to slip by an overload more than the set value on the basis of the prest transmitting torque so as to effectively realize the overload prevention.

According to the invention as set forth in claim 10, the heat-treatment temperature of the plated layer is set to an austenite transformation point temperature of the driving side and driven side members for forming the plated layer and the plated layer is diffused and permeated onto the raw material surface of the respective driving side and driven side members, whereby the surface hardness can be made to be 600 or more of Vickers hardness. Accordingly, the attack resistance and

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transmitting torque can be held effectively and for a long time.

These and other objects of the invention will become more apparent in the detailed description and examples which follow.

It will be understood that the description is given by way of example only and not by way of limitation.

In the drawings:-

Fig. 1 is a partial, longitudinally sectional, view of a first embodiment of the present invention;

Fig. 2 is an enlarged sectional view of a principal portion of an embodiment in which a friction control layer is provided at a friction surface of a mechanical brake.

Fig. 3 is an enlarged sectional view of another example when provided with the friction control layer, showing a principal portion only;

Fig. 4 is a partially omitted longitudinally sectional view of a second embodiment of the present invention;

Fig. 5 is an enlarged sectional view of the principal portion of the embodiment provided at the friction surface of an overload prevention device with the friction control layer;

Fig. 6 is an enlarged sectional view of a third embodiment of the present invention, showing a principal portion and corresponding to Fig. 5; and

Fig. 7 is a schematic illustration of the conventional example, showing the problem therein.

A first embodiment of the present invention shown in Fig. 1 is a manual chain block having no overload prevention device, in which a mounting shaft 4a for mounting a hook 4 is provided between a pair of side plates 1 and 2, a load sheave 3 engageable with a load chain 110 is rotatably supported between the side plates 1 and 2 through bearings 5 and 6, a driving shaft 7 is inserted into a shaft bore of the load sheave 3, with one axial side of the driving shaft 7 is integrally coupled a driven member 10 comprising a driven disc 8 and a cylindrical portion 9, a handwheel 11 is screwably mounted onto the one axial end of the driving shaft 7, at the cylindrical portion 9 of the driven member 10 are supported a braking ratchet wheel 12 and first and second lining plates 13 and 14 positioned at both axial sides of the braking ratchet wheel 12, to the first side plate 1 is supported, through a pawl shaft 16a and a pawl spring 16b, a braking pawl 16 engageable with teeth 15 at the braking ratchet wheel 12, and the driven member 10, handwheel 11, braking ratchet wheel 12, braking pawl 16 and the pair of first and second lining plates 13 and 14, form a mechanical brake 17. Furthermore, at the other axial side of the driving shaft 7 is provided a reduction gear mechanism 18 having a plurality of reduction gears.

The above-mentioned construction is well-known, so that an endless hand chain 100 engageable with the handwheel

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11 is operated to rotatably drive the handwheel 11 and a driving force is transmitted to the driving shaft 7 through operation of the mechanical brake 17 and the load sheave 3 can be driven through the reduction gear mechanism 18, whereby a load can be hoisted through the load chain 110 engageable with the load sheave 3.

The first embodiment of the invention shown in Fig.1 is so constructed that in the manual chain block the handwheel 11 can be made smaller in diameter, displaced at the axial position toward the first side plate 1, and reduced not only in a radial length but also in an axial length, whereby, while the chain block can be miniaturized as a whole, deflection caused by a load acting on the handwheel 11 can be reduced and the entire chain block, when not-loaded, can be less slanted.

In detail, the handwheel 11 is provided at the inside surface of a boss 19 with a friction surface 19a, a wheel portion 20 in continuation of the boss 19 is axially swollen toward the first side plate 1 with respect to the boss 19, at the wheel portion 20 are provided the minimum number of pockets 20a for receiving therein lateral links of the hand chain, an outer diameter of each pocket is made smaller, as shown in Fig.2, an outer diameter r_1 of the first lining plate 13 in contact with the friction surface 19a is made smaller than an inner diameter R of the inside swollen portion of the wheel portion 20, at the braking ratchet wheel



12 is provided a cylindrical portion 21 extending from the outer periphery thereof toward the load sheave 3 and overlapping on the outer periphery of the bearing 6, at the outer periphery of the cylindrical portion 21 are provided teeth 15 engageable with the braking pawl 16, the teeth 15 are displaced toward the load sheave 3 with respect to the inside swollen portion of the wheel portion 20, an outer diameter r_2 of the second lining plate 14 and that r_3 of the driven disc 8 at the driven member 10 are made smaller than an inner diameter of the cylindrical portion 21, and the first and second lining plates 13 and 14 are formed of the following lining raw material.

In other words, the lining raw material comprises heat resistant fiber, a friction regulating agent and a bonding agent, and has the performance of a coefficient of friction of 0.35 to 0.60 at a surfacial temperature of 200° C of the respective friction surfaces, hardness (HRS) of 90 to 120, compressive strength of 1500 (kg/cm²) or more, and the maximum strain of $12(10^{-3} \text{ mm/mm})$ or more.

In greater detail, in the first embodiment shown in Fig. 1, the number of pockets at the handwheel 11 is six, the outer diameters r_1 through r_3 of the first lining plate 13, second lining plate 14 and driven disc 8 at the driven member 10, are equal to each other, the outer diameters r_1 through r_3 being made smaller than an inner diameter R of the inside



swollen portion at the wheel portion 20 and smaller than an outer diameter of the bearing 6.

The heat resistant fiber constituting the first and second lining plates 13 and 14 uses inorganic fiber, such as, glass fiber, rock wool, metallic fiber, ceramic fiber, and carbon fiber; or organic fiber, such as, alamode fiber, acrylic fiber, or phenol fiber. The friction regularizing agent uses powder or whiskers comprising metal, such as, iron, brass, copper, zinc, or aluminum; inorganic salt, such as, sulfate, barium sulfate, potassium carbonate, or potassium titanium; or inorganic material, such as, graphite or carbon; or organic material, such as, rubber, fluororesin, high molecular phenol resin, or cashew dust; and further the bonding agent uses binder of resin material, such as, phenol resin, denatured phenol resin, polyimido resin, epoxy resin, cashew resin or melamine resin.

The heat resistant fiber is used as the aggregate and the friction regulating agent and bonding agent are mixed in the following ratio (volume %):

heat resistant fiber: 28 to 35 (V%)

friction regulating agent: 20 to 37 (V%)

bonding agent: 35 to 45 (V%).

The lining raw material is molded to the lining plates 13 and 14 and pressurized and heated. The lining plates 13 and 14 each molded by mixing the materials in the



above-mentioned ratio to be pressurized and heated obtain the following performances:

hardness (HRS) : 90 to 120

bending strength (Kgf/mm²) : 9 to 15

maximum strain (10⁻³ mm/mm) : 12 to 16

compressive strength (Kgf/mm²) : 15 to 20

coefficient of friction (200 °C) : 0.35 to 0.60.

In addition, when the above-mentioned performance is compared with that of the usual brake lining of resin series of non-asbestors. especially the compressive strength is stronger by 15 to 20 %, which is obtained because the ratio (V%) of heat resistant fiber and bonding agent is 63 to 80 % to be larger than the ratio of usual brake lining and then molded by being pressurized and heated. Such performance can miniaturize the lining plates 13 and 14 at the mechanical brake 17 which are tightened toward the driven disc 8 by forward screw movement of the handwheel 11 and have the function to transmit the driving force to the driving shaft 7.

Accordingly, since the lining plates 13 and 14 each are reduced in diameter more than the inner diameter R of the inside swollen portion of the wheel 20 at the handwheel 11, the handwheel 11 can be smaller in diameter. Moreover, in the embodiment shown in Fig.1, the cylindrical portion 21 of the braking ratchet wheel 12, as the above-mentioned, is overlapped on the outer periphery of the bearing 6 so that the braking

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pawl 16 engageable with the teeth 15 at the cylindrical portion 21 can be displaced toward the first side plate 1, whereby together with this construction, the handwheel 11 can be made smaller in diameter and also its axial position can be displaced in proximity to the side plate 1. In brief, the first lining plate 13 and the boss of braking ratchet wheel 12 can be contained in the plane of projection of the inside surface of the wheel 20 at the handwheel 11, thereby enabling the chain block to be reduced in axial length to that extent .

Thus, since the handwheel 11 can be miniaturized and displaced at the axial position thereof toward the side plate, the chain block can be miniaturized as a whole. Moreover, the handwheel 11 can be axially positioned at the side-plate side, that is, near the bearing 6 at the side plate 1, whereby, when the handwheel 11 is driven by the hand chain, the driving shaft 7, even when subjected to a large hoisting load, can be restrained from deflection and stable hoisting operation can be performed. Also, the entire chain block can be less stanted in the no-load state, so that, when the hand chain 100 is operated to rotate the handwheel 11 in the no-load state, the hand chain 100 can be prevented from coming into contact with the wheel cover 25 and smoothly operated, thereby reducing noises. Also, the handwheel 11, when rotated by the hand chain 100, can be inertia-rotated, thereby enabling the handwheel 11 rotated by the hand chain 100 to



quickly operate to that extent, and the hook of the load chain 110 to be quickly lifted.

In addition, in the above-mentioned construction, the number of pockets at the handwheel 11 is six, but may be five. The minimum number of pockets means that the number of pockets is added by 1, in the case where, when the handwheel 11 is manually operated by the hand chain 100, variation in magnitude of manual power becomes larger to deteriorate the operability, thereby lowering the efficiency. The number of pockets depends on chain pitch of the hand chain, and, in the present pitch of 23.5 pitch at a line diameter of 5 mm and 28.0 pitch of 23,5 pitch at a line diameter of 5 mm and 28.0 pitch at that of 6 mm, the minimum number of pockets is five.

The driving shaft 7 is supported at one axial end to a bearing 23 provided at a gear cover 22 for covering the reduction gear mechanism 18 and at the other axial end to a roller bearing 24 fitted into the shaft bore of the load sheave 3. In this case, a bearing may be provided at the wheel cover 25 for covering the handwheel 11 so that an extending shaft portion of the driving shaft 7 may be supported to the bearing.

Furthermore, it is preferable that in the above-mentioned construction, the friction surfaces of the braking ratchet wheel 12 and driven disc 8 of the driven

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member 10, with which the first and second lining plate 13 and 14 axially biased by forward screw movement of the handwheel 11 come into frictional contact, are, as shown in Fig. 3, provided plated layers of nickel phosphate, nickel chromium, or chromium, of 8 to 20 micron thick, the plated layers being heat-treated to form friction control layers 26 respectively.

The friction control layers 26 each are not merely plated layer, but it formed by heat-treating the plated layer by a heating furnace at a temperature of 300 to 400 °C, or at the austenite transformation point temperature of, for example, 850°C of each member constituting the friction surface, and by diffusing and permeating the plated layer into the raw material of each member. Hence, the heat treatment raises the surface hardness and improves the attack resistance, and the coefficient of friction can be controlled to a predetermined value. Moreover, variation between the products can be reduced, and, even when used for a long time, the coefficient of friction of the friction surface can be stably maintained to enable the braking property to be prevented from deterioration after a long use and the stable use to be performed for a long time.

In addition, it is preferable that the friction control layer 26 is provided also at the friction surface 19a of the handwheel 11. In this case, a plated layer may be

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formed on the entire surface of the handwheel 11, but, as shown in Fig.3, the boss 19 and wheel 20 may be independently formed and then coupled with a rivet 80 or the like, so that the plated layer is provided on the entire surface of the boss 19. Or, a contact plate (not shown) provided with the friction control layer is separately formed so as to be integrally coupled with the boss 19 by riveting, a fixing method using adhesive, or the like. Thus, the friction control layer 26 is provided at the friction surface 19a of the handwheel 11, so that, when the mechanical brake 17 is released, that is, when the handwheel 11 is screwably backward moved to release the operation of mechanical brake 17, such releasing is smooth, thereby eliminating the inconvenience that the friction surface 19a is caught onto the lining plate 13 to cause not-releasing of the mechanical brake 17. Also, in the case where the plated layer is heat-treated at the austenite transformation point temperature, it is preferable that the plated layer is quenched with cold water or cold oil after the heat treatment and thereafter is tempered at a temperature of 200 to 500°C, normally 300 to 450 °C, so as to be formed to a martensite structure.

Next, explanation will be given on a second embodiment of the present invention shown in Fig.4. The second embodiment assembles an overload prevention device 30 in the chain block of the first embodiment, in which the

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handwheel 11 is provided with a brake holder 31 screwably mounted on the driving shaft 7 and comprising a flange 32 having at the inside a friction surface and a cylindrical portion 33, to which a boss 19 of the handwheel 11 is rotatably supported and to which a load setting and adjusting member 34 is screwably mounted, between the flange 32 of the brake holder 31 and the boss 19 is interposed a first friction plate 35 and between the boss 19 and the load setting and adjusting member 34 is interposed a second friction plate 36, and between the second friction plate 36 and the load setting and adjusting member 34 is interposed an elastic member 37 mainly comprising a disc spring, thereby forming the overload prevention device 30.

In the above-mentioned construction, outer diameters r of the flange 32 and friction plates 35 and 36, of the elastic member 37 and load setting and adjusting member 34, and of the holder 38 interposed between the second friction plate 36 and the elastic member 37 at the brake holder 31, are made smaller than inner diameters R of the inside and outside swollen portion of the wheel 20 at the handwheel 11, so that the overload prevention device 30 may be contained within the plane of projection of both axial side surfaces at the wheel 20 of the handwheel 11.

Although the friction surfaces 35 and 35 may use known friction plates, it is preferable to use the same lining



raw material as the lining plates 13 and 14 at the mechanical brake 17.

In this case, it is preferable that the friction surfaces of the members with which the friction plates 35 and 36 come into frictional contact, in other words, the friction surface of the flange 32 at the brake holder 31 and that of the holder 38 are , as shown in Fig.5, provided with friction control layers 39 formed of plated layers of nickel phosphate, nickel chromium or chromium, and of 8 to 20 micron thick and heat-treated.

The friction control layers 39 each are not merely the plate layer as the same as those 26 at the friction surfaces of the mechanical brake 17, but are formed in such a manner that the plated layer is heat-treated in a heating furnace at a tempearture of 300 to 400°C , or at the austenite transformation point temperature of, for example, 850 °C of the above-mentioned members for constituting the friction surfaces, and diffused and permeated into the raw material of each member, whereby the surface hardness can be raised and attack resistance can be improved by the heat treatment and also the coefficient of friction can be controlled to reduce variation between the products.

It is preferable that the friction control layers are formed also at the friction surfaces at both sides the boss 19 of the handwheel 11.

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In this case, a plated layer may be formed at the entire surface of the hand wheel 11 for this purpose, but a friction plate provided with the friction control layer may be separately formed so that the friction plate may be integrally coupled with the boss 19 by riveting or a fixing method with adhesive.

The aforesaid embodiments both are applied to the manual chain block which uses the handwheel 11 so as to operate the hand chain 100 for driving the load sheave 3. Besides this, they are applicable to a lever type hoist and traction machine comprising, as the driving member a driving gear 52 having at the outer periphery thereof teeth 51 and an operating lever 54 having a driving pawl 53 engageable with the teeth 51 at the driving gear 52 as shown in Fig.6.

The lever type hoist and traction machine shown in Fig.6, as the same as the second embodiment shown in Fig. 4, assembles an overload prevention device 60. The overload prevention device 60 is provided with a brake holder 61 separate from the driving gear 52, a boss 55 thereof is rotatably supported to a cylindrical portion 62 of the brake holder 61, a first friction plate 64 is interposed between a flange 63 of the brake holder 61 and the boss 55 of the driving gear 52, a load setting and adjusting member 65 is screwably mounted onto the cylindrical portion 62, between the adjusting member 65 and the boss 55 of the driving gear



52 is interposed a second friction plate 66, and between the second friction plate 66 and the load setting and adjusting member 65 is interposed a holding plate 67 having a friction surface and an elastic member 68 formed mainly of a disc spring.

In Fig.6, the brake holder 61, as the same as the second embodiment, is screwably mounted to the driving shaft 7, and a mechanical brake is provided at the lateral side facing the first side plate, that is, at the left side in Fig.6, and at the left side surface of the flange 63 at brake holder 61 is provided a friction surface 63a coming in frictional contact with the first lining plate at the mechanical brake.

The operating lever 54 is elongated and couples a pair of lever plates 56 and 57 opposite to each other through bolt. The lever plate 57 is rotatably supported through a bearing member 70 to a brake cover 69 fixed to the first side plate 1 and for covering the mechanical brake, and in the vicinity of the supporting portion of lever plate 57 it supported the driving pawl 53 through a pawl shaft 71 so as to be capable of being positioned at three positions of hoist and traction, lowering and releasing traction, and the neutral, so that an operating lug 72 fixed to the axial end of pawl shaft 71 is operated to switch the driving pawl 53 to the three positions.

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In a third embodiment of the invention shown in Fig. 6, onto the entire surfaces of the brake holder 61, driving gear 52 and holding plate 67 are formed plated layers of nickel phosphate, nickel chromium or chromium and of 8 to 20 micron thick by means of electrolytic plating, and then heat-treated for 1 to 2 hours at a temperature of 300 ° C by a heating furnace, so as to form a friction control layer 73 of the surface hardness of Vickers hardness of 350 to 450.

Thus, the friction control layers 73 are formed at the surfaces of the brake holder 61, driving gear 52 and holding plate 67 at the driving side and opposite to the friction plates 64 and 66, and can control the surface condition, that is, the coefficient of friction with respect to the surface of raw material as the same as the second embodiment. Moreover, variation between the products can be reduced and the adjusting member 65 is tightened to set a transmitting torque, whereby the set value can properly be held, an overload more than the set transmitting torque can ensure a slip of the load sheave, and effective overload prevention can be realized.

Moreover, the friction control layer 73 is not a mere plated layer, but it is formed by heat-treating a plated layer, whereby the surface hardness can be raised and the coefficient of friction be lowered to that extent to be constantly controlled. Hence, the transmitting torque can



further accurately be set and variation between the products is eliminated, and also the surface condition of the layer 73, that is, the coefficient of friction, can be prevented from being varied due to attack of the first and second friction plates 64 and 66, and is not affected by generation of rust, thereby enabling the set transmitting torque to be held in a proper value for a long time.

The heat treatment of the above-mentioned plated layer is performed by the heating furnace at a temperature of 300 °C . However, the plated layer may be heat-treated by the heated furnace at a temperature 400 °C for 1 to 2 hours. In this case, the surface hardness of the friction control layer 100 can be Vickers hardness of 400 to 450.

Furthermore, the heat treatment temperature of the plated layer, as the same as the second embodiment, may be set to an austenite transformation point temperature of, for example, 850 °C , of the raw material (structural steel) constituting the brake holder 61, driving gear 52 and holding plate 67, and the plated layer is diffused and permeated into the raw material, whereby the diffused and permeated layer may form the friction control layer 73.

In this case, the heat treatment may be carried out at the heating furnace, but is preferable to be done by high frequency induction heating. Also, the plated layer is preferred to be quenched by cold water or cold oil after the



heat treatment and then tempered usually at a temperature of 300 to 450 °C to be formed in martensite structure.

Thus, the friction control layer 100 can have the surface hardness of Vickers hardness of 600 or more, for example, 800 through 1000.

The first and second lining plates used for the mechanical brake in the third embodiment shown in Fig.6, as the same as the first and second embodiments, use the lining raw material respectively. Also, in the third embodiment, the brake holder 61 and driving gear 52 can be smaller in diameter. Accordingly, the operating lever 54 can further be miniaturized and the brake holder 61, driving gear 52 and operating lever 54 can be axially positioned to proximity to the first side plate.

Although several embodiments have been described, they are merely exemplary of the invention and not to be constructed as limiting, the invention being defined solely by the appended claims.

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What is Claimed is:

1. A manual hoist and traction machine provided with first (1) and second (2) side plates, a load sheave (3) supported between said first and second side plates through a pair of bearings (5, 6), a driving shaft (7) for driving said load sheave (3), a driven member (10) coupled with said driving shaft (7) and having a friction surface, and a driving member (11) screwably mounted to said driving shaft and having a friction surface (19a) opposite to the friction surface of said driven member, and provided between said driven member and said driving member with a mechanical brake (17) having a braking ratchet wheel (12) having at both axial sides friction surfaces and engageable at the outer periphery with a braking pawl (16) and having first and second lining plates (13, 14) interposed between the friction surfaces of said driven member (10) and braking ratchet wheel (12) and between the friction surfaces of said braking ratchet wheel (12) and driving member (11), said hoist and traction machine including the construction that said respective lining plates (13, 14) are formed of lining raw material comprising heat resistant fiber, a friction regulating agent and a bonding agent and provided with performances of a coefficient of friction of 0.35 or more at a surface temperature of 200°C of each of said friction





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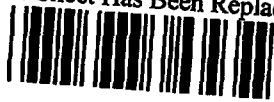
surfaces with which each of said lining plates comes into contact when said mechanical brake operates due to forward screw movement of said driving member, hardness (HRS) of 90 to 120, compressive strength of 15 (Kgf/mm²) or more, and the maximum strain of 12 (19⁻³mm/mm) or more.

2. A hoist and traction machine according to claim 1, wherein said driving member comprises a handwheel (11) provided with a wheel (20) and boss (19) screwably mounted to said driving shaft (7) and a hand chain (100) engageable with said wheel of said handwheel (11), the side surface of said boss at the mechanical brake side has a friction surface, said wheel has the minimum number of pockets (20a) for receiving therein horizontal links of said hand chain and said wheel has an inside swollen portion swollen at an inside portion thereof toward said first side plate beyond said friction surface, said hoist and traction machine including the construction that:

an outer diameter of said first lining plate (13) is smaller than an inner diameter of said inside swollen portion at said wheel,

said braking ratchet wheel (12) is provided with a cylindrical portion extending from the outer periphery of said ratchet wheel (12) toward said side plate, at the outer periphery of said cylindrical portion are provided teeth with which said braking pawl comes into contact, said teeth are displaced toward said first side plate with





respect to said inside swollen portion at said wheel, and
outer dimeters of said second lining plate (14)
and driven member provided with said friction surface and
made smaller than an inner diameter of said cylindrical
portion (21) of said braking ratchet wheel.

3. A manual hoist and traction machine according to
claim 2, wherein said cylindrical portion (21) at said
braking ratchet wheel (12) is overlapped on the outer
periphery of a bearing (6) for supporting therethrough a
load sheave (3) to said first side plate.

4. A manual hoist and traction machine according to
claim 2, wherein at the friction surfaces provided at at
least said driven member (10) and braking ratchet wheel
(12) among said friction surfaces with which said first
and second lining plates are axially biased by forward
screw movement of said handwheel so as to come into
frictional contact are provided friction control layers
(26) comprising plated layers, said plated layers being
heat-treated respectively.

5. A manual hoist and traction machine according to
claim 1, wherein said driving member comprises a brake
holder (31) screwably mounted to said driving shaft and
having a cylindrical portion (21) and a flange (32) having
at the inside thereof a friction surface, a handwheel
having a boss having at both axial sides thereof friction
surfaces and an inside swollen portion and rotatably
supported to said cylindrical portion of said brake holder





(31), and a hand chain engageable with said handwheel, to said cylindrical portion at said brake holder is screwably mounted a load setting and adjusting member, a first friction plate (35) is interposed between said flange of said brake holder and said boss of said handwheel, a second friction plate (36) is interposed between said boss and said load setting and adjusting member, and a holding plate and an elastic member are interposed between said second friction plate and said load setting and adjusting member, thereby forming an overload prevention device (30), and outer diameters of said flange at said brake holder and first and second friction plates (35, 36) are made smaller than an inner diameter of said inside swollen portion at said handwheel.

6. A manual hoist and traction machine according to claim 5, wherein the outer diameter of said elastic member (37), holding plate (38) and load setting and adjusting member (34) at said overload prevention device (30) are made smaller than the inner diameter of a swollen portion at the an axially outside surface (20), and said overload prevention device (30) is contained within the plane of projection of both said axial surfaces at said wheel of said handwheel.

7. A manual hoist and traction machine according to claim 5, said friction surfaces of at least said flange of said brake holder and holding plate among said friction





surfaces with which said first and second friction plate come into frictional contact are provided with friction control layers comprising heat-treated plated layers.

8. A manual hoist and traction machine according to claim 1, wherein said driving member comprises a brake holder (61) having a cylindrical portion (62) and screwably mounted to said driving shaft and having a cylindrical portion and a flange having at the inside surface a friction surface, a driving gear (52) which has a boss (55) having at both axial sides friction surfaces, and teeth positioned at the outer periphery; and an operating lever having a driving pawl engageable with said teeth at said driving gear, to said cylindrical portion (62) of said brake holder is screwably mounted a load setting and adjusting member, between said flange (63) of said brake holder and the boss of said driving gear is interposed a first friction plate (64), between said boss of said driving gear and said load setting and adjusting member is interposed a second friction plate (66), and between said second friction plate (66) and said load setting and adjusting member (65) are interposed a holding plate (67) having a friction surface and an elastic member (68) to thereby form an overload prevention device, and at the friction plates of said flange at said brake holder, driving gear, and holding plate, are each provided with a friction control layer formed of a plated layer which is heat-treated.



9. A manual hoist and traction machine according to claim 8, wherein said friction control layer each are formed of nickel phosphate, nickel chromium, or chromium.

10. A manual hoist and traction machine according to claim 8, wherein the heat treatment temperature of said plated layer is set to an austenite transformation point temperature of raw material of each of said brake holder, driving gear and holding plate, and said plated layer is diffused onto the surface of said each raw material.

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* C L N S *

MANUAL HOIST AND TRACTION MACHINE

ABSTRACT OF THE DISCLOSURE

The invention relates to a manual hoist and traction machine wherein an outer diameter of a first lining plate (13) constituting a mechanical brake is made smaller than an inner diameter mainly of a driven disc at a wheel of a handwheel (11), outer diameter of a second lining plate (14) and a driven disc are made smaller than an inner diameter of a cylindrical portion of a braking ratchet wheel (12), and the first and second lining plates (13, 14) are formed of lining raw material having performance of compressive strength of $15(\text{Kgf/mm}^2)$ or more and the maximum strain of $12(10^{-3}\text{mm/mm})$ or more.

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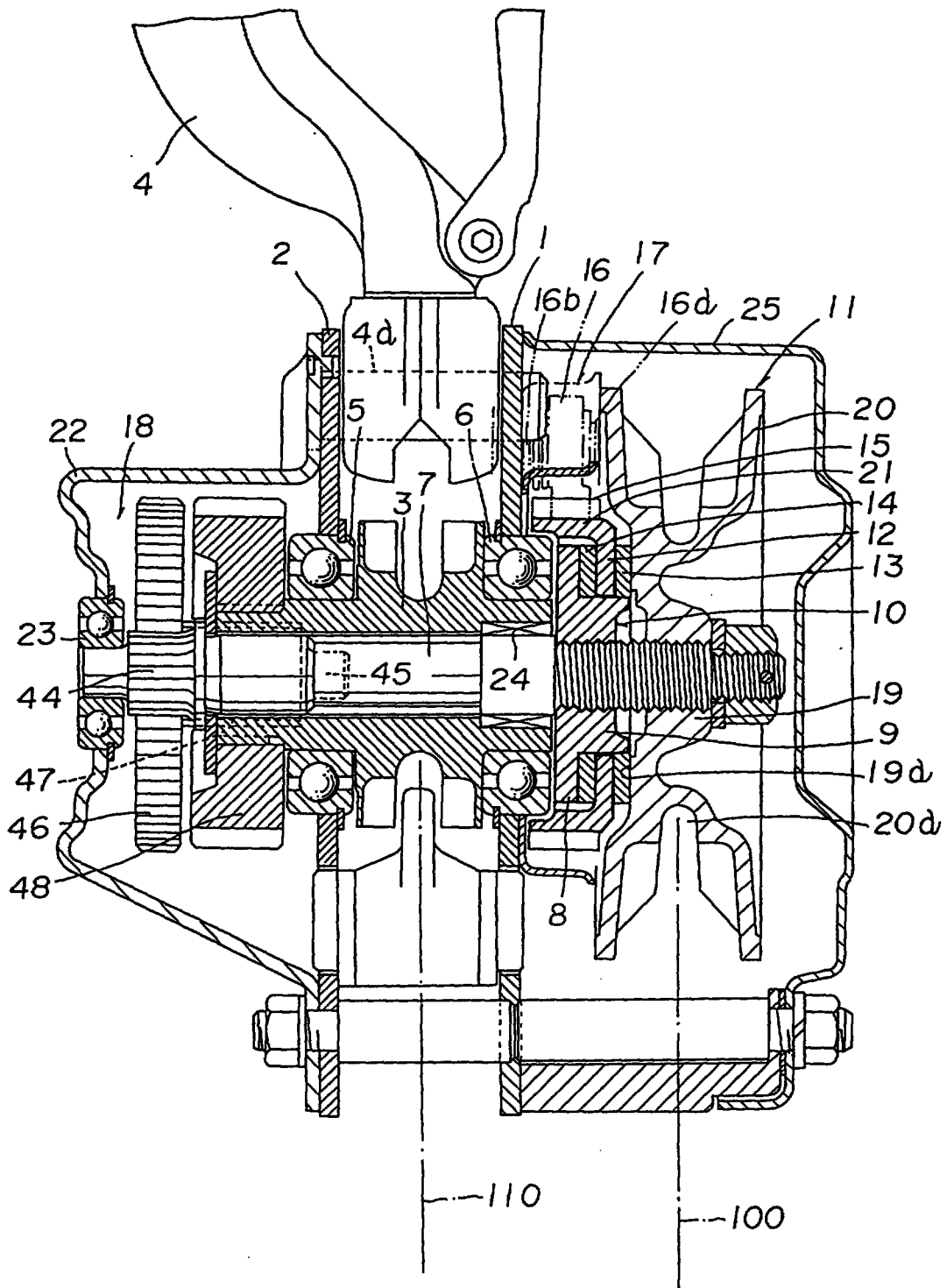


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FIG. 1

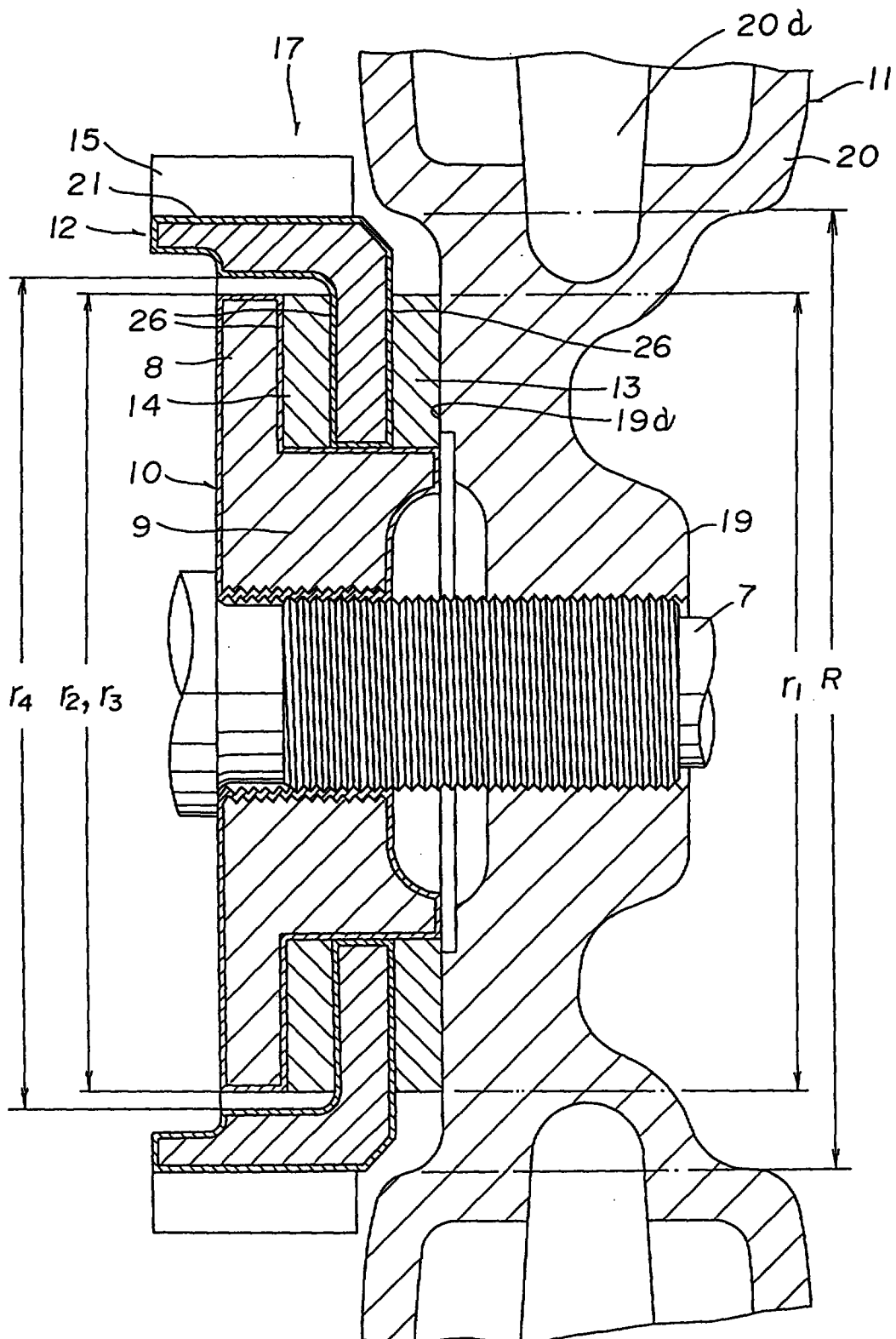


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FIG. 2

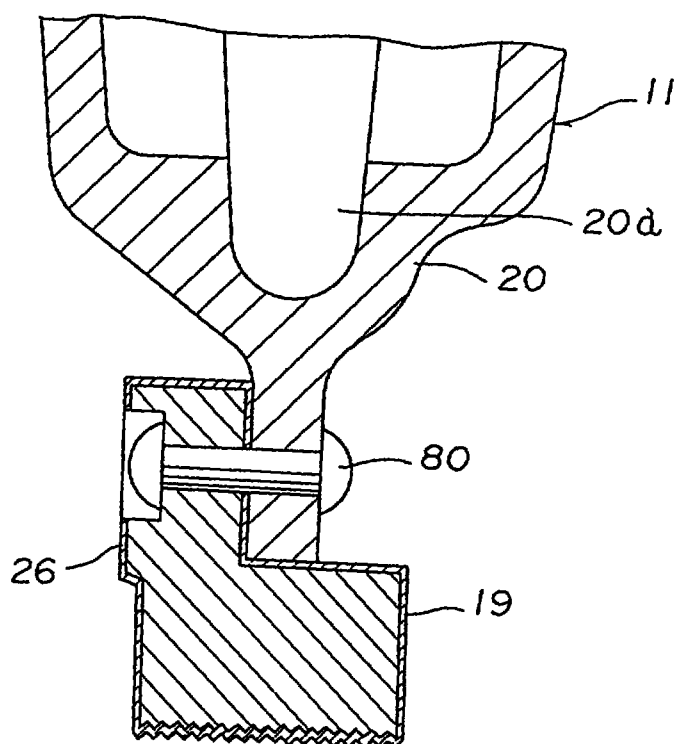


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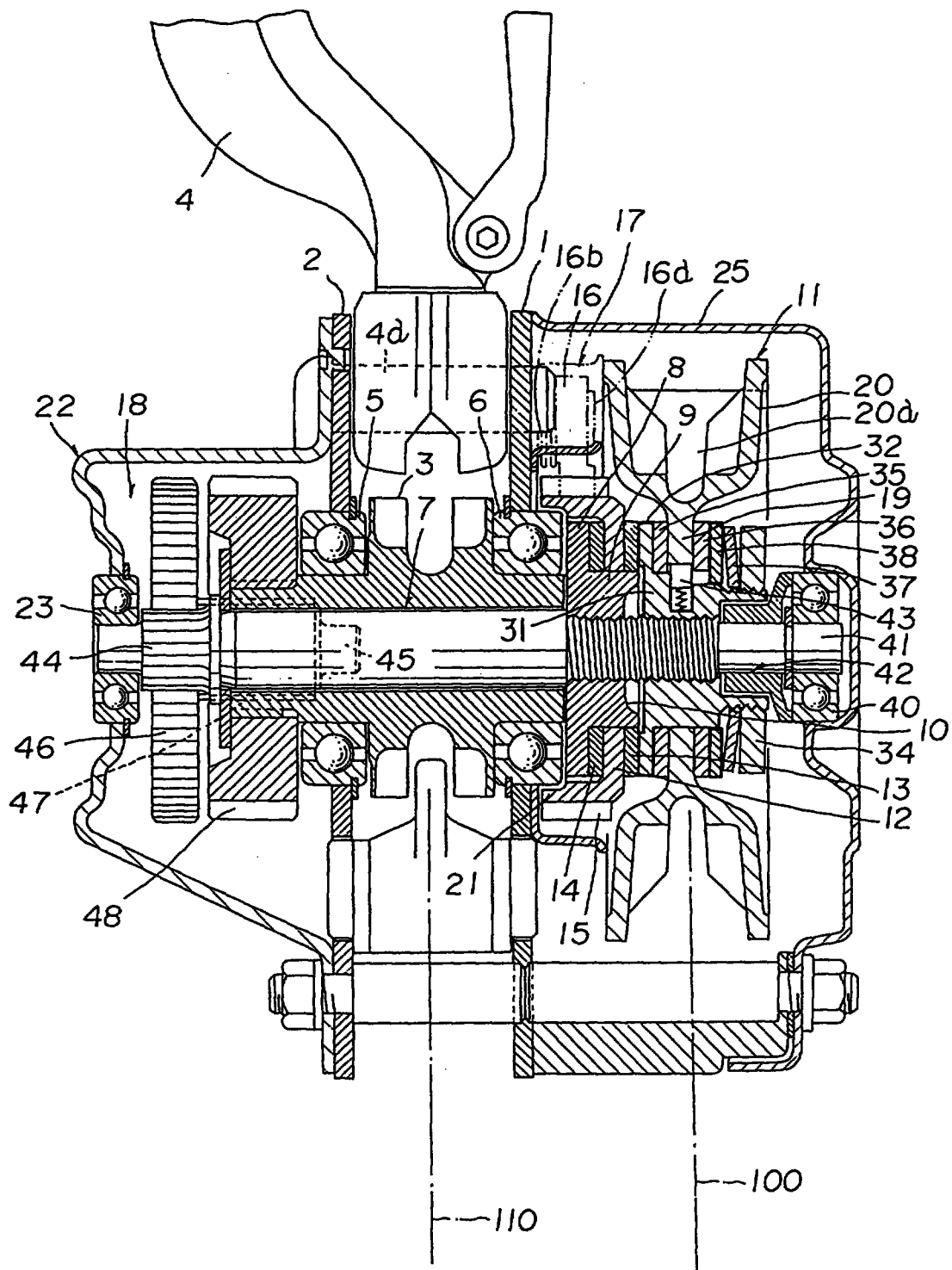
FIG. 3





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FIG. 4

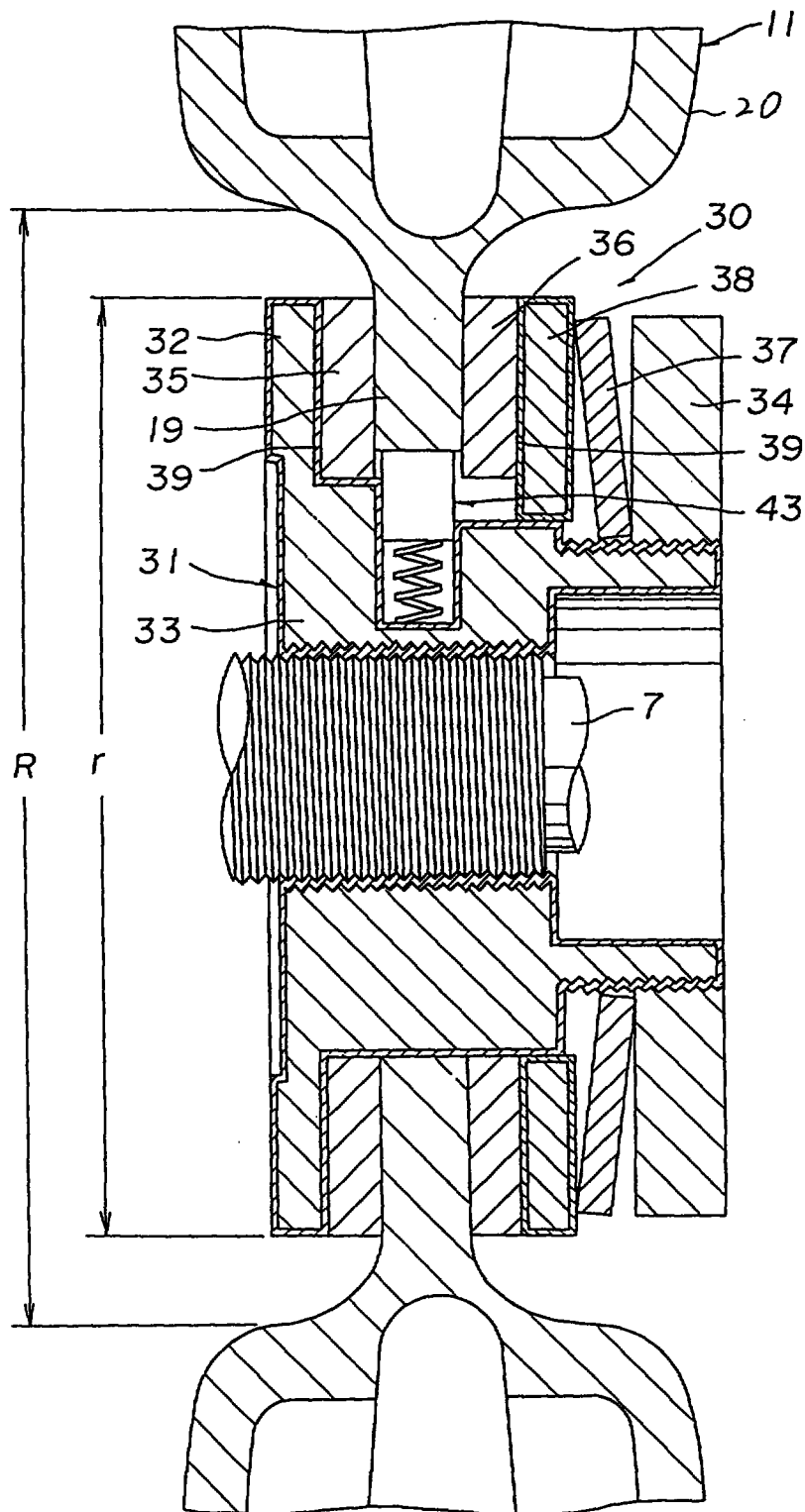


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FIG. 5



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FIG. 6

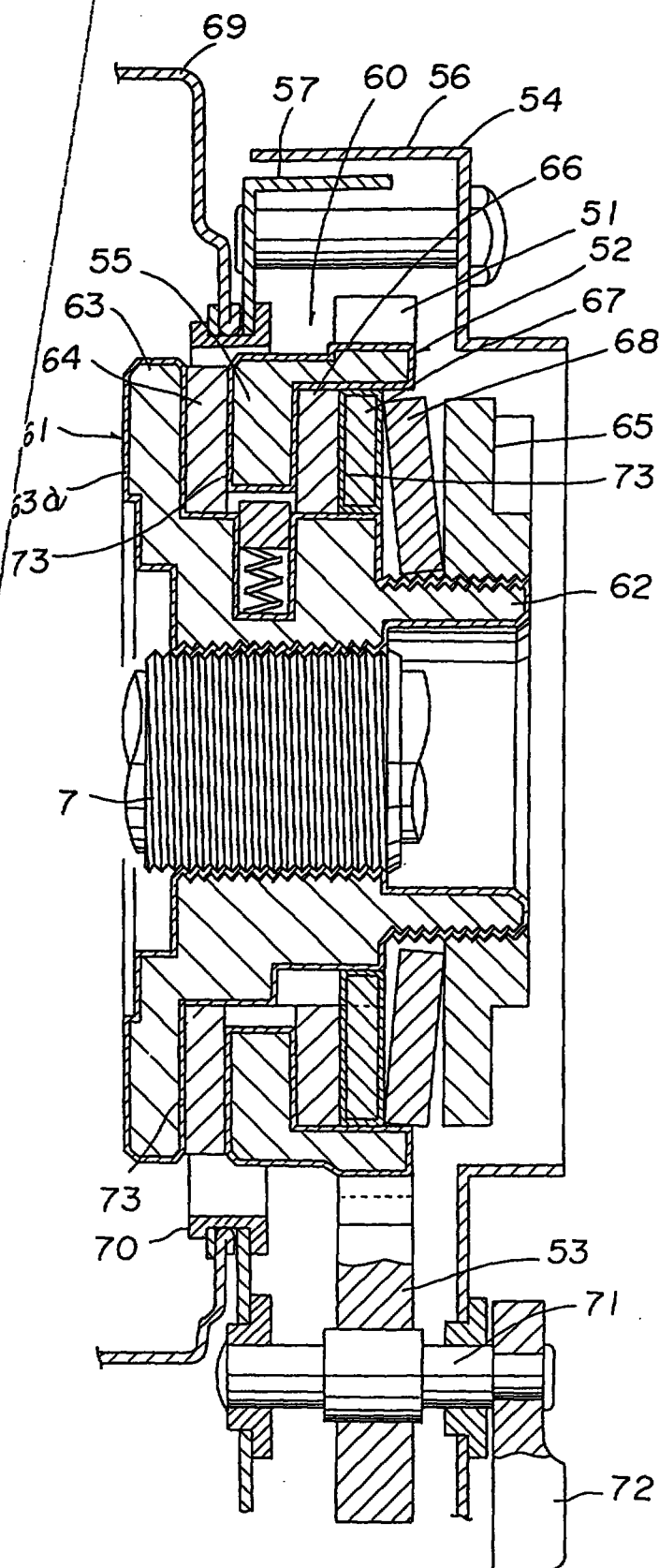
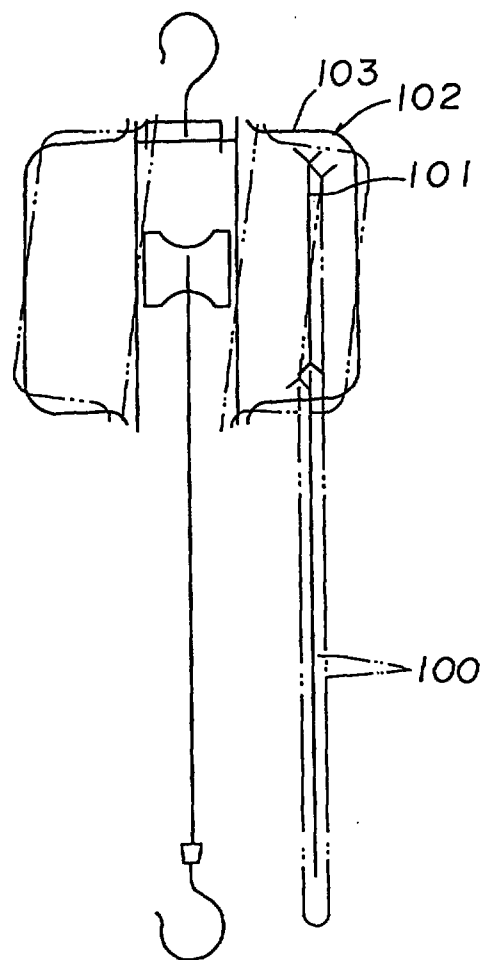


FIG. 7



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MANUAL HOIST AND TRACTION MACHINE

The present invention relates to a manual hoist and traction machine, and more particularly to a manual hoist and traction machine which is provided with a manual driving member mainly comprising a handwheel and with a mechanical brake operated by the manual driving member so that the manual driving member operates to rotatably drive a load sheave to hoist, haul, or lower a load, or to release traction thereof.

The conventional manual chain block, one of the manual hoist and traction machines, has been well-known as disclosed in, for example, the Japanese Utility Model Publication Gazette No. Sho 54-39231.

The manual chain block disclosed in the above Gazette is so constructed that a driving shaft is supported between side plates through a pair of bearings, a load sheave in association with the driving shaft through a reduction gear mechanism is rotatably supported to the driving shaft, a driven member having at one side thereof a driven disc is coupled with the driving shaft, a boss of a handwheel is screwably mounted thereto, and a braking ratchet wheel engageable with a braking pawl and a pair of lining plates positioned sandwiching therebetween the braking ratchet wheel, are supported at the outer periphery of a cylindrical

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portion of the driven member, so that these members constitute a mechanical brake. A hand chain engaging with the handwheel is adapted to operate for rotatably driving the driving shaft through the mechanical brake and drive the load sheave to hoist a load or release the mechanical brake to lower the hoisted load.

The manual chain block constructed as the above-mentioned, however, uses a usual lining plate commercially available as a brake lining for a bicycle or the like for the lining plate to be used in the mechanical brake. Therefore, a diameter of the lining plate is made approximately equal to that of the handwheel at the handwheel and opposite to the side surface of the wheel.

The brake lining generally used for industrial machines, even when it is the most superior in property, may have a coefficient of friction of 0.20 or more at a friction surface temperature of 200 °C in consideration its function, and compressive strength may be 1000 (kg/cm²) at the largest and the maximum strain about 8 (10⁻³ mm/mm), which will comply with the provisions of Japanese Industrial Standard. When the usually commercial product is used for the mechanical brake at the manual chain block, in consideration of performance and quality, the lining plate is made larger in diameter, the friction surface of the wheel opposite to the lining plate increases in area and decreases in surface

pressure, so that the mechanical brake is adapted to operate corresponding to a hoist load without hindrance.

Meanwhile, the manual chain block has recently been required to be small-sized from simplicity in handling, which is realized by improving the quality of material of each component to raise its durability. However, the handwheel is limited to its diameter from a limit to a diameter of the lining plate, thereby being restricted in its miniaturization. Also, the axial position of the handwheel needs to be set at the axially outside of the mechanical brake so that the axial size of the handwheel also is limited in the miniaturization thereof. When the handwheel is axially outwardly positioned, a distance between the mounting portions of the handwheel and bearing for supporting the driving shaft to the side plates, so that, when the handwheel is driven by the hand chain, the driving shaft is easy to deflect due to a load acting on the handwheel. Hence, in some cases where the hand-chain is forcibly operated, the problem is created in that the driving shaft is deformed. Also, in the no-load state where a hook at the load chain engaged with the load sheave hangs no load and the load sheave is not affected by the load, the body of chain block, as shown by the two-dot chain line in Fig. 7 which illustrates a prior art arrangement, is slanted due to weight of the hand chain engageable with the handwheel, whereby, when the hand chain 100 is operated to rotate the handwheel 101, not only the hand chain 100 comes

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into contact with a wheel cover 103 at the chain block body 102 so as to generate noises, but also resistance is generated against the operation of hand chain 100. Hence, there is no inertia resistance of handwheel 101 caused by the operation of hand chain 100, so that the hand chain 100 cannot quickly rotate the hand wheel 101, thereby creating the problem in that the hook of the load chain cannot be lifted rapidly.

An object of the present invention is that in the manual chain block mainly having the handwheel, the number of pockets thereof can be minimized and also the wheel of the handwheel is lapped on the mechanical brake so that the handwheel can be axially positioned in proximity to a side of the side plate for supporting the load sheave and moreover a diameter of the wheel can be small so as to enable the chain block to be miniaturized.

Another object of the present invention is that in the manual hoist and traction machine including the above-mentioned manual chain block, the friction surface of the mechanical brake or an overload prevention device is improved to stabilize the performance thereof.

In order to attain the above-mentioned objects, a manual hoist and traction machine which is provided with first and second side plates, a load sheave supported therebetween through a pair of bearings, a driving shaft for

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driving the load sheave, a driven member coupled with the driving shaft and having the friction surface, and a driving member screwably mounted on the driving shaft and having a friction surface opposite to that of the driven member, and which is also provided between the driven member and the driving member with a mechanical brake having at both axial sides thereof the friction surfaces and the outer peripheral portion with which a braking pawl is engageable, and first and second lining plates interposed between the friction surfaces of the driven member and braking ratchet wheel and between the friction surfaces of the braking ratchet wheel and driving member respectively, is characterized in that the lining plates each are formed of a lining raw material comprising heat-resistant fiber, a friction regulating agent and a bonding agent, and having the performance such that, when the mechanical brake operates due to forward screw movement of the driving member, the raw material having a friction coefficient of 0.35 or more at a temperature of 200°C of the respective friction surfaces, compressive strength of 15 (kgf/mm²) at hardness (HRS) of 90 to 120, and the maximum strain of 12 (10⁻³ mm/mm) or more.

The present invention is further characterized in that at the manual chain block in which the driving member comprises a handwheel provided with a wheel and a boss screwably mounted to the driving shaft and with a hand chain

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engageable with the wheel of the handwheel, a friction surface is provided at the side surface of the boss at the mechanical brake side ; the wheel has pockets in the minimum number for receiving therein horizontal links of the hand chain and is provided at the inside surface with an inside swollen portion swollen from the friction surface toward the first side plate, and furthermore, an outer diameter of the first lining plate is smaller than an inner diameter of the inside swollen portion at the wheel, the braking ratchet wheel is provided with a cylindrical portion extending from the outer periphery thereof toward the first side plate, the cylindrical portion is provided at the outer periphery thereof with teeth engageable with the braking pawl, and the teeth are displaced toward the first side plate with respect to the inside swollen portion of the wheel, and furthermore outer diameters of the second lining plate and driven member with the friction surface are made smaller than the inner diameter of the cylindrical portion at the braking ratchet wheel.

The cylindrical portion at the braking ratchet wheel is preferable to be overlapped on the outer periphery of the bearing supporting the load sheave to the first side plate. Also, it is preferable that, among the friction surfaces with which the first and second lining plates come into frictional contact because they are axially biased by

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forward screw movement of the handwheel, the friction surfaces provided on at least the driven member and braking ratchet wheel are each provided with a friction control layer plated and heat-treated.

Furthermore, the present invention is still further characterized in that in the manual chain block wherein the the driving member comprises a brake holder screwably mounted to the driving shaft and having a flange having at the inside surface a friction surface and a cylindrical portion, a handwheel having a boss having at both axially side surfaces the friction surfaces and an inside swollen portion and rotatably supported to the cylindrical portion at the brake holder, and a hand chain engageable with the handwheel; a load setting and adjusting member is screwably mounted to the cylindrical portion of the brake holder, a first friction plate is interposed between the flange of the brake holder and the boss of the handwheel, a second friction plate is interposed between the boss and the load setting and adjusting member, and a holding plate and an elastic member are interposed between the second friction plate and the load setting and adjusting member to thereby form an overload prevention device, and also the respective outer diameters of the flange at the brake holder and first and second friction plates are made smaller than the inner diameter of the inside swollen portion at the handwheel.

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It is preferable that in the overload prevention device , the respective outer diameters of the elastic member, holding plate and load setting and adjusting member are made smaller than the inner diameter of the axially outside swollen portion at the handwheel and the overload prevention device is adapted to be contained in a plane of projection of both the axially side surfaces at the wheel of the handwheel.

Also, it is preferable that, in the manual hoist and traction machine provided with the overload prevention device, at the friction surfaces of at least the flange at the brake holder and of the holding plate among the friction surfaces with which the first and second friction plates come into frictional contact is provided a friction control layer formed of a heat-treated plated layer.

The present invention is yet further characterized in that in a lever type hoist and traction machine, the driving member comprises a brake holder screwably mounted to the driving shaft and having a flange having at the inside surface the friction surface and a cylindrical portion, a driving gear having a boss having at both axial side surfaces friction surfaces and teeth positioned at the outer periphery, and an operating lever having a driving pawl engageable with the teeth at the driving gear, an overload setting and adjusting member is screwably mounted to the cylindrical portion at the brake holder, a first friction

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plate is interposed between the flange of the brake holder and the boss of the driving gear, a second friction plate is interposed between the boss of the driving gear and the load setting and adjusting member, and a holding plate having the friction surface and an elastic member are interposed between the second friction plate and the load setting and adjusting member to thereby form an overload prevention device, and also the respective friction surfaces of the flange at the brake holder, driving gear and holding plate are provided a friction control layers each formed of a heat-treated plated layer.

Also, it is preferable that in the aforesaid lever type hoist and traction machine, the plated layer at the friction control surface is formed of nickel phosphorus, nickel chromium, or chromium, and that the heat-treatment temperature of the plated layer is set to an austenite transformation point temperature at the respective raw materials of the brake holder, driving gear and holding plate provided with the layer and the plated layer being diffused onto the surface of each raw material.

Therefore, according to the invention as set forth in claim 1, the first and second lining plates of the mechanical brake are formed of the above-mentioned lining raw material, whereby an outer diameter of the respective lining plates can be smaller.

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Accordingly, when the present invention is applied to the manual chain block having a handwheel according to a first example, the handwheel can be smaller in diameter thereof to thereby enable the chain block to be miniaturized as a whole.

Also, according to the invention as set forth in claim 2, in the manual chain block provided with the handwheel,

a friction surface is provided at the side surface of the boss of the handwheel at the mechanical brake side, the number of pockets at the wheel at the handwheel

made minimum, at the inside thereof, that is, at the side surface at a side of the first side plate is provided an inside swollen portion swollen beyond the friction surface

toward the first side plate, an outer diameter of the first lining plate is made smaller than an inner diameter of the inside swollen portion, the cylindrical portion is provided at the braking ratchet wheel, the teeth are provided at the cylindrical portion and displaced from the inside swollen portion toward the first side plate, and the outer diameters of the second lining plate and driven member which is provided with the friction surface are made smaller than the inner diameter of the cylindrical portion, whereby while enabling the handwheel to be smaller in diameter, the handwheel can be axially displaced toward the load sheave, in other words, the side plate supported to the load sheave.

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Accordingly, the handwheel can be made smaller in the size not only radially but also axially, thereby enabling the chain block to be miniaturized and also the driving shaft to be less deflected, and the entire chain block when no-loaded can be less slanted and the handwheel is inertial-rotatable, whereby the hand chain can be operated smoothly, rapidly, and without noises.

Accordingly to the invention as set forth in claim 3, the cylindrical portion of the braking ratchet wheel is overlapped on the outer periphery of the bearing for supporting therethrough the load sheave to the second side plate, whereby the braking pawl engageable with the teeth at the cylindrical portion can be displaced toward the side plate so that the handwheel also can be displaced toward the same to that extent, thereby enabling the chain block to be further reduced in axial length and the driving shaft to be reduced in deflection when the handwheel is driven, and the chain block as a whole can be less slanted during the no loading.

According to the invention as set forth in claim 4, the friction control layer is provided at the friction surface, whereby, while forming the lining plate and of the lining raw material, the attack resistance of the friction surface is improvable and the coefficient of friction is controllable, whereby, even in long use, the

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coefficient of friction of the friction surface can be stabilized and the braking property can be prevented from being varied after long use, thereby enabling stable use to be performed for long use.

Furthermore, according to the invention as set forth in claim 5, in the chain block assembling therein the overload prevention device since the outer diameter of the flange and those of the friction plates and at the brake holder are made smaller than the inner diameter of the inside swollen portion at the wheel of the handwheel, the friction plates can be contained in the plane of projection of the wheel at the handwheel whereby, while providing the overload prevention device the handwheel can further be reduced in axial length and miniaturized as the whole.

According to the invention as set forth in claim 6, the outer diameter of the elastic member, holding plate and load setting and adjusting member at the overload prevention device are made smaller than the inner diameter of the wheel and the overload prevention device is contained in the plane of projection at the wheel, whereby, while providing the overload prevention device, the chain block can effectively be prevented from increasing in axial length due to the overload prevention device.

According to the invention as set forth in claims

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8 and 9, the manual chain block and lever-type hoist and traction machine each are provided at the friction surface of the overload prevention device with the friction control layer 39, whereby the coefficient of friction of the friction surface is controllable to be a desired value, a transmitting torque by the load setting and adjusting member can accurately be set, variation between the products is eliminated, and the surface condition of the friction surface is never changed by attack of friction plates. Also the hoist and traction machine is not affected by rust, thereby enabling the set value of transmitting torque to be held to a proper value for a long time. Hence, the load sheave is ensured to slip by an overload more than the set value on the basis of the prest transmitting torque so as to effectively realize the overload prevention.

According to the invention as set forth in claim 10, the heat-treatment temperature of the plated layer is set to an austenite transformation point temperature of the driving side and driven side members for forming the plated layer and the plated layer is diffused and permeated onto the raw material surface of the respective driving side and driven side members, whereby the surface hardness can be made to be 600 or more of Vickers hardness. Accordingly, the attack resistance and

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transmitting torque can be held effectively and for a long time.

These and other objects of the invention will become more apparent in the detailed description and examples which follow.

It will be understood that the description is given by way of example only and not by way of limitation.

In the drawings:-

Fig. 1 is a partial, longitudinally sectional, view of a first embodiment of the present invention;

Fig. 2 is an enlarged sectional view of a principal portion of an embodiment in which a friction control layer is provided at a friction surface of a mechanical brake.

Fig. 3 is an enlarged sectional view of another example when provided with the friction control layer, showing a principal portion only;

Fig. 4 is a partially omitted longitudinally sectional view of a second embodiment of the present invention;

Fig. 5 is an enlarged sectional view of the principal portion of the embodiment provided at the friction surface of an overload prevention device with the friction control layer;

Fig. 6 is an enlarged sectional view of a third embodiment of the present invention, showing a principal portion and corresponding to Fig. 5; and

Fig. 7 is a schematic illustration of the conventional example, showing the problem therein.

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A first embodiment of the present invention shown in Fig. 1 is a manual chain block having no overload prevention device, in which a mounting shaft 4a for mounting a hook 4 is provided between a pair of side plates 1 and 2, a load sheave 3 engageable with a load chain 110 is rotatably supported between the side plates 1 and 2 through bearings 5 and 6, a driving shaft 7 is inserted into a shaft bore of the load sheave 3, with one axial side of the driving shaft 7 is integrally coupled a driven member 10 comprising a driven disc 8 and a cylindrical portion 9, a handwheel 11 is screwably mounted onto the one axial end of the driving shaft 7, at the cylindrical portion 9 of the driven member 10 are supported a braking ratchet wheel 12 and first and second lining plates 13 and 14 positioned at both axial sides of the braking ratchet wheel 12, to the first side plate 1 is supported, through a pawl shaft 16a and a pawl spring 16b, a braking pawl 16 engageable with teeth 15 at the braking ratchet wheel 12, and the driven member 10, handwheel 11, braking ratchet wheel 12, braking pawl 16 and the pair of first and second lining plates 13 and 14, form a mechanical brake 17. Furthermore, at the other axial side of the driving shaft 7 is provided a reduction gear mechanism 18 having a plurality of reduction gears.

The above-mentioned construction is well-known, so that an endless hand chain 100 engageable with the handwheel

11 is operated to rotatably drive the handwheel 11 and a driving force is transmitted to the driving shaft 7 through operation of the mechanical brake 17 and the load sheave 3 can be driven through the reduction gear mechanism 18, whereby a load can be hoisted through the load chain 110 engageable with the load sheave 3.

The first embodiment of the invention shown in Fig.1 is so constructed that in the manual chain block the handwheel 11 can be made smaller in diameter, displaced at the axial position toward the first side plate 1, and reduced not only in a radial length but also in an axial length, whereby, while the chain block can be miniaturized as a whole, deflection caused by a load acting on the handwheel 11 can be reduced and the entire chain block, when not-loaded, can be less slanted.

In detail, the handwheel 11 is provided at the inside surface of a boss 19 with a friction surface 19a, a wheel portion 20 in continuation of the boss 19 is axially swollen toward the first side plate 1 with respect to the boss 19, at the wheel portion 20 are provided the minimum number of pockets 20a for receiving therein lateral links of the hand chain, an outer diameter of each pocket is made smaller, as shown in Fig.2, an outer diameter r_1 of the first lining plate 13 in contact with the friction surface 19a is made smaller than an inner diameter R of the inside swollen portion of the wheel portion 20, at the braking ratchet wheel

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12 is provided a cylindrical portion 21 extending from the outer periphery thereof toward the load sheave 3 and overlapping on the outer periphery of the bearing 6, at the outer periphery of the cylindrical portion 21 are provided teeth 15 engageable with the braking pawl 16, the teeth 15 are displaced toward the load sheave 3 with respect to the inside swollen portion of the wheel portion 20, an outer diameter r_2 of the second lining plate 14 and that r_3 of the driven disc 8 at the driven member 10 are made smaller than an inner diameter of the cylindrical portion 21, and the first and second lining plates 13 and 14 are formed of the following lining raw material.

In other words, the lining raw material comprises heat resistant fiber, a friction regulating agent and a bonding agent, and has the performance of a coefficient of friction of 0.35 to 0.60 at a surfacial temperature of 200° C of the respective friction surfaces, hardness (HRS) of 90 to 120, compressive strength of 1500 (kg/cm²) or more, and the maximum strain of 12(10⁻³ mm/mm) or more.

In greater detail, in the first embodiment shown in Fig. 1, the number of pockets at the handwheel 11 is six, the outer diameters r_1 through r_3 of the first lining plate 13, second lining plate 14 and driven disc 8 at the driven member 10, are equal to each other, the outer diameters r_1 through r_3 being made smaller than an inner diameter R of the inside

swollen portion at the wheel portion 20 and smaller than an outer diameter of the bearing 6.

The heat resistant fiber constituting the first and second lining plates 13 and 14 uses inorganic fiber, such as, glass fiber, rock wool, metallic fiber, ceramic fiber, and carbon fiber; or organic fiber, such as, alamode fiber, acrylic fiber, or phenol fiber. The friction regulating agent uses powder or whiskers comprising metal, such as, iron, brass, copper, zinc, or aluminum; inorganic salt, such as, sulfate, barium sulfate, potassium carbonate, or potassium titanium; or inorganic material, such as, graphite or carbon; or organic material, such as, rubber, fluororesin, high molecular phenol resin, or cashew dust; and further the bonding agent uses binder of resin material, such as, phenol resin, denatured phenol resin, polyimido resin, epoxy resin, cashew resin or melamine resin.

The heat resistant fiber is used as the aggregate and the friction regulating agent and bonding agent are mixed in the following ratio (volume %):

heat resistant fiber: 28 to 35 (V%)

friction regulating agent: 20 to 37 (V%)

bonding agent: 35 to 45 (V%).

The lining raw material is molded to the lining plates 13 and 14 and pressurized and heated. The lining plates 13 and 14 each molded by mixing the materials in the

above-mentioned ratio to be pressurized and heated obtain the following performances:

hardness (HRS) : 90 to 120

bending strength (Kgf/mm²) : 9 to 15

maximum strain (10⁻³ mm/mm) : 12 to 16

compressive strength (Kgf/mm²) : 15 to 20

coefficient of friction (200 °C) : 0.35 to 0.60.

In addition, when the above-mentioned performance is compared with that of the usual brake lining of resin series of non-asbestors. especially the compressive strength is stronger by 15 to 20 %, which is obtained because the ratio (V%) of heat resistant fiber and bonding agent is 63 to 80 % to be larger than the ratio of usual brake lining and then molded by being pressurized and heated. Such performance can miniaturize the lining plates 13 and 14 at the mechanical brake 17 which are tightened toward the driven disc 8 by forward screw movement of the handwheel 11 and have the function to transmit the driving force to the driving shaft 7.

Accordingly, since the lining plates 13 and 14 each are reduced in diameter more than the inner diameter R of the inside swollen portion of the wheel 20 at the handwheel 11, the handwheel 11 can be smaller in diameter. Moreover, in the embodiment shown in Fig.1, the cylindrical portion 21 of the braking ratchet wheel 12, as the above-mentioned, is overlapped on the outer periphery of the bearing 6 so that the braking

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pawl 16 engageable with the teeth 15 at the cylindrical portion 21 can be displaced toward the first side plate 1, whereby together with this construction, the handwheel 11 can be made smaller in diameter and also its axial position can be displaced in proximity to the side plate 1. In brief, the first lining plate 13 and the boss of braking ratchet wheel 12 can be contained in the plane of projection of the inside surface of the wheel 20 at the handwheel 11, thereby enabling the chain block to be reduced in axial length to that extent .

Thus, since the handwheel 11 can be miniaturized and displaced at the axial position thereof toward the side plate, the chain block can be miniaturized as a whole. Moreover, the handwheel 11 can be axially positioned at the side-plate side, that is, near the bearing 6 at the side plate 1, whereby, when the handwheel 11 is driven by the hand chain, the driving shaft 7, even when subjected to a large hoisting load, can be restrained from deflection and stable hoisting operation can be performed. Also, the entire chain block can be less stanted in the no-load state, so that, when the hand chain 100 is operated to rotate the handwheel 11 in the no-load state, the hand chain 100 can be prevented from coming into contact with the wheel cover 25 and smoothly operated, thereby reducing noises. Also, the handwheel 11, when rotated by the hand chain 100, can be inertia-rotated, thereby enabling the handwheel 11 rotated by the hand chain 100 to

quickly operate to that extent, and the hook of the load chain 110 to be quickly lifted.

In addition, in the above-mentioned construction, the number of pockets at the handwheel 11 is six, but may be five. The minimum number of pockets means that the number of pockets is added by 1, in the case where, when the handwheel 11 is manually operated by the hand chain 100, variation in magnitude of manual power becomes larger to deteriorate the operability, thereby lowering the efficiency. The number of pockets depends on chain pitch of the hand chain, and, in the present pitch of 23.5 pitch at a line diameter of 5 mm and 28.0 pitch of 23,5 pitch at a line diameter of 5 mm and 28.0 pitch at that of 6 mm, the minimum number of pockets is five.

The driving shaft 7 is supported at one axial end to a bearing 23 provided at a gear cover 22 for covering the reduction gear mechanism 18 and at the other axial end to a roller bearing 24 fitted into the shaft bore of the load sheave 3. In this case, a bearing may be provided at the wheel cover 25 for covering the handwheel 11 so that an extending shaft portion of the driving shaft 7 may be supported to the bearing.

Furthermore, it is preferable that in the above-mentioned construction, the friction surfaces of the braking ratchet wheel 12 and driven disc 8 of the driven

member 10, with which the first and second lining plate 13 and 14 axially biased by forward screw movement of the handwheel 11 come into frictional contact, are, as shown in Fig. 3, provided plated layers of nickel phosphate, nickel chromium, or chromium, of 8 to 20 micron thick, the plated layers being heat-treated to form friction control layers 26 respectively.

The friction control layers 26 each are not merely plated layer, but it formed by heat-treating the plated layer by a heating furnace at a temperature of 300 to 400 °C, or at the austenite transformation point temperature of, for example, 850°C of each member constituting the friction surface, and by diffusing and permeating the plated layer into the raw material of each member. Hence, the heat treatment raises the surface hardness and improves the attack resistance, and the coefficient of friction can be controlled to a predetermined value. Moreover, variation between the products can be reduced, and, even when used for a long time, the coefficient of friction of the friction surface can be stably maintained to enable the braking property to be prevented from deterioration after a long use and the stable use to be performed for a long time.

In addition, it is preferable that the friction control layer 26 is provided also at the friction surface 19a of the handwheel 11. In this case, a plated layer may be

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formed on the entire surface of the handwheel 11, but, as shown in Fig.3, the boss 19 and wheel 20 may be independently formed and then coupled with a rivet 80 or the like, so that the plated layer is provided on the entire surface of the boss 19. Or, a contact plate (not shown) provided with the friction control layer is separately formed so as to be integrally coupled with the boss 19 by riveting, a fixing method using adhesive, or the like. Thus, the friction control layer 26 is provided at the friction surface 19a of the handwheel 11, so that, when the mechanical brake 17 is released, that is, when the handwheel 11 is screwably backward moved to release the operation of mechanical brake 17, such releasing is smooth, thereby eliminating the inconvenience that the friction surface 19a is caught onto the lining plate 13 to cause not-releasing of the mechanical brake 17. Also, in the case where the plated layer is heat-treated at the austenite transformation point temperature, it is preferable that the plated layer is quenched with cold water or cold oil after the heat treatment and thereafter is tempered at a temperature of 200 to 500°C, normally 300 to 450 °C, so as to be formed to a martensite structure.

Next, explanation will be given on a second embodiment of the present invention shown in Fig.4. The second embodiment assembles an overload prevention device 30 in the chain block of the first embodiment, in which the

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handwheel 11 is provided with a brake holder 31 screwably mounted on the driving shaft 7 and comprising a flange 32 having at the inside a friction surface and a cylindrical portion 33, to which a boss 19 of the handwheel 11 is rotatably supported and to which a load setting and adjusting member 34 is screwably mounted, between the flange 32 of the brake holder 31 and the boss 19 is interposed a first friction plate 35 and between the boss 19 and the load setting and adjusting member 34 is interposed a second friction plate 36, and between the second friction plate 36 and the load setting and adjusting member 34 is interposed an elastic member 37 mainly comprising a disc spring, thereby forming the overload prevention device 30.

In the above-mentioned construction, outer diameters r of the flange 32 and friction plates 35 and 36, of the elastic member 37 and load setting and adjusting member 34, and of the holder 38 interposed between the second friction plate 36 and the elastic member 37 at the brake holder 31, are made smaller than inner diameters R of the inside and outside swollen portion of the wheel 20 at the handwheel 11, so that the overload prevention device 30 may be contained within the plane of projection of both axial side surfaces at the wheel 20 of the handwheel 11.

Although the friction surfaces 35 and 35 may use known friction plates, it is preferable to use the same lining

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raw material as the lining plates 13 and 14 at the mechanical brake 17.

In this case, it is preferable that the friction surfaces of the members with which the friction plates 35 and 36 come into frictional contact, in other words, the friction surface of the flange 32 at the brake holder 31 and that of the holder 38 are , as shown in Fig.5, provided with friction control layers 39 formed of plated layers of nickel phosphate, nickel chromium or chromium, and of 8 to 20 micron thick and heat-treated.

The friction control layers 39 each are not merely the plate layer as the same as those 26 at the friction surfaces of the mechanical brake 17, but are formed in such a manner that the plated layer is heat-treated in a heating furnace at a tempearture of 300 to 400°C , or at the austenite transformation point temperature of, for example, 850 °C of the above-mentioned members for constituting the friction surfaces, and diffused and permeated into the raw material of each member, whereby the surface hardness can be raised and attack resistance can be improved by the heat treatment and also the coefficient of friction can be controlled to reduce variation between the products.

It is preferable that the friction control layers are formed also at the friction surfaces at both sides the boss 19 of the handwheel 11.

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In this case, a plated layer may be formed at the entire surface of the hand wheel 11 for this purpose, but a friction plate provided with the friction control layer may be separately formed so that the friction plate may be integrally coupled with the boss 19 by riveting or a fixing method with adhesive.

The aforesaid embodiments both are applied to the manual chain block which uses the handwheel 11 so as to operate the hand chain 100 for driving the load sheave 3. Besides this, they are applicable to a lever type hoist and traction machine comprising, as the driving member a driving gear 52 having at the outer periphery thereof teeth 51 and an operating lever 54 having a driving pawl 53 engageable with the teeth 51 at the driving gear 52 as shown in Fig.6.

The lever type hoist and traction machine shown in Fig.6, as the same as the second embodiment shown in Fig. 4, assembles an overload prevention device 60. The overload prevention device 60 is provided with a brake holder 61 separate from the driving gear 52, a boss 55 thereof is rotatably supported to a cylindrical portion 62 of the brake holder 61, a first friction plate 64 is interposed between a flange 63 of the brake holder 61 and the boss 55 of the driving gear 52, a load setting and adjusting member 65 is screwably mounted onto the cylindrical portion 62, between the adjusting member 65 and the boss 55 of the driving gear

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52 is interposed a second friction plate 66, and between the second friction plate 66 and the load setting and adjusting member 65 is interposed a holding plate 67 having a friction surface and an elastic member 68 formed mainly of a disc spring.

In Fig.6, the brake holder 61, as the same as the second embodiment, is screwably mounted to the driving shaft 7, and a mechanical brake is provided at the lateral side facing the first side plate, that is, at the left side in Fig.6, and at the left side surface of the flange 63 at brake holder 61 is provided a friction surface 63a coming in frictional contact with the first lining plate at the mechanical brake.

The operating lever 54 is elongated and couples a pair of lever plates 56 and 57 opposite to each other through bolt. The lever plate 57 is rotatably supported through a bearing member 70 to a brake cover 69 fixed to the first side plate 1 and for covering the mechanical brake, and in the vicinity of the supporting portion of lever plate 57 it supported the driving pawl 53 through a pawl shaft 71 so as to be capable of being positioned at three positions of hoist and traction, lowering and releasing traction, and the neutral, so that an operating lug 72 fixed to the axial end of pawl shaft 71 is operated to switch the driving pawl 53 to the three positions.

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In a third embodiment of the invention shown in Fig.6, onto the entire surfaces of the brake holder 61, driving gear 52 and holding plate 67 are formed plated layers of nickel phosphate, nickel chromium or chromium and of 8 to 20 micron thick by means of electrolytic plating, and then heat-treated for 1 to 2 hours at a temperature of 300 ° C by a heating furnace, so as to form a friction control layer 73 of the surface hardness of Vickers hardness of 350 to 450.

Thus, the friction control layers 73 are formed at the surfaces of the brake holder 61, driving gear 52 and holding plate 67 at the driving side and opposite to the friction plates 64 and 66, and can control the surface condition, that is, the coefficient of friction with respect to the surface of raw material as the same as the second embodiment. Moreover, variation between the products can be reduced and the adjusting member 65 is tightened to set a transmitting torque, whereby the set value can properly be held, an overload more than the set transmitting torque can ensure a slip of the load sheave, and effective overload prevention can be realized.

Moreover, the friction control layer 73 is not a mere plated layer, but it is formed by heat-treating a plated layer, whereby the surface hardness can be raised and the coefficient of friction be lowered to that extent to be constantly controlled. Hence, the transmitting torque can

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further accurately be set and variation between the products is eliminated, and also the surface condition of the layer 73, that is, the coefficient of friction, can be prevented from being varied due to attack of the first and second friction plates 64 and 66, and is not affected by generation of rust, thereby enabling the set transmitting torque to be held in a proper value for a long time.

The heat treatment of the above-mentioned plated layer is performed by the heating furnace at a temperature of 300 °C . However, the plated layer may be heat-treated by the heated furnace at a temperature 400 °C for 1 to 2 hours. In this case, the surface hardness of the friction control layer 100 can be Vickers hardness of 400 to 450.

Furthermore, the heat treatment temperature of the plated layer, as the same as the second embodiment, may be set to an austenite transformation point temperature of, for example, 850 °C , of the raw material (structural steel) constituting the brake holder 61, driving gear 52 and holding plate 67, and the plated layer is diffused and permeated into the raw material, whereby the diffused and permeated layer may form the friction control layer 73.

In this case, the heat treatment may be carried out at the heating furnace, but is preferable to be done by high frequency induction heating. Also, the plated layer is preferred to be quenched by cold water or cold oil after the

heat treatment and then tempered usually at a temperature of 300 to 450 °C to be formed in martensite structure.

Thus, the friction control layer 100 can have the surface hardness of Vickers hardness of 600 or more, for example, 800 through 1000.

The first and second lining plates used for the mechanical brake in the third embodiment shown in Fig.6, as the same as the first and second embodiments, use the lining raw material respectively. Also, in the third embodiment, the brake holder 61 and driving gear 52 can be smaller in diameter. Accordingly, the operating lever 54 can further be miniaturized and the brake holder 61, driving gear 52 and operating lever 54 can be axially positioned to proximity to the first side plate.

Although several embodiments have been described, they are merely exemplary of the invention and not to be constructed as limiting, the invention being defined solely by the appended claims.

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What is Claimed is:

1. A manual hoist and traction machine provided with first (1) and second (2) side plates, a load sheave (3) supported between said first and second side plates through a pair of bearings (5, 6), a driving shaft (7) for driving said load sheave (3), a driven member (10) coupled with said driving shaft (7) and having a friction surface, and a driving member (11) screwably mounted to said driving shaft and having a friction surface (19a) opposite to the friction surface of said driven member, and provided between said driven member and said driving member with a mechanical brake (17) having a braking ratchet wheel (12) having at both axial sides friction surfaces and engageable at the outer periphery with a braking pawl (16) and having first and second lining plates (13, 14) interposed between the friction surfaces of said driven member (10) and braking ratchet wheel (12) and between the friction surfaces of said braking ratchet wheel (12) and driving member (11), said hoist and traction machine including the construction that said respective lining plates (13, 14) are formed of lining raw material comprising heat resistant fiber, a friction regulating agent and a bonding agent and provided with performances of a coefficient of friction of 0.35 or more at a surface temperature of 200°C of each of said friction



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surfaces with which each of said lining plates comes into contact when said mechanical brake operates due to forward screw movement of said driving member, hardness (HRS) of 90 to 120, compressive strength of 15 (Kgf/mm²) or more, and the maximum strain of 12 (19⁻³mm/mm) or more.

2. A hoist and traction machine according to claim 1, wherein said driving member comprises a handwheel (11) provided with a wheel (20) and boss (19) screwably mounted to said driving shaft (7) and a hand chain (100) engageable with said wheel of said handwheel (11), the side surface of said boss at the mechanical brake side has a friction surface, said wheel has the minimum number of pockets (20a) for receiving therein horizontal links of said hand chain and said wheel has an inside swollen portion swollen at an inside portion thereof toward said first side plate beyond said friction surface, said hoist and traction machine including the construction that:

an outer diameter of said first lining plate (13) is smaller than an inner diameter of said inside swollen portion at said wheel,

said braking ratchet wheel (12) is provided with a cylindrical portion extending from the outer periphery of said ratchet wheel (12) toward said side plate, at the outer periphery of said cylindrical portion are provided teeth with which said braking pawl comes into contact, said teeth are displaced toward said first side plate with



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respect to said inside swollen portion at said wheel, and

outer dimeters of said second lining plate (14) and driven member provided with said friction surface and made smaller than an inner diameter of said cylindrical portion (21) of said braking ratchet wheel.

3. A manual hoist and traction machine according to claim 2, wherein said cylindrical portion (21) at said braking ratchet wheel (12) is overlapped on the outer periphery of a bearing (6) for supporting therethrough a load sheave (3) to said first side plate.

4. A manual hoist and traction machine according to claim 2, wherein at the friction surfaces provided at at least said driven member (10) and braking ratchet wheel (12) among said friction surfaces with which said first and second lining plates are axially biased by forward screw movement of said handwheel so as to come into frictional contact are provided friction control layers (26) comprising plated layers, said plated layers being heat-treated respectively.

5. A manual hoist and traction machine according to claim 1, wherein said driving member comprises a brake holder (31) screwably mounted to said driving shaft and having a cylindrical portion (21) and a flange (32) having at the inside thereof a friction surface, a handwheel having a boss having at both axial sides thereof friction surfaces and an inside swollen portion and rotatably supported to said cylindrical portion of said brake holder

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(31), and a hand chain engageable with said handwheel, to said cylindrical portion at said brake holder is screwably mounted a load setting and adjusting member, a first friction plate (35) is interposed between said flange of said brake holder and said boss of said handwheel, a second friction plate (36) is interposed between said boss and said load setting and adjusting member, and a holding plate and an elastic member are interposed between said second friction plate and said load setting and adjusting member, thereby forming an overload prevention device (30), and outer diameters of said flange at said brake holder and first and second friction plates (35, 36) are made smaller than an inner diameter of said inside swollen portion at said handwheel.

6. A manual hoist and traction machine according to claim 5, wherein the outer diameter of said elastic member (37), holding plate (38) and load setting and adjusting member (34) at said overload prevention device (30) are made smaller than the inner diameter of a swollen portion at the an axially outside surface (20), and said overload prevention device (30) is contained within the plane of projection of both said axial surfaces at said wheel of said handwheel.

7. A manual hoist and traction machine according to claim 5, said friction surfaces of at least said flange of said brake holder and holding plate among said friction



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surfaces with which said first and second friction plate come into frictional contact are provided with friction control layers comprising heat-treated plated layers.

8. A manual hoist and traction machine according to claim 1, wherein said driving member comprises a brake holder (61) having a cylindrical portion (62) and screwably mounted to said driving shaft and having a cylindrical portion and a flange having at the inside surface a friction surface, a driving gear (52) which has a boss (55) having at both axial sides friction surfaces, and teeth positioned at the outer periphery; and an operating lever having a driving pawl engageable with said teeth at said driving gear, to said cylindrical portion (62) of said brake holder is screwably mounted a load setting and adjusting member, between said flange (63) of said brake holder and the boss of said driving gear is interposed a first friction plate (64), between said boss of said driving gear and said load setting and adjusting member is interposed a second friction plate (66), and between said second friction plate (66) and said load setting and adjusting member (65) are interposed a holding plate (67) having a friction surface and an elastic member (68) to thereby form an overload prevention device, and at the friction plates of said flange at said brake holder, driving gear, and holding plate, are each provided with a friction control layer formed of a plated layer which is heat-treated.



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9. A manual hoist and traction machine according to claim 8, wherein said friction control layer each are formed of nickel phosphate, nickel chromium, or chromium.

10. A manual hoist and traction machine according to claim 8, wherein the heat treatment temperature of said plated layer is set to an austenite transformation point temperature of raw material of each of said brake holder, driving gear and holding plate, and said plated layer is diffused onto the surface of said each raw material.



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MANUAL HOIST AND TRACTION MACHINE

ABSTRACT OF THE DISCLOSURE

The invention relates to a manual hoist and traction machine wherein an outer diameter of a first lining plate (13) constituting a mechanical brake is made smaller than an inner diameter mainly of a driven disc at a wheel of a handwheel (11), outer diameter of a second lining plate (14) and a driven disc are made smaller than an inner diameter of a cylindrical portion of a braking ratchet wheel (12), and the first and second lining plates (13, 14) are formed of lining raw material having performance of compressive strength of $15(\text{Kgf/mm}^2)$ or more and the maximum strain of $12(10^{-3}\text{mm/mm})$ or more.

FIGURE 1.

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