

Description

FIELD OF THE INVENTION AND RELATED ART

The present invention relates to an image forming apparatus such as a laser beam printer, wherein an image bearing member is electrically charged by a charging member contacted to the image bearing member and supplied with a vibratory voltage, and the charged surface of the image bearing member is scanned line by line to be exposed to image information.

Contact charging is the charging in which a charging member supplied with a voltage is contacted to a member to be charged to apply electric charge to the member to be charged to a desired potential level. As compared with a widely used corona discharger, the voltage required for providing the potential level on the member to be charged is smaller; the quantity of ozone produced by the charging action is very small so that the ozone removing filter is not required, and the air discharging system is simplified; the maintenance operation is easy; and the structure is simple.

Because of these advantages, it is particularly noted as means which can replace the corona discharger to charge an image bearing member or other members to be charged such as a photosensitive member, a dielectric member or the like in an image forming apparatus such as an electrophotographic machine, digital copying machine, laser beam printer or an electrostatic recording machine.

U.S. Patent No. 4,851,960 which has been assigned to the assignee of this application has proposed a contact charging method and device in which a vibratory voltage is applied to the contact charging member, which is contacted to the member to be charged to uniformly charge the member to be charged (see preamble of Claim 1).

Referring first to Figure 4, there is shown an example of the structure. A member 1 to be charged, is an electrophotographic photosensitive member or an electrostatic recording dielectric member, which will hereinafter be called simply "photosensitive drum", in the form of a drum rotatable at a predetermined peripheral speed (process speed) in a direction indicated by an arrow, for example.

A contact charging member 2 is in the form of a conductive roller (charging roller) and comprises a core metal 2b and conductive roller 2a therearound made of conductive rubber or the like. The charging roller 2 is press-contacted to the surface of the photosensitive drum with a predetermined pressure provided by urging springs 10 acting on the opposite end portions of the core metal 2b. The conductive roller rotates following rotation of the photosensitive drum 1.

A voltage application source 9 applies a voltage to the charging roller 2 by way of a contact leaf spring 8 contacted to the core metal 2b of the charging roller

2. The voltage is a vibratory voltage (DC biased AC voltage) having a peak-to-peak voltage V_{pp} larger than twice a charge starting voltage relative to the photosensitive member. By the application of such a voltage, the outer peripheral surface of the photosensitive drum 1 is uniformly charged, while it is rotated.

The contact charging member is not limit to a roller configuration, but may be in the form of a blade, a rod, a block, a pad, a belt, a web, a brush or the like.

The image forming apparatus using the contact type charging means supplied with such a voltage so as to charge the image bearing member, involves the following problems.

Figure 5 shows an example of horizontal line pattern image 11a formed on a recording sheet 11. When such a pattern is produced, the image may have interference stripes 11b if the spatial frequency by the frequency of the voltage source 9 to the contact charging member 2 becomes close to the intervals between the horizontal lines 11a.

The frequency of the voltage source 9 can vary $\pm 10\%$ from the rated frequency because of parts error. With some voltage source 9, the spatial frequency thereof is the same as the intervals between horizontal lines 11a with the result of remarkable interference stripes 11b.

SUMMARY OF THE INVENTION

Accordingly, it is a principal object of the present invention to provide an image forming apparatus capable of producing good images without or with suppressed interference fringes or stripes.

These and other objects, features and advantages of the present invention will become more apparent upon a consideration of the following description of the preferred embodiments of the present invention taken in conjunction with the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 shows a general arrangement of an exemplary image forming apparatus in the form of a laser beam printer according to an embodiment of the present invention.

Figure 2 is a sectional view of an example of a multi-layered charging roller.

Figure 3 is a sectional view of an example of a charging blade.

Figure 4 is a sectional view of another example of a contact charging roller.

Figure 5 shows an example of interference stripes.

Figures 6A, 6B, 7A, 7B, 8A, 8B, 8C, 9A, 9B and 9C are graphs explaining causes of interference stripe production.

Figure 10 is a graph of spatial wavelength λ_{sp} vs.

wavelength number f of the voltage source.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

Referring to Figure 1, there is shown an exemplary image forming apparatus according to an embodiment of the present invention. The image forming apparatus is a laser beam printer using an electrophotographic process wherein a contact type charger is used to charge an image bearing member 1.

The image bearing member is an electrophotographic photosensitive member (photosensitive drum) in the form of a rotatable drum. In this embodiment, it comprises an aluminum base drum 1b coated with a photosensitive layer of organic photoconductor (OPC) 1a. The outer diameter thereof is 30 mm and is rotated at a predetermined process speed V_p (peripheral speed) in the clockwise direction A. As shown in the Figure, the drum base 1b is electrically grounded.

A contact type charging member 2 is in the form of a charging roller and comprises a core metal 2b covered with conductive roller 2a having elasticity and made of carbon-dispersed EPDM or urethane or the like. Similarly to the case of Figure 4, the opposite end portions of the core metal shaft 2b are urged by urging springs toward the photosensitive drum 1 surface to press-contact the charging member thereto. The charging roller rotates following rotation of the photosensitive drum 1. The charging roller 2 is provided with a resistance layer on the conductive roller 2a to prevent leakage to the photosensitive drum 1, the resistance layer being made of epichlorohydrin rubber having a larger volume, resistivity than the conductive roller 2a, and further, the resistance layer is coated with resin layer to prevent softening agent contained in the rubber, the resin layer being made of N methoxy methyl nylon. Although, these layers are not shown in the Figure, but it is preferable that they are provided.

The charging roller 2 is supplied by way of the contact leaf spring 8 with a vibratory voltage, that is, a DC biased AC voltage having a frequency f ($V_{dc} + V_{ac}$) to form an alternating electric field between the charging roller 2 and the photosensitive drum 1, by which the surface of the rotating photosensitive drum 1 is uniformly charged to a predetermined negative potential.

A laser beam scanner 3 is supplied with time series electric digital signals corresponding to picture elements representing an intended image from a host apparatus (not shown) such as a computer, a word-processor or an image reader. It emits a laser beam L imagewise modulated at a predetermined printing density D (dots per inch or $D/25.4$ dots per mm.) in accordance with the digital picture element signal. The surface of the photosensitive drum 1 electrically

charged in the manner described above, is exposed to the laser beam L from the scanner 3 controlled by the controller, so that the drum is scanned by the laser beam L in the main scan direction, that is, in the direction parallel to the generating line of the photosensitive drum. By repeating this, an electrostatic latent image corresponding to the intended image information is formed on the photosensitive drum 1 surface.

The latent image is developed by a developing sleeve 4 of the developing device, more particularly, the portion of the photosensitive drum 1 having been exposed to the laser beam L receives negatively charged toner. The developed image is transferred onto a transfer material 7 made of paper and introduced from an unshown sheet feeding station at a proper timing with the developed image to an image transfer station where the photosensitive drum 1 and the transfer roller 5 supplied with a positive DC voltage are contacted or faced.

The transfer material 7 having passed through the transfer station is separated from the photosensitive drum and is conveyed to an unshown image fixing station.

The surface of the photosensitive drum 1, from which the image has been transferred, is cleaned by a cleaning blade 6, so that the residual toner or other contamination matter is removed to be prepared for the next image forming operation.

Referring to Figures 8A, 8B and 8C, the cause of production of the interference stripes 11b shown in Figure 5 will be described. Figures 8A, 8B and 8C show the projections of the laser beam on the moving photosensitive drum. In Figures 8A and 8B, the intervals between adjacent scanning lines are indicated by 1. The laser beam emitted from the laser scanner is reflected by one of rotating polygonal mirror surfaces to line scan once the photosensitive drum in the main scan direction. The printing density by the laser scanning line is assumed as being 200/25.4 dpm (200 dpi). Then, the one dot diameter d is

$$d = 25.4 \times 1000/200 = 127.0 \mu\text{m}.$$

That is, the interval l between the adjacent scanning lines is $l = d = 127.0 \mu\text{m}$.

As shown in Figure 9A in the solid line, in the contact type charging, the dark portion potential VD on the photosensitive drum has a charge pattern which is called "cycle pattern" having a spatial wavelength $\lambda_{sp} (= V_p/f)$ determined by the frequency f of the AC component of the voltage applied by the voltage source 9 and the process speed V_p (the peripheral speed of the photosensitive drum). See also document US-A-4 727 453 which describes such a "cycle pattern" as strobing.

The spatial wavelength λ_{sp} of the cycle pattern varies more or less depending on the variation of the frequency and the variation in the process speed. It can be measured in the following manner. First, the photosensitive drum is uniformly charged by the

charging roller, and then, is exposed to uniform light at its whole surface. The amount of exposure is adjusted so that the cycle pattern on the photosensitive drum is clearly developed.

Subsequently, the developed cycle pattern is transferred and fixed on the transfer sheet. The cycle pattern on the transfer sheet is measured using a magnifier, so that the variations of the spatial wavelength λ_{sp} is measured. The cycle pattern becomes smaller with increase of the frequency f of the AC component of the voltage source 9. If it is equal to or larger than several thousand hertz, for example, the pattern is hardly observable by human eyes. However, if the frequency f is higher than 600 Hz, the charging roller mechanically vibrates relative to the photosensitive drum, with the result of noise, and therefore, the frequency f is preferably not more than 600 Hz.

Figure 9A is a graph of the surface potential of the photosensitive drum vs. positions of the moving photosensitive drum surface.

When the process speed $V_p = 12\pi$ mm/s, and $f = 300$ Hz, then $\lambda_{sp} = 125.6$ μ m.

Then, the spatial wavelength $\lambda_{sp} = 125.6$ μ m is quite close to $l = 127.0$ μ m. If they become equal to each other due to the variation in the voltage of the voltage source, the falling of the potential across the developing bias V_{Dev} , as shown in Figure 9A by broken lines, and therefore, lines are developed thick, as shown in Figure 9A by hatched lines with the result of interference stripes.

The surface of the charging roller is contaminated with foreign matter such as toner particles, silica particles, paper dust or the like, and if this occurs, the contamination portion has come to have electrostatic capacity.

Therefore, even if the same voltage is applied to the core metal 2b of the charging roller by the same voltage source 9, the surface potential induced on the photosensitive drum 1 is deviated in the phase at the position where the surface of the charging roller has the electrostatic capacity.

If the electrostatic capacity is not uniform along the axis of the charging roller with the result of deviated phase, the interference stripes 11b may occur as shown in Figure 5.

If the phase of the charging potential is deviated from that of Figure 9A by the amount of half wavelength, for example, that is, if the interval l between adjacent scanning lines and the phase of the spatial wavelength λ_{sp} are deviated, the whole surface of the photosensitive drum receives the toner with the developing bias of V_{Dev} , as shown in Figures 8B and 10B. Thus, the interference stripes appear as shown in Figure 9A, or do not appear as in Figure 9B, depending on the difference of the foreign matter (difference in the electrostatic capacity) along the length of the charging roller.

It will be understood that even if the spatial wavelength and the interval between the scanning lines are not the same, the interference stripes are produced depending on the developing bias level if the spatial wavelength is an integer multiple (double in Figure 9C) or an integer reciprocal of the interval between adjacent scanning lines.

The spatial wavelength λ_{sp} is not determined only on the frequency f of the voltage source, but is dependent on the process speed V_p , and therefore, the variation in the process speed V_p is considered similarly as the variation in the spatial wavelength λ_{sp} as discussed above.

The production of the interference stripes will be prevented if the frequency and the process speed V_p are so determined that the scanning line interval l does not fall in the variation range of the spatial wavelength λ_{sp} determined by the frequency f of the voltage source and the process speed V_p . More particularly, the interference stripes can be prevented if an integer multiple of the scanning line interval or an integer reciprocal thereof is not in the variation range of the spatial wavelength λ_{sp} (= process speed divided by the frequency of the voltage source).

Since the interval l between the adjacent scanning lines is the diameter of one dot, as described hereinbefore, the condition of not producing the interference stripes is that the variation range of the wavelengths λ_{sp} does not contain an integer multiple or a reciprocal of an integer multiple of the diameter d .

In the laser beam printer, the frequency f of the vibratory voltage provided by the voltage source 9, and the process speed V_p are so determined that the range of the spatial wavelength λ_{sp} with its variation and the interval l between adjacent scanning lines multiplied by N or $1/N$ (N : integer) are not overlapped.

Then, the interference stripes attributable to the interference between the spatial wavelength λ_{sp} and the scanning line interval, can be prevented.

The laser beam printer described above is capable of forming line images of various patterns. In the following embodiment, the interference stripes are prevented from occurring in any line image patterns.

In the laser beam printer, various pattern of line images can be formed. In other words, assuming that n dot(s) of image portion continues in the sub-scan direction of the image bearing member (photosensitive drum) and that m dot(s) of non-image portion continues in the sub-scan direction, the laser beam printer is adjustable so that the numbers n and m are arbitrary.

Figure 6A shows an example of on and off of the laser beam. It is a graph of laser on/off vs. the position on the moving image bearing member. During the laser beam being on, the laser beam scans one line on the surface of the photosensitive drum in the main scan detection by one reflecting surface of the rotating polygonal mirror.

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The interval between the center of the off state and the center of the next off state of the laser beam in the sub-scan direction of the photosensitive member is given by equation (1) below, if the printed pattern is such a horizontal line pattern 11a wherein the lines each have a thickness of 1 dot spaced with the spaces each corresponds to 1 dot ($n = m = 1$) and if the printing density is 400/25.4 dpmm (400 dpi):

$$d = 25.4 \times 1000/400 = 63.5 \mu\text{m}, \quad (1)$$

the interval = $2 \times 63.5 \mu\text{m}$.

For the horizontal line pattern with n dots and m space, the interval is:

$$(n + m)d \quad (1)$$

if $n = m = 1$, the interval is $127.0 \mu\text{m}$.

Here, "n dots and m spaces" means that the laser beam scans (on) n lines, and thereafter the laser does not scan (off) m lines, and these operations are repeated.

The contact charging, as contrasted to corona charging, the charge distance G (Figure 4) is very short, more particularly, as short as approximately $30 \mu\text{m}$, and therefore, the charging action is easily influenced by the voltage source 9. In other words, the dark portion potential VD on the photosensitive drum, as shown in Figure 7A by solid lines, it involves charging pattern called "cycle pattern" having a spatial wavelength λ_{sp} ($= V_p/f$) determined by the frequency f of the AC component of the applied voltage from the voltage source 9 and the process speed V_p (the surface movement speed of the photosensitive drum).

The spatial wavelength λ_{sp} of the cycle pattern varies slightly because of the variations in the frequency and the process speed. The range of the variation can be determined by observing the cycle pattern formed on a transfer sheet, in the manner described in the foregoing.

Figure 7A is a graph of the surface potential of the photosensitive drum vs. position of the moving surface of the photosensitive drum.

If the process speed V_p is $12\pi \text{ mm/s}$, and $f = 300 \text{ Hz}$, then $\lambda_{sp} = 125.6 \mu\text{m}$.

Therefore, the wavelength of the horizontal line pattern given by the equation (1), that is, $(n+m)d = 127.0 \mu\text{m}$ becomes quite close to the spatial wavelength $\lambda_{sp} = 125.6 \mu\text{m}$. When the phases thereof becomes the same, the falling of the potential across the developing bias v_{Dep} becomes large as shown in Figure 7A, with the result that the lines are developed thick, and therefore, interference stripes are produced. On the contrary, the phase difference between the wavelength of $(n+m)d$ and the spatial wavelength λ_{sp} is the half wavelength, as shown in Figures 6B and 7B, the lines are developed thin, and the interference stripes are produced.

In use of the charging roller 2, foreign matter such as toner particles, silica particles or paper dust is deposited on a part of the surface of the roller, with the result that the part thus contaminated as electrostatic

capacity.

Therefore, even if the same voltage is applied to the core metal 2b of the charging roller from the same voltage source 9, the surface potential induced on the photosensitive drum 1 is different in the phase between the portion having the electrostatic capacity and the portion not having the capacity.

When the phase difference occurs due to the electrostatic capacity difference along the axis of the charging roller results in the production of the interference stripes 11b, as shown in Figure 5.

Figure 10 is a graph of a spatial wavelength λ_{sp} vs. voltage source frequency f under the condition that the process speed V_p is $12\pi \text{ mm/s}$, and the printing density is 400/25.4 dpmm (400 dpi). In this case, $(n+m)d$ of the horizontal line pattern with one dot and one space is $127.0 \mu\text{m}$; $(n+m)d$ of the horizontal line pattern with 1 dot and 2 spaces is $190.5 \mu\text{m}$; and $(n+m)d$ of the horizontal line pattern with 1 dot and 3 spaces is $254.0 \mu\text{m}$.

The rated frequency of the voltage source was 290 Hz , and the variation of the frequency due to the accuracy of the parts or the like was 10% , that is, the frequency was $290 \pm 10 \%$, more particularly, the frequency ranges from $261 - 319 \text{ Hz}$. The range is indicated by A in Figure 10. As a result, even if the process speed $V_p = 12\pi \text{ mm/s}$ is constant, the spatial wavelength λ_{sp} ranges from $118 - 114 \mu\text{m}$. Therefore, the wavelength $(n+m)d$ of the horizontal line pattern with 1 dot and 1 space, that is, $127 \mu\text{m}$ may fall in the range. Then, an integer multiple (one) of $(n+m)d$ may be equal to the spatial wavelength in the range, and therefore, the likelihood of the interference stripe 11b production is high.

When the frequency f of the voltage source is set to be 250 Hz , the actual frequency ranges from $250 \text{ Hz} + 10 \%$ to $250 \text{ Hz} - 10 \%$ ($225 - 275 \text{ Hz}$, as shown in Figure 10 by B. If the process speed V_p ($= 12\pi \text{ mm/s}$) is constant, the spatial wavelength changes within the range from $137 - 168 \mu\text{m}$. In this case, any of the horizontal line patterns with 1 dot and 1 space, with 1 dot and 2 spaces or with 1 dot and 3 spaces do not result in that $(n+m)d$ multiplied by N or by $1/N$ (N : integer) falls in the variable range of the spatial wavelength. This applies to any integers of n and m . In other words, it applies to any case where the laser beam printer produces any horizontal line patterns. Accordingly, the interference stripes are not produced when the frequency f of the voltage source and the process speed V_p are set in the manner described above.

When the frequency f of the voltage source is 210 Hz , the frequency is in the range of $210 \text{ Hz} \pm 10 \%$, as indicated by a reference C in Figure 10 ($189 - 231 \text{ Hz}$). When the process speed V_p ($= 12\pi \text{ mm/s}$) is constant, the spatial wavelength varies from $163 - 199 \mu\text{m}$. When the horizontal line pattern with 1 dot and 2 spaces is formed, it is probable that $(n+m)d = 190.5$

μm falls in the variable range of the spatial wavelength. Therefore, when the frequency f and the process speed V_p are set in this manner, the likelihood of the interference stripe production is high.

As described in the foregoing, even if the spatial wavelength and $(n+m)d$ are not equal to each other, the interference stripes are produced if the spatial wavelength is an integer multiple or a reciprocal of an integer of $(n+m)d$.

With respect to Figure 10, the description has been made on the assumption that the process speed V_p does not vary. However, the spatial wavelength λ_{sp} depends not only the voltage source frequency f but also the process speed V_p . Therefore, the same considerations made in the foregoing applies to the variation in the spatial wavelength λ_{sp} due to the process speed V_p variation.

As described in the foregoing, by determining the voltage source frequency f and the process speed V_p such that the wavelength $(n+m)d$ of the horizontal line pattern does not follow in the variable range of the spatial wavelength λ_{sp} determined by the voltage source frequency f and the process speed, the production of the interference stripes can be prevented. In other words, an integer multiple or a reciprocal of an integer of $(n+m)d$ does not follow in the variable range of the spatial frequency λ_{sp} , the process speed multiplied by the frequency of the voltage source, by which the interference stripe production can be related for any horizontal line pattern, that is, for any n and m (n, m : integers).

From the above equation (1), it is understood that the wavelength of the horizontal line pattern is an integer of the diameter of dot, and therefore, the non-interference-stripe condition is satisfied if the variable range of λ_{sp} does not contain an integer multiple of the dot diameter or a reciprocal of an integer multiplied by the dot diameter.

In the laser beam printer, the ranges for the frequency f of the AC component of the voltage source 9 and the process speed V_p is set such that the variable range of the spatial wavelength λ_{sp} does not overlap the range of $(n+m)d$.

By doing so, the interference stripes resulting from the overlapping between the spatial wavelength λ_{sp} and the wavelength of the horizontal line pattern can be removed for any of horizontal line patterns.

The member to be charged by the charging roller 2 might have a defect such as pin hole or the like. If such a member is charged, using the charging roller 2, it is possible that unusual electric discharge occurs such as electric current leakage. In order to avoid this, the surface of the charging roller is coated with protection layer, as described hereinbefore.

Figure 2 shows an example of such a charging roller. It comprises a core metal 2b, a low resistance layer may be EPDM or urethane rubber in which carbon is dispersed, a conductive layer 2d made of N me-

thoxy methyl nylon or Torezin (trade name) in which large amount of carbon is dispersed, a high resistance layer 2e made of epichlorohydrin rubber or the like, and a protection layer 2f of Torezin. The same effects can be provided, when such a charging roller 2 is used.

The contact type charging member is not limited to the roller type, but may be in the form of a blade, a rod, a block, a pad, a belt, a web, a brush or the like.

Figure 3 shows an example of a blade type charging member 20 (charging blade). It comprises a sheet metal for applying a bias voltage to the blade, a blade body having a low resistance made of EPDM in which carbon is dispersed, and a high resistance layer 20c of epichlorohydrin rubber.

In this example, the edge of the charging blade 20 is press-contacted to the photosensitive drum 1 counter directionally with respect to movement direction of the surface of the photosensitive drum 1 with a predetermined pressure.

The same results can be obtained with such a charging blade 20, by selecting the frequency f of the voltage source and the process speed V_p in the manner described above.

The charging blade 20 has an advantage over the charging roller in that the cost is low, and the required space is small.

The foregoing description has been made with respect to the case wherein the image bearing member in the form of a photosensitive member is charged by the contact type charging member, and is exposed to the laser beam which is deflected by a rotating polygonal mirror in the longitudinal direction of the image bearing member (generating line of the photosensitive drum) to form a latent image along the scanning line. However, the present invention is not limited to this, but is applicable to the case wherein an LED head having LED elements arranged along a length of the photosensitive member is faced to the photosensitive member, and the LED are selectively actuated by signals from controller to form a latent image along the scanning line of the group of the LED element.

The image bearing member is not limited to the photosensitive member but may be an insulating member. In this case, a multi-stylus recording head may be used which has electrode pins arranged along the length of the image bearing member and faced thereto downstream of the contact charging member with respect to movement direction of the image bearing member. The latent image is formed along the line of the multi-stylus pins after the insulating member is electrically charged.

The present invention is applicable not only to the reverse-development type described in the foregoing, but is usable also to a regular development type.

The vibratory voltage applied between the image bearing member and the contact type charging mem-

ber may be a sine wave, rectangular wave or triangular wave.

As described in the foregoing, according to the present invention, the frequency of the vibratory voltage applied between the contact type charging member and the image bearing member and the moving speed of the image bearing member are selected in the ranges described in the foregoing, by which the interference stripes appearing on the output image can be prevented.

While the invention has been described with reference to the structures disclosed herein, it is not confined to the details set forth and this application is intended to cover such modifications or changes as may come within the scope of the following claims.

Claims

1. An electrostatic image forming apparatus comprising:

- a) a movable image bearing member (1);
- b) charging means for charging said image bearing member (1), said charging means including a contact member (2) contactable to said image bearing member (1) and voltage applying means (9) for applying a vibratory voltage between said contact member (2) and said image bearing member (1);
- c) latent image forming means (3) for forming on said image bearing member (1) charged by said charging means (2) a latent image along the main scanning line being parallel to the contact portion between said contact charging member (2) and said image bearing member (1), said latent image consisting of a plurality of dots and being developed and transferred onto a transfer material (7), characterized in that

the frequency f of said vibratory voltage and the speed V_p of movement of said image bearing member (1) at the time of charging are selected such that a range in which a variable spatial wavelength $\lambda_{sp} (=V_p/f)$ (μm) lies, does not overlap with $(n+m)d$ (μm) multiplied by N or $1/N$, where N is an integer number, d a diameter of one of said dots of said latent image, n the number of dots of an image portion in the sub-scanning lines and m the number of dots of a non-image portion in the sub-scanning lines.

2. An electrostatic image forming apparatus according to claim 1, characterized in that a waveform of said vibratory voltage is sine.
3. An electrostatic image forming apparatus according to claim 1, characterized in that said vibratory voltage is a DC biased AC voltage.

4. An electrostatic image forming apparatus according to claim 1, characterized in that said contact member (2) is in the form of a roller.

5. An electrostatic image forming apparatus according to claim 1, characterized in that said contact member is in the form of a blade (20).

6. An electrostatic image forming apparatus according to claim 1, characterized in that said latent image forming means (3) forms a latent image on said image bearing member (1) in accordance with image signals corresponding to image information.

7. An electrostatic image forming apparatus according to claim 6, characterized in that said image bearing member is a photosensitive member (1), and said latent image forming means includes a laser scanner (3) for exposing said photosensitive member (1) in accordance with image signals corresponding to image information.

8. An electrostatic image forming apparatus according to claim 1, characterized in that said frequency f of said vibratory voltage is not more than 600 Hz.

Patentansprüche

1. Elektrostatishes Bilderzeugungsgerät mit
 - a) einem bewegbaren Bildtragelement (1),
 - b) einer Ladeeinrichtung zum Aufladen des Bildtragelements (1), wobei die Ladeeinrichtung ein Kontaktelement (2), das mit dem Bildtragelement (1) in Kontakt bringbar ist, und eine Spannungsanlegeeinrichtung (9) zum Anlegen einer Wechselspannung zwischen dem Kontaktelement (2) und dem Bildtragelement (1) aufweist,
 - c) einer Latentbilderzeugungseinrichtung (3) zum Erzeugen eines latenten Bildes auf dem durch die Ladeeinrichtung (2) aufgeladenen Bildtragelement (1) entlang der Hauptabtastzeile, die parallel zu dem Kontaktabschnitt zwischen dem Kontaktaufladeelement (2) und dem Bildtragelement (1) ist, wobei das latente Bild aus einer Vielzahl von Punkten besteht und entwickelt und auf ein Übertragungsmaterial (7) übertragen wird, dadurch gekennzeichnet, daß

die Frequenz f der Wechselspannung und die Geschwindigkeit V_p der Bewegung des Bildtragelements (1) zu der Zeit der Aufladung derart gewählt sind, daß sich ein Bereich, in welchem eine variable räumliche Wellenlänge $\lambda_{sp} (=V_p/f)$ (μm) liegt, nicht mit $(n+m)d$ (μm) multipliziert



ber may be a sine wave, rectangular wave or triangular wave.

As described in the foregoing, according to the present invention, the frequency of the vibratory voltage applied between the contact type charging member and the image bearing member and the moving speed of the image bearing member are selected in the ranges described in the foregoing, by which the interference stripes appearing on the output image can be prevented.

While the invention has been described with reference to the structures disclosed herein, it is not confined to the details set forth and this application is intended to cover such modifications or changes as may come within the scope of the following claims.

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- b) charging means for charging said image bearing member (1), said charging means including a contact member (2) contactable to said image bearing member (1) and voltage applying means (9) for applying a vibratory voltage between said contact member (2) and said image bearing member (1);
- c) latent image forming means (3) for forming on said image bearing member (1) charged by said charging means (2) a latent image along the main scanning line being parallel to the contact portion between said contact charging member (2) and said image bearing member (1), said latent image consisting of a plurality of dots and being developed and transferred onto a transfer material (7), characterized in that

the frequency f of said vibratory voltage and the speed V_p of movement of said image bearing member (1) at the time of charging are selected such that a range in which a variable spatial wavelength $\lambda_{sp} (=V_p/f)$ (μm) lies, does not overlap with $(n+m)d$ (μm) multiplied by N or $1/N$, where N is an integer number, d a diameter of one of said dots of said latent image, n the number of dots of an image portion in the sub-scanning lines and m the number of dots of a non-image portion in the sub-scanning lines.

2. An electrostatic image forming apparatus according to claim 1, characterized in that a waveform of said vibratory voltage is sine.
3. An electrostatic image forming apparatus according to claim 1, characterized in that said vibratory voltage is a DC biased AC voltage.

4. An electrostatic image forming apparatus according to claim 1, characterized in that said contact member (2) is in the form of a roller.

5. An electrostatic image forming apparatus according to claim 1, characterized in that said contact member is in the form of a blade (20).

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7. An electrostatic image forming apparatus according to claim 6, characterized in that said image bearing member is a photosensitive member (1), and said latent image forming means includes a laser scanner (3) for exposing said photosensitive member (1) in accordance with image signals corresponding to image information.

8. An electrostatic image forming apparatus according to claim 1, characterized in that said frequency f of said vibratory voltage is not more than 600 Hz.

Patentansprüche

1. Elektrostatishes Bilderzeugungsgerät mit
 - a) einem bewegbaren Bildtrageelement (1),
 - b) einer Ladeeinrichtung zum Aufladen des Bildtragelements (1), wobei die Ladeeinrichtung ein Kontaktelement (2), das mit dem Bildtragelement (1) in Kontakt bringbar ist, und eine Spannungsanlegeeinrichtung (9) zum Anlegen einer Wechselspannung zwischen dem Kontaktelement (2) und dem Bildtragelement (1) aufweist,
 - c) einer Latentbilderzeugungseinrichtung (3) zum Erzeugen eines latenten Bildes auf dem durch die Ladeeinrichtung (2) aufgeladenen Bildtragelement (1) entlang der Hauptabtastzeile, die parallel zu dem Kontaktabschnitt zwischen dem Kontaktaufladeelement (2) und dem Bildtragelement (1) ist, wobei das latente Bild aus einer Vielzahl von Punkten besteht und entwickelt und auf ein Übertragungsmaterial (7) übertragen wird, dadurch gekennzeichnet, daß

die Frequenz f der Wechselspannung und die Geschwindigkeit V_p der Bewegung des Bildtragelements (1) zu der Zeit der Aufladung derart gewählt sind, daß sich ein Bereich, in welchem eine variable räumliche Wellenlänge $\lambda_{sp} (=V_p/f)$ (μm) liegt, nicht mit $(n+m)d$ (μm) multipliziert



mit N oder $1/N$ überdeckt, wobei N eine ganze Zahl, d ein Durchmesser von einem der Punkte des latenten Bilds, n die Anzahl von Punkten eines Abbildungsabschnitts in den Nebenabtastzeilen und m die Anzahl von Punkten eines Nichtabbildungsabschnitts in den Nebenabtastzeilen ist.

2. Elektrostatisches Bilderzeugungsgerät gemäß Anspruch 1, dadurch gekennzeichnet, daß eine Wellenform der Wechselspannung der Sinus ist. 10
3. Elektrostatisches Bilderzeugungsgerät gemäß Anspruch 1, dadurch gekennzeichnet, daß die Wechselspannung eine mit einer Gleichstrom-Spannung vorgespannte Wechselstrom-Spannung ist. 15
4. Elektrostatisches Bilderzeugungsgerät gemäß Anspruch 1, dadurch gekennzeichnet, daß das Kontaktelement (2) die Form einer Walze hat. 20
5. Elektrostatisches Bilderzeugungsgerät gemäß Anspruch 1, dadurch gekennzeichnet, daß das Kontaktelement die Form einer Klinge (20) hat. 25
6. Elektrostatisches Bilderzeugungsgerät gemäß Anspruch 1, dadurch gekennzeichnet, daß die Latentbilderzeugungseinrichtung (3) in Übereinstimmung mit Bildsignalen entsprechend der Bildinformation ein latentes Bild auf dem Bildtragelement (1) ausbildet. 30
7. Elektrostatisches Bilderzeugungsgerät gemäß Anspruch 6, dadurch gekennzeichnet, daß das Bildtragelement ein lichtempfindliches Element (1) ist, und die Latentbilderzeugungseinrichtung eine Laserabtasteinrichtung (3) zum Belichten des lichtempfindlichen Elements (1) in Übereinstimmung mit Bildsignalen entsprechend der Bildinformation aufweist. 35
8. Elektrostatisches Bilderzeugungsgerät gemäß Anspruch 1, dadurch gekennzeichnet, daß die Frequenz f der Wechselspannung nicht mehr als 600 Hz beträgt. 40

Revendications

1. Un dispositif de formation d'image électrostatique comprenant :
 a) un organe support d'image (1) déplaçable;
 b) un moyen de chargement, pour charger ledit organe support d'image (1), ledit moyen de chargement comprenant un organe de contact pouvant être mis en contact avec ledit organe de support d'image (1), et un moyen d'application de tension (9) pour appliquer 50

une tension alternative entre ledit organe de contact et ledit organe support d'image (1);
 c) un moyen de formation d'image latente (3) pour former sur ledit organe support d'image (1) chargé par ledit moyen de chargement (2) une image latente, sur une ligne d'exploration principale parallèle à la partie de contact entre ledit organe de chargement par contact (2) et ledit organe support d'image (1), ladite image latente étant composée d'une pluralité de points et étant développée et transférée sur un matériau de transfert (7) caractérisé en ce que

la fréquence f de ladite tension alternative et la vitesse de déplacement V_p dudit organe support d'image (1) au moment du chargement sont choisies de manière à ce qu'une plage, dans laquelle une longueur d'onde spatiale $\lambda_{sp} (=V_p/f)$ variable (μm) se situe, ne soit pas recouverte par $(n+m)d$ (μm) multiplié par N ou par $1/N$, dans laquelle N est un entier, d est le diamètre de l'un desdits points de ladite image latente, n est le nombre de points d'une partie à image des lignes d'exploration secondaires et m est le nombre de points d'une partie sans image des lignes d'exploration secondaires.

2. Dispositif de formation d'image électrostatique selon la revendication 1, caractérisé en ce que la forme d'ondulation de ladite tension alternative est sinusoïdale.
3. Dispositif de formation d'image électrostatique selon la revendication 1, caractérisé en ce que ladite tension alternative est une tension alternative pure soumise à l'influence d'une tension continue.
4. Dispositif de formation d'image électrostatique selon la revendication 1, caractérisé en ce que ledit organe de contact (2) se présente sous la forme d'un rouleau.
5. Dispositif de formation d'image électrostatique selon la revendication 1, caractérisé en ce que ledit organe de contact se présente sous la forme d'une lame (20).
6. Dispositif de formation d'image électrostatique selon la revendication 1, caractérisé en ce que ledit moyen de formation d'image latente (3) forme une image latente sur ledit organe de support d'image (1) selon des signaux d'image correspondant à la formation d'image.
7. Dispositif de formation d'image électrostatique selon la revendication 6, caractérisé en ce que ledit support d'image est un organe photosensible 55



(1) et ledit moyen de formation d'image latente comprend un appareil d'exploration à laser (3) destiné à effectuer l'exposition dudit organe photosensible (2) d'après les signaux d'image correspondant à la formation d'image.

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8. Dispositif de formation d'image électrostatique selon la revendication 1, caractérisé en ce que ladite fréquence f de ladite tension alternative ne dépasse pas 600 Hz.

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