

COMPOSITION AND METHOD TO REMOVE ASBESTOS

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RELATED APPLICATIONS

10 This application is related to the following commonly assigned
applications, which have been filed simultaneously herewith and the disclosures of
which have been incorporated herein by reference in their entirety:

(1) Serial number 08/721,854 (Docket No. 8903), entitled COMPOSITION
AND METHOD TO REMOVE ASBESTOS;

15 (2) Serial number 08/721,859 (Docket No. 9032), entitled COMPOSITION
AND METHOD TO REMOVE ASBESTOS;

(3) Serial number 08/721,858 (Docket No. 9161), entitled COMPOSITION
AND METHOD TO REMOVE ASBESTOS;

20 (4) Serial number 08/721,863 (Docket No. 9225), entitled COMPOSITION
AND METHOD TO REMOVE ASBESTOS;

(5) Serial number 08/721,857 (Docket No. 9166), entitled FOAM
COMPOSITION FOR TREATING ASBESTOS-CONTAINING MATERIALS
AND METHOD OF USING SAME; and

(6) Serial number 08/721,853 (Docket No. 9130), entitled CORROSION INHIBITING COMPOSITION FOR TREATING ASBESTOS CONTAINING MATERIALS.

5. **BACKGROUND OF THE INVENTION**

This invention relates to methods and compositions for digesting the chrysotile form of asbestos ("chrysotile asbestos") to provide a non-asbestos material while the chrysotile asbestos is a component of a gypsum-containing cementitious composite, and especially to methods and compositions for the in-
10 place digestion of chrysotile asbestos present in composite material that is bonded to a support structure.

Chrysotile asbestos is a serpentine asbestos fibrous-like material consisting of alternating layers of silica and magnesium oxide/hydroxide bound to each other through covalently shared oxygen.

15 At least in part because of its availability and unique fire resistance and thermal properties, chrysotile asbestos has been used commercially in a variety of building products, including, for example, fire resistant roofing shingles, acoustical plasters, fire resistant and thermally insulating coating compositions and the like. In the formation of fire resistant coating compositions, found to be appropriate for
20 treatment by the present invention, small amounts of chrysotile asbestos were mixed with a settable bonding material, such as calcium sulfate hemihydrate and, optionally, other materials such as vermiculite and the like. The composition was

then applied to a structure where it forms a hardened gypsum-containing coating. For example, such compositions found considerable use in multi-story buildings wherein the gypsum-containing composition was applied as an adherent coating to steel girders, floor support plates, concrete decking and the like to provide fire resistance and high-temperature thermal insulation properties which aid in preventing damage and even possible collapse of such buildings in the event of fire.

In recent years asbestos has been classified as a regulated material in the United States. Federal, state and local government agencies also have promulgated regulations dealing with the use and disposal of asbestos-containing building materials. The U.S. Environmental Protection Agency ("EPA") has defined asbestos-containing material ("ACM") as a material containing therein greater than one percent (1%) asbestos. In accordance with various regulatory procedures, various safeguards are employed to protect workers from inhaling asbestos fibers during the removal or demolition activities. Such safeguards include, among others, requiring workers to wear approved respirator or breathing apparatus, as well as protective clothing, requiring any area in a building in which asbestos-containing material is being removed to be isolated or enclosed from the remainder of the building, and requiring the enclosed work area to be kept at a negative pressure by the use of special apparatus equipped with HEPA filters to prevent airborne asbestos fibers from leaving the work area. Such isolation of the work area is an expensive and time consuming part of the process.

Generally, prior art methods for handling asbestos-containing building materials have taken several approaches. One approach has been to chemically alter asbestos fibers before using them in building products. This approach is discussed, for example, in U.S. patents 4,328,197 and 4,401,636, both to Flowers, and in U.S. patent 4,474,742 to Graceffa et al.

Graceffa et al (U.S. 4,474,742) teach treatment of asbestos with hydroxamic acid and iron chelating agents to remove the iron present in the asbestos based on their presumption that the iron is the harmful component. In the Flowers patents (U.S. 4,328,197 and U.S. 4,401,636), one is taught to contact asbestos fibers with an aqueous solution of a weak base/strong acid or a strong base/weak acid salt of manganese, chromium, cobalt, iron, copper or aluminum or mixtures thereof, to convert the asbestos fibers into a metal-micelle product. In general, the process contemplated by Flowers is effected by preparing a slurry of asbestos fibers in an aqueous solution of the appropriate salt, effecting the conversion of the asbestos fibers to metal-micelle fibers in the slurry, and recovering the metal-micelle fibers from the slurry for use in the subsequent preparation of the desired fiber-containing end product.

Another approach is to treat previously formed asbestos-containing building materials by encapsulating the materials to thereby prevent the asbestos fibers from becoming airborne. A resinous encapsulating coating material typically would be applied by spraying, brushing or troweling. Care must be taken when using encapsulating methods so as not to physically damage the building material being

encapsulated. Encapsulation is a containment method and, thus, the encapsulated material remains in place during the life of the building.

A number of removal techniques have been proposed, and each has its advantages and disadvantages. For example, it has been proposed to simply scrape or chip away at dry untreated asbestos-containing material and to collect the scrapings for discard. This technique, which is referred to as dry removal, is generally considered unacceptable by regulatory agencies since it provides no safeguards against the release of airborne asbestos particles.

Dry vacuum methods have been attempted to overcome the problem of dry removal by incorporating an exhaust filtering system to prevent pollution to the outside environment and by using sealed containers for storing and discarding the collected asbestos-containing material. One of the disadvantages of this dry vacuum method is that the bond between the dry building material and the underlying surfaces on which it is coated may be stronger than the vacuum capabilities of the equipment. In those cases, it is necessary to dislodge at least a portion of the asbestos-containing material by scraping or chipping, which has the same limitations as the dry removal process described above.

Wet removal processes have been developed as a means for reducing the problems associated with the various dry removal techniques. Wet removal generally involves wetting a building material with water or water-surfactant solution to soften it and to thereby facilitate its removal. Wet removal clearly represents an improvement over dry removal. However, the use of water as a

softening agent is not entirely satisfactory because water penetrates slowly, does not completely wet most building materials, and tends to run off the surfaces being treated.

Over the past several years, wet removal techniques have been improved by
5 devising more effective wetting and/or softening compositions. Recent U.S. patents which relate to such improved wet removal techniques include, for example, U.S. patent 4,347,150 to Arpin; U.S. patent 4,693,755 to Erziner; and U.S. patent 5,258,562 to Mirick et al.

The Arpin patent discloses a technique for wetting and removing friable
10 insulating materials from an underlying substrate using a two-part wetting system. The first component comprises an aqueous alkali metal silicate dispersion blended with a cationic or nonionic surfactant and the second component comprises a mixture of an acrylic latex and a reagent that is reactive with the alkali metal silicates in the first part. The two parts are stored separately and are mixed shortly
15 before use to form a stripping composition which facilitates the removal of the building material while encapsulating the individual asbestos fibers contained therein. The removed material must be handled as an asbestos-containing material.

The Erzinger patent exemplifies a wet method for removing asbestos-
containing materials from a substrate. This patent discloses applying a
20 composition containing a cellulosic polymer to the asbestos-containing material, allowing the cellulosic polymer-containing composition time to penetrate and wet

the asbestos-containing material, removing the wet material from the underlying substrate by mechanical forces, and collecting the removed material for discard.

The Mirick et al patent is centered on the concept of removing asbestos fiber containing building material by applying a dilute aqueous solution of an acid, which may include a separate source of fluoride ions such as an alkali metal or ammonium salt of hydrofluoric acid, to the building material for the purpose of conditioning the material to aid in its removal while partially converting the asbestos fibers. The building material, after having been treated with the dilute acid solution, preferably is removed for further treatment and/or discard. Mirick et al further contemplate that the wet building material, once removed, can then be digested by immersing the material into a bath of an acid solution, preferably with heating and agitation, until all of the asbestos material has been destroyed.

The problems of wet removal techniques include the requirements of physical removal and handling of the wet asbestos-containing material. In addition, the removed material must be further treated to destroy the remaining asbestos component if the material is to be discarded as a non-asbestos-containing material.

In the process described in Mirick et al, in which a combination of acid and fluoride source is used, the formed solution generates excessive hydrogen fluoride noxious gas while in storage and during application which presents a health hazard to the applicator. The Office of Safety and Health Administration ("OSHA") has

set an upper permissible exposure limit of three (3) parts per million of hydrogen fluoride in the atmosphere.

U.S. Patent 5,472,562 to Ziger relates to etch baths containing a combination of phosphoric acid, nitric acid and hydrofluoric acid to selectively remove silicon nitride from an integrated circuit having a silicon substrate. This reference discloses that various soluble silicon compounds can be used as part of the etch bath. However, the concentration of the acids and the soluble silicon compound to be used is not disclosed; nor is there any suggestion of using the etch bath in applications other than integrated circuit manufacture.

While there have been improvements in the treatment and handling of asbestos-containing building materials in recent years, the search continues for still further improvements.

SUMMARY OF THE INVENTION

It is an object of the invention to provide an improved composition for digesting chrysotile asbestos to provide non-asbestos material.

It is another object of the invention to provide an improved composition and method for treating gypsum-containing cementitious building materials which contain chrysotile asbestos to transform the building materials to non-asbestos materials (i.e., materials which contain less than 1% chrysotile asbestos), while they are part of the building environment and supported on an underlying substrate.

Another object is to treat a building material which contains gypsum, chrysotile asbestos and, optionally, other fillers such as vermiculite, while part of a building structure, to transform the building material to a non-regulated material, without removing the building material from its underlying substrate and without
5 substantially impairing the physical integrity and heat insulating properties of the building material.

An additional object is to provide a composition which is capable of treating a chrysotile asbestos containing gypsum material while part of a building structure to transform the building material to a non-regulated material which
10 exhibits enhanced toughness while retaining its heat-insulating properties.

A still further object is to provide a treating composition which fulfills the objects stated above without generating hydrogen fluoride gas in excess of present OSHA limits during storage and use.

In accordance with the invention, these and other objects and advantages
15 are achieved by the present composition and method for transforming chrysotile asbestos material to non-asbestos material. The composition comprises a unique combination of water, a high concentration of phosphoric acid, and a catalytic amount of a fluoride ion source. The present composition is applied to the building materials in a manner which permits absorption of from about 8 to 20 parts by
20 weight of treating composition per part by weight of chrysotile asbestos in the material being treated.

DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS

The present invention is intended for the treatment of gypsum-containing cementitious materials which contain chrysotile asbestos fibers to transform the building materials to non-asbestos materials having enhanced toughness and, thereby, a desired product for retention as a building material. The present invention is especially useful for digesting chrysotile asbestos fibers contained in gypsum-based building materials that have been previously applied to the structural components, such as steel beams, decking and the like of buildings as coatings thereon to provide fire and heat resistance thereto. The process of the present invention provides an asbestos-free coating which retains its integrity and fire and heat resistance properties on the substrate. Finally, the present invention provides a preferred composition which can digest chrysotile asbestos fibers without generating noxious hydrogen fluoride under both storage and use conditions.

The present invention is directed to treating composition which is an aqueous solution or dispersion of a high concentration of phosphoric acid and a catalytic amount of a source of fluoride ions, as fully described hereinbelow.

The acid component of the present composition may comprise phosphoric acid as the sole acid. However, phosphoric acid may be used in combination with small amounts of up to about 20% by weight of the total acid content, of other inorganic acids, inorganic acid salts or mixtures thereof. In addition, small amounts (up to about 5%, preferably up to about 2%, by weight of the acid content) can be in the form of an organic acid.

The acid component is employed in the present compositions in high concentrations of at least about 30% by weight based on the weight of the treating compositions, up to the saturation point of the acid in the aqueous system. It is preferred that the acid component be present in from about 30% to about 45% by weight based on the total weight of the treating composition.

The present treating compositions must contain at least one source of fluoride ions, typically a fluorine-containing salt which is soluble in the aqueous treating compositions in the amounts described hereinbelow. Fluorine-containing salts which may be used in the present treating compositions include, for example, the fluorides, bifluorides, fluoroborates and fluorosilicates of ammonia, alkali metals and alkaline earth metals. Mixtures of such salts also may be used. The preferred fluorine-containing salts are hexafluorosilicates and tetrafluoroborates, more specifically, ammonium hexafluorosilicate, magnesium hexafluorosilicate, and sodium tetrafluoroborate.

It has unexpectedly been found that by employing a preferred composition of the present invention which contains high concentrations of phosphoric acid in combination with a catalytic amount of a hexafluorosilicate or tetrafluoroborate salt, the treating compositions of the present invention can be stored and used to transform chrysotile asbestos-containing building materials to non-asbestos materials while in place in a building environment without generating noxious hydrogen fluoride gas in amounts which are unacceptable for commercial application, as exemplified by OSHA standards. This represents a major

improvement over prior art asbestos treating compositions which rapidly generate large quantities of hydrogen fluoride gas when used, thus creating a dangerous work area.

The catalytic amount of the fluorine-containing salt in the present treating
5 compositions is very small relative to the concentration of the phosphoric acid. Concentrations of the fluorine-containing salt should be in the range of from about 0.1% to about 4% by weight based on the total weight of the treating composition, with concentrations of from about 0.5% to about 2% by weight being preferred.

It has been found that the present treating compositions, regardless of which
10 fluorine-containing salts employed, are particularly useful for treating building materials which contain gypsum in combination with chrysotile asbestos, since the use of the present composition results in the digestion of the chrysotile asbestos to provide a non-regulated material (i.e., a material containing less than 1% by weight asbestos) while permitting the gypsum building material to remain in place as part
15 of the building structure, retain its integrity and provide the heat insulating properties for which it was initially intended.

It has been unexpectedly found that the present treating composition can be readily used to transform chrysotile asbestos containing cementitious building materials into non-asbestos building material without degradation of the building
20 material. It has been further unexpectedly found that the present treating composition causes the resultant building material to exhibit heat insulating and

fireproofing properties as well as toughness which is equal to or greater than that of the initial untreated material.

It has been unexpectedly found that the present compositions, particularly those which employ a hexafluorosilicate or tetrafluoroborate salt as the source of fluoride ions, do not produce hydrogen fluoride in excessive amounts while in storage nor directly or indirectly cause generation of HF gas when in contact with chrysotile asbestos. For this reason, only a small, essentially catalytic amount of the source of fluoride ions needs to be used in the treating compositions.

The present treatment composition may be readily applied to chrysotile asbestos containing cementitious coatings in any manner so that from about 8 to 20 parts by weight, preferably 9 to 15 parts by weight, of the aqueous treating composition is applied per part by weight of the chrysotile asbestos in the material being treated. The amount to be applied will depend on the amount of chrysotile asbestos initially present in the material, the concentration of the acid in the treating composition and the thickness and absorptive capacity of the material being treated. The exact amount can be readily determined by small scale application and testing.

When further occupancy of the building or treated area is planned, the present treating composition, preferably, should further contain agents which will inhibit the corrosion of metallic substrate materials (e.g. steel beams, galvanized corrugated decking, steel pipes and the like) to which the material being treated is attached and/or in vicinity thereof. It has been found that certain specific materials

are useful as corrosion inhibiting agents for a broad spectrum of metals when part of the present acidic treating composition. These agents, and their incorporation in acidic treating compositions such as that described herein which digests chrysotile asbestos to provide non-asbestos material and the utilization to transform the asbestos-containing cementitious material to a non-regulated material are fully described in a concurrently filed, copending application, U.S. Serial Number 08/721,853, (Docket No. 9130), entitled CORROSION INHIBITING COMPOSITION FOR TREATING ASBESTOS-CONTAINING MATERIALS, the teachings of which are incorporated herein in its entirety by reference.

The method of the present invention transforms chrysotile asbestos-containing material into a material which contains very little, if any, chrysotile asbestos when measured, for example, by polarizing light microscopy, X-ray diffraction, or other conventional method. The resultant treated material contains less than one percent (1%), and normally less than one-half of one percent (0.5%) chrysotile asbestos in the overall structure of the resultant material. Thus, the material treated by the present composition results in a product which meets the U. S. governmental standards of a non-regulated asbestos-free material which may be safely handled by ordinary means. Further, it has been unexpectedly found that the present composition and method provides this transformation without causing a degradation of the cementitious material and, thereby, permits the material to remain in place and to continue to provide the functions of fire resistance, etc. for which it was initially installed.

The chrysotile asbestos contained in the cementitious material is substantially completely digested to a non-asbestos product while in place and part of the cementitious material. Typically, at least about eighty five percent, and preferably at least about ninety percent, of the chrysotile fibers are digested by the present composition and method to provide a non-regulated product without causing degradation of the cementitious material and, thereby, not requiring removal of the material nor detracting from the properties of the cementitious coating material.

All that is necessary to achieve the digestion of the chrysotile asbestos fibers in accordance with the present invention is to wet the material containing the chrysotile fibers with the treating composition, for example, by spraying or brushing the material with the treating composition. In the case of asbestos-containing building materials, such as fireproofing materials coated on girders, beams and floor support plates, this can be done by spraying the treating composition in the form of a solution, dispersion, gel or foam (e.g., a foam which is stable for at least about 1 minute, and preferably for at least about 60 minutes) directly onto the asbestos-containing material, preferably while it is in place in the building environment. It is unnecessary to disturb the asbestos-containing materials since the treating compositions typically will penetrate into the building materials and contact the asbestos fibers contained therein. In those cases where it is desirable to increase the rate of penetration of the treating composition into the building material, one or more wetting agents may be added to the treating

composition. For example, an anionic surfactant, such as linear alkyl sulfonates, sodium lauryl sulfates, polyalkoxy carboxylates, or a non-ionic surfactant, such as alcohol alkoxyates, alkyl phenol ethoxylates, polyoxyethylene esters and polyalkylene oxide block copolymers, can be added to the treating composition in conventional amounts, e.g., in amounts of up to about 5 % by weight based on the total weight of the composition, to increase the rate of penetration of the treating composition into the building material and the resultant wetting of the asbestos fibers. Excellent wetting has been achieved in most cases, however, with the treating composition alone, without additional wetting agents.

The present treating composition should be applied to the gypsum-containing cementitious building material in manners which permit a total application of from about 100 to 200% by weight, preferably from about 125 to about 175% by weight, of the subject composition based on the weight of the cementitious building material. The exact amount will depend on the concentration of the chrysotile asbestos contained in the building material being treated.

Because of the high concentration of phosphoric acid in the treating compositions of the invention and the catalytic presence of fluorine-containing salt, the desired asbestos transformation may be achieved by a single application of the treating composition on the building material while it is in place in the building environment. However, in some cases it may be necessary or desirable to

make successive applications, preferably without any intermediate drying step, until the desired degree of digestion of the chrysotile asbestos fibers is achieved.

The preferred manner of applying the subject treating composition to the material is by applying the composition in the form of a foam directly onto the major free surface(s) of the building material. As the material to be treated is in the form of a coating on a substrate building component, usually one major surface is exposed and free for application of the subject composition. Spraying of the aqueous treating composition may require successive applications, preferably without any intermediate drying step(s) between applications. Application of a foamed aqueous treating composition provides an extended contact time and a pseudo-encapsulation of the material being treated while the transformation is occurring. The formation of the foamed composition and its specific utilization in the instant method of transforming chrysotile asbestos-containing building materials to non-asbestos materials is fully described in concurrently filed, copending U.S. application Serial Number 08/721,857, (Docket No. 9166), entitled **FOAM COMPOSITION FOR TREATING ASBESTOS-CONTAINING MATERIALS AND METHOD OF USING SAME**, the text of which is incorporated herein in its entirety by reference.

It has been found that when a chrysotile asbestos-containing material is transformed in place in accordance with the present invention, the physical integrity and adherence of the resulting non-asbestos material to the underlying substrate are such that it may be left in place to perform the fireproofing or other

function for which the asbestos-containing material was originally installed. The resultant material subsequently may be treated by spraying or the like with a mild alkaline solution, such as sodium bicarbonate, calcium carbonate, sodium carbonate, magnesium hydroxide or the like in order to neutralize any remaining acid in the material.

The method of the invention, as applied to the abatement of asbestos in buildings, may typically include the step of removing any obstructions, such as interior partitions, ceilings and column covers, to expose the asbestos-containing material to be treated. This will enable the sampling and testing of the material to determine its composition and other relevant characteristics, thereby facilitating the selection of an optimum asbestos treatment composition and treatment procedure in accordance with the present invention. The treatment composition is then applied directly to the asbestos-containing material while in place in amounts described above to provide a non-regulated material. The resultant material may be further treated with a neutralizing agent.

One of the advantages of the invention is that it enables building materials to be treated in place without destroying their physical integrity and adherence to their substrate such that the materials may be left in place to perform their originally intended function after the asbestos has been transformed to non-asbestos material.

The following examples are intended to illustrate the invention without imposing limits on the scope of the invention, as defined by the claims appended hereto. All parts and percentages are by weight unless otherwise indicated.

5

EXAMPLE 1

Several phosphoric acid solutions were prepared by mixing concentrated (85%) phosphoric acid and water. To each solution a weighed quantity of ammonium bifluoride was added. These solutions were added to a simulated fireproofing material which contained 0.7 parts chrysotile asbestos, 1.5 parts vermiculite and 3.8 parts of gypsum. The weight ratio of solution to material was 1.5. The mixture was allowed to remain in contact with the simulated fireproofing material for three days in a closed plastic container. After three days, the mixture was filtered, washed with water, dried and analyzed for chrysotile asbestos by X-ray diffraction. The composition of the various solutions and the results of the analyses are shown in Table I.

15

TABLE 1

	<u>85% H₃PO₄ (parts)</u>	<u>NH₄HF₂ (parts)</u>	<u>H₂O (parts)</u>	<u>Residual Chrysotile (%)</u>
	5.0	0.1	4.0	0.15
	4.75	0.1	4.25	0.15
5	4.50	0.1	4.50	0.23
	4.25	0.1	4.75	0.15
	4.0	0.1	5.0	0.23
	3.75	0.1	5.25	0.23
	3.5	0.1	5.5	0.15
10	3.25	0.1	5.75	0.23

The results show that substantially complete transformation of chrysotile asbestos within the treated material was achieved to provide a material having less than about 0.2 percent by weight asbestos and, thus, produces a non-regulated material.

EXAMPLE 2

Five 5" x 5" fire-proofing test panels of the composition described in example 1 were prepared on galvanized steel backing. These panels were treated with a phosphoric acid conversion agent compositions composed of a solution made up in the proportions of 3.5 parts of 85% phosphoric acid, 0.15 parts of ammonium hexafluorosilicate and 5.5 parts of water. The weight ratio of

conversion agent to fire-proofing was 1.5:1. After allowing to remain undisturbed for four days, small core samples (~10g) were removed and analyzed for chrysotile asbestos by x-ray diffraction. The results showed that all samples contained less than 0.5% chrysotile. These panels were then fire-tested by a modified ASTM E-
5 119 procedure. All samples passed the test.

EXAMPLE 3

The procedure described in Example 1 was repeated except that ammonium hexafluorosilicate was used instead of ammonium bifluoride. The concentrations
10 used and the results obtained are summarized in the Table 3 below.

TABLE 3

<u>85% H₃PO₄(g)</u>	<u>(NH₄)₂SiF₆(g)</u>	<u>H₂O(g)</u>	<u>Residual</u> <u>Chrysotile(%)</u>
3.25	0.12	5.75	0.38
3.25	0.14	5.75	0.26
3.25	0.15	5.75	0.26
3.25	0.20	5.75	0.14
3.50	0.12	5.50	0.35
3.50	0.14	5.50	0.22
3.50	0.15	5.50	0.22
3.50	0.20	5.50	0.14

The results show that the resultant product can be obtained which is substantially free of asbestos. The resultant material is therefore a non-regulated material having less than 1% chrysotile asbestos.

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EXAMPLE 4

This example shows MgSiF_6 substituted for $(\text{NH}_4)_2\text{SiF}_6$. The procedure described in Example 3 was repeated with the exception that $\text{MgSiF}_6 \cdot 6\text{H}_2\text{O}$ was used as the fluoride source. The results are summarized in the table below.

10

TABLE 4

<u>85% $\text{H}_2\text{PO}_4(\text{g})$</u>	<u>$\text{MgSiF}_6 \cdot 6\text{H}_2\text{O}(\text{g})$</u>	<u>$\text{H}_2\text{O}(\text{g})$</u>	<u>Residual</u> <u>Chrysotile(%)</u>
3.25	0.20	5.75	0.49
3.25	0.26	5.75	0.38
3.50	0.20	5.50	0.50
3.50	0.26	5.50	0.28

The results show that the resultant product can be obtained which is substantially free of asbestos. The resultant material is therefore a non-regulated material having less than 1% chrysotile asbestos.

15

EXAMPLE 5

Fireproofing coatings were formed as 5' x 5' test panels by forming a coating composed of 3.8 parts gypsum, 1.5 parts vermiculite and 0.7 chrysotile asbestos onto a galvanized steel plate. Each panel was treated with an aqueous composition composed of a high concentration of an acid or acid salt component and a fluoride source in amounts and identity stated in Table 5 below. The compositions were applied to each panel in a weight ratio of 1.5 based on the weight of the coating. Prior to the testing, the coatings were allowed to remain in place for five days after application of the digestion compositions.

Each panel was tested to determine the amount of residual chrysotile asbestos, if any, contained in the fireproofing composition.

Each panel was tested for fireproofing properties according to a procedure of subjecting the panels to a gas flame using the temperature cycle of ASTM-E-119 and observing if the coating remained adhered to the metal substrate after a sixty minute test period.

TABLE 5

<u>Acid I.D./Conc. (%)</u>	<u>Fluoride I.D./Conc. (%)</u>	<u>Pass/Fail</u>
H ₃ PO ₄ (33)	(NH ₄) ₂ SiF ₆ (1.6)	3/0
H ₃ PO ₄ (31)	NH ₄ HF ₂ (1.1)	11/0
H ₃ PO ₄ (17) H ₂ SO ₄ (15)	NH ₄ HF ₂ (2)	2/0
NH ₄ HSO ₄ (50)	NH ₄ HF ₂ (1.2)	2/13
NH ₄ HSO ₄ (33)	NH ₄ HF ₂ (1.6)	0.2
NaHSO ₄ (54)	NH ₄ HF ₂ (2.3)	0.2
H ₃ PO ₄ (8) H ₂ SO ₄ (23)	NH ₄ HF ₂ (2)	3/5

Each of the test panels provided a non-regulated (less than 1% residual asbestos) coating material substantially free of asbestos. The panels treated with the high content phosphoric acid, in comparison to panels treated with other compositions, provided fireproofing which remained adherent to the substrate and which were a tough material capable of withstanding mechanical impact and the like.

**What is claimed is:**

1. A method of treating a chrysotile asbestos containing cementitious material installed on a substrate in a building, to provide a fireproofing asbestos-free building material thereon, comprising:

- 5 .
- (a) providing an admixture composition derived from admixing (i) water, (ii) at least about 30% by weight of phosphoric acid, and (iii) from about 0.1 to about 4% of a source of fluoride ions;
- 10 (b) applying said admixture composition to the chrysotile asbestos-containing building material;
- (c) permitting said admixture composition to penetrate the building material and contact the chrysotile asbestos contained therein;
- (d) allowing said composition to remain in contact with the chrysotile
- 15 asbestos containing building material for a sufficient period of time to reduce the amount of chrysotile asbestos contained therein to less than 1% by weight.

2. The method of Claim 1, wherein the cementitious material is a gypsum-containing cementitious building material in the form of a coating on a building component substrate.

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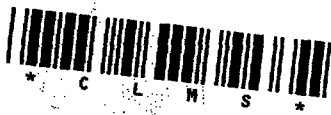
3. The method of Claim 2, wherein said composition is applied in the form of a foam.

4. The method of Claim 2, wherein said composition further contains a
5 metal corrosion inhibiting agent.

5. The method of Claim 2, wherein the acid is phosphoric acid present in a concentration of from about 30 to about 45 weight percent, and wherein the source of fluoride ions is a salt selected from the group consisting is a
10 hexafluorosilicate or tetrafluoroborate salt of an alkali metal, alkaline earth metal, or ammonia, or mixtures of said salts present in a concentration of from about 0.5 to about 2 percent by weight based on the total weight of said composition.

6. The method of Claim 5, wherein said composition further contains a
15 component capable of inhibiting corrosion of metals in contact therewith.

7. The method of Claim 1, 2, 3, 4, 5 or 6, wherein said composition is applied in an amount of from about 8 to about 20 parts by weight based on the weight of chrysotile asbestos contained in the building material being treated.



8. A composition capable of transforming an asbestos-containing material to a cementitious material containing less than 1% by weight of chrysotile asbestos, comprising a mixture of (a) water, (b) phosphoric acid, and (c) a source of fluoride ions; wherein the phosphoric acid is present in a concentration of from
5 at least about 30 weight percent of the composition and the source of fluoride ions is present in a concentration of from about 0.1 to about 4 weight percent of the composition.

9. A composition capable of transforming an asbestos-containing
10 material to a cementitious material containing less than 1% by weight of chrysotile asbestos having fireproofing properites derived from admixing (a) water, (b) phosphoric acid, and (c) a source of fluoride ions; wherein the phosphoric acid is present in a concentration of at least about 30 weight percent of the composition and the source of fluoride ions is present in a concentration of from about 0.1 to
15 about 4 weight percent of the composition.

10. The composition of Claim 8 or 9, wherein the source of fluoride ions is selected from an ammonium, alkali metal or alkaline earth metal hexafluorosilicate or tetrafluoroborate.

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11. The composition of Claim 8 or 9, wherein the acid is present in a concentration of from about 30 to about 45 weight percent of the composition.



12. The composition of Claim 10, wherein the acid is present in a concentration of from about 30 to about 45 weight percent of the composition.

5 13. The composition of Claim 8 or 9, wherein the source of fluoride ions is present in a concentration of from about 0.5 to about 2 weight percent based on the weight of the composition.

10 14. The composition of Claim 10, wherein the source of fluoride ions is present in a concentration of from about 0.5 to about 2 weight percent based on the weight of the composition.

15 15. The composition of Claim 8 or 9, wherein said phosphoric acid is present in a concentration of from about 30 to about 45 weight percent and the source of fluoride ions is an alkali metal alkaline earth metal or ammonium hexafluorosilicate or mixtures thereof present in a concentration of from about 0.5 to about 2 weight percent based on the weight of the composition.

20 16. The composition of Claim 10, wherein said fluoride source is selected from ammonium hexafluorosilicate, magnesium hexafluorosilicate or sodium tetrafluoroborate or mixtures thereof.



17. The composition of Claim 8 or 9, wherein said mixture further contains a component capable of causing said composition to be in the form of a foam which is stable for at least about 1 minute.

5 18. The composition of Claim 10, wherein said mixture further contains a component capable of inhibiting corrosion of metals in contact therewith.

19. The composition of Claim 10, wherein said mixture further contains a component capable of causing said composition to be in the form of a foam
10 which is stable for at least about 1 minute.

20. The composition of Claim 8 or 9, wherein said phosphoric acid is present in a concentration of from about 30 to about 45 weight percent and the source of fluoride ions is an alkali metal, alkaline earth metal, or ammonium
15 tetrafluorosilicate or mixtures thereof present in a concentration of from about 0.5 to about 2 weight percent based on the weight of the composition.