

Description

5 The invention relates to a power-supply circuit for charging a battery, comprising a primary winding of a transformer and a first semiconductor switch arranged in series between two input terminals for an input voltage, further comprising the series arrangement of a secondary winding of the transformer and a diode between connection terminals for connecting the battery, and also comprising first means for turning off the first semiconductor switch at a specific value of the current through the primary winding.

10 Such a circuit can be employed for charging a battery by input voltages of different values. The input voltage may be either a rectified alternating voltage or a direct voltage. Such a circuit is particularly suitable for use in an electric shaver in which the circuit is employed for charging the battery and/or energising the motor. The shaver can then operate on the different mains voltages in various countries without adaptation or change-over.

15 A power-supply circuit of the type defined in the opening paragraph is known, for example from European Patent Specification 30026 and from British Patent Application 2,138,977. In these known circuits a current flows in the primary winding during the so-called forward interval, as a result of which energy is stored in the transformer. At a specific value of the primary current the first semiconductor switch is turned off, thereby interrupting the primary current. The energy stored is then delivered to the battery in the form of a charging current via the secondary winding and the diode during the so-called flyback interval.

20 During the forward interval the primary current increases as a linear function of time, the slope being proportional to the input voltage. As a result of this, the value of the primary current for which the semiconductor switch is turned off is reached more rapidly as the input voltage increases. This leads to a higher switching frequency of the power-supply circuit, causing the average charging current to increase as the input voltage increases.

25 In order to keep the charging current as constant as possible over a wide range of input voltages the circuit known from said European Patent Specification 30026 compensates for this effect by feedforward control, the first semiconductor switch being turned off at a primary current which decreases as the input voltage increases.

30 In the circuit known from British Patent Application 2,138,977 the average charging current is maintained constant by means of negative feedback, which also results in turning-off at a primary current which decreases as the input voltage increases.

35 These known circuits are both high-speed charging devices by means of which a battery is charged with a comparatively large and constant charging current. However, in these known charging devices additional steps are required in order to enable a battery to be charged with a comparatively small charging current. In order to obtain a small charging current it is possible to reduce the value at which the primary current is turned off and consequently to reduce the length of the forward intervals, but this has the disadvantage that the charging current becomes strongly dependent on the turn-off delay of the first semiconductor switch. This turn-off delay is constant and results in the primary current overshooting the turn-off value increasingly as the input voltage increases, so that the charging current is likely to become much larger than the desired value.

40 Therefore, it is the object of the invention to provide a power-supply circuit is also suitable for delivering a comparatively small charging current. According to the invention a power-supply circuit of a type defined in the opening paragraph is characterized in that the circuit comprises second means for maintaining the average value over the time of the voltages sensed during the on-state intervals of the first semiconductor switch across the secondary winding substantially constant. As the average value of the secondary voltage is maintained constant during the forward intervals, the supply circuit constitutes a constant power source, the power supplied to the battery being constant and independent of the input voltage. By means of such a constant-power source a small charging current can be obtained in that instead of the primary current the secondary voltage during the forward intervals is used as the control criterion. The means for maintaining this voltage constant interrupt the operation of the circuit each time and consequently do not influence the length of the forward intervals, so that the effect of the turn-off delay is negligible.

45 The power supply circuit may be further characterized in that the second means comprise :

- 55 - an integrator having an output for integrating the voltage across the secondary winding in the on-state of the first semiconductor switch,
- a second semiconductor switch for turning off the first semiconductor switch, and
- 60 - a threshold circuit for turning on the second semiconductor switch above a first voltage on the output of the integrator and for turning off the second semiconductor switch below a second voltage on the output of the integrator. In such a case the threshold circuit may comprise a Schmitt trigger and/or the integrator may comprise the series arrangement of a first resistor and a capacitor, which series arrangement is coupled by a third semiconductor switch to that end of the secondary winding which is positive in the on-state of the first semiconductor switch. The third semiconductor switch may then comprise a transistor whose emitter is coupled to said positive end, whose base is coupled to the other end of the
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secondary winding by a second resistor, and whose collector is coupled to the first resistor. As an alternative the third semiconductor switch may comprise a diode.

The first means may comprise a third resistor which is arranged in series with the first semiconductor switch and which is coupled to a fourth semiconductor switch for turning off the first semiconductor switch. As a modification to this it may be advantageous if the second and the fourth semiconductor switch are replaced by one semiconductor switch.

Embodiments of the invention will now be described in more detail, by way of example, with reference to the accompanying drawings, in which

Figure 1 is a basic diagram of a power-supply circuit in accordance with the invention,

Figure 2 shows some characteristics to explain the operation of the circuit shown in Figure 1,

Figure 3 shows a first embodiment of the invention,

Figure 4 shows the waveform of the voltage on the output of the integrator in the circuit of Figure 3, and

Figure 5 shows a second embodiment of the invention.

Figure 1 is a basic diagram of a power-supply circuit in accordance with the invention. The circuit comprises two input terminals 1 and 2 for an input voltage, which may be a rectified alternating voltage or a direct voltage. A primary winding n_1 of a transformer T_1 , the collector-emitter path of a transistor T_1 which constitutes the first semiconductor switch S_1 and a resistor R_1 are arranged in series between these terminals 1 and 2. This resistor R_1 is connected to the base of a transistor T_4 constituting the fourth semiconductor switch S_4 . The resistor R_1 together with the semiconductor switch S_4 constitutes the first means 3 for turning off the first semiconductor switch S_1 depending on the value of the primary current. The circuit further comprises the series arrangement of a secondary winding n_2 and a diode D_1 with terminals 4 and 5 between which a battery 6 is connected. In the present example this battery 6 comprises two series-connected nickel-cadmium cells 7 and 8. The end 9 of the secondary winding n_2 is connected to the base of the transistor T_1 by a positive-feedback network comprising the series arrangement of a resistor R_2 and a capacitor C_1 . Further, the base of the transistor T_1 is connected to the input terminal 1 via a starting resistor R_3 .

The circuit further comprises second means 10 for turning off the first semiconductor switch S_1 depending on the average voltage across the secondary winding n_2 during the forward intervals. These means 10 comprise an integrator 11, which is connected to the end 9 of the secondary winding n_2 by means of the collector-emitter path of a transistor T_3 constituting the third semiconductor switch S_3 . The base of this transistor T_3 is connected to the other end 4 of the winding n_2 by a resistor R_4 . The output of the integrator 11 is connected to the input of a threshold circuit 12, which comprises for example a Schmitt trigger. Above a first threshold voltage this threshold circuit 12 turns on a transistor T_2 constituting the second semiconductor switch S_2 , so that the first semiconductor switch S_1 is turned off. Below a second threshold voltage the transistor T_2 is cut off, enabling the first semiconductor switch S_1 to be turned on again.

The circuit operates as follows. If an input voltage is present on the terminals 1 and 2 a small current flows into the base of the transistor T_1 via the starting resistor R_3 , so that this transistor is partly driven into conduction. The resulting current through the primary winding n_1 causes the voltage across the secondary winding n_2 to increase so that the transistor T_1 is driven further into conduction via the positive-feedback network comprising the resistor R_2 and the capacitor C_1 . This positive feedback ensures that the transistor T_1 is rapidly bottomed. The current through the primary winding n_1 subsequently increases as a linear function of time during the forward interval. For a value of the primary current which is defined by the resistance value of the resistor R_1 the transistor T_4 is turned on, so that the transistor T_1 is cut off. Owing to the absence of the primary current the polarity of the voltage across the secondary winding n_2 is reversed, so that the diode D_1 is turned on. The energy stored in the transformer T_1 during the forward interval is then supplied to the battery 6 in the form of a charging current in the flyback interval. This current decreases to zero as a linear function of time. During the flyback interval the voltage on the end 9 of the secondary winding is dictated by the voltage across the diode D_1 . At the end of the flyback interval the voltage across the winding n_2 becomes zero volts, so that the voltage on the end 9 becomes equal to the battery voltage. This positive voltage step on the end 9 ensures that the next forward interval is started, unless this is inhibited by the means 10 whose operation will now be described in more detail.

The voltage across the secondary winding n_2 is constant during the forward intervals and is governed by the input voltage and the winding ratio of the transformer T_1 . The voltage on the end 9 is then positive relative to the voltage on the end 4, so that the transistor T_3 conducts during the forward intervals. The voltage pulses appearing across the secondary winding during the forward intervals are therefore applied to the integrator 11, which integrates these voltage pulses. Consequently, a voltage will appear on the output of the integrator 11 which is substantially proportional to the output average value of the voltage across the secondary winding n_2 over the preceding forward intervals. If after a

number of forward intervals this voltage exceeds the first threshold value of the threshold circuit 12 the transistor T₂ is turned on and consequently the transistor T₁ is turned off. The transistor T₁ remains cut off until the voltage on the output of the integrator 11 decreases below the second threshold value of the threshold circuit 12 owing to the absence of charging pulses. The transistor T₂ is then turned off, so that the transistor T₁ is enabled for a new forward interval. In this way the operation of the circuit is interrupted for a number of intervals each time that the first threshold value of the threshold circuit is exceeded. As the input voltage increases the voltage across the secondary winding n₂ increases during the forward intervals. Moreover, as the input voltage increases the frequency of the forward intervals also increases because at an increasing input voltage the primary current rises more rapidly and consequently the value at which the primary current is turned off is reached more rapidly. Therefore, the time covered by the number of forward intervals required for reaching the first threshold value of the threshold circuit 12 decreases as the input voltage increases, so that at increasing input voltage the operation of the circuit is always interrupted after shorter periods.

Thus, in the manner described above the maximum value of the primary current during the forward intervals in the circuit in accordance with the invention is maintained constant and independent of the input voltage, and the average value of the voltage across the secondary winding during the forward intervals is also maintained substantially constant and independent of the input voltage. By maintaining these two parameters constant the power-supply to the battery is maintained constant and independent of the input voltage. This is not the case in the known circuits which constitute a constant-current source, in which the average charging current is maintained constant and independent of the input voltage. However, in accordance with the inventive idea the average charging current need not be constant but should be inversely proportional to the battery voltage, i.e. the charging current is comparatively large when the battery is almost exhausted and comparatively small when the battery is almost full. For such a dependence of the charging current the circuit constitutes a constant-power source. By means of Figure 2 it will be explained that a constant-power source can be obtained by maintaining the maximum primary current and said average secondary voltage substantially constant.

The power P_u supplied to the battery is substantially equal to the power built up during the forward intervals, i.e.:

$$P_u = \frac{1}{2} L_{\text{prim}} \cdot \hat{I}_{\text{prim}}^2 \cdot f \cdot \eta \quad (1)$$

or $P_u = \hat{I}_{\text{prim}}^2 \cdot f$

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where

L_{prim} = the inductance of the primary winding

$\hat{I}_{\text{prim}}$ = the maximum value of the primary current,

f = the frequency of the forward intervals and

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η = the efficiency of the circuit.

In Figure 2a the variation of the current through the primary winding I_{prim} is plotted as a function of time for a specific input voltage V_i, this variation being represented in broken lines for a higher input voltage V_i. The switching means 3 (see Figure 1) switch off the primary current I_{prim} independently of the input voltage at the same maximum value $\hat{I}_{\text{prim}}$. The time within which this value is reached is given by:

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$$t_1 = \frac{L_{\text{prim}}}{V_{\text{in}}} \cdot \hat{I}_{\text{prim}} \quad (2)$$

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It follows that as the input voltage V_i increases this time decreases, or the frequency of the forward intervals increases.

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In Figure 2b the variation of the voltage V_{sec} across the secondary winding is plotted as function of time. The value of this voltage during the forward intervals for a given transformation ratio is proportional to the input voltage V_i. From equation (2) it therefore follows that the area of the voltage pulses during the forward intervals is proportional to the maximum value of the primary current $\hat{I}_{\text{prim}}$ and is independent of the input voltage V_i. The average value V_{gem} of the voltage across the secondary winding during the forward intervals then complies with:

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$$V_{\text{gem}} = \hat{I}_{\text{prim}} \cdot f \quad (3)$$

From expressions (1) and (3) it then follows that the output power is:

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$$P_u = V_{\text{gem}} \cdot \hat{I}_{\text{prim}} \quad (4)$$

This shows that a constant output power is obtained by maintaining the maximum value of the primary current and the average value of the voltage across the secondary winding constant during the forward intervals.

Figure 3 shows a first embodiment of the invention. Identical parts bear the same reference numerals as in Figure 1. An alternating voltage is applied to a rectifier bridge 22 via two terminals 20 and 21. The rectified voltage is smoothed by means of a filter 23 comprising two capacitors C_2 and C_3 and a coil L_1 . A Zener diode Z_1 in series with a diode D_2 is arranged in parallel with the primary winding n_1 in order to prevent switching transients when the current through the primary is turned off. In the present embodiment the first means 3 for turning off the transistor T_1 depending on the value of the primary current comprise a current-sensing resistor R_1 across which the series arrangement of a Zener diode Z_2 and a resistor R_{12} is connected, the base-emitter junction of a transistor T_4 being connected in parallel with this resistor R_{12} . The Zener diode Z_2 accurately defines the voltage at which the transistor T_4 is turned and consequently the value at which the primary current is switched off.

The base of the transistor T_3 is connected to the end 4 of the secondary winding n_2 by means of the series arrangement of a light-emitting diode D_3 and a resistor R_4 . The diode D_3 blinks at the rate at which the transistor T_3 is turned on. However, as a result of the high blinking rate, this diode appears to be lit continuously the human eye. In this way the diode D_3 provides an indication that the battery 6 is being charged. The resistor R_4 is a current-limiting resistor.

The integrator 11 comprises the series arrangement of a capacitor C_4 and a resistor R_{14} which is connected to the collector of the transistor T_3 . The resistor R_{14} determines the magnitude of the current pulses which correspond to the voltage appearing across the secondary winding during the forward intervals. A resistor R_{15} connects the output 15 of the integrator 11 to the input of the threshold circuit 2, which in the present embodiment comprises a Schmitt trigger. This Schmitt trigger comprises a transistor T_5 whose collector is connected to the positive pole 4 of the battery 6 via a resistor R_{16} and to the base of a transistor T_6 via a resistor R_{17} , which transistor T_6 has its emitter also connected to the pole 4 of the battery 6. A large capacitor C_5 is arranged across the battery 6 to protect the circuit in the case of an open-circuited battery. A resistor R_{18} provides feedback from the collector of the transistor T_6 , which constitutes the output of the threshold circuit 12, to the base of the transistor T_5 . By means of a voltage divider comprising the resistors R_{19} and R_{20} the collector of the transistor T_6 is connected to the base of a transistor T_2 , whose collector is connected to the base of the transistor T_1 .

The operation of the Schmitt trigger 12 is assumed to be well-known and will not be explained any further. As a result of the integration of the current pulses which are proportional to the secondary voltage the voltage on the output 15 of the integrator 11 increases gradually. If this voltage exceeds the first threshold value V_1 the voltage on the collector of the transistor T_6 changes from a low to a high value, so that the transistor T_2 is turned on and consequently the transistor T_1 is turned off. When the capacitor C_4 is discharged via the resistors R_{15} , R_{21} and R_{22} the voltage on the output 15 decreases gradually. If this voltage has decreased below the second threshold value V_2 the voltage on the collector of the transistor T_6 again changes from a high value to a low value, so that the transistor T_2 is turned off and the transistor T_1 can be turned on again. Figure 4 shows the voltage waveform on the output 15 of the integrator 11. The average value of the voltage on this output 15 is substantially constant, so that the average value of the voltage appearing across the secondary winding during the forward intervals is also constant.

By means of a switch S_5 a motor M can be connected in parallel with the battery 6. This motor M is, for example, the motor of an electric shaver. In the emitter line of the transistor T_3 a switch S_6 is arranged which is opened at the same time that the switch S_5 is closed. The series arrangement of a Zener diode Z_3 and the resistor R_{21} is connected in parallel with the motor M . The anode of the Zener diode Z_3 is connected to the input of the threshold circuit 12 via the resistor R_{22} . In the closed positions of the switches S_5 the circuit supplies the full motor current. The Zener diode Z_3 then limits the voltage across the motor M and consequently that across the battery 6. If this voltage becomes too high the Zener diode Z_3 breaks down, so that the transistor T_2 is turned on via the threshold circuit 12, as a result of which the transistor T_1 is cut off. In the absence of an input voltage on the terminals 20 and 21 the motor M is energised by the battery when the switch S_5 is closed.

Figure 5 shows a power-supply circuit constituting a second embodiment of the invention, identical parts bearing the same reference numerals as in Figure 3. The circuit differs from the circuit shown in Figure 3 in that the transistor T_2 and the transistor T_4 are replaced by a single transistor T_4 . The output of the threshold circuit 12 is connected to the tapping of a voltage divider which comprises the resistors R_{12} and R_{20} and which is arranged in parallel with the base-emitter junction of the transistor T_4 . Another difference with respect to the circuit of Figure 3 is that the light-emitting diode D_3 , which indicates that the battery 6 is being charged is not arranged in the base line of the transistor T_3 but is arranged in series with a resistor R_{23} across the output of the threshold circuit. In the present circuit the resistor R_4 may be replaced by an open circuit and the third semiconductor switch S_3 may be constituted by a diode or a diode-connected transistor in which last-mentioned case the base of the transistor T_3 is connected directly to the collector. Otherwise, the circuit operates in the same way as that shown in Figure 3.

The invention is not limited to the present embodiments. Instead of single transistors the transistor switches S_1 to S_4 may comprise compound transistors or a combination of one or more transistors with

other elements. Instead of by a Schmitt trigger the threshold circuit may be constituted by any other circuit having two different threshold voltages. Further, the integrator 11 may be constructed in another manner than shown.

5. Claims

1. A power-supply circuit for charging a battery (6), comprising a primary winding (n_1) of a transformer (T_1) and a first semiconductor switch (S_1) arranged in series between two input terminals (1, 2) for an input voltage, further comprising the series arrangement of a secondary winding (n_2) of the transformer and a diode (D_1) between connection terminals for connecting the battery, and also comprising first means (3) for turning off the first semiconductor switch (S_1) at a specific value of the current through the primary winding (n_1), characterized in that the circuit comprises second means (10) for maintaining the average value over the time of the voltage sensed during the on-state intervals of the first semiconductor switch across the secondary winding substantially constant.
2. A power-supply circuit as claimed in Claim 1, characterized in that the second means (10) comprise:
 - an integrator (11) having an output for integrating the voltage across the secondary winding (n_2) in the on-state of the first semiconductor switch (S_1),
 - a second semiconductor switch (S_2) for turning off the first semiconductor switch, and
 - a threshold circuit (12) for turning on the second semiconductor switch (S_2) above a first voltage on the output of the integrator and for turning off the second semiconductor switch below a second voltage on the output of the integrator.
3. A power-supply circuit as claimed in Claim 2, characterized in that the threshold circuit (12) comprises a Schmitt trigger.
4. A power-supply circuit as claimed in Claim 2 or 3, characterized in that the integrator (11) comprises the series arrangement of a first resistor (R_{14}) and a capacitor (C_4), which series arrangement is coupled by a third semiconductor switch (S_3) to that end (9) of the secondary winding which is positive in the on-state of the first semiconductor switch (S_1).
5. A power-supply circuit as claimed in Claim 4, characterized in that the third semiconductor switch (S_3) comprises a transistor (T_3) whose emitter is connected to said positive end (9), whose base is connected to the other end (4) of the secondary winding by a second resistor (R_4), and whose collector is coupled to the first resistor (R_{14}).
6. A power-supply circuit as claimed in Claim 5, characterized in that a light emitting diode (D_3) is arranged in the base line of the transistor (T_3).
7. A power supply circuit as claimed in Claim 4, characterized in that the third semiconductor switch (T_3) comprises a diode whose anode is coupled to the end (9) of the secondary winding which is positive in the on-state of the first semiconductor switch (S_1).
8. A power-supply circuit as claimed in Claim 2 or 3, characterized in that an output of the threshold circuit (12) is connected to a point (5) of fixed potential by a light-emitting diode (D_3).
9. A power-supply circuit as claimed in any one of the preceding Claims, characterized in that the first switching means (3) comprise a resistor (R_1) which is arranged in series with the first semiconductor switch (S_1) and which is coupled to a further semiconductor switch (S_4) for turning off the first semiconductor switch (S_1).
10. A power-supply circuit as claimed in Claim 9 when appendent to Claim 2, characterized in that the second semiconductor (S_2) switch and further semiconductor switch (S_4) are replaced by one semiconductor switch (S_4).
11. A power-supply circuit as claimed in any one of the preceding Claims 2 to 10, characterized in that the circuit comprises a switch (S_5) for connecting a motor (8) in parallel with the battery (6) and a switch (S_6) for simultaneously disconnecting the integrator (11) from the secondary winding (n_2).
12. A power-supply circuit as claimed in Claim 11, characterized in that the motor (8) is connected to an input of the threshold circuit by a zener diode (Z_3).
13. A shaving apparatus characterized in that it is provided with a power-supply circuit as claimed in any one of the preceding Claims.

55 Patentansprüche

1. Stromversorgungsschaltung zum Aufladen einer Batterie (6), mit einer Primärwicklung (n_1) eines Transformators (T_1) und einer ersten Halbleiterschaltung (S_1) in Reihenschaltung zwischen zwei Eingangsklemmen (1, 2) für eine Eingangsspannung, außerdem mit der Reihenschaltung aus einer Sekundärwicklung (n_2) des Transformators und einer Diode (D_1) zwischen Verbindungsklemmen zum Anschließen der Batterie, und weiter noch mit einem ersten Mittel (3) zum Abschalten des ersten Halbleiterschalters (S_1) beim Erreichen eines spezifischen Werts des Stroms durch die Primärwicklung (n_1), dadurch gekennzeichnet, daß die Schaltung ein zweites Mittel (10) zum in der Zeit im wesentlichen Konstanthalten des Mittelwerts der in den Leitzustandsintervallen des ersten Halbleiterschalters detektierten Spannung an der Sekundärwicklung enthält.

other elements. Instead of by a Schmitt trigger the threshold circuit may be constituted by any other circuit having two different threshold voltages. Further, the integrator 11 may be constructed in another manner than shown.

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Claims

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1. A power-supply circuit for charging a battery (6), comprising a primary winding (n_1) of a transformer (T_1) and a first semiconductor switch (S_1) arranged in series between two input terminals (1, 2) for an input voltage, further comprising the series arrangement of a secondary winding (n_2) of the transformer and a diode (D_1) between connection terminals for connecting the battery, and also comprising first means (3) for turning off the first semiconductor switch (S_1) at a specific value of the current through the primary winding (n_1), characterized in that the circuit comprises second means (10) for maintaining the average value over the time of the voltage sensed during the on-state intervals of the first semiconductor switch across the secondary winding substantially constant.

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2. A power-supply circuit as claimed in Claim 1, characterized in that the second means (10) comprise:
 - an integrator (11) having an output for integrating the voltage across the secondary winding (n_2) in the on-state of the first semiconductor switch (S_1),
 - a second semiconductor switch (S_2) for turning off the first semiconductor switch, and
 - a threshold circuit (12) for turning on the second semiconductor switch (S_2) above a first voltage on the output of the integrator and for turning off the second semiconductor switch below a second voltage on the output of the integrator.

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3. A power-supply circuit as claimed in Claim 2, characterized in that the threshold circuit (12) comprises a Schmitt trigger.

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4. A power-supply circuit as claimed in Claim 2 or 3, characterized in that the integrator (11) comprises the series arrangement of a first resistor (R_{14}) and a capacitor (C_4), which series arrangement is coupled by a third semiconductor switch (S_3) to that end (9) of the secondary winding which is positive in the on-state of the first semiconductor switch (S_1).

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5. A power-supply circuit as claimed in Claim 4, characterized in that the third semiconductor switch (S_3) comprises a transistor (T_3) whose emitter is connected to said positive end (9), whose base is connected to the other end (4) of the secondary winding by a second resistor (R_4), and whose collector is coupled to the first resistor (R_{14}).

6. A power-supply circuit as claimed in Claim 5, characterized in that a light emitting diode (D_3) is arranged in the base line of the transistor (T_3).

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7. A power supply circuit as claimed in Claim 4, characterized in that the third semiconductor switch (T_3) comprises a diode whose anode is coupled to the end (9) of the secondary winding which is positive in the on-state of the first semiconductor switch (S_1).

8. A power-supply circuit as claimed in Claim 2 or 3, characterized in that an output of the threshold circuit (12) is connected to a point (5) of fixed potential by a light-emitting diode (D_3).

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9. A power-supply circuit as claimed in any one of the preceding Claims, characterized in that the first switching means (3) comprise a resistor (R_1) which is arranged in series with the first semiconductor switch (S_1) and which is coupled to a further semiconductor switch (S_4) for turning off the first semiconductor switch (S_1).

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10. A power-supply circuit as claimed in Claim 9 when appendent to Claim 2, characterized in that the second semiconductor (S_2) switch and further semiconductor switch (S_4) are replaced by one semiconductor switch (S_4).

11. A power-supply circuit as claimed in any one of the preceding Claims 2 to 10, characterized in that the circuit comprises a switch (S_5) for connecting a motor (8) in parallel with the battery (6) and a switch (S_6) for simultaneously disconnecting the integrator (11) from the secondary winding (n_2).

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12. A power-supply circuit as claimed in Claim 11, characterized in that the motor (8) is connected to an input of the threshold circuit by a zener diode (Z_3).

13. A shaving apparatus characterized in that it is provided with a power-supply circuit as claimed in any one of the preceding Claims.

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Patentansprüche

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1. Stromversorgungsschaltung zum Aufladen einer Batterie (6), mit einer Primärwicklung (n_1) eines Transformators (T_1) und einer ersten Halbleiterschaltung (S_1) in Reihenschaltung zwischen zwei Eingangsklemmen (1, 2) für eine Eingangsspannung, außerdem mit der Reihenschaltung aus einer Sekundärwicklung (n_2) des Transformators und einer Diode (D_1) zwischen Verbindungsklemmen zum Anschließen der Batterie, und weiter noch mit einem ersten Mittel (3) zum Abschalten des ersten Halbleiterschalters (S_1) beim Erreichen eines spezifischen Werts des Stroms durch die Primärwicklung (n_1), dadurch gekennzeichnet, daß die Schaltung ein zweites Mittel (10) zum in der Zeit im wesentlichen Konstanthalten des Mittelwerts der in den Leitzustandsintervallen des ersten Halbleiterschalters detektierten Spannung an der Sekundärwicklung enthält.

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2. Stromversorgungsschaltung nach Anspruch 1, dadurch gekennzeichnet, daß das zweite Mittel (10) folgende Elemente enthält:

- einen Integrator (11) mit einem Ausgang zum Integrieren der Spannung an der Sekundärwicklung (n_2) im leitenden Zustand des ersten Halbleiterschalters (S_1),
- einen zweiten Halbleiterschalter (S_2) zum Abschalten des ersten Halbleiterschalters, und
- eine Schwellenschaltung (12) zum Einschalten des zweiten Halbleiterschalters (S_2) über einer ersten Spannung am Integratorausgang und zum Abschalten des zweiten Halbleiterschalters unter einer zweiten Spannung am Integratorausgang.

3. Stromversorgungsschaltung nach Anspruch 2, dadurch gekennzeichnet, daß die Schwellenschaltung (12) einen Schmitt-Trigger enthält.

4. Stromversorgungsschaltung nach Anspruch 2 oder 3, dadurch gekennzeichnet, daß der Integrator (11) die Reihenschaltung aus einem ersten Widerstand (R_{14}) und einem Kondensator (C_4) enthält, die über einen dritten Halbleiterschalter (S_3) mit jenem Ende (9) der Sekundärwicklung gekoppelt ist, das im leitenden Zustand des ersten Halbleiterschalters (S_1) positiv ist.

5. Stromversorgungsschaltung nach Anspruch 4, dadurch gekennzeichnet, daß der dritte Halbleiterschalter (S_3) einen Transistor (T_3) enthält, dessen Emittor mit dem positiven Ende (9), dessen Basis über einen zweiten Widerstand (R_4) mit dem anderen Ende (4) der Sekundärwicklung und dessen Kollektor mit dem ersten Widerstand (R_{14}) verbunden sind.

6. Stromversorgungsschaltung nach Anspruch 5, dadurch gekennzeichnet, daß eine lichtemittierende Diode (D_3) in der Basisleitung des Transistors (T_3) angeordnet ist.

7. Stromversorgungsschaltung nach Anspruch 4, dadurch gekennzeichnet, daß der dritte Halbleiterschalter (S_3) eine Diode enthält, deren Anode mit jenem Ende (9) der Sekundärwicklung gekoppelt ist, das im leitenden Zustand des ersten Halbleiterschalters (S_1) positiv ist.

8. Stromversorgungsschaltung nach Anspruch 2 oder 3, dadurch gekennzeichnet, daß ein Ausgang der Schwellenschaltung (12) über eine lichtemittierende Diode (D_3) an einen Punkt (5) mit festem Potential angeschlossen ist.

9. Stromversorgungsschaltung nach einem oder mehreren der vorangehenden Ansprüche, dadurch gekennzeichnet, daß das erste Schaltmittel (3) einen Widerstand (R_1) enthält, der mit dem ersten Halbleiterschalter (S_1) in Reihe geschaltet und mit einem weiteren Halbleiterschalter (S_4) zum Abschalten des ersten Halbleiterschalters (S_1) gekoppelt ist.

10. Stromversorgungsschaltung nach Anspruch 9, wenn abhängig vom Anspruch 2, dadurch gekennzeichnet, daß der zweite Halbleiterschalter (S_2) und der weitere Halbleiterschalter (S_4) durch einen einzigen Halbleiterschalter (S_4) ersetzt werden.

11. Stromversorgungsschaltung nach einem oder mehreren der Ansprüche 2 bis 10, dadurch gekennzeichnet, daß die Schaltung einen Schalter (S_5) zum Parallelschalten eines Motors (8) mit der Batterie (6) sowie einen Schalter (S_6) zum gleichzeitigen Abschalten des Integrators (11) bei der Sekundärwicklung (n_2) enthält.

12. Stromversorgungsschaltung nach Anspruch 11, dadurch gekennzeichnet, daß der Motor (8) über eine Zenerdiode (Z_3) an einen Eingang der Schwellenschaltung angeschlossen ist.

13. Rasierer, dadurch gekennzeichnet, daß er mit einer Stromversorgungsschaltung nach einem oder mehreren der vorangehenden Ansprüche ausgerüstet ist.

Revendications

1. Circuit d'alimentation pour charger une batterie (6), comportant un enroulement primaire (n_1) d'un transformateur (T_1) et un premier commutateur semiconducteur (S_1) disposé en série entre deux bornes d'entrée (1, 2) pour une tension d'entrée, circuit comportant en outre le montage série d'un enroulement secondaire (n_2) du transformateur et d'une diode (D_1) entre des bornes de raccordement pour raccorder la batterie ainsi que de premiers moyens (3) pour bloquer le premier commutateur semiconducteur (S_1) à une valeur déterminée du courant traversant l'enroulement primaire (n_1), caractérisé en ce qu'il comporte de seconds moyens (10) pour maintenir sensiblement constante la valeur moyenne dans le temps des tensions aux extrémités de l'enroulement secondaire, mesurées au cours des intervalles conductibles du premier commutateur semiconducteur.

2. Circuit d'alimentation selon la revendication 1, caractérisé en ce que les seconds moyens (10) comportent:

- un intégrateur (11) présentant une sortie pour intégrer la tension aux extrémités de l'enroulement secondaire (n_2) dans l'état conductible du premier commutateur semiconducteur (S_1),
- un deuxième commutateur semiconducteur (S_2) pour bloquer le premier commutateur semiconducteur et
- un circuit à seuil (12) pour rendre conducteur le deuxième commutateur semiconducteur (S_2) au-dessus d'une première tension sur la sortie de l'intégrateur et pour bloquer le deuxième commutateur semiconducteur au-dessous d'une seconde tension sur la sortie de l'intégrateur.

3. Circuit d'alimentation selon la revendication 2, caractérisé en ce que le circuit à seuil (12) comporte un déclencheur de Schmitt.



4. Circuit d'alimentation selon la revendication 2 ou 3, caractérisé en ce que l'intégrateur (11) comporte le montage série d'une première résistance (R_{14}) et d'un condensateur (C_4), montage série qui, par un troisième commutateur semiconducteur (S_3), est couplé à l'extrémité (9) de l'enroulement secondaire qui est positive dans l'état conductible du premier commutateur semiconducteur (S_1).
- 5 5. Circuit d'alimentation selon la revendication 4, caractérisé en ce que le troisième commutateur semiconducteur (S_3) comporte un transistor (T_3) dont l'émetteur est couplé à ladite extrémité positive (9), dont la base est couplée par une deuxième résistance (R_4) à l'autre extrémité (4) de l'enroulement secondaire et dont le collecteur est couplé à la première résistance (R_{14}).
- 10 6. Circuit d'alimentation selon la revendication 5, caractérisé en ce qu'une diode électroluminescente (D_3) est disposée dans la ligne de base du transistor (T_3).
7. Circuit d'alimentation selon la revendication 4, caractérisé en ce que le troisième commutateur semiconducteur (T_3) comporte une diode dont l'anode est couplée à l'extrémité (9) de l'enroulement secondaire qui est positive à l'état conductible du premier commutateur semiconducteur (S_1).
- 15 8. Circuit d'alimentation selon la revendication 2 ou 3, caractérisé en ce qu'une sortie du circuit à seuil (12) est reliée à un point (5) à potentiel fixe par l'intermédiaire d'une diode électroluminescente (D_3).
9. Circuit d'alimentation selon l'une quelconque des revendications précédentes, caractérisé en ce que les premiers moyens de commutation (3) comportent une résistance (R_1) disposée en série avec le premier commutateur semiconducteur (S_1) et couplée à un autre commutateur semiconducteur (S_4) pour bloquer le premier commutateur semiconducteur (S_1).
- 20 10. Circuit d'alimentation selon la revendication 9, en tant que dépendante de la revendication 2, caractérisé en ce que le deuxième commutateur semiconducteur (S_2) et l'autre commutateur semiconducteur (S_4) sont remplacés par un seul commutateur (S_4).
11. Circuit d'alimentation selon l'une quelconque des revendications 2 à 10, caractérisé en ce qu'il comporte, d'une part, un commutateur (S_5) pour connecter un moteur (8) en parallèle avec la batterie (6) et, d'autre part, un commutateur (S_6) pour supprimer simultanément la connexion de l'intégrateur à l'enroulement secondaire (n_2).
- 25 12. Circuit d'alimentation selon la revendication 11, caractérisé en ce que le moteur (8) est relié à une entrée du circuit à seuil par l'intermédiaire d'une diode Zener (Z_3).
13. Rasoir électrique caractérisé en ce qu'il est muni d'un circuit d'alimentation selon l'une quelconque des revendications précédentes.
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