

AUSTENITIC STAINLESS STEEL
EXCELLENT IN FINE BLANKABILITY

BACKGROUND OF THE INVENTION

5 The present invention relates to an austenitic stainless steel excellent in blankability, especially fine blankability.

 Shear process, especially blanking, with a press has been applied to various kinds of metal sheets such as common steel, stainless steel and
10 nonferrous metal, since the metal sheets can be efficiently sized to an objective shape. However, a plane formed by blanking is rugged with poor dimensional accuracy, a metal sheet is likely to be drooped at its broader surface, and thickness of the metal sheet is reduced at a part near the blanking plane.

15 When blanking is adopted to a process for manufacturing a product which needs high dimensional accuracy, a blanking plane is ground by post-treatment such as barrel finishing. Such post-treatment is basically extra process and causes poor productivity. In this regard, a fine blanking method has been adopted for manufacturing a product with high
20 dimensional accuracy. In the fine blanking method, clearance is determined at a very small value to suppress formation of a fracture plane, and inflow of metal is suppressed to reduce generation of drooping during blanking.

 On the other hand, stainless steel has been used so far for use exposed to a corrosive or high-temperature atmosphere. Especially, SUS304
25 is representative stainless steel suitable for such use.

 SUS 304 austenitic stainless steel is hard material, so a life of fine blanking dies is shortened. Hardness of SUS 304 austenitic stainless steel also causes increase of a ratio of a fracture plane, which degrades quality of a blanking plane, as well as increase of drooping. Even if a shear plane is

formed with high dimensional accuracy by blanking, a working cost is higher compared with a cost for blanking common steel. Accounting these disadvantages, SUS 304 austenitic stainless steel is blanked by a usual method and then ground for manufacturing a product which shall have a 5 blanking plane with high dimensional accuracy.

SUMMARY OF THE INVENTION

The present invention aims at provision of an austenitic stainless steel, in which softening and stability of an austenite phase are controlled so as to increase a ratio of a shear plane, especially suitable for fine blanking.

In accordance with an aspect of the invention, there is provided a austenitic stainless steel, which has an excellent property in fine blankability consisting of (C+1/2N) up to 0.060 mass %, Si up to 1.0 mass %, Mn up to 5 mass %, S up to 0.006 mass %, 15-20 mass % Cr, 5-12 mass % Ni, Cu up to 5 mass %, optional Mo up to 3.0 mass % and the balance being essentially Fe except inevitable impurities, under the condition that a value Md_{30} which represents a ratio of a strain-induced martensite phase, defined by the under-mentioned formula is adjusted within a range of -60 to -10, which has metallurgical structure minimized to #8 to #10 by grain size number.

$$Md_{30} = 551 - 462(C+N) - 9.2Si - 29(Ni+Cu) - 8.1Mn - 13.7Cr - 18.5Mo$$

The austenitic stainless steel is manufactured by a conventional process involving hot-rolling, annealing, pickling, cold-rolling and finish annealing. A ratio of hardness increase in a cold-rolled state is preferably controlled at a value of 20% or more as Vickers hardness. The stainless steel in the finish annealed state is preferably conditioned to a metallurgical structure of grain size number (regulated in JIS G0551) within a range of 8-11.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a schematic view Fig. 1 is a schematic view for explaining generation of drooping in a blanked piece and positions for detection of drooped parts.

Fig. 2 is a schematic view for explaining formation of a shear plane at a blanking plane of a product and positions for measuring the shear plane.

Fig. 3 is a graph showing a relationship of Md₃₀ value with a ratio of a shear plane.

Fig. 4 is a graph showing a relationship of (C+1/2N) with a ratio of a shear plane.

Fig. 5 is a graph showing a relationship of S content with a ratio of a shear plane at a clearance ratio of 2%.

Fig. 6 is a graph showing a relationship of S content with a ratio of a shear plane at a clearance ratio of 5%.

Fig. 7 is a graph showing a relationship of Vickers hardness with a ratio of a shear plane.

Fig. 8 is a graph showing a relationship of hardness increase caused by temper-rolling with a shear droop ratio.

Fig. 9 is a graph showing a relationship of a grain size number with a ratio of a shear plane.

Fig. 10 is a graph showing a relationship of a grain size number with a shear droop ratio.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

The inventors have researched from various aspects on the relationship of material properties of austenitic stainless steel with a state of a blanking plane formed by fine blanking, and discovered that a ratio of a strain-induced martensite (α' phase) puts a significant influence on a ratio of a shear plane to a blanking plane.

The strain-induced martensite (α' phase) is harder and inferior of ductility, compared with an austenitic (γ phase) matrix. Excessive generation of the strain-induced martensite (α' phase) means degradation of

ductility, early occurrence of fracture at a blanking plane and decrease of a ratio of shear plane. If generation of the strain-induced martensite (α' phase) is too little on the contrary, the austenitic stainless steel is blanked as such in the γ phase inferior of ductility, resulting in early occurrence of fracture at a blanking plane and decrease of a ratio of shear plane.

Softness of the austenitic stainless steel is well balanced with the effect of the strain-induced martensite (α' phase) on the quality of the fracture plane, so as to suppress occurrence of drooping. Thus, a blanking plane is improved in dimensional accuracy, and die life is prolonged.

The proposed austenitic stainless steel contains various alloying components at predetermined ratios as follows:

(C+1/2N) up to 0.060 mass %

C and N are components effective for adjusting stability of an austenite phase. However, excessive addition of C and N makes the austenite phase harder due to solution-hardening, and also makes a strain-induced martensite phase harder. The hardening causes increase of blanking load and short life of dies. Therefore, a ratio of (C+1/2N) is controlled at 0.060 mass % or less.

Si up to 1.0 mass %

Si is an alloying component added as a deoxidizing agent at a steel refining step. Excessive addition of Si makes an austenite phase harder due to solution-hardening, and degrades blankability of the stainless steel. In this regard, an upper limit of Si content is determined at 1.0 mass %.

Mn up to 5 mass %

Mn is an alloying component effective for stabilizing the austenite phase and improving blankability of the stainless steel. These effects become apparent as increase of Mn content. But, excessive addition of Mn more than 5 mass % causes increase of nonmetallic inclusions which put harmful

influences on corrosion resistance and workability.

S up to 0.006 mass %

A ratio of a shear plane to a blanking plane is reduced as increase of S content. The element S also puts harmful influences on corrosion resistance, which is most important property of stainless steel. In this regard, an upper limit of S content is determined at 0.006 mass %. Especially, for such a product which shall have a blanking plane with high dimensional accuracy, S content is preferably controlled to 0.003 mass % or less so as to increase a ratio of a shear plane.

10 Cr: 15-20 mass %

Cr content of 15 mass % or more is necessary to ensure corrosion resistance of stainless steel. But, excessive addition of Cr more than 20 mass % makes the stainless steel harder and put harmful effects on die life.

Ni: 5-12 mass %

15 Ni is an alloying element for stabilizing the austenite phase. Such the effect is realized by addition of Ni at a ratio of 5 mass % or more. Blankability of the stainless steel is also improved as increase of Ni content. However, Ni is an expensive element and raises a steel cost, so that an upper limit of Ni content is determined at 12 mass %.

20 Cu up to 5 mass %

Cu is an alloying element effective for improvement of blankability and also stabilization of the austenite phase. However, excessive addition of Cu more than 5 mass % puts harmful influences on hot workability.

Mo: 0-3.0 mass %

25 Mo is an optional alloying element effective for improvement of corrosion resistance. But, excessive addition of Mo more than 3.0 mass % makes the stainless steel too harder, resulting in degradation of fine blankability.

A value Md_{30} (representing a ratio of a strain-induced martensite): -60 to -10

An effect of a strain-induced martensite (α' phase) on a ratio of a shear plane to a blanking plane is a result discovered by the inventors from various experiments. A ratio of the strain-induced martensite (α' phase) can be calculated from components and contents of an austenitic stainless steel.

- 5 In the case where the austenitic stainless steel is designed to the composition having the value Md_{30} controlled within a range of -60 to -10 , a ratio of a shear plane is higher as explained in under-mentioned Examples, and a blanking plane is formed with high dimensional accuracy.

A ratio of hardness increase of an austenitic stainless steel:

- 10 20% or more by Vickers hardness

- A cold-rolled austenitic stainless steel sheet is harder due to introduction of many transpositions during cold rolling, compared with an annealed sheet which involves less transpositions. When a degree of hardening caused by cold-rolling is adjusted at a ratio of 20% or more by
15 Vickers hardness, metal flow toward a lower part of a blank is suppressed, resulting in reduction of drooping.

- The ratio of hardness increase is defined by the formula of $[(\text{Vickers hardness of a cold-rolled steel sheet}) - (\text{Vickers hardness of an annealed steel sheet})] / (\text{Vickers hardness of an annealed steel sheet}) \times 100 (\%)$ in this
20 specification. The ratio of hardness increase of 20% or more is necessary to suppress occurrence of drooping caused by blanking to a half or less of drooping which is generated by blanking an as-annealed steel sheet. However, a, extremely hardened steel sheet causes increase of shear resistance during blanking and promotes abrasion of dies. In this regard, an upper limit of the
25 ratio of hardness increase is preferably determined at 150%, accounting the effect on reduction of drooping in balance with die life.

Grain Size Number : #8 to #11

As crystal grains are coarsened, the stainless steel is softer, and a ratio of a shear plane to a blanking plane is higher, but the blanked steel

sheet is heavily drooped. In this regard, coarse crystal grains are unfavorable for manufacturing a product which shall have dimensional accuracy at its blanking plane as well as smoothness. On the other hand, the proposed austenitic stainless steel is conditioned to a metallurgical structure composed of minimized grains at a grain size number within a range of #8 to #11 in a finish annealed state. Said grain size number is bigger, compared with an ordinary grain size number of #6 to #8. The minimized grains are realized by reduction of an input energy, e.g. annealing the stainless steel at a relatively lower temperature or in a relatively short time. Due to such the conditioning of grain sizes, occurrence of drooping is suppressed while a ratio of a shear plane is kept at the same level.

Example 1

Various stainless steels having compositions shown in Table 1 were melted, cast, soaked at 1230°C, and hot-rolled to thickness of 10mm. Thereafter, the hot-rolled steel sheet was annealed 1 minute at 1150°C, pickled with an acid, cold-rolled to thickness of 5mm, annealed 1 minute at 1050°C and pickled again with an acid.

Table 1: AUSTENITIC STAINLESS STEELS USED IN EXAMPLE 1

Sample No.	Alloying components (mass %)									Md30	note
	C	Si	Mn	Ni	Cr	S	Cu	Mo	N		
1	0.01	0.5	1.0	10.75	18.25	0.001	0.10	0.08	0.01	-37.1	inventive examples
2	0.02	0.6	1.2	8.21	18.70	0.003	2.10	0.07	0.03	-43.8	
3	0.03	0.5	1.0	8.32	18.10	0.002	1.92	0.07	0.03	-35.6	
4	0.04	0.4	1.0	10.23	17.16	0.001	0.10	0.06	0.05	-38.1	comparative
5	0.02	0.3	1.7	8.01	17.10	0.001	3.21	0.07	0.01	-40.3	inventive examples
6	0.01	0.4	1.0	10.01	18.26	0.002	0.08	0.08	0.01	-14.3	
7	0.02	0.5	0.8	11.15	18.42	0.002	0.08	0.05	0.02	-57.5	
8	0.01	0.4	1.2	11.20	19.10	0.001	0.10	0.08	0.01	-62.5	comparative examples
9	0.02	0.6	0.5	11.82	18.33	0.001	0.10	0.08	0.02	-75.3	
10	0.01	0.5	0.7	9.83	18.25	0.001	0.10	0.08	0.01	-8.0	
11	0.03	0.6	0.7	8.21	18.25	0.001	0.10	0.08	0.04	15.0	inventive examples
12	0.05	0.5	0.8	8.81	18.25	0.001	0.81	0.08	0.02	-22.9	
13	0.03	0.6	1.0	10.27	18.91	0.004	0.10	0.09	0.02	-47.2	
14	0.02	0.6	1.0	9.89	19.10	0.006	0.10	0.07	0.02	-33.8	comparative examples
15	0.01	0.4	0.8	10.27	18.91	0.007	0.08	0.09	0.02	-33.9	
16	0.03	0.6	0.6	9.21	19.10	0.009	0.08	0.09	0.02	-15.2	

Each annealed steel sheet was examined by the under-mentioned blanking test to research shear resistance, a ratio of a shear plane to a blanking plane and a ratio of droop to thickness, and its Vickers hardness was measured as Rockwell B hardness regulated at JIS Z2240.

5 A test piece cut off each annealed steel sheet was blanked to a disc shape with clearance of 0.1mm or 0.25mm (a clearance ratio calculated as clearance/thickness of a test piece is 2% or 5%, respectively) at a blanking speed of 600 mm/minute, using a punch of 50mm in outer diameter and a die of 50.2mm or 50.5mm in inner diameter.

10 Each disc (a blanked piece) was measured with a laser-type noncontacting position sensor at 8 points, i.e. every 2 points along a rolling direction, a crosswise direction and a direction inclined with 45 degrees with respect to the rolling direction as shown in Fig. 1, to detect a degree of droop Z at each point. The measured values were averaged, and a ratio of droop to
15 thickness was calculated as a ratio of the mean value to thickness of the test piece.

Thickness of a shear plane S of each disc (a blanked piece) was also measured at 8 points, i.e. every 2 points along a rolling direction, a crosswise direction and a direction inclined with 45 degrees with respect to
20 the rolling direction, as shown in Fig. 2. The measured values were averaged, and a ratio of a shear plane was calculated as a ratio of the mean value to thickness of the test piece.

The ratio of a shear plane formed by blanking each test piece with a clearance ratio of 2% was researched in relationship with a value Md30 of
25 each test piece. Results are shown in Fig. 3. It is noted that a blanking plane with a ratio of a shear plane being 100% was gained at a Md30 value within a range of -60 to -10. Although Sample Nos. 4, 15 and 16 had Md30 values within a range of -60 to -10, their blanking planes were exceptionally poor with ratios of a shear plane being 85%, 95% and 71%, respectively.

A relationship of $(C+1/2N)$ with a ratio of shear plane was researched, as for Sample Nos. 1-4 and 12 each having value Md_{30} within a range of -60 to -10. Results are shown in Fig. 4. It is noted that Sample Nos. 1-3 and 12 each containing $(C+1/2N)$ less than 0.06 mass % were blanked with a ratio of a shear plane being 100%. On the other hand, Sample No. 4 containing $(C+1/2N)$ more than 0.06 mass % was blanked with a ratio of a shear plane of 85%.

Sample Nos. 1-3 and 13-16, which had values Md_{30} within a range of -60 to -10 and contained $(C+1/2N)$ less than 0.06 mass %, were blanked with a clearance ratio of 2%. A ratio of a shear plane formed by the blanking was researched in relationship with S content of each Sample. Results are shown in Fig. 5. It is noted that Sample Nos. 1-3, 13 and 14 containing S less than 0.006 mass % were blanked with a ratio of a shear plane being 100%, while Sample Nos. 15 and 16 containing S more than 0.006 mass % were blanked with ratios of a shear plane being 95% and 71%, respectively.

The relationship of S content with a ratio of a shear plane is also varied in response to a clearance ratio even in case of blanking the same steel sheet. That is, when Sample Nos. 13 and 14 were blanked with a clearance ratio of 2%, a blanking plane was formed with a ratio of a shear plane being 100%. The ratio of a shear plane was reduced to 92% and 88%, respectively, when Sample Nos. 13 and 14 were blanked with a clearance ratio of 5%, as shown in Fig. 6. The results prove that controlling S content less than 0.003 mass % is effective for blanking the steel sheet with a big clearance ratio which causes reduction of a ratio of a shear plane.

Example 2

Stainless steels having compositions shown in Table 2 were melted, cast, hot-rolled to thickness of 10mm at an initial temperature of 1230°C. Thereafter, each hot-rolled steel sheet was annealed 1 minute at 1150°C,

pickled with an acid, cold-rolled to intermediate thickness of 5-8mm, annealed 1 minute at 1050°C, and pickled again with an acid. Some of the steel sheets were provided as annealed steel sheets (A1, B1) of 5mm in thickness. The other annealed steel sheets of intermediate thickness were
5 further cold-rolled to thickness of 5mm and provided as temper-rolled steel sheets (A2-A6, B2,B3).

Table 2: AUSTENITIC STAINLESS STEELS USED IN EXAMPLE 2

Steel Kind	alloying components (mass %)								Md ₃₀	NOTE
	C	Si	Mn	Ni	Cr	S	Cu	Mo	N	
A	0.01	0.5	0.8	10.43	18.40	0.001	0.09	0.07	0.01	-27.8 an inventive example
B	0.06	0.6	0.6	8.02	18.21	0.003	0.08	0.08	0.04	8.6 a comparative example

A test piece was cut off each of the annealed and temper-rolled steel sheets, and blanked with a clearance ratio of 2% under the same conditions as in Example 1. Fig. 7 shows a relationship of Vickers hardness of each test piece with a ratio of a shear plane. It is noted that any of annealed or
 5 temper-rolled Sample Nos. A1 to A6 was blanked with a ratio of a shear plane being 100%. On the other hand, Sample Nos. B1 to B3 corresponding to SUS304 were blanked with low ratios of a shear plane near 45%.

A shear droop ratio was calculated as (a ratio of droop to thickness in a temper-rolled steel sheet) / (a ratio of droop to thickness in an annealed
 10 steel sheet), to research an effect of hardness increase by temper-rolling on generation of drooping. Results are shown in Fig. 8. It is noted that a shear droop ratio of any temper-rolled steel sheet A3 to A6 hardened by 20% or more as Vickers hardness was less than 50%, i.e. less than a half of droop generated in the annealed steel sheet A1. On the other hand, a shear droop
 15 ratio of the temper-rolled steel sheet A2 hardened at a ratio of hardness increase less than 20% was about 70% compared with the annealed steel sheet A1. The results prove that hardness increase of 20% or more is effective for sufficient reduction of drooping.

Each test piece was continually blanked until exchange of dies, to
 20 research an effect of material properties of the steel sheets on life of dies. Die life was evaluated as blanking cycles until exchange of dies. Results are shown in Table 3. It is noted that any steel sheet of type-A can be blanked with greater cycles until exchange of dies, compared with the steel sheets of type-B. That is, type-A steel sheets are effective for extension of die life. It
 25 is also noted from comparison of the type-A steel sheets each other that excessive hardness increase unfavorably causes decrease of blanking cycles. For instance, the blanking cycles until exchange of dies were somewhat reduced as for the steel sheet A6 hardened more than 150%.

Table 3: EFFECTS OF MATERIAL PROPERTIES
OF STEEL SHEETS ON DIE LIFE

No.	blanking cycles until exchange of dies	evaluation	note
A1	302969	⊙	inventive examples
A2	323341	⊙	
A3	309629	⊙	
A4	314211	⊙	
A5	354824	⊙	
A6	248142	○	
B1	103288	×	comparative examples
B2	52783	×	
B3	9879	×	

⊙ : the same or longer die life, compared with the steel sheet A1

○ : die life inferior to the steel sheet A1 but superior to the steel sheet B1

×

 : remarkable abrasion of dies

Example 3

- 5 Stainless steels C, D having compositions shown in Table 4 were melted, cast and hot-rolled to thickness of 10mm at an initial temperature. Thereafter, each hot-rolled steel sheet was annealed 1 minute at 1150°C, pickled with an acid, cold-rolled to thickness of 5 mm, annealed 1 minute at 800-1100°C, and then pickled again with an acid.

Table 4: AUSTENITIC STAINLESS STEELS USED IN EXAMPLE 3

Sample No.	Alloying components (mass %)								Md30	note
	C	Si	Mn	Ni	Cr	S	Cu	Mo	N	
C	0.02	0.6	0.7	10.21	18.71	0.002	0.08	0.05	0.02	-34.3
D	0.06	0.6	0.6	8.02	18.21	0.003	0.08	0.08	0.04	8.6
										an inventive example
										a comparative example

A test piece was cut off each steel sheet pickled after being annealed, and blanked with a clearance ratio of 2% under the same conditions as in Example 1. A ratio of a shear plane in the blanked test piece was calculated to research its relationship with grain size number of the steel sheet. Results are shown in Fig. 9. It is noted that any of type-C steel sheets according to the present invention was blanked with a ratio of a shear plane being 100% regardless its grain size number. On the other hand, any of type-D steel sheets corresponding to SUS304 was blanked with a lower ratio of a shear plane near 45%.

A relationship of a shear droop ratio with a grain size number is illustrated in Fig. 10. The relationship proves improvement of a shear droop ratio as increase of a grain size number (i.e. minimized metallurgical structure) regardless kinds of steel sheets. As for type-C steel sheets according to the present invention, a shear droop ratio of any steel sheet C3 to C6 each having grain size number more than #8 is reduced to a half or less, compared with steel sheets C1, C2 of grain size number less than #8.

Each test piece was continually blanked until exchange of dies, to evaluate die life from blanking cycles. Results are shown in Table 5. It is noted that any steel sheet of type-C can be blanked with greater cycles until exchange of dies, i.e. suitable for elongation of die life, compared with the steel sheets of type-D. But, blanking cycles somewhat were reduced as increase of grain size number more than #11, as noted in a steel sheet C6. This result proves that excessive minimization of a metallurgical structure is unfavorable for die life.

Table 5: A RELATIONSHIP OF DIE LIFE WITH
MATERIAL PROPERTIES OF STEEL SHEETS

No.	blanking cycles until exchange of dies	evaluation	note
C1	321962	◎	inventive examples
C2	339672	◎	
C3	321111	◎	
C4	342632	◎	
C5	315522	◎	
C6	236981	○	
D1	112011	×	comparative examples
D2	49876	×	
D3	5621	×	

◎ : the same or longer die life, compared with the steel sheet A1

○ : die life inferior to the steel sheet A1 but superior to the steel sheet B1

× : remarkable abrasion of dies

An austenitic stainless steel proposed by the present invention can be blanked to a product with high dimensional accuracy, due to excellent blankability, especially fine blankability. Even when the steel sheet is blanked with a small clearance ratio, a ratio of a shear plane to a blanking plane can be kept at a higher level without occurrence of substantial drooping. The stainless steel sheet is also advantageous for elongation of die life, compared with conventional austenitic stainless steel sheets such as SUS304. Consequently, blanked products with high dimensional accuracy are obtained from the proposed austenitic stainless steel sheet without increase of a manufacturing cost.

Claims

1. An austenitic stainless steel, which has an excellent property in fine blankability, consisting of (C+1/2N) up to 0.060 mass %, Si up to 1.0 mass %, Mn up to 5 mass %, S up to 0.006 mass %, 15-20 mass %, Cr, 5-12 mass % Ni, Cu up to 5 mass %, optionally Mo up to 3.0 mass % and the balance being Fe except inevitable impurities, under the condition that a value Md_{30} representing a ratio of a strain-induced martensite phase defined by the under-mentioned formula is within a range of -60 to -14.3, which has metallurgical structure minimized to #8 to #10 by grain size number.

$$Md_{30}=551-462(C+N)-9.2Si-29(Ni+Cu)-8.1Mn-13.7Cr-18.5Mo$$

2. The austenitic stainless steel according to Claim 1, which is hardened 20% or more by Vickers hardness by cold-rolling after annealing and pickling.

3. An article made from an austenitic stainless steel according to anyone of the preceding claims.

ABSTRACT

The newly proposed austenitic stainless steel has composition consisting of (C+1/2N) up to 0.060 mass %, Si up to 1.0 mass %, Mn up to 5 mass %, S up to 0.006 mass %, 15-20 mass % Cr, 5-12 mass % Ni, Cu up to 5 mass %, 0-3.0 mass % Mo and the balance being Fe except inevitable impurities under the condition that a value Md₃₀ (representing a ratio of a strain-induced martensite) defined by the under-mentioned formula is controlled within a range of -60 to -10. Hardness increase of the steel sheet after being cold-rolled is preferably 20% or more as Vickers hardness. A metallurgical structure of the steel sheet is preferably adjusted to grain size number of #8 to #11 in a finish annealed state. The steel sheet is blanked with high dimensional accuracy, and a die life is also prolonged.

$$\text{Md}_{30} = 551 - 462(\text{C} + \text{N}) - 9.2\text{Si} - 29(\text{Ni} + \text{Cu}) - 8.1\text{Mn} - 13.7\text{Cr} - 18.5\text{Mo}$$