

Q-switched Cavity Dumped Sub-nanosecond LaserRELATED APPLICATIONS DATA

This application claims priority to U.S. patent application number 62/635,174 filed on February 26, 2018 U.S. and patent application number 62/653,767 filed on April 6, 2018, each of which is hereby incorporated herein by reference in its entirety for all purposes.

FIELD

The present disclosure relates to apparatuses and methods for delivering laser energy having a short pulse duration (*e.g.*, less than about 1 nanosecond) and high energy output per pulse (*e.g.*, greater than about 100 millijoules). The desired operating parameters are achieved, in part, by a laser configuration including a laser cavity designed to have a sub-nanosecond round trip time so as to produce an output pulse duration in the sub-nanosecond range. The laser configuration also includes Q-switching and cavity dumping features. As a result, laser energy suitable for a number of applications, including cosmetic and medical applications, for example, treating and removing pigment particles such as those introduced to the human body as tattoos, may be generated using a relatively simple apparatus.

BACKGROUND

Lasers are recognized as controllable sources of radiation that are relatively monochromatic and coherent (*i.e.*, have little divergence). Laser energy is applied in an ever-increasing number of areas in diverse fields such as telecommunications, data storage and retrieval, entertainment, research, and many others. In the area of medicine, lasers have proven useful in surgical and cosmetic procedures where a

precise beam of high energy radiation causes localized heating and ultimately the destruction of unwanted tissues.

The principle of selective photothermolysis underlies many conventional medical laser therapies to treat diverse dermatological problems such as leg veins, portwine stain birthmarks, and other ectatic vascular and pigmented lesions. The dermal and epidermal layers containing the targeted structures are exposed to laser energy having a wavelength that is preferentially or selectively absorbed in these structures. This leads to localized heating to a temperature (*e.g.*, to about 70°C or higher) that denatures constituent proteins or disperses pigment particles. The fluence, or energy per unit area, used to accomplish this denaturation or dispersion is generally based on the amount required to achieve the desired targeted tissue temperature, before a significant portion of the absorbed laser energy is lost to diffusion. The fluence must, however, be limited to avoid denaturing tissues surrounding the targeted area.

In addition to fluence, pulse duration and pulse intensity can impact the degree to which laser energy diffuses into surrounding tissues during the pulse and/or causes undesired, localized vaporization. In terms of the pulse duration of the laser energy used, conventional approaches have focused on maintaining this value below the thermal relaxation time of the targeted structures, in order to achieve optimum heating. For the small vessels contained in portwine stain birthmarks, for example, thermal relaxation times and hence the corresponding pulse durations of the treating radiation are often on the order of hundreds of microseconds to several milliseconds.

The use of even shorter pulses, however, results in a change from photothermal to photomechanical processes. The latter mechanism is invoked by applying laser pulses having a duration that is below the acoustic transit time of a

sound wave through targeted particles. This causes pressure to build up in the particles, in a manner analogous to the accumulation of heat within a target irradiated by laser pulses having a duration that is below the thermal relaxation time.

Photomechanical processes described above are useful in the area of treating skin pigmentations including tattoos, portwine stains, and other birthmarks. Stable tattoos are likely composed of pigment particles having in one aspect exemplary diameters on the order of 1 to 4 micrometers. According to one exemplary aspect, each particle includes sub-particles with diameters on the order of 20 to 400 nanometers. According to one exemplary aspect, each particle includes sub-particles with diameters on the order of 40 to 100 nanometers. As the speed of sound in many solid media is approximately 3000 meters/second, the acoustic transit time across such particles, and consequently the laser pulse duration required to achieve their photomechanical destruction, is as low as hundreds of picoseconds. The acoustic transit time of a sound wave in a particle is calculated by dividing the radius of the particle by the speed of sound in the particle.

In addition to such short pulse durations, high energy laser pulses are needed for significant disruption of tattoo pigment particles and other pigmentations. Required fluences of several joules per square centimeter and treatment spot sizes of a few millimeters in diameter translate to a desired laser output with several hundred millijoules (mJ) per pulse or more. Unfortunately, current systems capable of such short pulse duration and high energy output can be too complex and/or expensive for practical use in the treatment or removal of tattoos and other pigmentations. These devices generally require two or more lasers and amplifier stages, together with multiple electro-optical and/or acousto-optic devices.

Consequently, there is a need in the art for laser apparatuses of relatively low complexity that can generate laser light in the picosecond pulse range and with energies high enough to provide usage in cosmetic or medical applications.

SUMMARY

Embodiments of the present disclosure are directed to a laser configuration or laser design or laser system that includes a laser oscillator having dimensions suitable to produce a sub-nanosecond cavity round trip time that is used to generate laser light with a sub-nanosecond pulse duration. Exemplary laser configurations also generate pulse energies on the order of a few hundred mJ per pulse and above. Representative laser configurations include a Q-switching feature. Representative laser configurations include a cavity dumping feature. According to one aspect, the laser configurations described herein are used to generate and deliver pulsed laser energy with pulse characteristics suitable for a number of practical applications. Such pulse characteristics include a sufficiently short duration and/or a sufficiently high energy for the photomechanical treatment of skin pigmentations and pigmented lesions, both naturally-occurring (*e.g.*, birthmarks), as well as artificial (*e.g.*, tattoos).

According to one aspect, a device and method are provided for generating high energy sub-nanosecond pulses from a laser oscillator without additional amplifier stages. In this aspect, the laser configuration lacks additional amplifier stages. In an additional aspect, the laser configuration lacks modelocking. In an additional aspect, the laser configuration lacks high frequency periodic loss modulation that can be associated with a laser oscillator.

In one aspect, the laser configuration includes only a single resonator and lasing (or gain) medium. The laser configuration includes two end mirrors between

which are positioned an electro-optical device such as a Pockels cell, a polarizer and a gain medium. The distance between the two reflective mirrors is designed to generate a cavity round trip time that is less than one nanosecond, i.e. a sub-nanosecond cavity round trip time. The laser configuration is designed for cavity dumping through the polarizer. According to one aspect, the cavity dumping is achieved by increasing the output coupling of the laser cavity so that all or substantially all of the energy circulating in the laser cavity is extracted out of the cavity. According to one aspect, the circulating energy is extracted from the cavity (or "dumped") over a period of time equal to or approximately equal to the cavity round trip time. In this manner, the pulse duration of the output pulse is equal to or substantially equal to the cavity round trip time. According to one aspect, in order to achieve a sub-nanosecond laser pulse duration, the cavity round trip time is less than one nanosecond. According to one aspect, in order to achieve an energy per pulse of 200mJ and higher, the laser resonator is first Q-switched and then cavity dumped, i.e. the laser energy is extracted from the laser resonator in a manner to achieve cavity dumping as that term is known in the art. In one aspect, cavity dumping is a method known in the art for extracting pulses from a laser using an optical switch in the laser resonator, such as an acousto-optic modulator or electro-optic modulator which is turned on briefly for pulse extraction.

According to one aspect, the laser configuration is simplified in terms of components required to produce a sub-nanosecond laser pulse output with energy of greater than 10 mJ or greater than 100 mJ. The resonator length need not be adjusted and the components are few and the laser configuration is compact. According to one aspect, the laser configuration and method includes reflecting laser energy between two totally reflective or two substantially totally reflective mirrors disposed at

opposite ends of a resonator and through a polarizer and an electro-optical device within the resonator and positioned along the optical path (or longitudinal axis) of the resonator. A lasing (or gain) medium, for example a flash lamp pumped laser rod, is also positioned along the optical axis. The laser resonator has a cavity round trip time of less than 1 nanosecond. According to one aspect, the laser resonator is Q-switched and cavity dumped to generate the sub-nanosecond pulses having an energy, for example, on the order of 100 mJ or 200 mJ. The pulse is expelled from the resonator at the polarizer.

According to one aspect, a representative apparatus includes a resonator having first and second mirrors, each of which is totally or substantially totally reflective, disposed at opposite ends of the resonator. The apparatus also includes a lasing material (*e.g.*, a solid state lasing medium), an electro-optical device (*e.g.*, a Pockels cell), and a polarizer, all of which are positioned along the optical axis of the resonator. The electro-optical device is positioned on the optical axis between the polarizer and the (arbitrarily denoted) “first” mirror. In other embodiments, the laser configuration or apparatus described herein may include a resonator of fixed length, and often includes a single resonator only of fixed length, which is configured to generate laser radiation with the desirable pulse duration and energy characteristics as discussed herein. In other embodiments, the first mirror and the second mirror are fixed within the housing to define a static resonator chamber having a sub-nanosecond round trip time. The resonator may be included in an apparatus, for example, in the absence of any other components that would materially affect its basic and novel characteristics.

The pulsed laser energy generated according to methods of the present disclosure may have at least about a 100 mJ/pulse, and often will have a pulse from

about 200 to about 900 mJ/pulse, as required for applications described herein, such as the removal or dispersion of pigment particles as often used to form tattoos. As is also desired in these applications, the pulsed laser energy generally has a pulse duration of between 100 picoseconds and 900 picoseconds, between 500 picoseconds and 900 picoseconds or between 500 picoseconds and 750 picoseconds. As stated previously, any of the methods described above may be performed without the need to adjust resonator length, as the resonator length is fixed to produce a sub-nanosecond round trip time, and with the few components comprising the laser resonator.

In another embodiment, the present disclosure provides a method for treating a skin pigmentation, such as a tattoo, a portwine stain, or a birthmark. According to one aspect, a diffractive lens array optic (i.e., a fractional lens array), such as described in Tanghetti, Lasers in Surgery and Medicine, 48:646-652 (2016) hereby incorporated by reference in its entirety can be used to deliver laser light from the device as described herein to the target tissue and as described by Anderson et al. US Patent No. 6,997,923 each of which are hereby incorporated by reference in its entirety. Accordingly, a fractional laser light treatment method is provided herein.

The method comprises exposing pigmented skin of a patient to pulsed laser energy with pulses having a duration of between 100 ps and 900 ps and an energy of at least 100 mJ. The pulsed laser energy is generated according to any of the methods, or using any of the apparatuses or laser configurations, discussed above.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a graphical representation of a resonator layout, wherein the cavity dumped pulse is extracted along the dashed arrow.

FIG. 2 illustrates the Pockels cell voltage waveform (not to scale).

FIGS. 3(a), 3(b), 3(c) and 3(d) are time plots, where the units are in cavity round trip time [trt].

FIG. 4(a) illustrates output pulse duration as a function of the Pockels cell voltage transient. Transient times and output pulse durations are in units of cavity round trip times.

FIGS 4(b), 4(c), 4(d) and 4(e) illustrate calculated voltage transients (dashed line) and output pulse shapes (solid line) from a cavity dumped resonator. Time scale, transient times and output pulse durations are in units of cavity round trip times. Pockels cell voltage amplitude in units of quarter wave voltage.

FIG. 4(f) shows a contour plot for the calculated output pulse duration.

FIG. 4(g) shows a contour plot for the calculated energy extraction efficiency. In the region enclosed between the two 99% contour lines, practically all the circulating resonator energy is extracted.

FIG. 5 illustrates an alternative resonator layout, wherein the cavity dumped pulse is extracted along the dashed arrow.

FIG. 6 illustrates an alternative Pockels cell voltage waveform (not to scale).

FIG. 7 shows Est/ESAT plotted as a function of the total energy stored in the gain medium. The solid line – 7 mm diameter Alexandrite crystal; the dashed line – 9.5 mm diameter Nd:YAG crystal.

FIG. 8 shows a contour plot for the stored energy extraction efficiency E_{out}/E_{st} for low gain materials. The two resonator end mirrors are assumed to have reflectivity $R_1 \cdot R_2 = 99\%$.

FIG. 9 shows a contour plot for the calculated number of round trips in the Buildup phase. The two resonator end mirrors are assumed to have reflectivity $R_1 \cdot R_2 = 99\%$.

FIG. 10 shows a contour plot for the stored energy extraction efficiency E_{out}/E_{st} for large gain media. The two resonator end mirrors are assumed to have reflectivity $R1 \cdot R2 = 99\%$.

FIG. 11 shows small signal gain as a function of the pumping diode; On-time Optical efficiency 80%; Quantum efficiency 650/750; Lines labeled with Alexandrite rod diameter and pumping diode peak power.

FIG. 12 shows a contour plot for output energy [J/pulse] from a Q-switched cavity dumped Alexandrite laser; Optical efficiency 80%; Quantum efficiency 650/750; 7 mm Alexandrite rod diameter; 10 kW pump diode peak power; 600 μ s pump diode on-time. The two resonator end mirrors are assumed to have reflectivity $R1 \cdot R2 = 99\%$.

FIG. 13 illustrates a side-pumped Nd:YAG laser.

FIG. 14 shows the end view of side-pumped Nd:YAG laser.

FIG. 15 shows a side-pumped Nd:YAG laser with long-pulse performance.

FIG. 16 shows a side-pumped Nd:YAG laser spatial beam profile.

FIG. 17 shows an end-pumped Alexandrite laser.

FIG. 18 shows a side-pumped Alexandrite laser.

FIG. 19 shows a side-pumped Alexandrite laser in an alternate configuration.

FIG. 20 shows a laser gain medium positioned transversely to flash lamps in a manifold.

FIG. 21 shows a laser gain medium and flash lamps positioned transversely in a ceramic diffuse reflector.

FIG. 22 shows a laser gain medium and flash lamps positioned transversely in separate glass flow tubes.

The features of the embodiments referred to in the figures are not necessarily drawn to scale and should be understood to present an illustration of aspects of the present disclosure and/or principles involved. Some features depicted in the figures have been enlarged or distorted relative to others, in order to facilitate explanation and understanding. The same reference numbers are used in the figures for similar or identical components or features shown in the various embodiments. Laser devices, as disclosed herein, will have configurations, components, and operating parameters determined, in part, by the intended application and also the environment in which they are used.

DETAILED DESCRIPTION

Aspects of the present disclosure are directed to embodiments of a laser configuration including a laser oscillator having a length providing a sub-nanosecond round trip time. According to one aspect, the length of the laser oscillator is fixed. According to certain embodiments, the laser oscillator has a cavity dumping feature. According to certain embodiments, the laser oscillator has a Q-switching feature. According to certain aspects, the laser oscillator is Q-switched and then cavity dumped. According to certain aspects, the laser oscillator is Q-switched and then cavity dumped over a period of time that is about equal to the laser oscillator round trip time. In this manner, the pulse duration of the output pulse is equal to or about equal to the laser oscillator round trip time. An exemplary output pulse is within the sub-nanosecond range. According to one aspect, the Q-switching feature provides energy on the order of a few hundred mJ and above.

Cavity dumping is a known technique where the output coupling of the laser cavity is increased very fast so that substantially all of the energy circulating in the

laser cavity is "dumped" out of the cavity as described, for example, in Siegman, "Lasers," University Science Books, 1986. Ideally, the circulating energy is dumped out of the cavity over a period of time equal to the cavity round trip time. Therefore, the pulse duration of the output pulse is equal to the cavity round trip time. Then, in order to achieve a sub-nanosecond laser pulse duration, the cavity round trip time is less than 1 nanosecond.

The requirement for relatively large energy per pulse, e.g., 200 mJ and above is achieved by the resonator being Q-switched and then cavity dumped. Q-switched cavity dumped designs have been reported and are useful in aspects of the laser designs and methods described herein. See for example, Thomas, *Opt. Expr.*, v. 24, p. 27212; Coyle, *J. Phys. D.*, v. 28, p. 452; Wayne, U.S. Patent No. 4,176,327; Guch, U.S. Patent No. 6,580,732; Rieger, U.S. Patent No. 7,006,540; and Zucker US 2007/0280305 each of which is hereby incorporated herein by reference in its entirety.

According to one aspect, the laser configurations described herein generate light pulses having a pulse duration of several hundred picoseconds to cause the photomechanical disruption, through the use of sound (or pressure) waves, of tattoo pigment particles and other components of pigmented lesions. Mechanical disruption of the pigment particles facilitates removal of the pigment particles by the body's natural removal processes such as those associated with the immune system. These pulse durations are of the same order as the acoustic transit time across particles having an exemplary diameter according to one aspect of from about 1 to about 4 micrometers, which are otherwise sufficiently large to remain stable in skin tissue (e.g., without being cleared by normal immune system responses).

Embodiments of the present disclosure generate and optionally deliver laser energy having a pulse duration generally less than about 1 nanosecond, typically less

than about 900 picoseconds (ps), about 800 picoseconds (ps), about 700 picoseconds (ps), about 600 picoseconds (ps), about 500 picoseconds (ps), about 400 picoseconds (ps), about 200 picoseconds (ps), and often less than about 250 ps. Common pulse duration values according to some embodiments are in the range from about 100 ps to about 900 ps, from about 150 ps to about 800 ps, from about 200 ps to about 700 ps, from about 300 ps to about 600 ps, from about 100 ps to about 300 ps, from about 500 ps to about 900 ps or from about 500 ps to about 750 ps. The above values generally represent less than several (*e.g.*, from about one to about three or from about one to about five) acoustic transit times for pigmentation particles having a diameter in the range from about 1 to about 10 microns.

Also characteristic of laser energy that is effective for treating or removing skin pigmentations is a relatively high level of energy output. For example, fluences required to achieve significant disruption of pigment particles are generally in the range from about 1 to about 10 J/cm². For viable treatment methods having a treatment area or spot size of a few millimeters in diameter, the required laser output is at least about 100 mJ per pulse, and often in the range from about 200 to about 800 mJ per pulse.

FIG. 1 depicts a representative embodiment of a laser resonator 10 according to the present disclosure, which is capable of achieving the above pulse duration and energy output parameters, suitable for the effective treatment of pigmented lesions through photomechanical means. Advantageously, the apparatus includes a resonator (or laser cavity) capable of generating laser energy having the desirable pulse duration and energy per pulse, as described herein. The resonator has a characteristic longitudinal or optical axis 20 (*i.e.*, the longitudinal flow path for radiation in the resonator), as indicated by the solid line. According to one aspect, the length of the

optical axis is fixed. Also included in the representative apparatus shown are an electro-optical device, in this case a Pockels cell 22 (PC), a polarizer 24 (P) (*e.g.*, a thin-film polarizer) and a gain medium 26 (Gain). During operation, the laser pulse output will be obtained along output path 28 indicated by the dashed line. According to one aspect, the laser pulse output is delivered to a target tissue using a laser light delivery device known to those of skill in the art. Such a laser light delivery device can include a single lens as is known in the art or a lens array as is known in the art. An exemplary lens array can be a fractional lens array as is known in the art.

At opposite ends of the optical axis 20 of the resonator are a first mirror 30 (M1) and a second mirror 32 (M2) having complete reflectivity or substantially complete reflectivity. The term “substantially complete reflectivity”, and equivalent terms such as “substantially totally reflective” are used to indicate that the mirrors 30 and 32 completely reflect incident laser radiation of the type normally present during operation of the resonator, or reflect at least 90%, preferably at least 95%, and more preferably at least 99% of incident radiation. The length of the laser resonator, *i.e.* the length between the incident faces where light is reflected along the axis 20 of the first mirror 30 and the second mirror 32 supports a cavity round trip time of less than one nanosecond. The mirror reflectivity is to be distinguished from the term “effective reflectivity,” which is not a property of the mirror itself but instead refers to the effective behavior of the combination of second mirror 32, Pockels cell 22, and polarizer 24 that is induced by the particular operation of the Pockels cell 22 to cause the light to be extracted from the laser cavity through polarizer 24.

In particular, a laser pulse traveling from lasing or gain medium 26 towards first mirror 30 will first pass through polarizer 24, then Pockels cell 22, reflect at first mirror 30, traverse Pockels cell 22 a second time, and finally pass through polarizer

24 a second time before returning to gain medium 26 and to second mirror 32 where the laser pulse will reflect and return to the gain medium 26. Depending upon the bias voltage applied to Pockels cell 22, the entirety of the energy in the pulse will be rejected at polarizer 24 and exit the resonator along output path 28 which is exemplary of "cavity dumping".

The lasing or gain medium 26 may be pumped by any conventional pumping device known to those of skill in the art (not shown) such as an optical pumping device (*e.g.*, a flash lamp) or possibly an electrical or injection pumping device. A solid state lasing medium and optical pumping device are preferred for use as described in the present disclosure.

According to one aspect, the laser resonator 10 includes Q-switching and cavity dumping capabilities. The orientation or positioning or arrangement of the resonator elements depicted in FIG. 1 is designed, such as to be compact, so that the cavity round trip time is less than 1 nanosecond (ns). The two end mirrors 30 (M1) and 32 (M2) are static, *i.e.* are not moveable along the axis and have high reflectivity, such as about 100%, at the laser-operating wavelength. In case of coaxial laser pumping of the gain medium, mirror 32 (M2), proximal to the gain medium, is dichroic coated and has high reflectivity, such as about 100%, at the laser operating wavelength, and minimum reflectivity, such as about 0%, at the pumping wavelength.

Representative solid state lasers operate with an Alexandrite or a titanium doped sapphire (Ti:S) crystal. Alternative solid lasing media include a yttrium - aluminum garnet crystal, doped with neodymium (Nd:YAG laser). Similarly, neodymium may be used as a dopant in the pervoskite crystal (Nd:YAP or Nd:YAlO₃ laser) or a yttrium -lithium -fluoride crystal (Nd:YLF laser). Other rare earth and transition metal ion dopants (*e.g.*, erbium, chromium, and titanium) and other crystal

and glass media hosts (*e.g.*, vanadate crystals such as YVO_4 , fluoride glasses such as ZBLN, silicaglasses, and other minerals such as ruby) of these dopants may be used as lasing media. According to one aspect, the gain (or laser) medium is preferably a compact solid-state laser crystal. Examples include Alexandrite, Nd:YAG, Nd:YLF, Yb:YAG, or other rare earth, or Cr doped crystals or glasses (*e.g.*, Cr:LiSAF). Preferably, the gain medium is a relatively low gain material such as Alexandrite.

The above mentioned types of lasers generally emit radiation, in predominant operating modes, having wavelengths in the visible to infrared region of the electromagnetic spectrum. In an Nd:YAG laser, for example, population inversion of Nd^{+3} ions in the YAG crystal causes the emission of a radiation beam at 1064 nm as well as a number of other near infrared wavelengths. It is also possible to use, in addition to the treating radiation, a low power beam of visible laser light as a guide or alignment tool. Alternative types of lasers include those containing gas, dye, or other lasing media. Semiconductor or diode lasers also represent possible sources of laser energy, available in varying wavelengths. In cases where a particular type of laser emits radiation at both desired and undesired wavelengths, the use of filters, reflectors, and/or other optical components can aid in targeting a pigmented lesion component with only the desired type of radiation.

In cases when the gain medium has relatively low absorption at the wavelength of coaxial pumping through the dichroic mirror M2 (32), the optical surface of the gain that is distal with respect to dichroic mirror M2 (32) can be dichroic coated to achieve about 0% reflectivity for the lasing wavelength and about 100% reflectivity for the pumping wavelength. According to this aspect, the dichroic coating on the gain medium allows for two-pass pumping with the pump light.

The apparatuses and methods disclosed herein are in many cases significantly simplified due to the reduced number of components and/or reduced demands in terms of bias voltage and other operating parameters. Devices may be operated using a modulated waveform according to the requirements and parameters set forth herein, and using suitable electronic configuration or various equivalent configurations as would be apparent to one of ordinary skill, having the benefit of the present disclosure. Other embodiments of the disclosure may involve the introduction of conventional optical components for use in conjunction with the apparatuses disclosed herein, such as shutters or beam attenuators, reflecting prisms or other reflecting components, filters, light focusing components such as concentrators or condensers, collimating lenses, additional polarizers, electro-optical devices, and/or mirrors, *etc.* These variations are readily contemplated, and the above modifications are therefore well within the purview of one of ordinary skill, having regard for the present disclosure.

According to one aspect, a method and apparatus is provided that utilizes a fractional treatment modality with diffractive lens array optics of fractional lens array optics. Diffractive lens array optics are known in the art and have been described in Tanghetti, Lasers in Surgery and Medicine 48:646-652 (2016) hereby incorporated by reference in its entirety and summarized as follows. Diffractive lens array optics have been demonstrated on millisecond-pulsed laser systems for the treatment of acne scars and photo-damaged skin. These arrays created high fluence regions separated by a low fluence background to produce focal areas of ablative or non-ablative injury in the skin. To realize the advantages of a fractional treatment with the picosecond laser system of Tanghetti, a hand piece with a diffractive lens array was added for the treatment of acne scars and wrinkles. A 755nm picosecond Alexandrite laser with a

diffractive lens array optic was used to treat in vivo skin at three different fluence and spot size settings as shown in Table 1 of Tanghetti. The diffractive lens array consisted of closely packed individual hexagonal lenses with 500 micrometer pitch, the center-to-center lens distance. The diffractive lens array modifies the intensity profile of the Alexandrite laser beam to produce a hexagonal array of high intensity regions surrounded by low intensity background. Approximately 70% of the total energy is delivered in the high fluence regions comprising less than 10% of the treated area for a single non-overlapping pass. The remaining 30% of the energy provides the low fluence background.

According to Tanghetti, microscopic analysis was performed on three dimensional images taken immediately and 24 hours post treatment with a Vivascope 1500, Caliber Imaging and Diagnostics confocal microscope (formerly Lucid Inc., Andover, MA). Basic images are 500x500 μm^2 tiles that are stitched together to provide a larger field of view, up to 8x8 mm^2 at a given depth. Stitched images at different depths with 10 μm spacing were then stacked to form a three-dimensional cubic image for analysis.

As described in Tanghetti, immediate post-treatment histology demonstrated well defined, approximately spherical, intra-epidermal spaces (vacuoles) void of H&E staining and measuring from 35 to 65 μm in diameter (See Tanghetti, FIG. 3). Degenerating necrotic keratinocytes were seen around the vacuoles but did not extend beyond one or two cellular layers. Location of the vacuoles varied from stratum granulosum to the dermal/epidermal junction. The vacuoles in tissue samples taken 24 hours after the treatment in darker skin types contained cellular debris positively stained with Fontana Masson, suggesting the presence of melanin (see Tanghetti, FIG. 4). Vacuoles found in lighter skin types MI<12 contained red blood cells. There was

no apparent damage to surrounding cells or underlying structures found either immediately or 24 hours post treatment in any skin types. The darker skin subjects presented clinically at 24 hours and up to 3 weeks post treatment with dark spots in a hexagonal pattern at a pitch matching that of the corresponding lens array for all fluences although the intensity of the darkened dots significantly decreased with lower fluences. Mild to moderate lymphocytic perivascular inflammation was found in the papillary dermis (see Nielsen et al., *J. Photochem. Photobiol. B* 2008;93:23-31 hereby incorporated by reference in its entirety. At 5 days and at 2 weeks post treatment zones of microscopic epidermal necrotic debris (MENDS) were seen immediately inferior to or within the stratum corneum (see Tanghetti FIG. 7). These zones exfoliated around 3–5 weeks post treatment. Confocal imaging immediately post treatment revealed no abnormalities in the epidermis or the papillary dermis for all subjects and treatment parameters. However, 24 hours after treatment, well-defined spherical vacuoles characterized by bright areas in the image were observed. These vacuoles ranged in diameter from 25 to 70 nm and were located between 55 and 75 nm deep within the stratum spinosum. Tanghetti Fig. 10 exhibits vacuole diameters versus treatment fluence in two darker-skinned subjects. When adjacent confocal images of the darker skinned subjects were stitched to provide a larger surface area view, a hexagonal pattern of vacuoles emerged with a pitch approximately corresponding to that of the lens array optic used for the treatment (see Tanghetti Fig. 11).

As described in Tanghetti, a 755nm picosecond Alexandrite laser with a diffractive lens array optic delivered an array of unique, focal zones of intra-epidermal injury in the stratum spinosum characterized by vacuoles at the site of the high fluence zones. As measured with confocal microscopy and H&E staining, the

stratum corneum and all tissue surrounding the vacuoles appeared normal with no indication of collateral thermal damage. This injury profile is in stark contrast to epidermal and dermal damage apparent in non-ablative and ablative fractional treatments. In a recent clinical study with a fractional picosecond Alexandrite laser, these localized epidermal vacuoles were associated with the deposition of new dermal collagen, elastic tissue, and mucin (see Brauer et al., JAMA Dermatol 2015;151(3):278 hereby incorporated by reference in its entirety). Keratinocytes produce a number of growth factors, chemokines, and cytokines in response to injury or a wound (see Werner et al., J. Invest.Dermatol. 2007;127(5)998-1008. These factors and agents could stimulate and regulate the response to this injury through receptors on epidermal and dermal cells. It has been speculated that the rapid vacuole formation with the generation of a laser induced breakdown (LIOB) could create a pressure fluctuation in the skin (see Vogel et al., J. Acoust. Soc. Am. 1996;100(1):148 hereby incorporated by reference in its entirety. This could also result in the initiation of dermal remodeling from changes in cell signaling and the release of cytokines from alterations in cellular membranes (see Tanghetti et al., Lasers Surg. Med. 2015;47(S26):24 and McDaniel, Lasers Surg. Med. 2015;47(S26):22 each of which are hereby incorporated by reference in its entirety). The high fluence zones created vacuoles, but the likelihood of this depended on the fluence within the zones, that is, the diffractive lens array and the amount of pigmentation. In darker skin types with high melanin content the confocal microscopic signatures were distinctly bright, quasi-spherical regions presumably due to light scattered from cellular debris consisting of nuclei and melanosome clusters within the vacuoles. As the melanin content of the epidermis decreased, the size, location, and prevalence of the vacuoles also decreased. In lighter skin types the injury profile dramatically changed. In

histology the vacuoles accompanied by hemorrhage were found at the dermal-epidermal junction. The vascular injury was only seen at the higher fluence 0.71 J/cm². The target chromophore apparently had shifted to include hemoglobin in the superficial capillary loops. These findings illustrate the importance of melanin in confining the injury to vacuoles in the epidermis and suggest a fluence threshold for vacuole formation dependent on skin pigment concentration. The role the vacuoles play in bringing about clinical outcomes is a subject of further investigation but the physical process leading to their formation is known to proceed by a complex sequence of steps. The creation of vacuoles in retina by laser heating has been reported and analyzed theoretically in the literature (Gerstman et al., *Lasers Surg. Med.* 1996;18(1):10-21.) The theory posited expansion of a steambubble created by laser heating of retinal melanin. A short laser pulse (less than microseconds) resulted in essentially instantaneous heating followed by expansion of the bubble long after the pulse had ended. In the present case, the target chromophore is the melanin in the epidermis. However, absorption of laser radiation by these granules alone is insufficient explain the observed bubble formation. A chromophore with 100 times greater absorbance is required. Such a highly absorbing chromophore can be created transiently by the laser radiation, via the LIOB process. In the LIOB process thermionic emission of one or more electrons from laser-heated melanin provides initial free "seed" electrons during the laser pulse (see Tanghetti Fig. 12A). Free electrons very efficiently absorb the laser light to gain energy between collisions with the surrounding molecules. When the energy of the seed electron exceeds that required to ionize a melanin molecule the next collision can result in the generation of a second free electron. This process repeats and the free electron density and energy grow to form an ionized plasma that continues to very efficiently absorb the

remaining laser radiation of the pulse. The resulting hot plasma heats the surrounding tissue via electron-molecule collisions even after the laser pulse has ended (see Tanghetti Fig. 12C). Theoretical analysis shows that the energy of the plasma is sufficient to create a steam bubble causing the intra-epidermal vacuoles (see Tanghetti Fig. 12D) (see Mirkov et al., *Lasers Surg. Med.* 2016;48(S27):1.

The process for LIOB formation relies on the generation of initial seed electrons to efficiently absorb the laser radiation. The generation of these electrons by means of thermionic emission is statistical in nature. Theoretical analysis relates the probability of thermionic emission to the laser parameters and melanin concentration. The greater the laser fluence or melanin concentration, the earlier in the laser pulse a seed electron will initiate LIOB formation. This means more energy in the remaining pulse is absorbed by the electron plasma to create larger vacuoles. In light-skinned subjects the probability of LIOB formation is greatest in the deeper region of the epidermis, in proportion to the epidermal melanin concentration (see Nielsen et al., *J. Photochem. Photobiol. B* 2008;93:23-31 hereby incorporated by reference in its entirety. Hemorrhagic vacuoles within the epidermis or superficial papillary dermis suggest that the LIOB process itself can either disrupt neighboring blood vessels or be initiated by hemoglobin (see Habbema et al., *J. Biophotonics* 2012;5(2):194-1994 hereby incorporated by reference in its entirety.

The following examples are set forth as representative of aspects of the present disclosure. These examples are not to be construed as limiting the scope of the disclosure as other embodiments and aspects are apparent in view of the present disclosure.

EXAMPLE I**Exemplary Laser Resonator**

The laser device or laser resonator depicted in FIG. 1 requires building up of the Pockels cell charge. Exemplary lengths and transit times through individual components of an exemplary resonator are provided in Table 1:

TABLE 1

Component	Laser rod	Pockels	Polarizer	Polarizer air	Air gaps	Total
Length, mm	20	25	4	23	10	82
Transit time, ps	117	126	19	77	33	373

For a resonator employing the components listed in Table 1, the cavity transit time is 373 ps and the cavity round trip time is 746 ps. The polarizer, the Pockels cell and the M1 end mirror form a variable reflectivity output coupler. The Pockels cell allows the resonator to progress through three consecutive phases or states and generates a sub-nanosecond pulse.

The three consecutive phases or states are illustrated in FIG. 2 showing the voltage waveform applied to the Pockels cell. The processes in the laser resonator in the three consecutive states are "Hold -off", "Buildup" and "Cavity dumping" as explained below.

The Hold off state is illustrated from the t_0 to t_1 time points in FIG. 2. The quarter wave voltage applied to the Pockels cell at time t_0 prevents the buildup of optical field in the resonator while energy is pumped and stored in the laser gain medium. The quarter wave voltage refers to the voltage required across the Pockels cell to split the incident radiation into two components having equal intensities and retard the polarization electrical field vector of one component by one-quarter of a wavelength relative to the other component. If the polarizer 24 rejects radiation having an electric field vector that is orthogonal (or perpendicular) to the orientation of the initial electric field vector of radiation from the lasing material 26, the net effect of the combined components (first mirror 30 (or M1), Pockels cell 22, and polarizer 24) is that of a variable reflectivity mirror. The term “substantially equal to the quarter wave voltage” indicates an applied bias voltage to the electro-optical device of its quarter wave voltage or preferably at least 80% to 120%, typically at least 90% to 110%, and often at least 95% to 105% of its quarter wave voltage. Thus radiation, having been reflected at the second mirror 32 and therefore passing twice through the Pockels cell 22 with an applied voltage of $V_{\lambda/4}$, will have its polarization axis rotated 90° and will be completely rejected by polarizer 24. An applied voltage $V = V_{\lambda/4}$ therefore provides an effective reflectivity, R_{eff} , of “0%” or “substantially 0%,” meaning that the radiation is either completely rejected by the polarizer 24, or possibly all but a small amount of radiation is rejected, *e.g.*, an amount having an intensity or amplitude generally of less than about 10%, typically of less than about 5%, and often less than about 1%, of its initial intensity or amplitude, I_0 , prior to the first pass of the radiation through the polarizer 24 and Pockels cell 22. The hold-off time from t_0 to t_1 is in the range of 0.5 to 3 storage laser level lifetimes depending on the available pump power source. A higher pump power source can be used for

shorter hold off time. A lower pump power source requires a longer hold-off time. The upper limit for the hold-off time is set by a multiple of the storage level lifetime of the laser gain material.

The Buildup state is illustrated from the t_1 to t_2 time points. After storing a predetermined amount of energy in the laser gain medium, the Pockels cell is switched to 0 volts or substantially 0 volts, setting the resonator in a low-loss state. Electrically, the Pockels cell acts as a capacitor, with a typical capacitance of about 10 picofarads (pF). The term "substantially 0 volts" indicates that the electro-optical device may be completely discharged to 0 volts or that the applied voltage will generally be less than 10%, typically less than 5%, and often less than 1%, of the quarter wave voltage of the device. The two resonator end mirrors are nominally 100% reflective at the laser wavelength. In this condition, the laser energy oscillates between two totally reflective or substantially totally reflective mirrors 30 and 32 along axis 20. The relatively high gain in the laser gain medium and low resonator loss allow for buildup of the optical field inside the resonator with negligible leakage out of the resonator.

The Cavity dumping state is illustrated from the t_2 to t_3 time points. When the optical field inside the resonator builds up to its peak, the Pockels cell is switched to quarter wave voltage at time t_2 and kept at that voltage for about one cavity round trip time or longer, until t_3 . That leads to extraction of the optical energy from the resonator in an optical pulse that is equal to or longer than the resonator round trip time.

The laser resonator is cycled through these three consecutive states multiple times per second to achieve a repetition rate from a few hertz to a few hundreds of hertz. The Pockels cell voltage waveform plotted in FIG. 2 has three time points with

relatively large voltage transients at t_0 , t_1 and t_2 time points. There are large differences in the requirements for the voltage transients at these three time points.

The t_0 transient establishes the hold off voltage and the t_0 transient can be relatively slow, for example, microseconds to a few milliseconds. The pumping of the gain medium starts after the hold off voltage is established and lasts hundreds of microseconds.

The t_1 transient occurs when a predetermined amount of energy is stored in the gain medium. During that transient, the gain in the resonator is the highest and the optical field builds from noise levels. Longer t_1 transient would allow for more energy to leak out of the resonator before the resonator reaches the low loss buildup state. For a high-gain material like Nd:YAG, it is beneficial for the t_1 transient to be shorter. A lower gain material like Alexandrite can work with a longer t_1 transient, for example, tens of nanoseconds.

The t_2 transient allows for the operation of the Q-switched cavity dumped laser, as it determines the cavity-dumping transient which generates a sub-nanosecond pulse output. As is known in the art, so-called “perfect dumping” occurs “suddenly” and the output pulse duration is exactly one cavity round trip time. According to the present disclosure, if the requirement for cavity dumping is relaxed from “suddenly” to on the order of the cavity round trip time, the output laser pulse duration becomes a little longer than one cavity round trip time as illustrated in FIGS. 3A-3D. For FIGS. 3A-3D illustrating the calculated voltage transients (dashed line) and output pulse shapes (solid line) from a cavity-dumped resonator, the time units are in cavity round trip time [trt]. The Pockels cell voltage transients are plotted with dashed lines, and the voltage amplitude is normalized to the quarter wave voltage for the Pockels cell $V_{\lambda/4}$. The voltage transient time τ_{10-90} , is defined as the time needed for the voltage to

change from 10% to 90% of the quarter wave voltage. The transient time τ_{10-90} , is presented in units of cavity round trip time. The midpoint of the voltage transient, i.e., 50% of the quarter wave voltage, is set to occur on the N-th round trip for consistency of the plots. The output pulse shape is plotted with a solid line. The full width at half maximum is shown as τ_{pulse} calculated in units of cavity round trip time. In all four cases of FIGS. 3A-3D, the output pulse energy, the area under the pulse shape curve, is the same.

FIG. 3A is representative for the suddenly cavity-dumped resonator. The voltage transient is only 10% of the cavity round trip time and the output pulse duration is 0.1% longer than the cavity round trip time. FIGS. 3B-3D are representative for the much more practical voltage transients that are of the order of the cavity round trip time and the corresponding output pulse durations that are from 3 to 34% longer than the cavity round trip time. For example, for a resonator with a 750 picosecond cavity round time, FIG. 3B shows output pulse duration around a 772 picosecond pulse and is desirable. FIG. 3C is on the order of acceptable, but is closer to the high end of the desired output of the specification range, e.g., about 900 picoseconds.

The calculated output pulse durations for a range of voltage transients are plotted on FIG. 4A in units of cavity round trip time [trt]. FIG. 4A summarizes the effect of realistic Pockels cell voltage transients on the cavity-dumped output pulse duration. As an example, using the example laser resonator depicted in FIG. 1 and with components in Table 1 with a round trip time of 746 ps, if the Pockels cell voltage transient is 746 ps, equal to the cavity round trip time, then the calculated output pulse duration is 1.03 round trip times, which is 768 ps. That is the desired sub-nanosecond output pulse duration for the example resonator with realistic Pockels

cell voltage transient. Accordingly, an exemplary output pulse is from 700 ps to 800 ps. According to one aspect, sub-nanosecond voltage transient technology in a Pockels cell known to those of skill in the art is useful in the present disclosure. For example, Bishop, A. I. and P. F. Barker "Subnanosecond Pockels cell switching using avalanche transistors." Review of scientific instruments 77.4 (2006): 044701 hereby incorporated by reference in its entirety discloses methods of pulse shaping and pulse termination using subnanosecond Pockels cell switching using avalanche transistors.

According to one aspect, the Pockels cell voltage transients from 0 to quarter wave voltage (or QW to 0), allow for complete extraction of the energy circulating in the resonator and lead to output pulse durations similar to the resonator round trip time and longer as plotted in FIG. 4A. According to one aspect, output pulses can be generated with duration shorter than the resonator round trip time by applying to the Pockels cell voltage transients larger than the quarter wave voltage and leaving some of the circulating energy in the resonator. Examples of such voltage transients larger than the quarter wave voltage and the generated output pulse shapes are plotted in FIGS. 4B-4E. In all of these plots, the pulse shape is plotted with a solid line using the y-axis on the left, and the voltage transient is plotted with a dashed line using the y-axis on the right. The voltage transients are normalized with respect to the quarter wave voltage. In all plots, the voltage transient time τ_{10-90} and the full width at half maximum of the output pulse τ_{pulse} are calculated in units of cavity round trip time. The output energy pulse fraction ϵ_{pulse} is calculated taking into account only the first pulse and ignoring the lower energy post pulses.

FIG. 4E shows a clean output pulse with no post pulses and with pulse duration about half of the resonator round trip time, carrying 56% of the available circulating resonator energy. The absence of post pulses is due to the fact that when

the voltage applied to the Pockels cell, as depicted in FIG. 1, reaches the level of two-times the quarter wave voltage (i.e., it is equal to the half wave voltage), there is no energy extraction from the resonator.

FIG. 4F is a contour plot for the calculated output pulse duration in units of cavity round trip times for a range of Pockels cell transient times and voltage amplitudes.

The Pockels cell voltage transient from zero to quarter wave voltage needed for cavity dumping shown at time t_2 in FIG. 2 is generally more difficult for electronics design than the transient from quarter wave voltage to zero. According to one aspect, an alternate resonator can be designed by adding a quarter wave plate 33 (Q) as shown in FIG. 5 that will lead to the alternate Pockels cell voltage waveform as shown in FIG. 6.

The embodiment of FIG. 5 enables the Pockels cell to be discharged in a manner that is relatively simple from an electrical standpoint. The arrangement of components depicted in FIG. 5 may employ a high gain material, for example, Nd:YAG. The electronics benefits of the alternative resonator layout and Pockels cell voltage waveform, as depicted in FIG. 5 and FIG. 6, are balanced against the drawbacks of the extra added component in the resonator, i.e. the quarter wave plate. The extra resonator component makes the resonator round trip time longer and therefore the output pulse duration gets longer for a fixed Pockels cell voltage transient time. In addition, the quarter wave plate adds two extra coated surfaces in the resonator with very low, but not exactly 0% reflectivity. Small resonator losses have a large effect on the output energy from the Q-switched cavity dumped laser, especially for low gain laser media like Alexandrite.

EXAMPLE II

Exemplary Laser Energy Output

The output energy from the Q-switched cavity dumped resonator can be calculated following the standard actively Q-switched laser formalism as described in Degnan IEEE Journal of Quantum Electronics v. 25 p. 214 hereby incorporated by reference in its entirety. The main difference from the pure Q-switched formalism is that for the cavity-dumped mode of operation, the energy is extracted from the cavity when the intra-cavity energy density reaches its peak. In a practical design, it is not always necessary to detect the peak of the intra-cavity energy density to trigger the cavity dump transient at time t_2 . For example, it is possible to optimize the time delay t_2-t_1 for maximum cavity dumped pulse energy at t_2 .

Alternatively, it is possible to monitor the rate of change of the intra-cavity energy density by monitoring the parasitic reflection from the polarizer or leakage from one of the end mirrors. Then the cavity dump transient will be triggered at time t_2 when the rate of change of the intra cavity energy density approaches zero.

The laser operation starts with pump energy delivery and storage in the gain medium during the hold-off period from t_0 to t_1 . The pump energy source may consist of flash lamps, LEDs, or another laser. Specifically, a semiconductor laser may be matched to absorption bands in the gain material and provide for higher than 90% pump power absorption in a gain material of relatively short length, for example 10 to 40 mm. The gain material may also have a dichroic coating as previously discussed. The semiconductor pump laser may consist of arrays of emitters. The individual emitters may be edge emitters or vertical cavity surface emitting lasers (VCSEL).

The performance of a Q-switched cavity dumped resonator is dependent on the stimulated emission cross section of the laser material σ . A material parameter called saturation fluence E_{SAT} can be defined for any laser gain material:

$$E_{SAT} = \frac{h\nu}{\sigma}$$

where $h\nu$ is the photon energy for the lasing wavelength. At the end of the hold-off period, from t_0 to t_1 , the energy stored per unit area in the gain material is E_{st} . The ratio of the stored energy per unit area and the saturation fluence is a convenient parameter describing the initial condition for the laser Buildup state, from t_1 to t_2 . An example for the range of values of the dimensionless small signal gain parameter E_{st}/E_{SAT} is plotted in FIG. 7 for an Alexandrite and a Nd:YAG crystal.

The difference by more than 10X for E_{st}/E_{SAT} for equal stored energy is mainly due to the large difference in the saturation fluence for the two materials, 26 J/cm² for Alexandrite and 0.67 J/cm² for Nd:YAG. After the energy is stored in the gain medium, it is extracted during the Buildup stage, from t_1 to t_2 , and then cavity dumped out of the resonator, from t_2 to t_3 . The energy extraction efficiency is plotted in FIG. 8 for the range of E_{st}/E_{SAT} typical for small stimulated emission cross section, large E_{SAT} material and a range of resonator single pass loss.

FIG. 8 depicts use of low-gain materials (e.g., Alexandrite) and demonstrates the importance of keeping single pass resonator loss as small as possible, especially for low-gain material like Alexandrite. For 5% single-pass loss and the plotted range of E_{st}/E_{SAT} , the maximum energy conversion efficiency is around 25%. Alternatively, for 3% single-pass loss, the conversion efficiency can be up to 40%. The large sensitivity to single-pass resonator loss is due to the relatively large number of round trips during the Buildup phase. The calculated number of Buildup round trips is plotted in FIG. 9.

The consistent trend for FIG. 8 and FIG. 9 is that larger E_{st}/E_{SAT} and smaller single-pass loss lead to smaller number of Buildup round trips and more efficient extraction of the stored energy. The energy extraction efficiency for the Q-switched cavity dumped resonator improves for gain media with larger stimulated emission cross section, and smaller E_{SAT} , as plotted in FIG. 10. On the other hand, gain media with larger stimulated emission cross section present more difficulty with parasitic amplified spontaneous emission and preleasing during hold off.

A Q-switched cavity dumped resonator using the Alexandrite gain medium can be stimulated by diode pumping and can have a relatively low stimulated emission cross section and relatively short storage level lifetime. The calculated small signal gain, E_{st}/E_{SAT} , in the Alexandrite rod achieved at the end of the Hold off phase is plotted in FIG. 11.

The data plotted in FIG. 11 shows what is required to build up a resonator with Alexandrite. FIG. 11 depicts data using a 7 mm diameter Alexandrite rod versus an 8 mm rod diameter. For equal pumping power, the gain in a 7 mm rod is about 24% larger than the gain in an 8 mm rod. That increased gain has to be balanced versus the 24% smaller area of the 7 mm rod and potentially 24% higher loading of the optical coatings on the rod.

FIG. 11 also illustrates that for the Alexandrite crystal with storage level lifetime between 200 μs and 260 μs there is very little added benefit in pumping on-times beyond 600 μs (2 to 3 lifetimes). The storage level lifetime and the stimulated emission cross-section of Alexandrite are temperature dependent. The temperature dependence for these two parameters can be approximated by polynomials between 30°C and 60°C based on published data in Shand et al., IEEE Journal of Quantum Electronics v. 19 p. 480 hereby incorporated by reference in its entirety. The

temperature set point of the Q-switched cavity dumped resonator can be optimized for maximum energy extraction. The output energy as a function of single pass loss and temperature, for fixed diode pump power and on-time, is plotted in FIG. 12.

The temperature dependence in the FIG. 12 plot indicates that under the considered pumping conditions and resulting small signal gain, the optimum Alexandrite temperature for maximum energy output shifts from around 50°C for 5% single-pass loss to around 35°C for 2% single-pass loss. More importantly, the temperature dependence for optimal energy output is a relatively slowly varying function. That means the Q-switched cavity dumped Alexandrite resonator temperature control can be built to maintain the temperature to within $\pm 3^\circ\text{C}$ to $\pm 5^\circ\text{C}$ and keep the output energy stable to within $\pm 10\%$.

EXAMPLE III

Exemplary Pump Sources

According to certain aspects, several different light sources can be considered for pumping the gain medium. For the two gain media used as examples herein (Nd:YAG and Alexandrite), flash lamp pumping can produce the stored energy required to produce greater than 200 mJ of laser output. According to one aspect, the flash lamp and the gain medium are housed in a traditional close-coupled, cooled, reflective pump chamber in which light from the flash lamp pumps the gain medium from the side. According to one aspect, the flash lamp provides a spectral output that overlaps with the absorption bands of the gain medium. A power supply drives the flash lamp and a cooling system removes heat generated by the system. Narrow-bandwidth pump sources (e.g., LEDs and diode lasers) can be used to efficiently pump both Nd:YAG and Alexandrite. While LEDs have been used to pump Nd:YAG

and can be used to pump Alexandrite, low LED peak power requires a sufficient number of emitters to generate greater than 200 mJ of laser output. Diode lasers are a well-established pump source for Nd:YAG. Numerous geometries and pump source configurations have been used to produce efficient, high-power diode-pumped lasers.

A diode laser array suitable for use as a pump source was created using a 24-bar diode laser array emitting at 820 nm that generates 10 kW peak power in a 500 μ s pulse at 10 Hz. The array includes two 12-bar, water-cooled stacks side by side. Two gold mirrors with slots for the bars were used to retro-reflect a portion of the light escaping from the pump chamber. Such an exemplary pump source is illustrated in FIG. 13. As illustrated in FIG. 13, a side-pumped Nd:YAG laser pumped by the 10 kW array was built to assess the suitability of this design for use in a Q-switched cavity dumped sub-nanosecond laser. The pump chamber consisted of a 9.5 mm diameter x 80 mm long Nd:YAG rod 34 in a water-cooled flow tube inside a 3 cm diameter diffuse reflecting pump chamber (not shown) with a rectangular hole to accommodate the optical element 36 output used to couple light from the diode array 38 into the chamber. In one embodiment, the optical element 36 is a prism. Alternatively, the optical element 36 may be a lens or multiple lenses. The two 12-bar stacks 40 were placed at the 23 x 23 mm² NBK7 glass prism 36 input 42 as shown in the end view in FIG. 14.

The concave curve 44 in the prism expanded the fast-axis light emitted by the array such that, together with slow-axis compression, the 4 x 70 mm² prism output was filled. The entire Nd:YAG rod length between mirrors 46 and 48 was uniformly pumped to avoid areas of high pump density that could result in parasitic lasing during the "Hold off" state (see FIG. 2). While further beam compression is desirable to decrease the amount of pump light escaping the pump chamber, prism losses due to

the low brightness of the slow-axis diode light guide against further reduction in beam width. According to certain aspects, numerous other optical systems (e.g., parabolic concentrators, various combinations of cylindrical and spherical lenses, etc.) can be used to couple light from the array to the pump chamber.

To assess the efficiency of the pump chamber, the multimode laser cavity shown in FIG. 13 was run in long-pulse mode with the array operated at 500 μ s pulsewidth at a repetition rate of 10 Hz. The laser performance is shown in FIG. 15 where a maximum energy of 1 J was generated for 2.7 J of pump light (measured at the prism output). Taking into account the 85% prism transmission, the overall optical to optical efficiency is 31%. Given the typical 50% diode array electrical to optical efficiency, the overall efficiency (1064 nm laser output/electrical input to the array) is 16%, which is significantly higher than the about 6% efficiency observed in a typical flash lamp-pumped Nd:YAG laser.

In addition to high pumping efficiency, another advantage of diffuse pump chambers is uniform pumping. The spatial beam profile of the Nd:YAG laser operating at 1 J is shown in FIG. 16 where the excellent spatial homogeneity will prevent formation of hot spots during operation as a Q-switched cavity dumped sub-nanosecond laser. Diode-pumped Alexandrite lasers have been previously demonstrated (see Scheps et al., "Alexandrite Laser Pumped by Semiconductor Lasers," Appl. Phys. Lett. 56(23), 2288-2290 (1990) hereby incorporated by reference in its entirety), but the lack of a high peak-power pump source limited the output power. The GaInP/AlGaInP material system used to produce diode laser bars in the 650-680 nm range has been used to pump Alexandrite lasers.

As discussed above, the required array peak power is on the order of 10 kW, which requires twenty-five 400 W bars. For an Alexandrite laser, a polarized pump

source is used to counter asymmetric pump absorption along the crystalline axes. According to certain aspects, bars may be provided that provide greater than 300 W peak power.

According to one aspect, an end-pumping configuration depicted in FIG. 17 is provided that requires additional optics (when compared to side pumping discussed above) in order to couple light from a 24 bar array 50 into an Alexandrite crystal 52. In this case, the crystal is cut such that the pump light is polarized parallel to the b axis. For example, for the optimum 7 mm diameter rod identified previously, an exemplary spot size at the crystal is less than $5 \times 5 \text{ mm}^2$ to ensure the pump energy is deposited within the rod diameter. To efficiently couple the fast axis light into a 5 mm spot requires collimation of all the diode laser bars 50, which can be accomplished with either one rod lens 54 per bar or one rod lens 54 for every two bars (assuming the two 12 bar stacks are well aligned to each other). Once the fast axis is collimated, a glass prism 56 can be used to create a $5 \times 5 \text{ mm}^2$ spot at the rod input.

The gain-medium length and doping and pump wavelength are selected such that greater than 80% of the pump light is absorbed. The dichroic mirror 58 transmits at the 650 - 680 nm pump wavelength range and reflects at the 750 nm Alexandrite laser wavelength. The dichroic mirror 58 has minimal thickness and, if possible, high refractive index (e.g., undoped YAG) and the distance between the dichroic mirror and the Alexandrite rod 52 is less than 0.5 mm in order to minimize the spot size expansion as the pump beam propagates from the prism 56 into the Alexandrite rod 52.

If achieving the required 10 kW peak power in a single 24-bar array is not optimal, it is possible to combine the output of two 5 kW 24 bar arrays that operate at two different wavelengths within the Alexandrite absorption band. For example, if

one array emits at 650 nm and the second array emits at 670 nm with the same linear polarization, a dichroic mirror can be used to combine the output of the two arrays into a single beam that (with suitable beam shaping optics) can be used to end pump the Alexandrite rod. It is also possible to combine two arrays emitting at 650 and 670 nm in orthogonal linear polarization states and then use an optical rotator to make the polarization direction of both beams parallel.

According to one aspect, a pumping configuration is shown in FIG. 18, which can be used if achieving the required 10 kW in a single 24-bar array is not optimal. In this case, a block or crystal 60 of Alexandrite is side-pumped by two 24-bar 5 kW arrays 62 with lasing occurring straight down the length. The portion of the crystal 60 that faces opposite each array is coated for high reflection at the pump wavelength and high transmission at the lasing wavelength. High transmission at the lasing wavelength reduces the chances of parasitic lasing reducing the available inversion during the hold-off period. Similar to the end-pumped geometry, prisms 64 (or other optical means) can be used to couple pump light from the diode array 62 into the crystal 60. The crystal cross-section and doping level are chosen such that greater than 80% of the pump light is absorbed after double passing the crystal. In this case, the 100% reflectivity mirror 66 shown in FIG. 18 replaces mirror M2 in FIG. 1. The mirror 66 no longer needs to have minimum reflectivity at the pump wavelength. The benefit of eliminating the pump transmission requirement for the laser cavity mirror is significant. Even if the required 400 W bars are available, the side-pumped geometry may still be the optimum choice. In this case, each array consists of twelve bars located at the prism input. In addition, the side-pumped geometry eliminates the need for micro-optics to collimate the fast-axis diode light if the fast-axis divergence is sufficiently low to maintain high transmission through the prism.

According to one aspect, a side-pumped configuration is shown in FIG. 19. Similar to the pump geometry shown in FIG. 18, the two arrays 62 are configured with either 12 or 24 bars. Since pump light that is not absorbed in a single pass will be incident on the opposing diode array, it is advantageous to place a gold-coated mirror mask over each diode array. The mirror mask has slits that allow the outgoing diode light to propagate toward the crystal 60. By minimizing the area of the slits, the amount of unabsorbed diode light from the opposing array reflected back towards the crystal 60 is maximized. The crystal faces through which the pump passes are anti-reflection coated for the pump wavelength.

Since the pump light (not including light reflected from the mirror mask) is now absorbed in a single pass (as opposed to the geometry shown in FIG. 18), the crystal cross-section and doping level are chosen such that greater than 80% of the pump light is absorbed after a single pass through the crystal. The width of the prism output is chosen so as to nominally match the crystal length. The wide width allows the use of bars with high fast-axis divergence. In addition, referring to the geometry shown in FIG. 18, the requirement for a high reflectivity coating on the crystal face opposite each array is eliminated. The primary disadvantage is the requirement that the pump light be absorbed in a single pass instead of a double pass. High absorption can produce areas of high pump intensity near the pump faces, which can lead to hot spots in the laser beam.

Vertical-cavity surface-emitting lasers (VCSELs) are an alternative to diode laser bars that are typically used to pump solid state lasers. In this case, an array of twenty five 5 x 5 mm² chips (400 W per chip) is used to produce the required 10 kW peak power pump source. Each chip consists of thousands of emitters, which minimizes the chances of optical damage. VCSELs can be grown on large wafers and

then diced into chips with testing performed at the wafer level. Since the divergence of the light from each VCSEL chip is symmetric (unlike diode laser bars), the optical delivery system is simplified. Many different optical systems (e.g., a two-lens system, prisms, parabolic concentrators, etc.) can be used to couple the output of a VCSEL array into an Alexandrite crystal.

EXAMPLE IV

Transverse Positioning of the Laser Gain Medium to an Excitation or Pump Source

According to one aspect, the sub-nanosecond round trip time of the laser resonator as described herein may be achieved by a longitudinal laser gain medium having a length of 20 mm to 40 mm, depending on the length of the electro-optical, Q-switch and other resonator components. Aspects of the present disclosure are directed to the relative positioning of the laser medium to the excitation or pump source. Exemplary excitation or pump sources are described herein and are known to those of skill in the art and include a flash lamp. Cylindrical shaped flash lamps are known in the art, as are helical shaped flash lamps. It is to be understood that the present disclosure contemplates flash lamps known to those of skill in the art whether unitary in nature or composed of several or a plurality of individual flash lamps or excitation energy sources. The present disclosure contemplates the use of one or more excitation or pump sources. Various geometries of excitation sources known to those of skill are also contemplated.

Aspects of the present disclosure describe the positioning of the excitation or pump source, such as a longitudinal excitation or pump source, parallel to a laser medium (for example, such that the geometric axis of the excitation or pump source is parallel to the optical axis of the laser medium), such as a longitudinal or cylindrical laser medium as is known in the art, so that the excitation energy is directed along the

length of the longitudinal or cylindrical laser medium. Many flash lamp pumped lasers are configured such that the gain medium, which may be a crystal having a cylindrical shape, is positioned in parallel with cylindrically shaped flash lamp(s). One or more individual excitation or pump sources may be positioned along the length of the longitudinal or cylindrical laser medium to create a longitudinal source of excitation energy. One or more excitation or pump sources may be positioned along the same side of the longitudinal or cylindrical laser medium or on different sides or along different portions of the length. Excitation or pump sources may be positioned on opposite sides of the longitudinal or cylindrical laser medium or at any position or location around the longitudinal or cylindrical laser medium. Excitation or pump sources may be positioned to surround the longitudinal or cylindrical laser medium. Excitation or pump sources may be positioned at right angles to each other around the longitudinal or cylindrical laser medium, such as four excitation or pump sources positioned directly opposite each other along and around the length of the longitudinal or cylindrical laser medium. The excitation or pump source may be a singular excitation source or pump unit or a plurality of excitation source or pump units. The excitation or pump source may extend beyond the longitudinal or cylindrical laser medium, may be co-terminus with the longitudinal or cylindrical laser medium or may be within the length of the longitudinal or cylindrical laser medium. Flash lamps with a geometric axis parallel to the optical axis of the gain medium can extend beyond the length of the gain medium in the resonator, may be co-terminus with the length of the gain medium, or may be within the length of the gain medium.

Suitable optical elements may be used as described herein and as known in the art for channeling or directing the excitation energy from the excitation or pump

source to the laser medium along its length. According to one aspect, the laser head containing the gain medium and the flash lamp(s) may be optimized for optimal coupling of energy from the flash lamps into the gain medium, or rod through its length.

Aspects of the present disclosure also describe the positioning of the excitation or pump source at one end of the longitudinal or cylindrical laser medium such that the excitation energy is directed to and through the end of the longitudinal or cylindrical laser medium, such as along the optical or geometric axis of the longitudinal or cylindrical laser medium. Suitable optical elements may be used as described herein and as known in the art for channeling or directing the excitation energy from the excitation or pump source to the laser medium at its end and to enter the end of the laser gain medium. According to one aspect, the laser head containing the gain medium and the flash lamp(s) may be optimized for optimal coupling of energy from the flash lamps into the gain medium, or rod through its end.

In certain embodiments, the laser gain medium may be positioned transversely with respect to the excitation or pump source which may include one or more, or a pair or a plurality of radiation sources, such as a flash lamp(s). In this manner, a portion of the laser gain medium is directly exposed to the radiation produced by the excitation or pump source. A portion of the laser gain medium is not directly exposed to the radiation produced by the excitation or pump source. According to one aspect, a mid-portion of the laser gain medium is directly exposed to the radiation produced by the excitation or pump source. According to one aspect, an off-center portion of the laser gain medium is directly exposed to the radiation produced by the excitation or pump source. According to this aspect, the excitation or pump source includes at least one flash lamp having an axis (for example a geometric axis) transverse to the

optical axis of the lasing medium. According to this aspect, the excitation or pump source includes a pair of flash lamps, with each flash lamp having an axis (for example a geometric axis) transverse to the optical axis of the lasing medium. According to this aspect, the excitation or pump source includes a plurality of flash lamps, with each flash lamp having an axis (for example a geometric axis) transverse to the optical axis of the lasing medium. According to this aspect, the longitudinal laser gain medium is positioned perpendicular to the longitudinal excitation or pump source. One of skill in the art will understand that the perpendicular or transverse positioning need not be exactly a 90 degree offset, but that variations are allowed within suitable tolerances.

According to one aspect, the longitudinal laser gain medium is positioned at an angle relative to the longitudinal excitation or pump source. According to one aspect, the longitudinal laser gain medium has an optical axis that is positioned at an angle relative to the geometric axis of the longitudinal excitation or pump source. According to one aspect, the angle is greater than 0 degrees and less than 90 degrees, with 0 degrees being a parallel arrangement and 90 degrees being a transverse or perpendicular arrangement. According to one aspect, the angle is between 30 degrees and less than 90 degrees. According to one aspect, the angle is between 60 degrees and less than 90 degrees. According to one aspect, the angle is between 30 degrees and 60 degrees. According to one aspect, the angle is between 30 degrees and 75 degrees. According to one aspect, the angle of the laser gain medium (for example the optical axis) is between 30 degrees and 150 degrees relative to the excitation or pump source (for example the geometric axis). One aspect is the proviso and that angle is not 90 degrees. According to one aspect, the angle of the laser gain medium (for example the optical axis) is between 60 degrees and 120 degrees relative to the

excitation or pump source (for example the geometric axis). One aspect is the proviso and that angle is not 90 degrees. According to one aspect, the angle of the laser gain medium (for example the optical axis) is between 75 degrees and 105 degrees relative to the excitation or pump source (for example the geometric axis). One aspect is the proviso and that angle is not 90 degrees. One of skill in the art will understand that angling the laser gain medium less than 90 degrees towards zero degrees relative to the longitudinal excitation or pump source (i.e., toward being parallel with the longitudinal excitation or pump source) increases the excitation energy directly impinging the laser gain medium, as the laser gain medium and the excitation source become closer to being parallel.

According to one aspect, transverse or angled positioning of the longitudinal laser gain medium relative to the longitudinal excitation or pump source produces sufficient laser light in a suitable laser head design, even though the coupling efficiency for transverse positioning of the flash lamp(s) as described herein will be lower compared to parallel positioning as described herein.

FIGS. 20, 21 and 22 generally depict two longitudinal flash lamps 72 each having a geometric axis with a longitudinal laser gain medium having an optical axis positioned there between and in a transverse manner. The embodiments differ in the support structure or cooling structure interacting with the flash lamps and the laser gain medium.

According to one particular embodiment of a laser head design as seen in FIG. 20, a longitudinal laser gain medium or lasing medium 70 and two longitudinal flash lamps 72 (an upper flash lamp and a lower flash lamp) may be positioned in a manifold 74 providing water flow for cooling. The laser gain medium and its optical axis is positioned between the two flash lamps and transverse to the geometric axis of

the two flash lamps. In certain embodiments, manifold 74 may be formed of glass. Other suitable materials for manifold 74 will become readily apparent to those skilled in the art, given the benefit of this disclosure.

Each flash lamp 72 is positioned within and extends through a flash lamp channel 76 formed in manifold 74. Lasing medium 70 is positioned within and extends through a lasing channel 78 formed in manifold 74, with lasing channel 78 extending transversely with respect to flash lamp channels 76 through a central channel 80 of manifold 74. Water can be supplied to the channels of manifold 74 in known fashion to provided suitable cooling. In this manner of transverse positioning, a portion of the longitudinal laser gain medium is directly exposed to the excitation energy from the two longitudinal excitation or pump sources. In this manner of transverse positioning, a portion of the longitudinal laser gain medium is not directly exposed to the excitation energy from the two longitudinal excitation or pump sources. In this manner of transverse positioning, a portion of the longitudinal laser gain medium extends outside of the manifold and is not directly exposed to the excitation energy from the two longitudinal excitation or pump sources.

According to the embodiment of transverse positioning, a shorter laser gain medium can be used to generate significant laser light compared to an embodiment where excitation or pump sources are positioned parallel to a longer laser gain medium. According to one aspect, a 2-inch flash lamp arc length was used with a 21 mm Alexandrite rod as lasing medium 70 positioned transversely to the flash lamp. The stored energy in the 21 mm Alexandrite rod was approximately 50% of the stored energy of an 80 mm Alexandrite rod where the same flash lamps were positioned parallel to the length of the 80mm Alexandrite rod. In certain embodiments, a diffuse reflector may be disposed on the external surfaces of manifold 74.

Aspects of the present disclosure are directed to a resonator design that generates a sub-nanosecond round trip time. According to one aspect of the present disclosure, one or more flash lamps or excitation sources that are positioned parallel to the lasing or gain medium or rod can extend beyond the length of the rod and add to the length of the resonator and extend the round trip time of the resonator. Such extended length of the resonator due to additional flash lamp length can affect the ability of the resonator to generate a sub-nanosecond round trip time. As is known in the art, flash lamps include a glass tube enclosing a gas mixture for electrical discharge and two electrodes on both ends. An exemplary design for parallel flash lamps would match the rod length to the electrical discharge length, leaving the two electrodes, which can be around 25mm in length, extending beyond the rod length. According to one aspect, one or more optical elements can be positioned between the flash lamps to minimize or avoid the additional resonator length due to flash lamps extending beyond the length of the rod. According to this aspect and with reference to Fig. 1, the Polarizer and the M2 mirror may be positioned very close to the rod between the flash lamps. However, such a design adds complexity due to the high voltage power supply, such as between 300 to 900V, that would be connected to the flash lamps, as well as structure for water cooling of the device.

According to an alternate embodiment of a laser head design as seen in FIG. 21, both flash lamps 72 as described in Fig. 20 may extend through a ceramic diffuse reflector 84. Flash lamps 72 may extend in parallel through a single flash lamp channel 86 formed in the ceramic diffuse reflector 84. Lasing medium 70 as described in Fig. 20 may extend through a lasing medium channel 88 formed in the ceramic diffuse reflector 84, with the lasing medium channel 88 extending transversely with respect to flash lamp channel 86. In the case where lasing medium

70 is formed of Alexandrite, the ceramic material may be selected for high reflectivity in the Alexandrite pumping bands so as to provide an acceptable lifetime.

According to an alternate embodiment of a laser head design as seen in FIG. 22, flash lamps 72 as described in Fig. 20 extend through separate glass flash lamp flow tubes 90. Lasing medium 70 as described in Fig. 20 is seated in a glass lasing medium flow tube 92, with lasing medium 70 and lasing flow tube 92 extending transversely with respect to flash lamps 72 and flash lamp flow tubes 90. It is to be appreciated that flow tubes 90 and 92 can be shaped as desired. In the illustrated embodiment, flash lamp flow tubes 90 are cylindrical tubes, while lasing flow tube 92 has an hourglass shape to allow for compact positioning of lasing medium 70 and the transverse flash lamps 72 and flash lamp flow tubes 90. Lasing flow tube 92 may also include peripheral channels 94 at opposed ends thereof in order to receive O-rings, to prevent leakage when water is provided to lasing flow tube 92. It is to be appreciated that flash lamp flow tubes 90 and lasing medium flow tube 92 are supported with the laser head design and may each have different shapes, and other suitable shapes will become readily apparent to those skilled in the art, given the benefit of this disclosure.

EXAMPLE V

Uses

A laser apparatus as described herein is used to generate pulsed laser energy having a pulse duration of 100 to 900 ps with 200 to 800 mJ/pulse. The laser apparatus includes a resonator with two substantially totally reflective mirrors at opposite ends of its optical axis. An Alexandrite crystal lasing medium, a polarizer, and a Pockels cell are positioned along this optical axis. An optical flash lamp is also

included for pumping the Alexandrite lasing medium, which generates laser energy having a wavelength in the range of 700 to 800 nm.

The pulsed laser energy described above is generated by pumping the lasing medium within a laser resonator having a sub-nanosecond round trip time and Q-switching and cavity dumping the laser energy to produce an output pulse having a sub-nanosecond pulse duration.

Laser energy having the pulse duration and energy as described above is applied to a patient undergoing treatment for the removal of a tattoo. This laser energy is applied over the course of a 30-minute treatment session to all areas of the skin having undesired tattoo pigment particles. Photomechanical disruption of these particles is effected using the short pulse duration (similar to the transit time of a sound wave through the targeted tattoo pigment particles), together with a fluence in the range of 2 to 4 J/cm². This fluence is achieved with a laser energy spot diameter of about 5 mm.

Most if not all of the undesired tattoo pigment particles are effectively photomechanically disrupted, destabilized, and/or broken apart using one or two treatments. As a result, the disrupted particles are cleared from the body via normal physiological processes, such as the immune response. The tattoo is thus eventually cleared from the skin with no remaining visible signs. In this manner, various methods described herein are considered methods for treating or removing pigmented particles such as tattoo particles.

EXAMPLE V

Embodiments

Aspects of the present disclosure are directed to a laser oscillator for generating laser energy having a pulse duration of less than 1 nanosecond. The laser

oscillator includes (a) a first mirror and a second mirror within a housing, with the first mirror and the second mirror providing a sub-nanosecond round trip time for laser radiation along an axis between the first mirror and the second mirror; (b) an electro-optic device, a polarizer and a lasing medium positioned between the first mirror and the second mirror along the axis; (c) a pump source operatively coupled to the lasing medium; and (d) wherein the laser oscillator is capable of proceeding through at least three consecutive states comprising hold-off, buildup and cavity dumping. According to one aspect, the cavity dumping state has a range of acceptable transient times that are greater than the ideal step function transient time. According to one aspect, the cavity dumping state has a range of acceptable transient times that are greater than the ideal step function transient time, wherein a range of acceptable transient times includes from 0.5 round trip times to 5 round trip times which generates output pulse durations that range from 1 round trip time to 2.5 round trip times, the round trip time being sub-nanosecond. According to one aspect, the first mirror and the second mirror are fixed within the housing to define a static resonator chamber having a sub-nanosecond round trip time. According to one aspect, the lasing medium includes Alexandrite, Ti:S, Nd:YAG, Nd:YAP, Nd:YAlO₃, Nd:YLF, yttrium-aluminum garnet doped with a rare earth or a transition metal ion dopant, yttrium-aluminum perovskite doped with a rare earth or a transition metal ion dopant, yttrium aluminum oxide doped with a rare earth or a transition metal ion dopant, a vanadate crystal, YVO₄, fluoride glasses, ZBLN, silica glasses, minerals, ruby, crystals or glass media hosts. According to one aspect, the electro-optical device is a Pockels cell. According to one aspect, the sub-nanosecond round trip time is between 500 and 900 ps. According to one aspect, the sub-nanosecond round trip time is between 700 and 800 ps. According to one aspect, the pump source operatively

coupled to the lasing medium provides pumping radiation along a longitudinal side of the lasing medium. According to one aspect, the pump source operatively coupled to the lasing medium provides pumping radiation along a longitudinal side of the lasing medium via an optical element. According to one aspect, the pump source operatively coupled to the lasing medium provides pumping radiation along a longitudinal side of the lasing medium via a prism. According to one aspect, the pump source includes at least one flash lamp having an axis transverse to the optical axis of the lasing medium. According to one aspect, the pump source includes a pair of flash lamps, each flash lamp having an axis transverse to the optical axis of the lasing medium. According to one aspect, the pump source includes a plurality of flash lamps, each flash lamp having an axis transverse to the optical axis of the lasing medium. According to one aspect, the pump source operatively coupled to the lasing medium includes two pump sources providing pumping radiation along opposite longitudinal sides of the lasing medium via an optical element. According to one aspect, the pump source operatively coupled to the lasing medium provides pumping radiation along an end of the lasing medium via an optical element. According to one aspect, the pump source operatively coupled to the lasing medium provides pumping radiation along an end of the lasing medium via a prism.

Aspects of the present disclosure are directed to a method of generating sub-nanosecond pulsed laser energy. The method includes (a) providing a resonator having a first mirror at one end, a second mirror at the opposite end, a lasing medium, a polarizer, and an electro-optic device disposed therebetween, and wherein the resonator has a cavity round trip time of less than 1 nanosecond, and wherein the lasing medium is pumped by a pump source operatively connected to the lasing medium; (b) applying a first voltage to the electro-optic device to hold off laser

oscillation in the resonator while pumping energy into the lasing medium; (c) applying a second voltage to the electro-optic device to build up laser energy within the resonator; and (d) applying a third voltage to the electro-optic device to cavity dump a portion of the laser energy from the resonator. According to one aspect, the third voltage applied to the electro-optic device is a quarter wave voltage $V_{\lambda/4}$. According to one aspect, the transient time between the second applied voltage and the third applied voltage is greater than the ideal step function transient time. According to one aspect, the transient time between the second applied voltage and the third applied voltage is greater than the ideal step function transient time and wherein a range of acceptable transient times includes from 0.5 round trip times to 5 round trip times which generates output pulse durations that range from 1 round trip time to 2.5 round trip times, the round trip time being sub-nanosecond. According to one aspect, the pulsed laser energy has a pulse duration of between 100ps and 900ps. According to one aspect, the pulsed laser energy has a pulse duration of between 200ps and 800ps. According to one aspect, the pulsed laser energy has a pulse duration of between 600ps and 800ps. According to one aspect, the pulsed laser energy has at least 100 mJ/pulse. According to one aspect, the pulsed laser energy has from 200 to 800 m J/pulse. According to one aspect, the first mirror and the second mirror are fixed within the housing to define a static resonator chamber having a sub-nanosecond round trip time. According to one aspect, the lasing medium comprises Alexandrite, Ti:S, Nd:YAG, Nd:YAP, Nd:YAlO₃, Nd:YLF, yttrium-aluminum garnet doped with a rare earth or a transition metal ion dopant, yttrium-aluminum perovskite doped with a rare earth or a transition metal ion dopant, yttrium aluminum oxide doped with a rare earth or a transition metal ion dopant, a vanadate crystal, YVO₄, fluoride glasses, ZBLN, silica glasses, minerals, ruby, crystals or glass

media hosts. According to one aspect, the electro-optic device is a Pockels cell. According to one aspect, the sub-nanosecond round trip time is between 500 and 900 ps. According to one aspect, the sub-nanosecond round trip time is between 700 and 800 ps. According to one aspect, the pump source operatively coupled to the lasing medium provides pumping radiation along a longitudinal side of the lasing medium. According to one aspect, the pump source operatively coupled to the lasing medium provides pumping radiation along a longitudinal side of the lasing medium via an optical element. According to one aspect, the pump source operatively coupled to the lasing medium provides pumping radiation along a longitudinal side of the lasing medium via a prism. According to one aspect, the pump source includes at least one flash lamp having an axis transverse to the optical axis of the lasing medium. According to one aspect, the pump source includes a pair of flash lamps, each flash lamp having an axis transverse to the optical axis of the lasing medium. According to one aspect, the pump source includes a plurality of flash lamps, each flash lamp having an axis transverse to the optical axis of the lasing medium. According to one aspect, the pump source operatively coupled to the lasing medium includes two pump sources providing pumping radiation along opposite longitudinal sides of the lasing medium via an optical element. According to one aspect, the pump source operatively coupled to the lasing medium provides pumping radiation along an end of the lasing medium via an optical element. According to one aspect, the pump source operatively coupled to the lasing medium provides pumping radiation along an end of the lasing medium via a prism.

Aspects of the present disclosure include a method of generating sub-nanosecond pulsed laser energy and treating pigmented skin. The method includes (a) providing a resonator having a first mirror at one end, a second mirror at the opposite

end, a lasing medium, a polarizer, and an electro-optic device are disposed there between, and wherein the resonator has a cavity round trip time of less than 1 nanosecond, and wherein the lasing medium is pumped by a pump source operatively connected to the lasing medium; (b) applying a first voltage to the electro-optic device to hold off laser oscillation in the resonator while pumping energy into the lasing medium; (c) applying a second voltage to the electro-optic device to build up laser energy within the resonator; and (d) applying a third voltage to the electro-optic device to cavity dump a portion of the laser energy from the resonator; and (e) exposing pigmented skin of a patient to the laser energy with pulses having a duration of at most 990 ps and an energy of at least 10 mJ/pulse.

Aspects of the present disclosure includes a method for treating a skin pigmentation including (a) reflecting laser energy generated by a lasing medium between a first mirror at one end of a resonator and a second mirror at the opposite end of said resonator and through a polarizer and an electro-optical device within the resonator and wherein the resonator has a cavity round trip time of less than 1 nanosecond, and wherein the lasing medium is pumped by a pump source operatively connected to the lasing medium; (b) amplifying laser energy within the resonator by applying to the electro-optical device a first constant voltage; (c) Q-switching the resonator; and (d) then cavity dumping the amplified laser energy from the resonator by applying to the electro-optical device a quarter wave voltage $V_{\lambda/4}$; and exposing pigmented skin of a patient to the pulsed laser energy with pulses having a duration of at most 990 ps and an energy of at least 10 mJ/pulse.

In view of the above, it will be seen that several advantages may be achieved and other advantageous results may be obtained. Various changes could be made in the above apparatuses and methods without departing from the scope of the present

disclosure. It is intended that all matter contained in this application, including all theoretical mechanisms and/or modes of interaction described above, shall be interpreted as illustrative only and not limiting in any way the scope of the appended claims.

Throughout this disclosure, various aspects are presented in a range format. The description of a range should be considered to have specifically disclosed all the possible subranges as well as individual numerical values within that range. For example, description of a range such as from 1 to 6 should be considered to have specifically disclosed subranges such as from 1 to 3, from 1 to 4, from 1 to 5, from 2 to 4, from 2 to 5, from 3 to 6 *etc.*, as well as individual whole and fractional numbers within that range, for example, 1, 2, 2.6, 3, 4, 5, and 6. This applies regardless of the breadth of the range.

Thus, while there have been shown, described, and pointed out fundamental novel features of various embodiments, it will be understood that various omissions, substitutions, and changes in the form and details of the devices illustrated, and in their operation, may be made by those skilled in the art without departing from the spirit and scope of the invention. For example, it is expressly intended that all combinations of those elements and/or steps which perform substantially the same function, in substantially the same way, to achieve the same results are within the scope of the invention. Substitutions of elements from one described embodiment to another are also fully intended and contemplated. It is the intention, therefore, to be limited only as indicated by the scope of the claims appended hereto.