

The subject of the present invention is a shock absorber for a hydropneumatic suspension element of a vehicle, especially a heavy vehicle.

Hydropneumatic, especially oil-pneumatic suspension elements for heavy vehicles, comprising cartridges arranged in a hydraulic chamber between the piston and the gas chamber, are known. Thus, it is known to provide shock-absorbing cartridges consisting of an actual shock absorber and of a peak-limiting valve, the hydraulic fluid passing through these cartridges alternately during the movements of the piston in the hydraulic chamber when the vehicle runs over uneven ground. ^(cf e.g. FR-A-2,556,804) The shock absorber operates directly up to a certain maximum vehicle speed, below which, particularly on more or less uneven ground, the very rapid hydraulic pressure peaks and drops triggered when the vehicle passes over humps and hollows are absorbed by the bidirectional quick-opening peak-limiting valve associated with the shock absorber.

The latter is conventionally equipped with shutters elastically returned to their seat by springs or by elastic washers held in place by means of a screw.

Now for some categories of heavy vehicles travelling above a particular speed, especially on uneven ground, it has been found that the shock absorber does not operate and consequently does not allow the fluid to flow to and fro on either side of the shutters or elastic washers. This can be explained by the fact that, when the hydraulic pressure detaches a washer from its seat, there arises between the latter and the washer a vacuum which, added to the elastic restoring force of the washer or of the shutter, tends to close the passage again before a sufficient quantity of fluid has been able to pass through the shock absorber. Experience shows that it then becomes impossible to detach the shutter from its seat, so that the extremely high

hydraulic pressures (several hundred bars) prevailing inside the hydraulic chamber of the suspension element can cause the complete fracture of the arm of this element and consequently put the suspension out of action.

In other cases, the abrupt pressure variations destroy the washers, so that the suspension is likewise put out of action.

The object of the invention is, therefore, to provide a shock absorber which is capable of operating effectively and in an entirely reliable way at very high vehicle speeds, especially on uneven ground, despite extremely high pressures in the hydraulic chamber which can reach approximately 1000 bars on some types of vehicle.

The shock absorber to which the invention relates comprises a disk fastened in a supporting ring having ports for the passage of the hydraulic fluid on either side of the disk, means allowing this passage in only one direction for some ports and in the opposite direction for the other ports, and elements for fastening the said means to the disk.

According to the invention, the abovementioned means comprise, mounted on the two opposite faces of the disk, stacks of elastically flexible metal washers arranged in a rigid annular deflector located opposite the hydraulic-fluid passage ports.

The presence of this deflector, advantageously consisting of a sufficiently resistant metal or metal alloy (steel), protects the washers against any risk of being destroyed as a result of the abrupt peaks or falls of hydraulic pressure in the suspension element. According to another particular feature of the invention, each port is delimited by a tubular insert fastened in a bore passing right through the disk, some

of the inserts being equipped with end collars, at the rate of one collar per insert, which project on one face of the disk, whilst the other inserts are equipped with end collars projecting on the opposite face of the disk, and the dimensions of these projecting collars are such that the deflectors are held elastically up against the said collars, thereby shutting off the corresponding inserts as long as the hydraulic pressure is insufficient to move the deflectors away from the associated collars.

According to another characteristic of the invention, the deflectors bear against the collars of the inserts by means of the annular surface of a radial ring of the said deflector, the width of which and the thickness of the wall of the tubular inserts, equal to the width of the annular surface, are set between limits which effectively allow the deflector to move away from and keep away from the associated collar as long as the hydraulic pressure remains sufficient, at the same time preventing bruising of the said collar.

Tests conducted with such a shock absorber have shown that it operates to complete satisfaction at very high speeds of heavy vehicles, even on uneven ground.

Other particular features and advantages of the invention will emerge from the following description of a non-limiting embodiment of the shock absorber according to the invention and its uses in two hydropneumatic suspensions:

- Figure 1 is a view, half in longitudinal section and half in elevation, of a hydropneumatic suspension element which is intended particularly for a heavy vehicle and which can be equipped with a shock absorber according to the invention;
- Figure 2 is a view similar to that of Figure 1 of a second hydropneumatic suspension element

which can be equipped with a shock absorber according to the invention;

- Figure 3 is a view in axial section of a cartridge which is formed by the combination of a shock absorber according to the invention and of a bidirectional quick-opening peak-limiting valve and which is capable of equipping suspension elements, such as those of Figures 1 and 2, the shock absorber and the valve being shown at rest;
- Figure 4 is a view in axial section and partial elevation of the shock absorber of Figure 3;
- Figure 5 is an elevation view in a section along the line 5-5 of Figure 4;
- Figure 6 is a partial sectional view on an enlarged scale of a tubular insert and of a deflector equipping the shock absorber of Figure 3 to 5;
- Figures 7 and 8 are views similar to that of Figure 3, showing the shock absorber and the valve respectively in the position of compression and of expansion of the hydraulic fluid;
- Figure 9 is an end view of the shock absorber in an elevation according to 9-9 of Figure 10;
- Figure 10 is a view in axial section of an outer tubular casing forming part of the cartridge of Figures 3, 7 and 8;
- Figure 11 is a cross-sectional view according to 11-11 of Figure 10;
- Figure 12 is an end view in elevation according to the arrow F of Figure 10; and
- Figure 13 is a graph illustrating the variation, as a function of the vertical speed of the vehicle wheel, in the compression and expansion force necessary for the shock absorber and the peak-limiting valve of Figures 3 to 12 to operate.

Figure 1 shows a hydropneumatic suspension element 1 which is described in detail in the applicant's French Patent ^{FR-A-2,551,804} 83-20,063 and which it is therefore not

necessary to describe in detail here.

The element 1 comprises a wheel support arm 2, only a cross-section of this arm being shown here and the end of this arm opposite the part shown in the drawings being articulated on a vertically moveable roller (not shown). Articulated on a rocker 3 fixed to the arm 2 are the ends of the rods 4 of two pistons 5 capable of moving simultaneously in opposite directions within hydraulic chambers 6 during the oscillations of the arm 2. Associated with each chamber 6 are a gas accumulator 7 with a flexible diaphragm 8 separating the gas compartment 7a from the hydraulic compartment 7b communicating with the hydraulic chamber 6, and a shock-absorbing cartridge 9. The latter is accommodated in the end of the hydraulic chamber 6 opposite the piston 5, facing the hydraulic compartment 7b with which it communicates, the chamber 6 being delimited by means of a piece 11 connected sealingly to the accumulator 7.

Each cartridge 9 consists of an assembly comprising a shock absorber and a bidirectional quick-opening peak-limiting valve, and the shock absorber can advantageously conform to that which the invention relates.

Min Figure 2 illustrates a second suspension element 12 for heavy vehicles, of the type which is described in the applicant's French Patent ^{FR-A-2,571,935} ~~85-05,067~~ and which will therefore not be described in detail again.

The element 12 comprises an arm 13, through which passes an axle journal (not shown) of the vehicle and which is articulated rotatably on a stationary part 14 fixed to the chassis (not shown) of the vehicle). The stationary part 14 is coaxial relative to a shaft 15 connected to the chassis, rolling means being provided between the rotary arm 13 and the stationary part 14. In the arm 13 there is a hydraulic chamber 16 which contains a sliding piston 17 separating the chamber 16

from a receptacle 18. Articulated on the piston 17, which slides sealingly in the chamber 16, is a connecting rod 19, of which the end opposite the piston 17 is articulated on a pivot pin 21 fastened transversely in a lug 22 integral with the stationary part 14.

In the arm 13 there is also a pneumatic chamber 23 which has an axis parallel to that of the hydraulic chamber 16 and in which two freely sliding pistons 24, 25 delimit two gas chambers 26, 27. On the side opposite the gas chamber 26, the piston 24 receives the hydraulic pressure coming from the chamber 16 via a connecting conduit 28, one end of which opens into the chamber 16 opposite a cartridge 29 consisting of a shock absorber and of a bidirectional peak-limiting valve. The second end of the conduit 28 communicates with the hydraulic circuit (not shown) of the vehicle.

The shock absorber and the peak-limiting valve which can form the cartridges 9 and 29 of the suspension elements of Figures 1 and 2 will now be described with more particular reference to Figures 3 to 12 (these examples of the use of the shock absorber and of the peak-limiting valve not being limiting).

A) Description of the shock absorber (Figures 3 to 8)

The shock absorber 31 comprises a disk 32 equipped with an external thread 33 making it possible to screw it into a tubular casing 34 having an annular gasket 35 ensuring sealing relative to the wall of the hydraulic chamber. Machined in the disk 32, the axis X-X of which is the general axis of the cartridge (9 or 29, Figure 1 or 2), are bores 36 which are parallel to the axis X-X and are uniformly distributed round this and in each of which is fastened a tubular insert 37a, 37b, the internal port 38, 30 of which opens at its opposite ends onto the two faces of the disk 32.

Figure 5 shows that, in this example, there are ten bores 36 and corresponding inserts, but of course this number can vary. Some of the inserts, namely half of them, denoted by 37a, are equipped with respective end collars 39 projecting relative to that face of the disk 32 which confronts the hydraulic chamber, whilst the other inserts, designated by 37b, are each equipped with an end collar projecting relative to the opposite face of the disk 32.

The ends of the inserts 37a, 37b opposite the collars 39, 41 open into respective recesses 42, 43, made in the corresponding faces of the disk 32, these recesses 42, 43 preferably being cylindrical and offset axially relative to the axes of the corresponding inserts 37a, 37b. The recesses 42 and 43 are distributed uniformly round the axis X-X in an alternating arrangement, as are therefore the associated inserts 37a, 37b. In the example described, the recesses 43 are made on the face of the disk 32 confronting the hydraulic chamber of the suspension element, and the collars 39 diametrically opposite the recesses 43 project on this same face of the disk 32, opposite the peak-limiting valve 65 associated with the shock absorber 31. This arrangement is reversed for the recesses 42 and the associated inserts 37b. The inserts are fastened in the disk 32 by any suitable means, for example by a thread 44 screwed into an internal thread of the associated bore 36, and by an annular shoulder 45 integral with the rest of the insert 37a, 37b and projecting radially into a corresponding receptacle of the disk 32.

The shock absorber 31 is equipped with means allowing the hydraulic fluid to pass through the disk 32 in only one direction for the ports 38 of the inserts 37a and in only the opposite direction for the ports 30 of the inserts 37b. In the embodiment described, these means comprise, mounted on the two opposite faces of the disk 32, stacks 46, 47 of elastically flexible

metal washers arranged in a rigid annular deflector 48, 49 located opposite the ports 38, 30 of the inserts 37a, 37b. In the example illustrated in Figure 4, each stack 46, 47 consists of three washers 46a, 46b, 46c and 47a, 47b, 47c, the outer edges of which are retained radially by means of a circular wing 51, coaxial relative to the axis X-X, of the corresponding deflector 48, 49. Each wing 51 is extended by a radial ring 52 which is perpendicular to the axis x-x and the surface of which comes up against the annular end of the respective inserts 37a and 37b.

The shock absorber 31 is completed by a screw 53 passing axially through the disk 32, the stacks of washers 46, 47 and the two deflectors 48, 49. The stacks 46, 47 and the deflectors 48, 49 are held in place by means of annular members 54, 55 through which the screw 53 passes and which are arranged up against the washers 46a, etc. and 47a, etc. in the region of these adjacent to the screw 53 and are themselves fixed in place respectively by means of an end washer 56 of the screw 53 and by means of a nut 57. Two washers 58, 59 are interposed between the disk 32 and the stacks 46, 47, and a third washer 61 is inserted between the nut 57 and the annular member 55.

The dimensions of the washers 46a, etc. and 47a, etc., of the two deflectors 48, 49 and of the projecting collars 39, 41 are such that the rings 52 are held elastically by means of the corresponding washers 46a, etc. and 47a, etc. against the annular surfaces of the respective collars 39, 41 when the shock absorber 31 is at rest. In this position (Figures 3 and 4), the parts of the surface of the rings 52 which are not up against the collars 39, 41 are therefore at a distance from the recesses 43, 42 which is equal to the depth of these, plus the spacing between the rings 52 and the faces of the disk 32 confronting them.

This shock absorber operates as follows:

When the hydraulic pressure increases abruptly on one face of the disk 32 up to a predetermined sufficient value, the fluid moves the deflector 49 or 48 away from the corresponding collar 39 or 41, and the fluid flows to the other side of the disk 32 via the port 38 or 30. This flow of the fluid is opposed by a hydrodynamic vacuum, generated precisely as a result of this flow between the deflector 48 or 49 and the annular surface of the corresponding collar 41 or 39, and the elastic restoring force exerted by the stacks of washers 46 or 47. The fluid therefore continues to flow as long as the hydraulic pressure and the upstream force so generated are greater than the hydrodynamic vacuum and the elastic restoring force of the deflector which tend to lay the latter down on the collars 39 or 41.

Now the hydrodynamic vacuum and the corresponding force exerted on the deflector are directly proportional to the annular surface of the collar 39 or 41 in contact with the particular deflector. The result of this is that, to ensure that the fluid can in fact flow from a certain hydraulic pressure, this annular contact surface must not exceed a certain value.

Conversely, if this annular surface of the inserts 37a, 37b which is in contact with the deflectors 48, 49 is too small, the bearing force of these on the collars 41, 39 risks exceeding the yield limit of the material of the inserts 37a, 37b and consequently causing bruising of the collars 39, 41. It will therefore be appreciated that the thickness of the wall of the inserts, that is to say the width of their annular surface receiving the deflectors 48, 49, must be between specific limits, depending on the materials used and on the hydraulic pressure in the chamber of the suspension element.

Referring now to Figure 6, these limits can be determined from the following data:

- d_1 = the diameter of the port 38 or 30 of the projecting collar 39, 41 of the insert 37a or 37b;
- d_2 = the outside diameter of the collar 39 or 41;
- x = the distance between the surface of the ring 52 and the deflector 48 or 49 and the annular surface of the collar 39 or 41 when hydraulic fluid at sufficient pressure flows from the port 38 (30) towards the outside of the deflector 48 (49);
- p_1 = the hydraulic pressure in the port;
- p_2 = the hydraulic pressure in the deflector;
- S = the deflector surface equal to the cross-section of the port 38 (30) and receiving the pressure p_1 .

The dynamic balance is obtained when the below-mentioned relation is satisfied, in this F_1 being the force exerted on the surface S of the deflector by the pressure p_1 , F_2 being the elastic restoring force of the deflector, and F_3 being the force generated as a result of the hydrodynamic vacuum between the collar 39 and the deflector 48.

$$F_1 = F_2 + F_3 \left(\frac{d_2}{d_1}, x \right)$$

$$\text{hence } (p_1 - p_2)S = F_2 + F_3$$

$$\text{from which } (p_1 - p_2)\pi \left(\frac{d_1}{2} \right)^2 = F_2 + x \propto F_2$$

$$\text{and } x = f \left[(p_1 - p_2) \frac{d_1^2}{d_2}; \frac{d_1}{d_2} \right]$$

In fact, the hydrodynamic vacuum is also a function of the elastic restoring force F_2 of the deflector. However, this hydrodynamic restoring force is, first and foremost a function of the ratio d_2/d_1 , so that if this ratio is too high, that is to say if the contact surface is too large, the deflector does not move away from the insert, or is laid down on it again

immediately after moving away from it, and shuts it off permanently. Conversely, if the ratio $d2/d1$ is too low (being at the limit equal to one), the yield limit of the material of the insert will be reached or exceeded, and there will be bruising of the periphery of the collar 39 or 41 which will make the shock absorber unfit for operation.

Thus, the below-mentioned relation must hold true.

$$A < \frac{d2}{d1} < B$$

in which A is a coefficient corresponding to the yield limit of the material of the insert and B is the value of the ratio $d2/d1$ from which the deflector closes again and blocks the shock absorber.

As an example to give an indication, depending on the materials used for the shock absorber and on the hydraulic pressure prevailing in the suspension element (which can reach approximately 1000 bars in some heavy vehicles), there can be $\alpha = 0.25$. It is therefore possible to determine the limiting values of the ratio $d2/d1$.

Of the possible alternative embodiments of the shock absorber 31, the following will be mentioned in particular: the number of elastic washers 46a-47c can vary, these washers being made of a suitable material, the same applying to the deflectors 48, 49 which can be produced preferably from steel. The number of inserts 37a, 37b and of bores 36 can also vary, and they can be fastened in a disk 32 by any suitable means.

It will be seen that the surfaces of the annular members 54, 55 facing the washers 46a-47c are first plane and then fustoconical, starting from the screw 53, in order to reserve between these washers and the

said fustoconical surfaces a gap which increases up to the periphery of the members 54, 55. This arrangement allows the elastic movement necessary for the washers and the deflectors 48, 49.

B) Description of the peak-limiting valve (Figures 3 and 7 to 12)

A two-fold disadvantage, which can be explained with reference to Figure 13, can be seen in the known bidirectional quick-opening peak-limiting valves. Figure 13 shows, on the ordinate, the force (in kN) necessary for opening a known peak-limiting valve as a function of the speed V of the vehicle (in m/s) that is to say as a function of the peak-limiting rate which is proportional to the speed. The part of the curve A for positive speeds (abscissa) corresponds to the compression of the fluid, whilst the part on the negative abscissa corresponds to expansion. The two parts of the curve A with a very steep slope (peaks) on either side of $V = 0$ correspond to the flow of the fluid to and from via the shock absorber only (throttling flow).

It will be seen that, at the mean vertical speeds of the wheel, that is to say at a vehicle speed of approximately 5 to 10 m/s, the thrust necessary for opening the valve under compression is relatively low. As a result of this, when the vehicle passes over a hump at these speeds, there occurs the phenomenon of tail-gating of the body of the vehicle and therefore an unpleasant jolt for its occupants. Above these speeds, the triggering force increases rapidly. On the other hand, under expansion, at negative vertical speeds of between 0 and approximately - 2 m/s, it can be seen from this part of the curve A that the force necessary to ensure that fluid actually passes first into the shock absorber and then through the valve is very high. This means that, after the vehicle passes over a hump at low speed, the wheels or rollers of the vehicle do

not fall back sufficiently quickly to make contact with the ground again before the body. The body and wheels as a whole therefore fall at the same time, and this causes another highly uncomfortable jolt for the occupants of the vehicle.

The peak-limiting valve 65 illustrated in Figures 3 and 7 to 12 is designed so that these disadvantages of the prior valves can be eliminated.

The valve 65 is accommodated in the tubular casing 34 containing the shock absorber 31 (the latter can be replaced by any other suitable shock absorber) and comprises a tubular body 66 screwed into the casing 34 by means of a thread 66a and having a central orifice 67 on that side of the bottom of the hydraulic chamber opposite the piston, that is to say on the same side as the accumulator (in Figure 1: the chamber 6, piston 5 and accumulator 7), this orifice 67 being intended for the passage of the hydraulic fluid.

The valve 65 also possesses a hollow slide 68 mounted slideably along the general axis X-X of the valve 65 and of the shock absorber 31 within a sleeve 69, itself mounted slideably along the axis X-X in the body 66 and being coaxial relative to the slide 68. An elastic member consisting, in this example, of a helical spring 71 bears on an annular shoulder 72 of the body 66 delimiting the central orifice 67 and pushes the slide 68 up against a first annular end 73 of the sleeve 69. For this purpose, the end of the spring 71 opposite the orifice 67 bears on a second annular shoulder 74 of the slide 68, formed at its end opposite the orifice 67 and delimiting a second central orifice 75 in the slide 68. The end part 76 of the slide 68 adjacent to the orifice 67 and consisting of a radial flange has a fustoconical annular seat 77 normally held up against an end edge 78 of the sleeve 69 by means of the spring 71.

The second annular end 79 of the sleeve 69 opposite the end part 76 has radial orifices 81 shut off by the slide 68 as long as the latter is held up against the sleeve 69 by means of the spring 71.

Furthermore, the valve 65 possesses a cover 82 for closing the body 66 on the side of the latter opposite its central orifice 67, that is to say on the same side as the orifice 75 in the slide 68. The cover 82, consisting of a bottom 83 perpendicular to the axis X-X and of an annular skirt 84 coaxial relative to the axis X-X, is fastened between a cylindrical inner shoulder 85 of the body 66 and another annular shoulder 87 of the casing 34. The periphery of the bottom 83 is therefore up against the shoulder 87, whilst the annular end of the skirt 84 is up against the shoulder 85 (Figures 3, 7 and 8). In the skirt 84 are formed radial ports 88 communicating with the radial orifices 81 via corresponding chambers 89 delimited between the sleeve 69 and the skirt 84.

The end part 79 of the sleeve 69 adjacent to the cover 82 has a fustoconical seat 91 for bearing on a circular edge 90 which belongs to the cover 82 and up against which it is stressed by the end 76 of the slide 68, itself stressed by the spring 71. The annular cross-section of the seat 91 is greater than the annular cross-section of the seat 77 for the bearing of the slide 68 against the end part 73 of the sleeve 69. Longitudinal conduits 92 which are made in the casing 34 and are distributed around the axis X-X, and of which there are 24 in this example (Figure 12), open, on the one hand, into chambers 80 (Figure 9) communicating with the ports 88 and, on the other hand, into a cavity 70 of the casing 34 and into the hydraulic chamber of the suspension element, in the region of the deflector 49 of the shock absorber 31, that is to say on the opposite side of the casing 34 to the cover 82.

Longitudinal conduits 93 are arranged in the sleeve 69 and communicate, on the one hand, with the chambers 89 and, on the other hand, with transverse bores 94 located in the sleeve 69 and adjacent to its end part 73. The bores 94 themselves communicate with longitudinal clearances 95 reserved between the adjacent end 76 of the slide 68 and the end part 73 of the sleeve 69. These clearances 95 are closed by means of the annular seat 77 for the bearing of the slide 68 on the edge 78 of the sleeve 69 as long as the slide 68 is laid up against the said sleeve 69.

Longitudinal conduits 96 made in the body 66 open out, at one of their ends, on the side opposite the cover 82, whilst their opposite ends are shut off by the corresponding end 73 of the sleeve 69 when the latter is up against the cover 82 by means of its seat 91.

The annular shoulder 85 of the body 66 delimits, on the one hand, the chambers 89, and, on the other hand, the longitudinal conduits 96 and, by means of the inner wall of its shoulder 85, the longitudinal conduits 93 in the sleeve 69.

Longitudinal conduits 98, of which there are four in this example, are formed in the casing 34, and their ends open respectively onto the face of the casing 34 opposite the cover 82 and into a receptacle 99 located inside the casing 34 and containing the shock absorber 31 for throttling the hydraulic fluid.

The peak-limiting valve 65 just described operates as follows.

1 - At rest, the valve 65 is in the position shown in Figure 3, the hydraulic pressures are balanced on either side of the valve, the spring 71 keeps the slide 68 up against the sleeve 69 by means of its seat

77 laid against the edge 78, so that the clearances 95 are closed, the sleeve 69 is up against the edge 90 of the cover 82 by means of its seat 91, and the radial orifices 81 are closed by the slide 68. There can therefore be no passage of fluid through the valve 65.

2 - Operation of the valve 65 under compression
(Figure 7)

If a sudden increase in the hydraulic pressure beyond a specific value occurs in the chamber of the suspension element, some of the fluid moves the deflector 48 away from the inserts 37b and therefore enters the receptacle 99, from which it flows via the conduits 98 towards the opposite side of the valve 65, that is to say towards the accumulator.

Another fraction of the fluid flows by way of the conduits 92, the chamber 80, the ports 88, the chambers 89, the conduits 93, the bores 94 and the clearances 95. The pressure exerted on the slide 68 in the clearances 95 then moves the seat 77 away from the edge 78 and consequently the slide 68 away from the sleeve 69, the end 76 of the slide 68 coming up against that of the body 66. Because of this, a small stream of fluid flows off from the clearances 95 between the ends 73 and 76 and then between the end 76 and the body 66 and passes out via the orifice 67. At the same time, hydraulic fluid flows through the open ports 81 between the end 79 of the sleeve 69 and the adjacent end 74 of the slide 68. This fluid therefore passes through the slide 68 which it leaves via the orifice 67.

The various paths followed by the fluid during compression are symbolized by the arrows marked in Figure 7, most of it flowing via the conduits 92 and the valve 65.

The curve B of Figure 13 illustrates an example of

the operation of the assembly composed of the valve 65 and of the shock absorber 31: it can be seen that, at low positive speeds (compression) below approximately 1 m/s, the shock absorber 31 suffices to ensure that fluid passes via the conduits 98, whilst at higher vehicle speeds the valve 65 opens and its peak-limiting flow is added to the throttling flow of the shock absorber 31. The throttling peak is clearly higher than that of the curve A, and the curve B shows that the force necessary for opening the valve 65 is likewise much greater than that of the known prior valves (curve A), thus preventing the harmful phenomenon of tailgating explained above.

3 - Operation of the peak-limiting valve 65 under expansion (Figure 8)

In this case, a sudden hydraulic pressure peak occurs within the slide 68 after the vehicle has passed over a hump. The pressure is exerted on the bottom 83 of the cover 82 and then on the seat 91 of the sleeve 69 as a result of an annular passage gap 40 reserved between the end part 79 of the sleeve 69 and the bottom 83. Since the annular cross-section of the seat 91 is greater than that of the seat 77, on which the same pressure is exerted, between the ends 73 and 76 of the sleeve 69 and of the slide 68, the differential pressure thus generated at the seat 91 moves the latter away from the edge 90, whereas the seat 77 remains laid against the edge 78. The sleeve 69 slides and drives the slide 68 up against the annular end of the body 66. Because of this, the hydraulic fluid enters the chambers 89, the ports 88 and the chambers 80 and from there flows into the hydraulic chamber via the conduits 92.

At the same time, another fraction of the fluid flows from the conduits 96 into the conduits 93 via the open gap between the body 66 and the sleeve 69 and from there into the conduits 92 via the ports 88, whilst the throttling flow of the fluid flows via the conduit

98, the receptacle 99 and the inserts 37a, at the same time moving these away from the deflector 49.

Most of the peak-limiting flow of the valve 65 passes laterally via the conduits 96, 93, the chambers 89 and the ports 88 and not between the cover 82 and the end 79 of the sleeve 69.

The valve 65 absorbs the surplus of the throttling flow of the shock absorber 31, and this surplus flows through the conduits 98.

The part of the curve B of Figure 13 corresponding to negative abscissae shows that the force necessary for opening the valve 65 under expansion is first slightly less than the corresponding force for a curve A and then decreases rapidly beyond a speed of 1 m/s up to approximately 5 m/s, and this means that, immediately after the vehicle has passed over a hump, the wheel or roller associated with the suspension element falls again much more quickly than with a prior valve (curve A), thus preventing the abovementioned jolt when the body of the vehicle comes to rest on the suspension element again.



CLAIMS

1. Shock absorber (31) for a hydropneumatic suspension element (1, 12) of a vehicle, especially a heavy vehicle, comprising a disk (32) fastened in an outer casing (34) having ports (30, 38) for the passage of the hydraulic fluid on either side of the disk, means (48, 49, 37a, 37b) allowing this passage in only one direction for some ports (30) and in the opposite direction for the other ports (38), and elements (53, 54, 55) for fastening the said means to the disk, characterized in that the abovementioned means comprise, mounted on the two opposite faces of the disk (32), stacks (46, 47) of elastically flexible metal washers (46a-46c; 47a-47c) arranged in rigid annular deflectors (48, 49) located opposite the hydraulic-fluid passage ports (30, 38).

2. Shock absorber according to Claim 1, characterized in that each port (38, 30) is delimited by a tubular insert (37a, 37b) fastened in a bore (36) passing right through the disk (32), some (37a) of the inserts being equipped with end collars (39) projecting on one face of the disk, whilst the other inserts (37b) are equipped with end collars (41) projecting on the opposite face of the disk, and the dimensions of these projecting collars (39, 41) are such that the deflectors (48, 49) are held elastically up against the said collars (41, 39), thereby shutting off the corresponding inserts (37b, 37a), as long as the hydraulic pressure is insufficient to move the deflectors away from the associated collars.

3. Shock absorber according to Claim 2, characterized in that the ends of the tubular inserts (37a, 37b) opposite their projecting collars (39, 41) open into recesses (42, 43) made in the corresponding face of the disk (32), opposite the deflector (48, 49) mounted on the said face.



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4. Shock absorber according to Claim 3, characterized in that it possesses a screw (53) passing axially through the disk (32), and annular members (54, 55) intended for retaining the stacks (46, 47) of washers and the deflectors (48, 49) which are provided on each side of the disk (32), these annular members (54, 55) themselves being held against the washers (46a-46c, 47a-47c) at the two opposite ends of the axial screw (53).

5. Shock absorber according to one of the claims 2 to 4, characterized in that each deflector (48, 49) bears against the end collars (41, 39) of the inserts (37b, 37a) by means of the annular surface of a radial ring (52) of the said deflector, and the thickness of the wall of the tubular inserts, equal to the width of the said annular surface, is set between limits effectively allowing the deflector (48, 49) to move away from and keep away from the associated collar (41, 39) as long as the hydraulic pressure remains sufficient, at the same time preventing bruising of the said collar.

6. Shock-absorbing and peak-limiting device for a hydrodynamic vehicle suspension element, characterized in that it is formed by the combination of a shock absorber according to one of the claims 1 to 5 and a bi-directional quick-opening peak-limiting valve (65).