

Hydrogen Torch

BACKGROUND OF THE INVENTION

In the manufacture of semiconductor devices, the surface of the silicon wafer must often be oxidized to form a silica layer on the surface. One conventional manner of achieving this is to place the wafer in a heated, uncontaminated container called a process tube and inject a highly pure water vapor into the process tube. The pure water vapor contacts and reacts with the surface of the wafer to produce the desired silica layer.

The pure water vapor is typically created by a hydrogen torch system housed either within or outside of the process tube. Figures 1 and 2 present prior art monolithic torches having a hydrogen inlet A and outlet B, and an oxygen inlet C and outlet D. This system delivers oxygen and hydrogen in separate streams into the process tube (or external combustion chamber), wherein these gases are mixed at temperatures above about 600°C. The high temperature mixing produces a controlled combustion which reaches temperatures of at least about 1200°C to form water vapor.

Some conventional hydrogen torches are complicated monolithic silica tubes. However, the temperature at the exit of the hydrogen delivery tube often reaches at least about 1200°C. The severity of this temperature combined with the steam atmosphere in the combustion chamber causes the typical silica delivery tube to disintegrate, initially releasing silica particles which can contaminate the semiconductor manufacturing process and eventually causing the tube to lose both dimensional and structural integrity (thereby degrading its ability to properly deliver the hydrogen).

Another family of hydrogen torches has been developed which addresses the need for performance under such extreme environmental conditions. In particular, silicon carbide torches which can tolerate the high temperature, corrosive environment of the water vapor are now available. However, relative to silica, silicon

carbide is more difficult to manufacture in complex shapes and is therefore more expensive to make.

Accordingly, there is a need for a hydrogen torch which can operate in an extreme environment at reasonable cost and is easily manufactured.

SUMMARY OF THE INVENTION

In accordance with the present invention, there is provided a fluid delivery system for combining two reactive fluids comprising inner and outer fluid delivery tubes, wherein;

- a) the outer tube comprises a first material, and
- b) the inner tube comprises a second material.

In preferred embodiments, the first and second materials are fused silica and silicon carbide, respectively, and are connected together by a reverse ball joint connection.

DESCRIPTION OF THE FIGURES

Figure 1 is a prior art hydrogen torch design typically used for silica monolithic designs.

Figure 2 is another prior art hydrogen torch design typically used for silica monolithic designs.

Figure 3 presents one embodiment of the hydrogen torch of the present invention.

Figure 4 presents a hydrogen torch of the present invention connected to a process tube.

Figure 5 presents an embodiment of a reverse ball joint connection.

DETAILED DESCRIPTION OF THE INVENTION

The torch of the present invention provides a heat resistant material, such as silicon carbide, in the regions of the system where high temperature resistance is important, and silica in the regions of the system where ease of fabrication is important. Accordingly, the torch of the present invention is easier to manufacture (and so is cheaper) than the monolithic silicon carbide torch and more durable than the silica monolithic torch, yet possesses the drawbacks of neither.

The second material comprising the inner tube should

be able to withstand a water vapor containing environment of at least about 1200°C without significant degradation. It should be gas tight and consist essentially of either high purity silicon carbide impregnated with silicon, high purity silicon carbide coated with CVD silicon carbide, or monolithic CVD silicon carbide. Preferably, the silicon carbide is CRYSTAR (TM) recrystallized silicon carbide, available from the Norton Company of Worcester, MA.

It is also contemplated that other heat resistant ceramic materials such as silicon nitride and silicon oxynitride can be substituted into the inner tube either as a monolith or as a coating. In some embodiments, the inner tube comprises a base ceramic material and a coating thereon, wherein the coating is either more pure or more temperature resistant than the base ceramic material.

The first material comprising the outer tube can be any silica which is easily formed, is of high purity and can withstand a water vapor-containing environment of at least about 600°C without significant degradation. Preferably, the first material is a glass. More preferably, it is fused silica.

In one preferred embodiment, as presented in Figure 3, the torch comprises a silicon carbide tube 1 and two silica tubes 2 and 3. Attachment of these pieces is achieved by the use of a double-sided ball joint connection 4 which holds the silicon carbide tube 1 in proper position with respect to the silica tubes 2 and 3 and provides sealing for separation of the different gases flowing through the system. This ball joint connection 4 comprises a silicon carbide ball section 5 (which is integral with silicon carbide tube 1) held between two opposing female silica sockets 6 and 7 (which are integral with silica tubes 2 and 3). The first silica tube 2 has an inlet 14 to accommodate the flow of oxygen gas therethrough and is large enough to allow passage of the silicon carbide tube 1 with enough

clearance that oxygen can flow through the annulus defined by the inside diameter of the first silica tube 2 and the outside diameter of the silicon carbide tube 1. At the opposite end 8 of the first silica tube 2 is another female socket to allow connection to a process tube (not shown) in which the desired combustion will occur. The second silica tube 3 has an inlet 14 to accommodate the flow of hydrogen gas therethrough. In some embodiments, a thermocouple 13 is also housed with the torch.

Referring now to Figure 4, the silicon carbide tube 1 has a length which allows it to extend through the first silica tube 2 and into a process tube 11 so that the hydrogen emerging from the tip end 9 of the silicon carbide tube 1 is properly located within the process tube 11. For ease of assembly, the outside diameter of silicon carbide tube 1 and tip end 9 should be able to pass through the first silica tube 2. Various conventional configurations may be used at the tip end 9 to control and direct the flow of the exiting hydrogen gas.

Due to the small size of the silica tube leading to the ball joint connection as well as the flow of room temperature gases on each side of the ball joint connection 4, the temperature at the silicon carbide ball 5 at the ball joint connection 4 will typically be less than about 300°C.

In some embodiments, the silicon carbide tube 1 has a 13 mm OD, an 8 mm ID and a 300 mm length; the silica tubes 2 and 3 have 20 mm OD's, 15 mm ID's and 50 mm lengths; and the ball joint connection 4 is 28/15, i.e., a 28 mm diameter spherical surface with a 15 mm ID clearance.

The connective ends of the present invention (e.g. element numbers 5,6,7,8,12 and 14 of Figure 3) can be designed for any typical connection commonly used in the semiconductor manufacturing industry. For example, the connectors can be of the ball, socket, taper, or flange

variety and may be constructed by conventional methods. Preferably, ball joint connections are held together with standard metal clamps. Although Figures 3 and 4 appear to show space between the SiC ball and silica sockets, it is understood these connectors are precision ground so that fluid will not pass through the connection. O-rings may be used to enhance the seal of the ball joint connection, if desired.

Figures 3 and 4 disclose a novel means for connecting dissimilar materials SiC tube 1 and silica tube 2, termed a "reverse ball joint connection". Therefore, also in accordance with the present invention, there is provided a reverse ball joint connection defining a multi-fluid delivery system. Referring now to Figure 5, this reverse ball joint connection comprises:

- a) a first component 50 comprising:
 - i) a first tube 51 having a first end 53, and
 - ii) a first hollow hemispherical projection 52 opening outwardly from the first end 53, and
 - b) a second component 54 comprising:
 - i) a second tube 55 having a first end 56,
 - ii) a second hollow hemispherical projection 58 opening outwardly from the first end 56 of the second tube 55, and
 - iii) a third tube 57 in fluid connection with the second tube 55,
- said second tube 55 having a larger diameter than and essentially concentric with the first tube 52, the first tube 52 being fitted within the second tube 55 such that the convex surface of the first projection 55 forms a reasonable seal with the concave surface of the second projection 58.

In contrast to the conventional ball joint connection, the reverse ball joint connection of the present invention defines an annulus between the tubes suitable for the introduction of a second fluid which can flow within the annulus isolated from fluid flowing

within the inner tube.

Any conventional means for fabricating the silica and silicon carbide components of the present invention may be suitably used.

5 For example, the casting of bimodal silicon carbide slips in plaster molds as disclosed in US Patent No. 3,951,587 ("the Alliegro processes") may be used to make siliconized silicon carbide tubes. However, when the desired SiC tube is small (i.e., less than about 20 mm in
10 diameter and/or less than about 3 mm in wall thickness), novel techniques have been identified which more reliably achieve these goals.

In particular, there is now provided in accordance with the present invention a drain cast, recrystallized
15 silicon carbide ceramic having a wall thickness of between about 0.75 and about 3 mm and a room temperature, 4 point flexure strength of at least about 250 MPa, preferably at least about 290 MPa. More preferably, the ceramic also possesses a 1200°C 4 point flexural strength
20 of at least about 300 MPa, most preferably at least about 375 MPa. In some preferred embodiments, this novel ceramic is made by a process comprising the steps of:

- a) preparing a plaster mold,
- b) coating the mold with a casting retardant,
- 25 c) filling the coated mold with a silicon carbide slip having a bimodal grain size distribution,
- d) dewatering the slip through the mold to produce a casting having a thickness of between about 0.75 and about 3 mm.

30 For the purposes of the present invention, a "drain cast" SiC ceramic includes products made by drain casting, slip casting or pressure casting, wherein the products possess a relatively smooth surface and isotropic grain orientation. Accordingly, "drain cast"
35 products do not include injection molded SiC ceramics, which are characterized by striations along the surface of the extrudate and preferential grain orientation. Similarly, a "recrystallized" SiC ceramic contains

essentially no free carbon and does not include SiC ceramics in which carbon green bodies have been reaction sintered with silicon and so contain unreacted free carbon or silicon.

5 It has been unexpectedly found that when an ammonium alginate coating is applied to the plaster mold prior to introduction of the slip, a thin wall casting having suitable strength may be made. It is known in the art that a primary concern in casting is the achievement of
10 high density. High density castings (i.e., about 85% of theoretical density) are typically achieved by using a bimodal slip, wherein the fine grains (typically 2-3 microns) fill in the voids created by the packing of the coarse grains (typically about 50 microns). However, it
15 is also known that plaster of paris molds are frequently very porous (i.e., they contain pores which are 2-3 microns in diameter). Therefore, without wishing to be tied to a theory, it is believed that the porous plaster's high porosity deleteriously affected the
20 casting of such bimodal slips in two ways. First, capillary forces generated by the interaction of the slip and the porous plaster yielded an excessively fast casting rate (i.e., a casting having a 1 mm wall would cast in about 0.5 minutes). This excessive casting rate
25 prevented the proper ordering of the bimodal slip at the casting front, resulting in non-uniform microstructure through the thickness of in the casting. Second, because of the initial fast casting rate, the SiC fines are drawn to the slip-plaster interface, resulting in a casting
30 surface predominated by the fine fraction. This second phenomenon is believed to be the cause for the orange peel appearance of the prior art castings.

 Without wishing to be tied to a theory, it is believed that when the casting retardant coats the highly
35 porous plaster mold surface, it reduces its effective porosity and permeability, thereby slowing the casting rate, promoting an ordered casting and increasing cast density. Its also retards the penetration of the fines

fraction into the mold, thus allowing the fines to be retained in the casting, resulting in a smooth finish and, therefore, in easy mold release.

The casting retardant may be any coating which reduces the porosity of the porous plaster. Preferably, it is ammonium or sodium alginate or polyacrylic acid. More preferably, it is ammonium alginate. Typically, it is applied as an aqueous solution in an amount of between about 0.01 and about 1.0 w/o of the solution, preferably about 0.03 w/o.

The plaster mold of the present invention can be any mold typically used in the casting art. Preferably it is plaster of paris and has channels (pores) of about 2 microns in size. Preferably, it has a 60% consistency.

The slip of this aspect of the present invention typically comprises a bimodal distribution comprising between about 45 and about 55 w/o coarse SiC grains with a particle size ranging from 10 to 100 microns ("the coarse fraction"), and between about 45 and about 55 w/o of a fine SiC grain with a size distribution of between 1 and 4 microns ("the fine fraction"). Preferably, the fine fraction has an average particle size of about 2-3 microns and the coarse fraction has an average particle size of about 60 microns.

Other components of the slip include conventional additives such as deflocculating agents like NaOH, NH₃OH and Na₂SiO₃; water present in an amount of from about 12 to 16 w/o solids; and acrylic binder present in the range from about 0.25 to 1.0 w/o solids.

In one especially preferred embodiment, a silicon carbide mixture consisting of about 48 w/o F240 sized green silicon carbide having an average size of about 60 microns and about 52 w/o green silicon carbide having an average size of 2-3 microns is prepared. To this mixture is added a deflocculating agent (NaOH) in an amount sufficient to achieve optimum deflocculation. Water is then added to provide a viscosity of between about 500 and about 750 cps. An acrylic latex binder is also added

in an amount of about 0.25 w/o of the solids. These components are mixed in a ball mill which has been evacuated to vacuum level of between about 27 and 30 inches Hg and rolled for at least about 17 hours.

5 Concurrently, a plaster mold with a 70% consistency is coated with a 0.03% solution of ammonium alginate. The mold is capped off at the bottom and the alginate solution is poured in to fill the cavity. Solution is continually added as the mold absorbs the solution.

10 After the mold has been filled with alginate for 3 minutes, the cap is removed and the solution drained.

 The drained mold is allowed to air dry for 10 minutes prior to introduction of the slip. The mold is recapped and the slip is poured into the cavity. Casting
15 time is dependent on both desired wall thickness and slip viscosity. At a desired viscosity of 750 cps and required nominal wall thickness of about 1.5 mm, the slip is allowed to remain in the mold 4-6 minutes prior to removing the cap.

20 After the slip has been drained from the mold, a small amount of de-ionized water is poured down the cavity to insure a lump free drained surface. The cast part is allowed to dry in the mold for 20-30 minutes. After that time, the mold is disassembled and the torch
25 is removed by using an appropriate stripping fixture. This fixture simulates the outside shape of the cast part enabling it to remain dimensionally correct during drying.

 The cast part is then allowed to air dry overnight
30 or oven dry at about 54°C for a minimum of 2 hours prior to green finishing. The dried alginate skin is removed from the cast part, the cast part is cut to length and any final finishing is performed.

 The cast part is now ready to be fired. The initial
35 firing step is conducted in a furnace which is heated to a temperature of about 1950°C under a vacuum of about 0.5 torr in Ar atmosphere. After this initial firing, the cast part is prepared for one of two possible final

firing steps which is dependent on part size and intended application. This second firing step consists of either impregnating with silicon to eliminate porosity or CVD coating with silicon carbide. After this second firing, the part is machined to its final dimension.

Silicon carbide ceramics having outside diameters of between about 4 and about 20 mm, preferably about 6 mm, and wall thicknesses between about 0.75 and about 3.0 mm, preferably about 1 mm are obtainable in accordance with this invention. Because the casting is sufficiently slow, ordered casting is promoted, the typically rough "orange peel" type drain cast surface is eliminated and a casting having a smooth surface is produced.

A cast, unfired body produced in accordance with the above especially preferred embodiment exhibits a bulk density of at least about 2.75 g/cc and a four point bending strength of at least about 7 MPa. Its pore size ranges from about 0.1 to 4.0 microns. Its average pore size is about 0.4 microns. In contrast, the conventional cast unfired, SiC body has an average pore size of about 1.8 microns.

Physical and mechanical analyses were undertaken on the siliconized silicon carbide product produced in accordance with the especially preferred embodiment of the present invention. Flexural strength testing was undertaken on 4 point quarter point fixtures having an upper span of 20 mm and a lower span of 40 mm. The flexure bar, whose dimensions were 3 mm x 4 mm x 50 mm, was flexed at a load rate of about 0.02 inches per minute. The room temperature flexural strength was found to be about 296 MPa. This represents a 38% increase in strength over the conventional siliconized silicon carbide product. The 1200°C flexural strength was found to be about 375 MPa, a 60% increase in strength over the conventional siliconized silicon carbide product. In addition, analysis of the variation in wall thickness was measured. The variation in thickness of a 1 mm wall of the present invention was found to be about 0.2 mm/m,

i.e., the thickness varied from about 0.9 to about 1.1 mm (top to bottom) over a 1 meter length. In contrast, the conventional siliconized silicon carbide ceramic possessed a variation of about 0.6 mm/m.

- 5 The novel recrystallized silicon carbide ceramics of the present invention may be used in conventional siliconized silicon carbide or CVD coated silicon carbide applications, including those applications disclosed in US Patent No. 3,951,587.



We claim:

1. A fluid delivery system for combining two reactive fluids comprising inner and outer fluid delivery tubes, wherein;
 - 5 a) the outer tube comprises a first material, and
 - b) the inner tube comprises a second material.
2. The system of claim 1 wherein the outer tube consists essentially of the first material.
3. The system of claim 2 wherein the first material is
10 a ceramic material.
4. The system of claim 2 wherein the first material is a glass.
5. The system of claim 2 wherein the first material is fused silica.
- 15 6. The system of claim 1 wherein the inner tube comprises silicon carbide.
7. The system of claim 1 wherein the inner tube consists essentially of silicon carbide.
8. The system of claim 1 wherein the outer tube is
20 fused silica and the inner tube comprises silicon carbide.
9. The system of claim 1 wherein the fluid delivery system is a hydrogen torch.
10. The system of claim 6 wherein the fluid delivery
25 system is a hydrogen torch.
11. The system of claim 8 wherein the fluid delivery system is a hydrogen torch.
12. The hydrogen torch of claim 11 wherein the inner tube consists essentially of silicon carbide.
- 30 13. The hydrogen torch of claim 9 wherein the inner tube consists essentially of a material selected from the group consisting of high purity silicon carbide impregnated with silicon, high purity silicon nitride, monolithic CVD silicon carbide, and high
35 purity silicon carbide coated with CVD silicon carbide.



14. The hydrogen torch of claim 9 wherein the inner tube has a first and a second end, and further comprising a third tube in fluid connection with the first end of the inner tube.
- 5 15. The hydrogen torch of claim 14 wherein the third tube is silica.
16. The hydrogen torch of claim 14 wherein the first end of the inner tube possesses a connector selected from the group consisting of a ball, a socket, a
10 taper, and a flange.
17. The hydrogen torch of claim 14 wherein the fluid connection is accomplished by a reverse ball joint connection.
18. The hydrogen torch of claim 17 wherein the outer
15 tube has a first and second end, the first end of the outer tube forming a sealing connection with the first end of the inner tube, and the second end of the outer tube adapted to form a fluid connection with a process tube.
- 20 19. The hydrogen torch of claim 18, wherein the outer tube has a first fluid inlet and the second silica tube has a second fluid inlet.
20. The hydrogen torch of claim 11 wherein the inner
25 tube comprises a base ceramic material and a coating thereon.
21. The hydrogen torch of claim 20 wherein the coating is selected from the group consisting of silicon nitride and silicon carbide.
22. The hydrogen torch of claim 20 wherein the base
30 ceramic material is selected from the group consisting of silicon nitride and silicon oxynitride.
23. A reverse ball joint connection comprising:
a) a first component comprising:
35 i) a first tube having a first end, and
ii) a first hollow hemispherical projection opening outwardly from the first end, and
b) a second component comprising:



- i) a second tube having a first end, and
 - ii) a second hollow hemispherical projection opening outwardly from the first end of the second tube,
- 5 said second tube having a larger diameter than and essentially concentric with the first tube, the first tube being fitted within the second tube such that the convex surface of the first projection forms a seal with the concave surface of the second projection.
- 10 24. The reverse ball joint connection of claim 23 wherein the first and second components are made from different materials.
25. The reverse ball joint connection of claim 23 wherein the first component comprises silicon
- 15 carbide.
26. The reverse ball joint connection of claim 23 wherein the second component comprises silica.
27. The reverse ball joint connection of claim 25 wherein the first component consists essentially of
- 20 siliconized silicon carbide.
28. The reverse ball joint connection of claim 26 wherein the second component consists essentially of silica.
29. The reverse ball joint connection of claim 23
- 25 wherein the first component consists essentially of siliconized silicon carbide and the second component consists essentially of silica.
30. A drain cast silicon carbide ceramic having a wall thickness of between about 0.75 and about 3 mm and a
- 30 room temperature flexural strength of at least about 250 MPa.
31. The ceramic of claim 30 having a wall thickness variation of less than about 0.2 mm/m.
32. The ceramic of claim 31 in the shape of a tube
- 35 having an outer diameter of between about 4 mm and about 20 mm.
33. The ceramic of claim 30 having a room temperature flexural strength of at least about 290 MPa.



34. The ceramic of claim 30 having a CVD silicon carbide coating.
35. The ceramic of claim 30 impregnated with silicon.
- 5 36. The ceramic of claim 33 having a density of at least about 3.02 g/cc.
37. The ceramic of claim 33 having a bimodal SiC grain distribution comprising a fine fraction of between about 2 um and about 3 um and a coarse fraction of about 60 um.
- 10 38. The ceramic of claim 30 having a wall thickness of about 1 mm.
39. The ceramic of claim 31 in the shape of a tube having an outer diameter of about 6 mm.
- 15 40. A recrystallized silicon carbide ceramic having a room temperature flexural strength of at least about 250 MPa.
41. The recrystallized silicon carbide ceramic of claim 40 having a room temperature flexural strength of at least about 290 MPa.
- 20 42. The ceramic of claim 41 having a wall thickness of between about 0.75 and about 3 mm.
43. The ceramic of claim 41 having a wall thickness variation of less than about 0.2 mm/m.
- 25 44. The ceramic of claim 41 in the shape of a tube having an outer diameter of between about 4 mm and about 20 mm.
45. The ceramic of claim 41 having a room temperature flexural strength of at least about 290 MPa.
- 30 46. The ceramic of claim 41 having a CVD silicon carbide coating.
47. The ceramic of claim 41 impregnated with silicon.
48. The ceramic of claim 41 having a density of at least about 3.02 g/cc.



49. The ceramic of claim 41 having a bimodal SiC grain distribution comprising a fine fraction of between about 2 μm and about 3 μm and a coarse fraction of about 60 μm .
- 5 50. The ceramic of claim 41 in the shape of a tube having an outer diameter of about 6 mm.
51. A recrystallized silicon carbide ceramic having a 1200°C flexural strength of at least about 300 MPa.
- 10 52. The ceramic of claim 51 having a 1200°C flexural strength of at least about 375 MPa.
53. The ceramic of claim 52 having a wall thickness of between about 0.75 and about 3 mm.
54. The ceramic of claim 52 having a wall thickness variation of less than about 0.2 mm/m.
- 15 55. The ceramic of claim 54 in the shape of a tube having an outer diameter of between about 4 mm and about 20 mm.
56. The ceramic of claim 52 having a room temperature flexural strength of at least about 250 MPa.
- 20 57. The ceramic of claim 52 having a CVD silicon carbide coating.
58. The ceramic of claim 52 impregnated with silicon.
59. The ceramic of claim 52 having a density of at least about 3.02 g/cc.
- 25 60. The ceramic of claim 52 having a bimodal SiC grain distribution comprising a fine fraction of between about 2 μm and about 3 μm and a coarse fraction of about 60 μm .
- 30 61. The ceramic of claim 52 having a wall thickness of about 1 mm.
62. The ceramic of claim 52 in the shape of a tube having an outer diameter of about 6 mm.
63. A drain cast silicon carbide ceramic having a wall thickness variation of about 0.2 mm/m.
- 35 64. The ceramic of claim 63 having a room temperature flexural strength of at least about 290 MPa.



65. The ceramic of claim 63 in the shape of a tube having an outer diameter of between about 4 mm and about 20 mm.
- 5 66. The ceramic of claim 63 having a flexural strength of at least about 375 MPa at 1200°C.
67. The ceramic of claim 63 having a CVD silicon carbide coating.
68. The ceramic of claim 63 impregnated with silicon.
- 10 69. The ceramic of claim 63 having a density of at least about 3.02 g/cc.
70. The ceramic of claim 63 having a bimodal SiC grain distribution comprising a fine fraction of between about 2 um and about 3 um and a coarse fraction of about 60 um.
- 15 71. The ceramic of claim 63 having a wall thickness of about 1 mm.
72. The ceramic of claim 63 in the shape of a tube having an outer diameter of about 6 mm.
- 20 73. A drain cast silicon carbide ceramic having a wall thickness of between about 0.75 and about 3 mm and a 1200°C flexural strength of at least about 300 MPa.
74. The ceramic of claim 73 a 1200°C flexural strength of at least about 375 MPa.
- 25 75. The ceramic of claim 74 having a wall thickness variation of less than about 0.2 mm/m.
76. The ceramic of claim 74 in the shape of a tube having an outer diameter of between about 4 mm and about 20 mm.
- 30 77. The ceramic of claim 74 a room temperature flexural strength of at least about 250 MPa.
78. The ceramic of claim 74 having a CVD silicon carbide coating.
79. The ceramic of claim 74 impregnated with silicon.
- 35 80. The ceramic of claim 74 having a density of at least about 3.02 g/cc.



81. The ceramic of claim 74 having a bimodal SiC grain distribution comprising a fine fraction of between about 2 um and about 3 um and a coarse fraction of about 60 um.
- 5 82. The ceramic of claim 74 having a wall thickness of about 1 mm.
83. The ceramic of claim 74 in the shape of a tube having an outer diameter of about 6 mm.
84. A cast, unfired silicon carbide body having an average pore size of about 0.4 um.
- 10 85. A process comprising the steps of:
- a) preparing a plaster mold,
 - b) coating the mold with a casting retardant,
 - c) filling the coated mold with a silicon carbide slip having a bimodal grain size distribution,
 - 15 d) dewatering the slip through the mold to produce a casting having a thickness of between about 0.75 and about 3 mm.
86. The process of claim 85 wherein the casting retardant is selected from the group consisting of ammonium alginate, sodium alginate and polyacrylate acid.
- 20 87. The process of claim 85 wherein the casting retardant is ammonium alginate.

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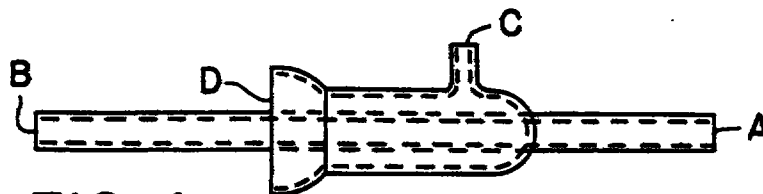


FIG. 1
PRIOR ART

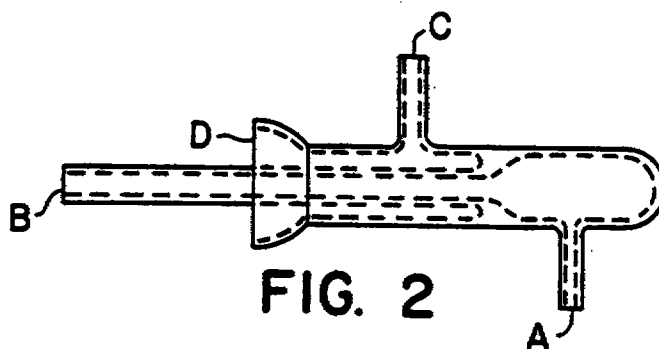


FIG. 2

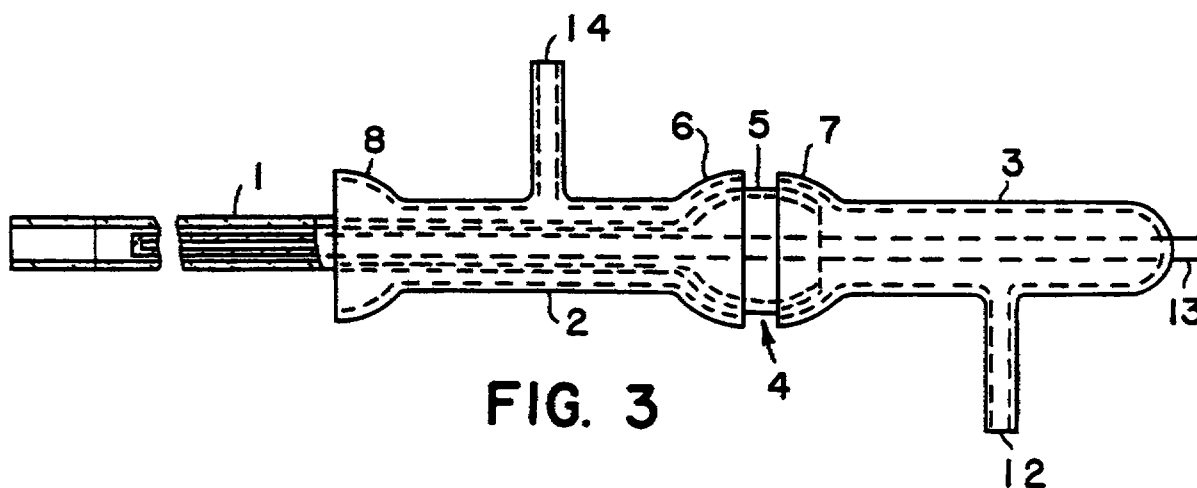
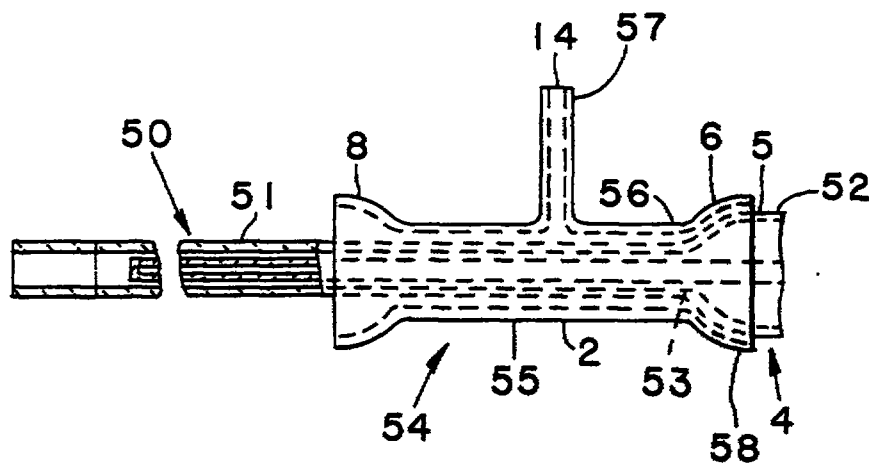
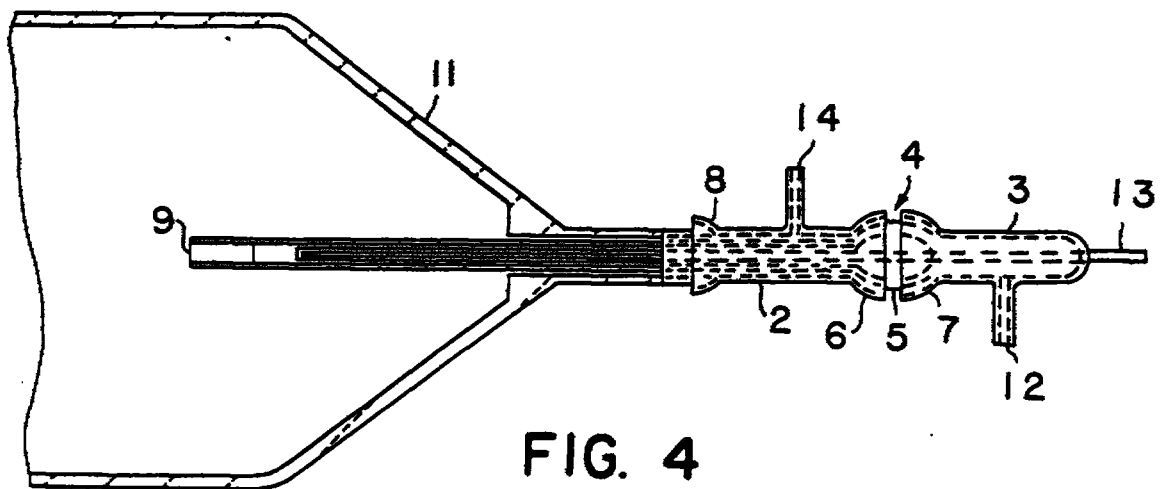


FIG. 3

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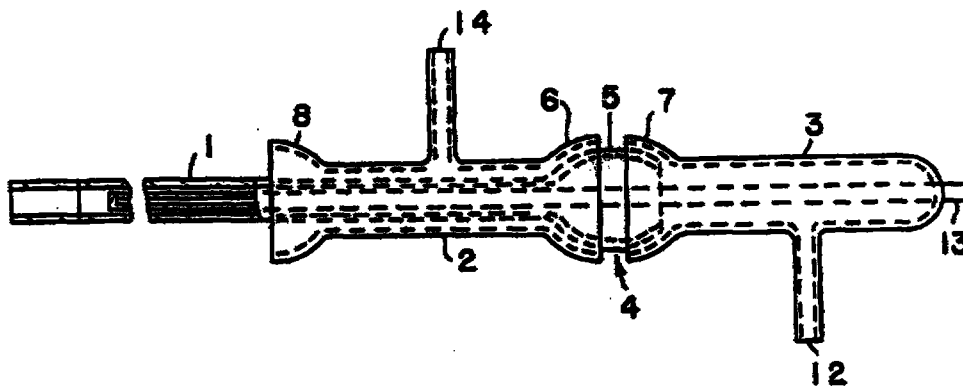




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(54) Title: HYDROGEN TORCH



(57) Abstract

A hydrogen torch comprising concentric inner (1) and outer (3) fluid delivery tubes, wherein: a) the outer tube (3) comprises silica, and b) the inner tube (1) comprises silicon carbide.

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ES	Spain	ML	Mali	US	United States of America
FI	Finland	MN	Mongolia	UZ	Uzbekistan
FR	France			VN	Viet Nam
GA	Gabon				

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