

CLINCH PIN FASTENER

RELATED APPLICATION

This patent application is related to provisional patent application serial number 61/254,467 entitled "Clinch Pin Fastener" filed on October 23, 2009, priority from which is hereby claimed.

FIELD OF THE INVENTION

The present invention relates to fasteners which attach to metal panels by the cold flow of panel material around the fastener. This type of fastener is generally referred to as a clinch-type fastener.

BACKGROUND OF THE INVENTION

Clinching fasteners are retained in the plates into which they are installed by a displacer feature of the fastener which is followed by an undercut directly beneath it. When pressed into a properly sized hole, metal from the edge of the hole is forced by the displacer to flow into the undercut around the circumference of the fastener. When a clinching or clinch-type stud is manufactured, typically a head and displacer are forged into a pin blank. The undercut is then rolled into the part in a secondary operation. Often, at the same time the threads are rolled onto the body of the pin. When threads are not necessary, the undercut still requires the secondary operation which also incurs the additional cost of cleaning the part. There is therefore a need in the art for forming a clinch-type fastener that includes all the necessary operative features without requiring a secondary operation.

SUMMARY OF THE INVENTION

In order to meet the above-described need in the art, the present invention eliminates secondary formation operations of a clinch-type fastener by creating an undercut during the same forging operation that creates the head and the displacer. Other features that are formed in the present fastener at the same time as the undercut are a tapered point and a tangential interference band provided by a curvilinear shaped bulge in the shank. The configuration of these elements according to the present invention are of paramount importance for fastening pins in the range of 1 millimeter in diameter because very small clinching features require a very tight tolerance to be held for the displacer diameter and height as well as the undercut diameter and shank diameters. The present clinching pin described herein includes a tangential interference band and a tapered point which work together to guide the part through a very small diameter hole in the attached plate while creating a slight interference fit between the hole and the fastener at the interference band diameter only. This creates minimal stresses in the plate while eliminating any tolerance between the inner wall of the hole and the outer diameter of the clinching pin.

More specifically, the Applicant has invented a unitary metal fastener having a top most head that is the largest diameter of the fastener. A shoulder extends axially downward immediately below the head and includes an annular bottom displacer surface for displacing material into which the fastener is installed. A barrel-shaped shank is located immediately below the displacer surface and forms the upper boundary of an undercut located at the juncture of the shank and the shoulder. An outwardly divergent tapered arcuate surface of a top portion of the shank extends downwardly from the undercut. The barrel-shaped shank has a midline bulge forming an interference band along the surface of the shank and is the largest diameter of the

shank. Extending downward from the interference band is a convergently tapered surface of the shank extending downward to a bottom end of the fastener.

The method of forming the above-described fastener comprises cold-forging a fastener blank having a head, a shoulder and a shank of reduced diameter. The blank is compressed end-to-end between a top die and a bottom die whereby the axial compression of the blank causes the outward bulging of the shank at its midline. Compression is continued until an undercut is formed between an annular surface of the shoulder and the bulge. The bottom die includes a cone-shaped pocket having a divergent side surface angle of 30° and a bottom pressing surface including a centered upwardly extending projection. The length of the fastener blank shank is within a selected slenderness ratio range such that said fastener bulges when formed and does not buckle during the step of compressing the fastener blank.

In one embodiment, the present invention is used to form an assembly of parts including a panel having an aperture and a plate located in face-to-face relationship with the panel. The plate has an aperture in alignment with the aperture of the panel. The shank of the fastener becomes rigidly affixed to the plate by the cold flow of plate material into the undercut caused by pressing a displacer surface of the shoulder against the plate as said fastener is passed through said panel aperture and into the plate aperture.

As such, those skilled in the art will appreciate that the conception upon which this disclosure is based may readily be utilized as a basis for the designing of other structures, methods, and systems for carrying out the several purposes of the present invention.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a bottom right isometric view of the clinch fastener of the invention.

FIG. 2 is a two-part diagrammatic view of the forging operation utilized to create the invention.

FIG. 3 is a two-part side sectional view showing the before and after sequence of installation of the invention.

FIG. 4 comprises a two-part front elevation sectional view of the invention showing a sequence of installation.

DESCRIPTION OF THE PREFERRED EMBODIMENT

Referring now to Figure 1, the present clinching pin is a forged metal part having a head 11, a displacer shoulder 13 and an undercut 15 that receives a cold flow of metal from the plate into which the part is pressed. It further includes a tapered tip 16 and a circumferential interference band 18 along the greatest diameter of its barrel-shaped shank. As will be described further below, all features of this pin are created in one forming operation. Typically, this part is used to hold two sheets of material together. A top panel can be captivated beneath the head of the pin while the body of the pin is clinched into the bottom plate.

Referring now to Figure 2, the present fastener is formed using well known cold forging equipment which includes a top die 21 and a bottom die 23 as shown. The head and displacer are formed first as in any heading operation for the creation of a standard bolt or screw. As shown in this figure, the body of the fastener is then formed by compressing the pin between its head and tip. The bottom die 23 includes a cone-shaped tool 26 which is used to form the shank body 25. The tool has an included angle of 30 degrees for easy release from the part. As depicted in the lower illustration, the forming tool presses on the end of the part causing it to form a bulge 18

above the tool. The original diameter of the pin remains relatively constant at the interface of the pin and the displacer which thus becomes the minor undercut diameter 15.

During the forming operation it is critical that the diameter and length of the pin cause the fastener to yield in compression and not buckle. This condition is designed for, using the slenderness ratio:

$S=L_e/r$ where S is the slenderness ratio, L_e is the effective length of the shank column, and r is the radius of gyration. For a simple cylinder:

$$r=D/4$$

where D is the shank diameter of the pin before forging.

The tack pin forming process can be modeled as a column with the head end fixed and the free end pinned. For this situation:

$$L_e=.707 \times L$$

where L is the actual length of the pin from under the head to the end.

The critical slenderness ratio is defined as:

$$S_{cr}=\sqrt{(2 \times \pi^2 \times E)/(\sigma_y)}$$
 where:

S_{cr} is the critical slenderness

E is the modulus of elasticity for a given material, and

σ_y is the yield stress for a given material.

The length of the pin is maintained such that its slenderness ratio “ S ” is less than the critical slenderness ratio “ S_{cr} ”. This condition guarantees that the pin will bulge when formed and not buckle during the process.

A second design variable for this pin is the ratio of the volume of the displacer to the volume of the undercut. For maximum pull-out performance it is best to completely fill the

undercut of the fastener. To achieve this, the diameter and height of the embedded portion of the displacer are adjusted to cause the volume ratio “VR” of (displacer volume) / (undercut volume) to be greater than 1. The displacer volume is a simple cylinder with a hole in it, and as such its volume is easy to calculate as :

$V_{\text{disp}} = (\pi \times h) \times (r^2 - r_h^2)$, where “r” is the radius of the displacer, r_h is the radius of the installation hole, and “h” is the embedded height of the displacer. The shape of the undercut can be approximated as a circumscribed triangle to calculate its volume, but a more accurate volume can be derived using graphical or computer modeling methods. This formation method is particularly suited to small clinch pins having a diameter in the range of 1.0 mm.

Referring now to Figure 3, when fully formed the present clinch pin has a head 11, a displacer 13, an undercut 15, an interference band 18, and a tapered tip 16. The purpose of the head is to retain panel 10 of any material to a metallic plate 12, much in the way that the head of a nail or a screw retains whatever it is fastening. As shown in the “after” side of this illustration, the displacer lies directly beneath the head of the fastener and consists of two sections. As depicted in this figure, the first section of the displacer comprises the portion directly under the head down to the point where the plate is joined. Thus, there is a portion of the displacer that does not get pressed into the plate. This portion of the displacer remains within the top panel 10 being joined and is very nearly the same height as the thickness of the top panel. As the “after” illustration depicts, the lower portion of the displacer 14 is the portion that is pressed into the plate 12 and displaces material into the undercut directly beneath it. Material that flows into the undercut is trapped above the interference band 18 of the fastener to retain the fastener in the plate.

Referring now to Figure 4, a specific application is shown where the clinch pin of the invention is employed to join three elements, a top panel 31, an intermediate sheet 33 and a bottom plate 35. The intermediate sheet 33 becomes clamped between the top panel and bottom plate when the pin is clinched into the bottom plate. Proper installation of the present clinch pin first requires preparation of the panel, sheet and plate to be joined. The bottom plate 35 must have a hole, in this instance a blind hole 34 that is equal to or slightly less than the diameter of the interference band 18 of the fastener. The top panel 31 must have a hole that is slightly greater than the diameter of displacer 30 and the thickness of the panel must be accommodated in the height of the displacer.

This assembly is created as follows. With the panel, sheet and plate properly prepared, the bottom plate 35 is first placed over an anvil, sheet and the top panel are placed over the bottom plate with the installation holes aligned. The tapered tip of the fastener 36 is then placed through the hole in the top panel and partway down the hole 34 in the bottom plate. Finally, a flat punch 38 is used to press against the head 37 of the fastener driving it downward into the hole until the underside of the head of the fastener contacts the top panel 31 as shown in the lower illustration. The height of displacer 30 is dimensioned so that the undercut 41 is filled with the cold flow of material from lower plate 35 as the underside of the head contacts the top panel. Additional force loading against the head after contact further tightens the joint.

Therefore, the foregoing is considered as illustrative only of the principles of the invention. Further, since numerous modifications and changes will readily occur to those skilled in the art, it is not desired to limit the invention to the exact construction and operation shown and described, and accordingly, all suitable modifications and equivalents may be resorted to, falling within the scope of the invention.

CLAIMS

1. A unitary metal fastener comprising:
 - a top most head, said head being the largest diameter of the fastener;
 - a shoulder extending axially downward from and located immediately below said head,
 - 5 said shoulder including an annular bottom displacer surface for displacing material into which said fastener is installed;
 - a barrel-shaped non-featured smooth shank located immediately below said displacer surface;
 - an undercut located at the juncture of said shank and said shoulder, said undercut being
 - 10 bounded above by said displacer surface and below by an outwardly divergent tapered arcuate surface of a top portion of the shank; and
 - further described in that the length of the fastener shank is within a selected slenderness ratio less than $\sqrt{(2 \times \pi^2 \times E)/(\sigma_y)}$, where E is the modulus of elasticity and σ_y is the yield stress for the shank material.
- 15 2. The fastener of claim 1 wherein said barrel-shaped shank further includes a midline bulge on the surface of said shank having a circumferential interference band, said band being the largest diameter of said shank.
3. The fastener of claim 2 where said shank further includes a convergently tapered bottom portion extending downward from said bulge to a bottom end of the fastener.
- 20 4. The fastener of claim 3 wherein the diameter of said interference band is less than the diameter of said shoulder.
5. The method of manufacturing by cold-forging a free-standing metal fastener comprising:

providing a fastener blank having a head, a shoulder, a solid shank of reduced diameter and a planar bottom end in that order top to bottom;

compressing end-to-end the fastener blank between a top die and a bottom die, which includes a die pocket with a pressing surface at a bottom thereof and an upwardly extending projection oriented coaxially with said fastener, whereby the axial compression of the blank causes the outward bulging of the shank at a midline thereof and the simultaneous inward tapering of the shank from said midline to the bottom end; and

continuing said compression until an undercut is formed continuously between the bulge and the shoulder.

6. The method of claim 5 wherein said bulge is an arcuate surface in the middle of said shank.

7. The method of claim 5 wherein said bottom die includes a cone-shaped pocket for receiving said fastener blank.

8. The method of claim 7 wherein said cone-shaped pocket has a divergent side surface angle of 30°.

9. The method of claim 5 wherein the length of the fastener blank shank is within a selected slenderness ratio range such that said fastener bulges when formed and does not buckle during the step of compressing the fastener blank.

10. An assembly including the fastener of claim 1 comprising:

a panel having an aperture; and

a plate located in face-to-face relationship behind said panel, said plate having a plate aperture in alignment with the aperture of said panel wherein the shank of said fastener is rigidly affixed to said plate by the cold flow of plate material into the undercut caused by pressing said

displacer surface against said panel as said fastener is passed through said panel aperture and then into said plate aperture.

11. The assembly of claim 10 wherein said fastener shank bulge provides an interference fit with said plate.

5 12. The assembly of claim 10 wherein said plate aperture is a blind hole.

13. The assembly of claim 11 wherein the interference fit is between the interference band on said shank bulge and an inner wall of said plate aperture.

14. The method of manufacturing by cold-forging a free-standing metal fastener comprising:
providing a fastener blank having a head, a shoulder, a solid shank of reduced diameter

10 and a planar bottom end in that order top to bottom;

compressing end-to-end the fastener blank between a top die and a bottom die whereby the axial compression of the blank causes the outward bulging of the shank at a midline thereof and the simultaneous inward tapering of the shank from said midline to the bottom end; and

continuing said compression until an undercut is formed continuously between the bulge

15 and the shoulder. The fastener blank being within a selected slenderness ratio less than $\sqrt{(2 \times \pi^2 \times E)/(\sigma_y)}$, where E is the modulus of elasticity and σ_y is the yield stress for the blank material such that said fastener bulges when formed and does not buckle during the step of compressing the fastener blank.

15. The method of claim 5 wherein said bottom die pocket includes a circular pressing
20 surface at the bottom thereof and an upwardly extending projection oriented coaxially with said fastener blank.

16. The method of claim 15 wherein the fastener is a clinch pin having a diameter of approximately 1.0 mm.