

## Description

The present invention relates to a process for manufacturing cones of drilling bits which have hard cutter inserts. More particularly, the present invention is directed to a process of laser hardening the outer shell and certain other surfaces of roller cone bits of the type which also have hard tungsten carbide or like cutter inserts.

One important type of rotary drill bit used for subterranean drilling includes cutter cones which have hard tungsten carbide or like cutter inserts. Usually such cutter cones are rotatably mounted on journal legs of the drill bit so as to rotate as the drill bit is rotated. The drill bit may be rotated from the surface, or by a "downhole" motor. The tungsten carbide or like hard cutter inserts of cutter cones are pressed into insert holes formed in the external surface of the cutter cones. These tungsten carbide inserts bear against the rock formation at the bottom of the hole, crushing and chipping the rock as drilling proceeds.

Because rock drilling is a technically very demanding service, and because failure of a drilling bit can cause very costly interruption in the drilling process, the construction of rock bits must be very rugged. Usually the cones of the drilling bit are made of forged alloy steel, although powder metallurgy and related cones have also been described in the patent and technical literature. Bearing surfaces are located within the interior of the cones to enable rotatable mounting to the journal leg. An effective seal must be provided between the rotating cone and the journal leg so as to prevent escape of lubricating grease from the bearings, and to prevent entry of drilling fluid and other foreign matter in the bearing.

The steel body of the cone itself must be sufficiently ductile and tough so as to avoid fracture or shattering. Certain parts of the interior of the cone, particularly the ball bearing races, must be quite hard in order to provide sufficiently long bearing life. The exterior of the cutter cone ideally should also be quite hard and abrasion resistant so as to avoid rapid wear due to its exposure to the formation, and the highly abrasive and erosive action of the drilling fluid.

The tungsten carbide or other hard inserts in the roller cones must be held sufficiently strongly so as to prevent premature loss. The inserts must also be prevented from rotating in the insert holes, because rotation in the insert hole leads to decreased drilling efficiency and eventually to loss of the insert.

In view of the economic importance of subterranean drilling for oil and other minerals, the prior art has developed a variety of technological approaches to more or less satisfy the above-

summarized requirements.

In accordance with one basic approach, the forged steel cone body is made of a "carburizable" low carbon steel, which however, has sufficient ductility and toughness to be adequately resistant to fracture. Certain parts of the interior of the cone, such as the bearing races, may be carburized to increase their hardness, leaving the exterior of the cone without a hardened case.

Alternatively, the bearing races and the exterior shell of the cone may both be carburized. However, this alternative procedure has not been employed widely, because it is difficult to drill insert holes into the exterior shell through a hardened carburized case. Moreover, the obvious alternative of first drilling the insert holes, and thereafter carburizing the exterior shell, is also impractical because the interior of insert holes should not be carburized. This is because a hardened case in the insert holes would render the wall of the insert holes less ductile and less fracture resistant, and therefore would make press-fitting of the hard inserts into the holes impractical or very difficult. Carburizing also tends to distort drilled holes.

In final analysis, carburizing rotary drilling bit cones is relatively labour consuming, because stop-off paint must be applied to the cone in several areas where hardening by carburization is not desired. Application of stop-off paint becomes particularly laborious, if carburization of the external shell is desired, because in this case the insert holes must be drilled first, and the stop-off paint must be applied to the insert holes as well. Moreover, little can be done to eliminate hole distortion from this high temperature heat treatment. In accordance with some prior art procedures, the exterior of the cone shell is carburized, but the carburized exterior case is removed in a finish machining operation before the insert holes are drilled.

In light of the foregoing difficulties, most roller cones have an exterior shell surface which is not carburized, and have a surface hardness of only approximately 42 Rockwell C (Rc) hardness units. Whereas the alloy steel of these cones is adequately ductile and tough, lack of external shell surface hardness and abrasion resistance results in relatively rapid wear and erosion of the cone shell during drilling, often resulting in loss of tungsten carbide inserts and inadequate bit performance.

Another alternative, described in United States Patent No. 4,303,137 is to selectively heat treat and rapidly quench an interior surface layer of the ball bearing races of the roller cones, so as to form a hard martensitic layer and a hard bearing surface therein. This selective heat treatment may be accomplished by bombardment of the bearing races with a laser beam, as is described in United States Patent No. 4,303,137.

As is apparent from the foregoing, there is still a substantial need in the prior art for a process for substantially hardening, in an economically feasible manner, the exterior shell surface and other surfaces of hard insert bearing roller cones. The present invention provides such a process.

According to the present invention there is provided a process for forming a hard cutter insert bearing cone for a rock bit comprising the steps of: forming a cone blank from a medium to high carbon hardenable steel, the cone blank including an external surface; rendering the external surface of the cone blank dark and absorbent to laser light; forming insert holes for the hard cutter inserts in the external surface of the cone; rendering the hole areas reflective so that the external surface of the cone includes dark, light absorbent surfaces and also reflective surfaces relatively unabsorbent to laser light; after the step of forming insert holes, bombarding the external surface of the cone with a laser beam of sufficient intensity and for sufficient time to austenitize an external layer in the light absorbent external surface of the cone; and cooling the austenitized layer sufficiently rapidly to form martensite in the external layer of the light absorbent external surface, whereby a cone having a hardened external case is obtained with insert holes having non-hardened wall and bottom.

A process for forming a hard cutter insert bearing cone for a rock bit and embodying the present invention will now be described by way of example, with reference to the accompanying diagrammatic drawings, in which:

Figure 1 is a cross-sectional view of a prior art roller cone of a rock bit mounted on a journal leg;

Figure 2 is an exploded cross-sectional view of the prior art roller cone and journal leg shown in Figure 1;

Figure 3 is a perspective view of a roller cone blank, being an intermediate in the process of the present invention;

Figure 4 is a cross-sectional view of the roller cone blank shown in Figure 3, the cross-section being taken on lines 4,4 of Figure 3;

Figure 5 is a side view of the roller cone blank after a step in the process of the present invention, wherein a black paint or etch has been applied to the surface of the blank;

Figure 6 is a side view of the roller cone blank after another step in the process of the present invention, wherein holes for holding hard tungsten carbide or like inserts, have been drilled in the blank;

Figure 7 is a cross-sectional view of the roller cone blank, schematically showing a stage in a step in the process of the present invention where the exterior shell of the cone is bombar-

ded by laser light;

Figure 8 is a cross-sectional view of the roller cone blank, schematically showing another stage in a step in the process of the present invention where the exterior shell of the cone is bombarded by laser light;

Figure 9 is a cross-sectional view showing the roller cone blank after the step of bombarding with laser light has been completed on the cone shell surfaces;

Figure 10 is a cross-sectional view of a roller cone having inserted hard cutter inserts, the roller cone being subjected to bombardment by laser light in accordance with another embodiment of the process of the present invention;

Figure 11 is a plan view of the bearing cavity containing side of the roller cone shown in Figure 9; and

Figure 12 is a schematic drawing representing a cross-section micrograph of an actual roller cone prepared in accordance with the process of the present invention, the micrograph representing an approximately six-fold magnification.

Figures 1 and 2 illustrate prior art roller cones mounted to the journal leg 22 of a rock drilling bit 24. As it will become apparent from the ensuing description in connection with Figures 3 through 11, in the herein-described preferred embodiments the process of the invention is applied to a roller cone 20 of substantially conventional overall configuration. Therefore, the mechanical features and configuration of the roller cone 20 and of the associated journal leg 22 are not described here in detail. Rather, for a detailed description of these conventional features, reference is made to United States Patent Nos. 4,303,137 and 3,680,873.

Although there is a similarity in overall appearance between the prior art roller cone illustrated in Figures 1 and 2, and the roller cones 20 made in accordance with the present invention, in the novel process of the invention, the roller cone 20 attains a hard case on its exterior shell 28 and in certain other portions of its surface. The hard exterior case and the other surfaces are very beneficial for the durability and reliability of operation of the drilling bit 24.

Thus, in accordance with the present invention, a forged steel body 30 of the roller cone 20 is machined to substantially close final dimensions. The forged steel body 30 includes an interior cavity 32 having a bearing race 34 lined, in accordance with practice in the art, with a "soft" aluminium bronze alloy. The bearing race 34 contacts a complementary race 36 of the journal leg 22. The race 36 of the journal leg 22 is shown on Figures 1 and 2. The interior cavity 32 also includes a ball race 38 for the balls 39 which retain the roller cone 20 on the journal leg 22. The balls 39 are shown on

Figure 1. The ball race 38 may be hardened by a laser hardening process described in United States Patent No. 4,303,137. The spindle bore 41 may also be similarly hardened in accordance with the present invention.

The exterior shell 28 of the steel body 30 of the roller cone 20 contains a plurality of spaced notches or flow channels 40. The flow channels 40 serve to facilitate flow of the drilling fluid (not shown) to the tungsten carbide or like hard cutter inserts 42 which are incorporated in the roller cone 20. The cutter inserts 42 are shown on Figures 1 and 2 in connection with the prior art, and also on Figure 10 in connection with another embodiment of the process of the present invention.

The steel body 30 of the roller cone 20 comprises, in accordance with the present invention, medium or high carbon steel, which can be readily hardened by heating to above austenitizing temperature, followed by rapid cooling. A preferred alloy steel for the steel body 30 of the roller cone 20 is known under the AISI designation 4340, although such other alloy steels as AISI 4140, 4330, and 4130 are also suitable. Generally speaking, for the practice of the present invention, the body 30 of the roller 20 can be made from the steels described in United States Patent No. 4,303,137. It will be readily understood by those skilled in the art that AISI 4340 steel, preferred for the practice of the present invention, contains approximately 0.40% carbon. The surface hardness of this steel body 30, without the further treatment described in the ensuing specification, is approximately 40-42 Rockwell C (Rc) hardness units.

In accordance with the present invention, a black paint or black etching liquid (not shown) is applied to the forged and machined steel body 30 of the roller cone 20, so as to obtain a darkened intermediate steel body 44. The black paint or black etch (not shown) may be of the type commonly known and used in the art, and need not be described here in detail. The intermediate steel body 44 bearing the light absorbing black paint or black etch is shown on Figure 5.

In the next step of the process, a plurality of insert holes 46 are drilled on the exterior shell 28. Drilling of insert holes 46 per se, is known in the art. More particularly, the insert holes are usually drilled to be approximately 0.0076 cm (0.003) inch smaller in diameter than the hard cutter inserts 42, which are to be press-fitted into the holes 46. Typically, a force of approximately 2224 N (500 pounds) may be required to press the cutter inserts 42 into place in the insert holes 46. A problem which has been substantially unsolved in the prior art in connection with the insert holes 46 is that drilling of the holes 46 through a hardened, carburized (or hardfaced) exterior shell is difficult. On

the other hand, walls of the insert holes 46 must not be carburized or otherwise hardened. This is because, as it was pointed out in the introductory section of the present patent application, hardening of the walls 48 of the insert holes 46 makes placement of the inserts 42 into the holes 46 very difficult, and creates a danger of cracking of the steel body 30 of the cone 20.

Referring now specifically to Figure 6, after the step of drilling of the insert holes 46, the intermediate steel body 44 has a black, light absorbent exterior shell 28, but the walls 48 of the insert holes 46 are shiny and light reflective.

Referring now to Figures 7 and 8, the next step in the process of the present invention is shown schematically. In this step the intermediate steel body 44 of Figure 6 is bombarded by a laser beam 52 of sufficient intensity to rapidly heat a surface layer of the exterior shell 28 to above austenitizing temperature (approximately 800° C). More specifically, Figure 7 schematically illustrates a source 50 of the laser beam 52. The laser beam 52 used in the process of the present invention must be powerful enough for the herein-described application; a continuous wave carbon dioxide laser of at least approximately 1500 watts power output is suitable. In the herein-described preferred embodiment of the process of the present invention, a carbon dioxide laser generator, Model 975 of Spectra Physics Company, San Jose, California, is used. The laser beam 52 used in this preferred process has 2000 watt power, and a beam diameter of approximately 1 cm (0.4").

In accordance with the invention, the entire exterior shell 28 of the intermediate steel body 44 is treated with the laser beam 52, in a raster pattern by using a mechanical scanner (not shown). Alternatively, an optical integrating mirror arrangement (not shown) can also be used to cover the surface of the exterior shell 28 with the laser beam 52. The purpose of the scanner or optical integrator would be to widen the coverage of the laser beam.

As it will be readily understood by those skilled in the art, the laser beam 52 rapidly heats a surface layer in the exterior shell 28 to above austenitizing temperature, that is, to approximately 800° C, or higher. Moreover, as the laser beam 52 is removed from contact with a localized area, the area is very rapidly cooled by sinking its heat into the surrounding large, cool steel body 44. As a result, "scanning" with the laser beam 52 serves as a very effective means for creating a hard martensitic layer 54 in the exterior shell 28. The hard martensitic layer 54 is schematically shown on Figures 7-10, indicating the procession of the process in which the martensitic surface layer 54 is formed.

Referring now particularly to Figures 8 through 10, a principal novel feature of the present invention lies in the fact that the treatment with the laser beam 52 of the exterior shell 28 need not be selective to exclude the insert holes 46. This renders the step of laser treating the exterior 28 of the cone 20 economically feasible. Figure 8 illustrates the phase in the laser treatment step wherein the laser beam 52 impacts into the bottom wall 48 of an insert hole 46. Walls 48 of the insert holes 46, however, are light reflective, and therefore do not absorb laser light, or absorb it only to a minimal extent, so that the walls 48 of the holes 46 are not heated above austenitizing temperature in the process.

Moreover, the laser beam 52 is focussed in relation to the exterior surface 28. Therefore, the beam 52 hitting the walls 48 of the holes 46 is essentially out of focus, and this further contributes to its ineffectiveness to austenitize an exterior layer of the walls 48.

As a further feature of the present invention, the seal gland area 56 and heel area 58 are also laser treated. These areas are best shown on Figures 9 and 11. Figure 9 indicates, with conspicuous cross-hatching, all areas of the steel body of the roller cone 20, which have attained the hard martensitic layer 54 as a result of the laser treatment followed by rapid self-quenching of the invention. The intermediate steel body of the roller cone 20, shown on Figures 9 and 11, bears the reference numeral 60. Cutter inserts 42 may be inserted into the insert holes 46 of the steel body 60 to yield the final roller cone 20. Because the walls 48 of the holes 46 have not been hardened in the laser treatment, their ductility is not adversely affected, and the process of inserting the cutter inserts 42 may be performed in a substantially conventional manner.

It will be readily appreciated by those skilled in the art that the intensity of the laser beam 52 and the duration of its impact on the intermediate steel body 44 of the roller cone 20 may be adjusted to obtain a martensitic layer 54 of virtually any desired practical thickness. Preferably, the martensitic layer 54 is between approximately 1.5 mm to 3 mm (0.06 to 0.12") thick, most preferred is a martensitic layer 54 of approximately 1.5 mm to 1.8 mm (0.060 to 0.070") thickness. A martensitic layer 54 of approximately 1 cm (0.04") is considered to be adequate in connection with the process of the present invention when it is applied to roller cones. The hardness of the surface layer 54 achieved in accordance with the present invention is approximately 57 to 60 Rockwell C (Rc) units. This is in contrast with the approximately 40 to 42 Rc hardness of the 4340 AISI steel utilized for the steel body 30 of the cone 20, and with the approximately

52-55 Rc hardness of carburized steel surfaces of some prior art roller cones. As it will be readily understood, the actual surface hardness of the roller cones 20 attained in the process of the present invention, is also dependent on the type of steel used for the forged steel body 30.

The hardness of the martensitic layer or case 54 attained on the surface of the exterior shell 28, and in the seal gland 56 and heel areas 58, is substantially uniform with respect to depth. In this regard, the martensitic layer 54 is superior to a carburized case, the hardness of which gradually diminishes with case depth.

Figure 10 schematically illustrates another embodiment of the process of the present invention. In this embodiment, insert holes 46 are drilled into the black painted or black etched steel body 44 of the roller cone 20. Thereafter, the hard cutter inserts 42 are inserted into the holes 46 in a conventional manner. The hard cutter inserts 42 preferably comprise tungsten carbide, although the present invention is not limited by the nature of the inserts 42.

The intermediate roller cone, bearing the reference numeral 62, is then subjected to laser treatment in the manner described above in connection with the first preferred embodiment. The laser beam 52 does not sufficiently raise the temperature of the inserts 42 to cause damage, because the inserts 42 are shiny and reflective to laser light. The laser beam 52 is also out of focus with respect to the inserts 42, and this also contributes to the lack of effectiveness of the laser beam 52 on the inserts 42.

Figure 11 illustrates the cavity containing side of the roller cone 20 after the process steps of the present invention have been performed. The seal gland 56 and heel 58 areas, which have been hardened by laser treatment, are shaded on Figure 11.

Significant advantages of the roller cones 20 prepared by the process of the present invention include the greatly increased hardness and dramatically improved abrasion and erosion resistance of the exterior shell. This, of course, results in dramatically less "wash out" of the cone shell, and prolonged life. Also, the finish cone has inserts surrounded by a high yield strength cone shell, as indicated on Figure 12. This retards any tendency for inserts to rock or rotate during drilling. Moreover, increased hardness of the seal gland 56 results in less abrasion in that very important area of the drilling bit also, and less "comet tail wear", which is normally caused by debris (not shown) caught between the sealing surfaces. Moreover, the laser treatment is relatively low in energy requirements, and can be performed within a short period of time, for example, in 3.5 minutes. Still further, laser treatment does not affect the dimensions of

the roller cone, so that little or no finish machining is required after the laser treatment. The medium to high carbon steel which is used in conjunction with the process of the present invention is also less expensive than the carburizable low carbon steel which is necessary for making a roller cone having a carburized, hard exterior shell. In light of the foregoing factors, the overall cost of laser treatment and of the roller cones attained thereby is low.

### Claims

1. A process for forming a hard cutter insert bearing cone for a rock bit comprising the steps of: forming a cone blank from a medium to high carbon hardenable steel, the cone blank including an external surface; rendering the external surface of the cone blank dark and absorbent to laser light; forming insert holes for the hard cutter inserts in the external surface of the cone; rendering the hole areas reflective so that the external surface of the cone includes dark, light absorbent surfaces and also reflective surfaces relatively unabsorbent to laser light; after the step of forming insert holes, bombarding the external surface of the cone with a laser beam of sufficient intensity and for sufficient time to austenitize an external layer in the light absorbent external surface of the cone; and cooling the austenitized layer sufficiently rapidly to form martensite in the external layer of the light absorbent external surface, whereby a cone having a hardened external case is obtained with insert holes having non-hardened wall and bottom.
2. The process of Claim 1 wherein the step of rendering the hole areas reflective comprises inserting into the insert holes hard cutter inserts having a surface relatively more reflective to laser light than the external surface of the cone.
3. The process of Claim 1 wherein the step of rendering the hole areas reflective comprises forming the insert holes with shiny reflective surfaces.
4. The process of any one of Claims 1 to 3 wherein the insert bearing cone is a roller cone and has an annular seal gland, the process comprising the further steps of bombarding, with a laser beam of sufficient intensity and for sufficient time, the external surface of the annular seal gland so as to austenitize the external surface of the seal gland and cooling the austenitized layer of the seal gland sufficiently

rapidly to form martensite in the external surface of the annular seal gland.

5. The process of any preceding claim wherein the step of cooling comprises cooling by self-quenching.
6. The process of any preceding claim wherein before the step of bombarding with a laser beam, the cone blank has a surface hardness of approximately 40 to 42 Rockwell C hardness units.
7. The process of any preceding claim wherein after the steps of bombarding and cooling, the surface hardness of the external surfaces of the cone is approximately 57 to 60 Rockwell C hardness units.
8. The process of any preceding claim wherein the step of bombarding is conducted with a CO<sub>2</sub> laser beam generator having an output power of at least approximately 1500 watts.
9. The process of any preceding claim wherein the laser beam used in the step of bombarding has a beam diameter of approximately 1 cm (0.4 inches).
10. The process of any preceding claim wherein the step of rendering comprises applying black paint or a black etch to the cone blank.
11. The process of any preceding claim wherein the laser beam is of sufficient intensity, and the shell surface is subjected to the beam for a sufficient period of time to austenitize the shell surface to a depth of at least 1 cm (0.04").
12. The process of Claim 11 wherein the hard martensitic layer on the external shell has a case depth of 1.5 mm to 3 mm (0.060" to 0.12").

### Patentansprüche

1. Verfahren zum Härten von konischen Schneideinsatzhaltern für Gesteinsbohrmeißel mit den Verfahrensschritten: des Herstellens eines Werkstück-Konus aus einem mittelharten bis harten Kohlenstoff-härtbaren Stahl, wobei der Werkstück-Konus eine äußere Oberfläche aufweist, des Bearbeitens der äußeren Oberfläche des Werkstück-Konus, so daß sie für Laserlicht dunkel und absorbierend ist, des Ausbildens von Einsatz-Löchern für die harten Schneideinsätze in der äußeren Oberfläche des Konus, des Erzeugens von spiegelnden Lochberei-

the roller cone, so that little or no finish machining is required after the laser treatment. The medium to high carbon steel which is used in conjunction with the process of the present invention is also less expensive than the carburizable low carbon steel which is necessary for making a roller cone having a carburized, hard exterior shell. In light of the foregoing factors, the overall cost of laser treatment and of the roller cones attained thereby is low.

## Claims

1. A process for forming a hard cutter insert bearing cone for a rock bit comprising the steps of: forming a cone blank from a medium to high carbon hardenable steel, the cone blank including an external surface; rendering the external surface of the cone blank dark and absorbent to laser light; forming insert holes for the hard cutter inserts in the external surface of the cone; rendering the hole areas reflective so that the external surface of the cone includes dark, light absorbent surfaces and also reflective surfaces relatively unabsorbent to laser light; after the step of forming insert holes, bombarding the external surface of the cone with a laser beam of sufficient intensity and for sufficient time to austenitize an external layer in the light absorbent external surface of the cone; and cooling the austenitized layer sufficiently rapidly to form martensite in the external layer of the light absorbent external surface, whereby a cone having a hardened external case is obtained with insert holes having non-hardened wall and bottom.
2. The process of Claim 1 wherein the step of rendering the hole areas reflective comprises inserting into the insert holes hard cutter inserts having a surface relatively more reflective to laser light than the external surface of the cone.
3. The process of Claim 1 wherein the step of rendering the hole areas reflective comprises forming the insert holes with shiny reflective surfaces.
4. The process of any one of Claims 1 to 3 wherein the insert bearing cone is a roller cone and has an annular seal gland, the process comprising the further steps of bombarding, with a laser beam of sufficient intensity and for sufficient time, the external surface of the annular seal gland so as to austenitize the external surface of the seal gland and cooling the austenitized layer of the seal gland sufficiently

rapidly to form martensite in the external surface of the annular seal gland.

5. The process of any preceding claim wherein the step of cooling comprises cooling by self-quenching.
6. The process of any preceding claim wherein before the step of bombarding with a laser beam, the cone blank has a surface hardness of approximately 40 to 42 Rockwell C hardness units.
7. The process of any preceding claim wherein after the steps of bombarding and cooling, the surface hardness of the external surfaces of the cone is approximately 57 to 60 Rockwell C hardness units.
8. The process of any preceding claim wherein the step of bombarding is conducted with a CO<sub>2</sub> laser beam generator having an output power of at least approximately 1500 watts.
9. The process of any preceding claim wherein the laser beam used in the step of bombarding has a beam diameter of approximately 1 cm (0.4 inches).
10. The process of any preceding claim wherein the step of rendering comprises applying black paint or a black etch to the cone blank.
11. The process of any preceding claim wherein the laser beam is of sufficient intensity, and the shell surface is subjected to the beam for a sufficient period of time to austenitize the shell surface to a depth of at least 1 cm (0.04").
12. The process of Claim 11 wherein the hard martensitic layer on the external shell has a case depth of 1.5 mm to 3 mm (0.060" to 0.12").

## Patentansprüche

1. Verfahren zum Härten von konischen Schneideinsatzhaltern für Gesteinsbohrmeißel mit den Verfahrensschritten: des Herstellens eines Werkstück-Konus aus einem mittelharten bis harten Kohlenstoff-härtbaren Stahl, wobei der Werkstück-Konus eine äußere Oberfläche aufweist, des Bearbeitens der äußeren Oberfläche des Werkstück-Konus, so daß sie für Laserlicht dunkel und absorbierend ist, des Ausbildens von Einsätz-Löchern für die harten Schneideinsätze in der äußeren Oberfläche des Konus, des Erzeugens von spiegelnden Lochberei-



chen, so daß die äußere Oberfläche des Konus dunkle, lichtabsorbierende Oberflächen und ebenfalls spiegelnde Oberflächen aufweist, die für Laserlicht relativ wenig absorbierend wirken, nach dem Schritt des Bildens von Einsatz-Löchern, des Beschießens der äußeren Oberfläche des Konus mit einem Laserstrahl genügender Intensität und für eine ausreichende Zeit, um eine äußere Schicht in der Licht absorbierenden äußeren Oberfläche des Konus zu austenitisieren, und des ausreichend schnellen Kühlens der austenitisierten Schicht, um Martensit in der äußeren Schicht der Lichtabsorbierenden äußeren Oberfläche zu bilden, wodurch ein Konus mit einem gehärteten äußeren Korpus mit nicht-gehärteten Wänden und Böden der Einsatz-Löcher erhalten wird.

2. Verfahren nach Anspruch 1, wobei der Schritt des Erzeugens von spiegelnden Lochbereichen den Schritt umfaßt, in die Einsatz-Löcher harte Schneideinsätze einzuführen, die eine relativ höhere Reflektivität für Laserlicht aufweisen als die äußere Oberfläche des Konus.

3. Verfahren nach Anspruch 1, wobei der Schritt des Erzeugens von spiegelnden Lochbereichen den Schritt umfaßt, die Einsatz-Löcher mit glänzenden reflektierenden Oberflächen auszustatten.

4. Verfahren nach einem der Ansprüche 1 bis 3, dadurch gekennzeichnet, daß der konische Schneideinsatzhalter ein Rollenkonus ist und eine ringförmige Dichtungsstopfbüchse aufweist, wobei das Verfahren die weiteren Schritte umfaßt: des Beschießens der äußeren Oberfläche der ringförmigen Dichtungsstopfbüchse mit einem Laserstrahl genügender Intensität und für eine ausreichende Zeit, so daß die äußere Oberfläche der Dichtungsstopfbüchse austenitisiert und des ausreichend schnellen Kühlens der austenitisierten Schicht der Dichtungsstopfbüchse, um Martensit in der äußeren Oberfläche der ringförmigen Dichtungsstopfbüchse zu bilden.

5. Verfahren nach einem der vorstehenden Ansprüche, bei dem der Schritt des Kühlens das Kühlen durch Selbstlöschung umfaßt.

6. Verfahren nach einem der vorstehenden Ansprüche, bei dem der Werkstück-Konus vor dem Schritt des Beschießens mit einem Laserstrahl eine Oberflächenhärte von ungefähr 40 bis 42 Rockwell C Härteeinheiten aufweist.

7. Verfahren nach einem der vorstehenden An-

sprüche, bei dem nach den Schritten des Beschießens und des Kühlens, die Oberflächenhärte der äußeren Oberflächen des Konus zwischen 57 und 60 Rockwell C Härteeinheiten beträgt.

8. Verfahren nach einem der vorstehenden Ansprüche, bei dem das Beschießen mit einem CO<sub>2</sub>-Laser durchgeführt wird, der eine Ausgangsleistung von mindestens ungefähr 1500 Watt aufweist.

9. Verfahren nach einem der vorstehenden Ansprüche, bei dem der verwendete Laserstrahl beim Schritt des Beschießens einen Strahldurchmesser von ungefähr 1 Zentimeter (0,4 Zoll) aufweist

10. Verfahren nach einem der vorstehenden Ansprüche, bei dem der Schritt des Bearbeitens der äußeren Oberfläche des Werkstück-Konus das Auftragen von schwarzer Farbe oder schwarzer Ätzflüssigkeit auf den Werkstück-Konus umfaßt.

11. Verfahren nach einem der vorstehenden Ansprüche, bei dem der verwendete Laserstrahl von genügender Intensität ist, und daß die Schalenoberfläche dem Strahl für eine genügende Zeitdauer ausgesetzt wird, um die Schalenoberfläche bis zu einer Tiefe von mindestens 1 Zentimeter (0,4 Zoll) zu austenitisieren.

12. Verfahren nach Anspruch 11, bei dem die harte Martensitschicht auf der äußeren Schalenoberfläche eine Korpus-tiefe von 1,5 bis 3 Millimeter (0,060 bis 0,12 Zoll) aufweist.

#### Revendications

1. Procédé pour la formation d'un cône portant des éléments d'attaque durs rapportés pour un trépan à roches, comprenant les opérations de : former une ébauche de cône dans un acier pouvant être trempé à teneur en carbone moyenne à élevée, cette ébauche de cône comprenant une surface extérieure ; rendre la surface extérieure de l'ébauche du cône sombre et absorbante pour un rayon laser ; former dans la surface extérieure du cône des trous d'insertion pour les éléments d'attaque durs rapportés ; rendre la zone des trous réfléchissante de façon que la surface extérieure du cône comprenne des surfaces sombres absorbant la lumière et aussi des surfaces réfléchissantes relativement non absorbantes d'un rayon laser ; après l'opération de formation



des trous d'insertion bombarder la surface extérieure du cône à l'aide d'un rayon laser ayant une intensité suffisante et pendant une durée suffisante pour rendre austénitique une couche extérieure de la surface extérieure du cône absorbant la lumière ; et refroidir la couche austénitique suffisamment rapidement pour former de la martensite dans la couche extérieure de la surface extérieure absorbant la lumière, de sorte qu'est obtenu un cône ayant une couche extérieure durcie avec des trous d'insertion ayant une paroi et un fond non durcis.

2. Procédé de la revendication 1 selon lequel l'opération pour rendre réfléchissante la zone des trous comprend l'introduction dans les trous d'insertion des éléments d'attaque durs rapportés ayant une surface relativement plus réfléchissante du rayon laser que la surface extérieure du cône. 15
3. Procédé de la revendication 1 selon lequel l'opération de rendre plus réfléchissante la zone des trous comprend la formation de trous d'insertion avec des surfaces luisantes réfléchissantes. 25
4. Procédé de l'une quelconque des revendications 1 à 3 selon lequel le cône portant des éléments d'attaque rapportés est un cône à roulement et il a un joint d'étanchéité annulaire, le procédé comprenant les opérations supplémentaires de bombarder à l'aide d'un rayon laser ayant une intensité suffisante et pendant une durée suffisante la surface extérieure du joint d'étanchéité annulaire de manière à rendre austénitique la surface extérieure du joint d'étanchéité et de refroidir la couche austénitique du joint d'étanchéité suffisamment rapidement pour former de la martensite dans la surface extérieure du joint d'étanchéité annulaire. 30 40
5. Procédé de l'une quelconque des revendications précédentes selon lequel l'opération de refroidissement comprend le refroidissement par autotrempe. 45
6. Procédé de l'une quelconque des revendications précédentes selon lequel avant l'opération de bombardement à l'aide d'un rayon laser l'ébauche du cône a une dureté superficielle approximative de 40 à 42 unités de dureté Rockwell C. 50 55
7. Procédé de l'une quelconque des revendications précédentes selon lequel après les opé-

rations de bombardement et de refroidissement la dureté superficielle des surfaces extérieures du cône est approximativement de 57 à 60 unités de dureté Rockwell C.

8. Procédé de l'une quelconque des revendications précédentes selon lequel l'opération de bombardement est exécutée à l'aide d'un générateur de rayon laser à CO<sub>2</sub> ayant une puissance de sortie de 1.500 watts au moins approximativement. 5
9. Procédé de l'une quelconque des revendications précédentes selon lequel le rayon laser utilisé pendant l'opération de bombardement a un diamètre de rayon laser de 1 cm approximativement (0,4 pouce). 10
10. Procédé de l'une quelconque des revendications précédentes selon lequel l'opération de rendre la surface sombre comprend l'application d'une peinture noire ou l'exécution d'une attaque chimique noircissante sur l'ébauche du cône. 20
11. Procédé de l'une quelconque des revendications précédentes selon lequel le rayon laser a une intensité suffisante et la couche superficielle est soumise au rayon pendant une durée suffisante pour rendre austénitique la couche superficielle jusqu'à une profondeur de 1 cm au moins (0,4 pouce). 25
12. Procédé de la revendication 11 selon lequel la couche dure martensitique de la couche extérieure a une profondeur de 1,5 mm à 3 mm (0,060 pouce à 0,12 pouce). 30 35 40 45 50 55

