

Title: Process and Apparatus for distillation**Field of Application**

The present invention refers to a process, apparatus and plant for distillation of methanol.

5 This method and apparatus may also be used to distillate other products such as ethanol.

Background Art

It is known that the product of plants for synthesizing methanol, commonly defined as crude methanol, is an aqueous solution of methanol containing by-products of the synthesis reaction including ethanol, ketones, higher alcohols, and some dissolved gases including mainly H₂, CO, CO₂, N₂, CH₄.

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The crude methanol is distilled to meet the purity specifications required on the market. For example, the grade AA specification requires a minimum methanol concentration of 99.85% by weight, wherein ethanol should not exceed 10 ppm by weight.

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Known distillation processes are based substantially on one or more distillation columns, where typically at least one column is able to separate light products (for example gas) recovered at the top of the column from methanol, and at least one column is able to separate the heavier product (e.g. aqueous solution) recovered at the bottom of the column from methanol.

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A specific process which is widely used for e.g. distillation of methanol, comprises two columns that operate at atmospheric pressure or close to atmospheric pressure. More specifically, said process uses a preliminary treatment column known as stabilizing column or pre-run column and a second distillation column. The first column substantially has the purpose of separating the more volatile components contained in the crude methanol, where it receives the crude methanol and separates the light components at the top and an aqueous solution at the bottom. The second column known as concentration column carries out the actual distillation, obtaining (i) refined methanol at the top, (ii) a prevalently aqueous stream at the bottom ("bottom water"), (iii) a side stream known as "fusel oil" mainly containing water, residual methanol (ca. 1 % of the total) and most of the by-products of the synthesis reaction. Said fusel oil has a certain heat value and is usually used as a fuel or feed in for synthesis gas generation.

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Each column comprises a reboiler that heats the bottom of the column and maintains heat input to the distillation process. Each column comprises also a condenser, which condenses the top product and recycles it (at least partially) to said column. The heat is provided to the concentration (or distillation) column by steam, or by a process gas -
5 when available - of suitable thermal level. The cooling medium for the condenser is normally water or air. Said configuration with two columns is simple in terms of a plant (e.g., a methanol distillation plant), but it has the major drawback of consuming a substantial amount of energy, both due to the heat supplied to the bottom reboilers, and due to the consumption of cooling water and/or electricity of the top condensers. Moreover, the col-
10 umns have a relatively large diameter in relation to the production capacity and the plant cost is consequently high.

The order of magnitude of the heat consumption for the two bottom reboilers of about 0.8 Gcal per ton of refined methanol. Since the energy consumption necessary to pro-
15 duce a ton of crude methanol is about 6-8 Gcal, the order of magnitude of the energy consumption of the distillation is estimated to be 10% of the total consumption of the plant. The heat to be disposed of in the condensers is comparable with the heat ex-
changed in the reboilers. In the theoretical case, for example, of removing said heat exclusively with cooling water, the flow rate circulating is relevant, i.e. about 80 m³ per
20 ton of methanol, and consequently there are high costs for pumping, etc.

There are other known distillation plants and processes that attempt to at least partially reduce these drawbacks.

25 US 4 210 495 describes a process with three distillation columns, i.e. a preliminary treat-
ment or stabilizing column and two concentration columns, a column operating at a me-
dium pressure of about 7-8 bar and a final concentration column, respectively. The sta-
bilizing and final concentration columns operate substantially at atmospheric pressure or
slightly higher pressure (e.g. 1.5 bar). Such a configuration makes it possible to con-
30 dense the top vapors of the medium pressure column in the bottom reboiler of the final
column at atmospheric pressure, recovering heat, and this concept is known as "stag-
gered columns" or "cascaded columns". The staggered column concept may be used
several times, for example by letting a high pressure concentration column deliver heat
to a concentration column operating at intermediate pressure, which in turn delivers heat
35 to a column operating at low pressure. However, both the stabilizing column and the

concentration column operating at highest pressure must be heated and consequently the specific consumption, whilst being lower than a plant with just two columns, is still high.

5 A further development of this idea was disclosed in WO2013110369, which describes a process in which the final distillation column is operating at the highest pressure thereby enabling the condensing of top vapors from the final concentration column to deliver heat to the reboiler for the stabilizing column. This configuration makes it possible to reduce the energy compared to the process configuration described in US 4 210 495, but this
10 configuration has the significant drawback that all concentration columns will be operating at higher pressure than otherwise necessary and a further drawback of this configuration is that there is a mismatch between the stabilizer condenser duty and the final concentration column reboiler duty as the amount of heat required for the stabilizing column is much (~30-70%) lower than the amount of heat required for the final concentration
15 column.

The implication of the mismatch between the stabilizer condenser duty and final concentration column reboiler duty is that either will part of the condensing duty for the final concentration column be supplied by a separate condenser cooled by air or water (extra
20 cost and energy consumption) or the stabilizing column will become unnecessarily large (in diameter).

The drawback of the increased pressure in the concentration columns is two-fold. In the first place, increasing the concentration column pressures puts more severe specifications on the heat source so that a heat source, which is acceptable for heating up two
25 staggered concentration columns may not be acceptable to heat up the three staggered columns that results from this configuration. A further drawback is that the separation efficiency in the concentration columns is reduced with increasing pressure. This in turn translates into an increased energy consumption for a given distillation column, as shown
30 in Tables 1 and 2.

Table 1 – Column feedstock, design and results achieved with the method and apparatus of the present invention.

Column feed, mole %	
MeOH	66,61
H ₂ O	33,00
EtOH	0,25
Higher alcohols	0,14
Number of equilibrium stages	49
Pressure drop across column, bar	0,9
MeOH recovery	98%
MeOH purity	99,999%
Water recovery	93%
Water purity	99,998%

5 Table 2 – Required reboiler duty (Gcal/h) at different pressure to

Pressure, barg	Reboiler duty, Gcal/h
0,1	62,3
0,6	72,75
1,1	83,6
2,1	108,3

10 Document WO2013110369 addresses the problem of consuming a substantial amount of energy, both due to the heat supplied to the bottom reboilers, and due to the consumption of cooling water and/or electricity of the top condensers. It does not, however provide (or suggest) a solution to efficiently solve this problem when having more than 2 concentration columns for distillation of methanol, allowing for comparable savings of energy.

15 This document suggests that the adoption of a substantially higher bottoming pressure (i.e., at the final distillation column which would correspond to column V3 of the present invention) allows an energy saving and makes it possible to optimize the heat flows and that by increasing the bottoming pressure (which would correspond to P3 in the present invention), the distilled methanol in gaseous state, produced in the bottoming stage, has a substantially higher temperature than the temperature in the topping stage (which
20 would correspond to stabilizing column V0 of the present invention) and sufficient to ensure that a stream of said distilled methanol can be used as a heat source for the

preliminary topping step. This document claims to make it possible to reduce or eliminate the consumption of heat (for example from condensing steam) for the heating of the topping stage. It discloses that pressure p_4 , in the bottoming stage, is substantially higher than the topping pressure p_1 , so that the temperature of gaseous methanol, distilled in column 400, is substantially greater than the temperature of the liquid in the bottom of column 100. It also discloses that such temperature difference is at least 10 °C, i.e., the temperature of the gaseous methanol at the top of column 400 is at least 10 degrees Celsius higher than the temperature of the liquid in the bottom of column 100. This is what allows that at least part of said gaseous methanol can be used to heat, at least partially, the topping column 100.

CN108101748, and other documents, also mention an energy-saving process method and device for methanol purification, which is an energy-saving process and device for producing methanol from crude methanol using four towers and refers to a reduction of the operating energy consumption, however it is not clear or suggested how this is achieved and what are the process conditions.

Description of the Invention

The present invention refers to an apparatus and process for distillation of methanol (Fig. 1), however may also be used in distillation of other products such as ethanol.

The present invention has the purpose of reducing the consumption of energy and of cooling water and/or electricity in a distillation process of crude intermediate products (e.g., methanol) comprising a pre-treatment stage, known as stabilizing stage, for the removal of the volatile components, and a concentration stage, comprising one or more columns for distillation.

Such a purpose is accomplished with a process for refining or distillation of a stream of crude methanol (A) comprising, in a preferred embodiment of the present invention:

- (i) pre-treatment of a crude stream A of methanol in a stabilizing column V0 at pressure P_0 , for separation of volatile components, obtaining a stream of light gases L from

the upper section of V0 and a liquid stream B0 comprising methanol from the lower section of V0,

(ii) B0 is then directed towards concentration column V1, at pressure P1,

(iii) gaseous stream T1 recovered from the upper section of V1 is condensed in heat exchanger E2, supplying energy to concentration column V2,

(iv) part of the condensed methanol obtained in step (iii) is sent to product C1, and the remaining part of the condensed methanol is added to the upper section of V1 and used as reflux flow,

(v) a liquid stream B1 comprising methanol is recovered from the lower section of V1 and passed on to V2, at pressure P2,

(vi) gaseous stream T2 recovered from the upper section of V2 is split (S) in two separate streams, one stream being condensed in a heat exchanger E0, supplying energy to V0, and the other stream being condensed in a heat exchanger E3, supplying energy to concentration column V3,

(vii) part of the condensed methanol obtained in step (vi) is sent to product, C2, and the remaining part of the condensed methanol is added to the upper section of V2 and used as reflux flow,

(viii) a liquid stream B2 comprising methanol is recovered from V2 and passed on to V3, at pressure P3,

(ix) gaseous stream T3, recovered from the upper section of V3, is condensed, part of the condensed methanol being sent to product, C3, and the remaining part being added to the upper section of V3 and used as reflux flow,

(x) one or more side streams H comprising higher alcohols and other minor bi-products is withdrawn from V3 and a liquid stream B3, is drawn from V3,

wherein:

- Columns V1, V2 and V3 operate at decreasing pressures, such that $P1 > P2 > P3$
- $P0 > 0$ barg and $P1 > 0$ barg
- each column V0, V1, V2 and V3 is correspondingly associated to a heat exchanger E0, E1, E2 and E3, which is a reboiler for the same column,
- heat exchangers E0 and E3 are condensers for column V2;
- heat exchanger E2 is condenser for column V1.

characterized in that:

- $P1 < 2$ barg; and
- Heat exchanger E1 is supplied by an external energy source.

And also an apparatus for distillation of methanol, comprising a stabilizing column V0, at pressure P0, connected in series with at least 3 distillation columns V1, V2 and V3 at correspondingly decreasing pressure P1, P2 and P3 wherein each column is associated to a heat exchanger E0, E1, E2 and E3, said heat exchanger being a reboiler for that column, characterized in that,

- a) heat exchangers E0 and E3 are condensers of column V2;
- b) heat exchanger E2 is condenser of column V1;.
- c) E1 has an incoming heat stream, external to said apparatus;
- d) $P1 < 2$ barg,

as well as a plant for distillation of methanol, comprising at least one apparatus according to the present invention, wherein the amount of steam required for E1 is less than 1.3 kg/kg of product methanol and also the use of said apparatus for distillation of methanol.

The process of the present invention preferably comprises at least 4 columns, V0, V1, V2 and V3, but may comprise more concentration columns, from V1 up to Vn, operating at decreasing pressure, preferably connected in series.

Said concentration columns all operate in a manner such that part of the distilled product, C1, C2, C3 and so forward, is recovered from the upper section of each of the concentration columns, and the remaining liquid, B0, B1, B2, B3 and so forward, is passed on to the other column(s) until the final concentration column, e.g. in the preferred embodiment of the present invention said column is V3, from which the final fraction of the product C3 is recovered from the upper section, stream B3 comprising mainly water is recovered from the bottom and a mixture frequently referred to as fusel oil is recovered from a side stream H from the last concentration column – typically taken out in between the feed tray and the bottom of the column.

The heat exchange preferably takes place in a condenser/reboiler E0, E1, E2 and E3. Said heat exchanger may be a tube bundle or plate exchanger, in which the distilled methanol condenses in the hot side, and the solution evaporates in the cold side.

Preferably, the pressure of the condensers for the stabilizing step and low pressure concentration column are both slightly above atmospheric pressure, for example 0.1 - 0.5

bar thereby typically leading to a pressure in the reboiler for the stabilizing step of 0.5-1.5 bar, and the pressure in the condenser for the concentration column which delivers heat is at least 2 bar. Consequently, the pressure in the reboiler for the column which delivers heat is in the range 2 - 8 bar; more preferably about 7 bar.

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Some embodiments comprise more than one concentration columns and several pressure levels but the column with the second lowest pressure level always supplies the heat to the stabilizing step.

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The described pre-treatment (stabilizing) and concentration stages can be implemented using a single column or many columns in parallel, if necessary.

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The final concentration column V3 produces distilled methanol C3, a solution B3 mainly made up of water, and can also produce a side stream H represented by the so-called fusel oil. Side streams of fusel oil can also be extracted, if suitable, from the intermediate distillation stages.

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The relative volatility between methanol and ethanol is highest at low pressure, so it is an advantage to conduct the separation at a pressure as low as possible.

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Each time a column 1 receives heat from another column 2, the temperature level in column 1 increases and therefore also the column 2 pressure needs to be higher than in column 1. This is necessary to obtain the desirable driving force in the heat exchangers which act as condenser for the warmer column and as reboiler for the colder column.

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This temperature difference should be preferably be 4-10 °C. The temperature level of the external heat source (typically steam) moreover has preferably to be 4-10 °C higher than the temperature level in the bottom of the column with highest temperature level. Some prior art documents show staggering of all the concentration columns on top of the stabilizing column, they will end up with a higher demand for the temperature level of the external heat source than in the present invention, where the final concentration column is working at the same pressure level and therefore also essentially the same temperature level as the stabilizing column.

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Brief Description of Drawings

Figure 1 represents a preferred embodiment of the process for distillation of methanol according to the present invention, where three concentration columns V1, V2 and V3 with decreasing pressures $P1 > P2 > P3$ are connected to a stabilizing column V0 at pressure P0, wherein:

- a. A: Feed of crude methanol
- b. V0: Stabilizing column at pressure P0
- c. V1, V2, V3: Concentration columns at pressure $P1 > P2 > P3$
- d. B0: Liquid stream comprising methanol, recovered from the lower part of stabilizing column V0,
- e. B1, B2, B3: Liquid streams comprising methanol, recovered from the lower part of concentrations columns V1, V2, V3,
- f. C1, C2, C3: Product liquid distilled methanol,
- g. E0, E1, E2, E3: Heat exchangers,
- h. T0: Gaseous stream recovered from the upper part of stabilizing column V0
- i. T1, T2, T3: Gaseous streams recovered from the upper part of concentration columns V1, V2, V3
- j. L: Light gaseous stream from V0,
- k. H: Side stream recovered from V3,
- l. S: Split of streams.

Definitions

"Atmospheric pressure" means 1,01325 bar, i.e., approximately 1 bar.

"Concentration column" or "distillation column" or "bottoming column", Vn where $n \neq 0$ (such as V1, V2 or V3), means a column divided into a series of stages. These correspond to a cascade of equilibrium stages. Liquid flows down the column from stage to stage and is contacted by vapor flowing upward. Traditionally, most columns have been built from a set of distinct "trays" or "plates", so these terms end up being essentially interchangeable with "stages". Each tray in a distillation column is designed to promote contact between the vapor and liquid on the stage. Distillation can be conducted in a packed column (just as absorption can be done in a trayed column). Stages may be numbered from top down or bottom up. The stream recovered from the upper section of

the column is called the overhead product, T, the "overhead", the "top product". Distillate product C may be liquid or vapor (or occasionally both) depending on the type of condenser used. The distillate flow rate is herein designated C and the product recovered from the lower section of the column may be called the bottom product and is herein given the symbol B. In some situations, one or more "sidedraw" products H may be removed from the column. The portion of the column above the feed tray is called the rectification section. In this section, the vapor is enriched by contact with the reflux. The portion of the column below the feed tray is called the stripping section. The liquid portion of the feed serves as the reflux for this section. The operating pressure of the column, Pn (such as P1, P2 and P3) is typically controlled by adjusting heat removal in the heat exchanger. The base of the column is typically used as a reservoir to hold liquid leaving the bottom tray. A heat exchanger, e.g. a reboiler, is used to boil this liquid. The vapor which results, the "boilup", is returned to the bottom of the column.

A "Condenser" is required to provide the cooling duty to condense the stream collected from the upper section of the concentration column, which is a gas or vapor. The condensed vapor is partially refluxed back into the top of the column to increase the sharpness of the separation – the greater the reflux ratio the better is the separation. The condenser can be a total condenser or a partial condenser. In a total condenser, all the top vapor product is condensed to liquid, whereas in a partial condenser, only part of the vapor is condensed, and the liquid is refluxed back to the column, the un-condensed vapor is drawn for further processing. In this case, the partial condenser can be viewed as an additional VLE separation stage, whereas in a total condenser the top product of the column has the same composition as the reflux stream.

"Crude methanol", A, means a solution comprising methanol, typically 65 to 95% methanol, water and other components. The crude methanol A contains low-boiling and high-boiling components (light and heavy ends). The light ends L include mainly dissolved gases (e.g., CO₂), dimethyl ether, methyl formate, and acetone. The heavy ends H include higher alcohols, long-chain hydrocarbons, higher ketones, and esters of lower alcohols with formic, acetic, and propionic acids.

"Distillation" or "fractional distillation" or "fractionation" means a process for separating liquid mixtures into two or more vapor or liquid products with different compositions. Distillation is an equilibrium stage operation. In each stage, a vapor phase is contacted with

a liquid phase and mass is from vapor to liquid and from liquid to vapor. The less volatile, "heavy" or "high boiling", components concentrate in the liquid phase; the more volatile, "light", components concentrate in the vapor. By using multiple stages in series with re-cycle, separation can be accomplished. The feed to a distillation column may be liquid, vapor, or a liquid-vapor mixture. It may enter at any point in the column. More than one stream may be fed to the system, and more than one product may be drawn. Vapor leaving the top of the column, such as T0, T1, T2 and T3, passes through a heat exchanger, where it is partially or totally condensed. The resulting liquid is temporarily held in the "accumulator" or reflux drum. A liquid stream is withdrawn from the drum and returned to the top tray of the column as reflux to promote separation.

"Equilibrium stage" or theoretical plate means, in many separation processes such as distillation, a hypothetical zone or stage in which two phases, such as the liquid and vapor phases of a substance, establish an equilibrium with each other. Such equilibrium stages may also be referred to as an ideal stage or a theoretical tray. The performance of many separation processes depends on having series of equilibrium stages and is enhanced by providing more such stages. In other words, having more equilibrium stages increases the efficiency of the separation process.

"Feed" or "column feed" to a distillation column may be liquid, vapor, or a liquid-vapor mixture. It may enter at any point in the column, although the optimal feed tray location should be determined and used. More than one stream may be fed to the system, and more than one product may be drawn. The thermal condition of the feed determines the column internal flows. If the feed is below its boiling point, heat is needed to raise it to where it can be vaporized. This heat must be obtained by condensing vapor rising through the column, so the liquid flow moving down the column increases by the entire amount of the feed plus the condensed material and the vapor flow upward is decreased.

"Gaseous stream, such as T0, T1, T2 or T3, recovered from the upper part of stabilizing column V0 and concentration columns, such as V1, V2 or V3, is the stream resulting from a distillation process, taken from the upper part of said columns. Such a stream is mainly made up of methanol, with progressively lower content of impurities until the gaseous stream, such as T3, recovered from the last concentration column, such as V3, has a very low content of impurities. The requirement is that the mixed product streams, C1 + C2 + C3, shall fulfil the required product specification (e.g. grade AA).

“Heat duty” or “Duty” means the amount of heat needed to transfer from a hot side to the cold side over a unit of time. The equation to calculate the heat duty is normally written in two ways: a) one that can be used for sensible heat transferred, which means that the fluid undergoes no phase change; b) the other can be used for latent heat transferred, which means that the fluid undergoes a phase change. i.e. condenses.

“Heat exchanger” means a system used to transfer heat between two or more fluids. Heat exchangers are used in both cooling and heating processes. The fluids may be separated by a solid wall to prevent mixing or they may be in direct contact. In particular, “heat exchanger” means a reboiler/condenser, e.g. E0, E1, E2 and E3, such as a tube bundle exchanger, for example with evaporation of the solution in the shell side and condensation of the distillate in the tube side (or vice-versa). It is also possible to use a plated heat exchanger with heat exchange plates housed inside a shell.

“Partial reboiler” means a reboiler where only part of the liquid in the column base is vaporized. The vapor produced is returned to the column, and the liquid stream is removed as product or feed to an additional column. The compositions of these three streams are different. Partial reboilers also provide an ideal separation stage. Side-stream reboilers can be used, which draw liquid off a tray, heat it, and then return the vapor liquid mixture to the same or similar trays.

“Heavy by-products” or “side streams”, H, means a stream comprising higher alcohols and other minor bi-products recovered from the last concentration column – typically taken out in between the feed tray and the bottom of the column. It is also known as “fusel oil” and comprises water, residual methanol (ca. 1 % of the total) and most of the by-products of the synthesis reaction. Said fusel oil has a certain heat value and is usually used as a fuel or feed to a synthesis gas generation section. Side streams of fusel oil can also be extracted, if suitable, from the intermediate distillation stages.

“Intermediate products” mean vapor and liquid streams between columns and exiting columns in a multi column distillation apart from the feed stream A, the product streams C1, C2, C3, L, H and B3.

"Light by-products" or "Light gases" or "Light ends", L, mean gaseous stream obtained from stabilizing column V0, preferably the upper section of V0 and includes mainly dissolved gases (e.g., CO₂), dimethyl ether, methyl formate, and acetone.

5 "Liquid stream comprising methanol", such as B0, B1, B2 or B3 means a stream recovered from the lower section of stabilizing column V0 and concentration columns, such as V1, V2 and V3. As the distillation progresses, this stream gradually comprises a lower amount of methanol and a higher amount of water, until the last stream, such as B3,
10 recovered from the last concentration column, such as V3, comprises mainly water and only residual amounts of methanol, preferably less than 50 ppm.

"Lower stream" or "bottom stream" means a stream obtained or recovered from the lower section of a column, such as V0, V1, V2 and V3.

15 "Pressure", P, means gauge pressure and is measured in bar(g). Gauge pressure is the pressure relative to atmospheric pressure and it is positive for pressures above atmospheric pressure, and negative for pressures below it. The difference between bar and bar(g) is the difference in the reference considered. Measurement of pressure is always
20 taken against a reference and corresponds to the value obtained in a pressure measuring instrument. If the reference in the pressure measurement is vacuum we obtain absolute pressure and measure it in bar only. If the reference is atmospheric pressure then pressure is cited in bar(g).

25 "Product", such as C1, C2 or C3, is liquid distilled methanol recovered from concentration columns such as V1, V2 and V3.

"Reboiler" means a heat exchanger typically used to provide heat to the bottom of industrial distillation columns. Reboilers boil the liquid from the bottom of a distillation column to generate vapors which are returned to the column, such as V0, V1, V2 and V3, to
30 drive the distillation separation. The heat supplied to the column by the reboiler at the bottom of the column is removed by the condenser at the top of the column. Most reboilers are of the shell and tube heat exchanger type and normally steam is used as the heat source in such reboilers. However, other heat transfer fluids like hot synthesis gas, oil or Dowtherm (TM) may be used. Fuel-fired furnaces may also be used as reboilers in some
35 cases.

“Split of streams”, S, means separation of at least one original stream (liquid or gaseous) in two separate streams or sub-streams (liquid or gaseous). Within the context of the present invention, S indicates the location where gaseous stream T2 recovered from the upper section of V2 is divided in two deriving streams or sub-streams, one stream or sub-stream being condensed in a heat exchanger E0, supplying energy to V0, and the other stream or sub-stream being condensed in a heat exchanger E3, supplying energy to concentration column V3.

“Stabilizing column” or Topping column or pre-run column or, V₀, is for separating the more volatile components from the heavier components, both contained in the crude product, such as crude methanol.

“Volatile components” or “volatile substances” means components or substances which vaporize readily at low temperatures. Volatility can also describe the tendency of a vapor to condense into a liquid or solid: less volatile substances will more readily condense from a vapor than highly volatile ones. *Vapor pressure* is a measurement of how readily a condensed phase forms a vapor at a given temperature. A substance enclosed in a sealed vessel initially at vacuum (no air inside) will quickly fill any empty space with vapor. After the system reaches equilibrium and no more vapor is formed, this vapor pressure can be measured. Increasing the temperature increases the amount of vapor that is formed and thus the vapor pressure. In a mixture, each substance contributes to the overall vapor pressure of the mixture, with more volatile compounds making a larger contribution. *Boiling point* is the temperature at which the vapor pressure of a liquid is equal to the surrounding pressure, causing the liquid to rapidly evaporate, or boil. It is closely related to vapor pressure, but is dependent on pressure. The normal boiling point is the boiling point at atmospheric pressure, but it can also be reported at higher and lower pressures.

“Upper stream” or “Top stream” means a stream obtained or recovered from the upper section of a column, such as V0, V1, V2 and V3.

Preferred embodiments

(1) Process for distillation of methanol, comprising:

- 5 (i) pre-treatment of a crude stream A of methanol in a stabilizing column V0 at pressure P0, for separation of volatile components, obtaining a stream of light gases L from the upper section of V0 and a liquid stream B0 comprising methanol from the lower section of V0,
- (ii) B0 is then directed towards concentration column V1, at pressure P1,
- 10 (iii) gaseous stream T1 recovered from the upper section of V1 is condensed in heat exchanger E2, supplying energy to concentration column V2,
- (iv) part of the condensed methanol obtained in step (iii) is sent to product C1, and the remaining part of the condensed methanol is added to the upper section of V1 and used as reflux flow,
- 15 (v) a liquid stream B1 comprising methanol is recovered from the lower section of V1 and passed on to V2, at pressure P2,
- (vi) gaseous stream T2 recovered from the upper section of V2 is split (S) in two separate streams, one stream being condensed in a heat exchanger E0, supplying energy to V0, and the other stream being condensed in a heat exchanger E3, supplying energy to concentration column V3,
- 20 (vii) part of the condensed methanol obtained in step (vi) is sent to product, C2, and the remaining part of the condensed methanol is added to the upper section of V2 and used as reflux flow,
- (viii) a liquid stream B2 comprising methanol is recovered from V2 and passed on to V3, at pressure P3,
- 25 (ix) gaseous stream T3, recovered from the upper section of V3, is condensed, part of the condensed methanol being sent to product, C3, and the remaining part being added to the upper section of V3 and used as reflux flow,
- (x) one or more side streams H comprising higher alcohols and other minor bi-products is withdrawn from V3 and a liquid stream B3, is drawn from V3,
- 30 wherein:
- Columns V1, V2 and V3 operate at decreasing pressures, such that $P1 > P2 > P3$
 - $P0 > 0$ barg and $P1 > 0$ barg
 - each column V0, V1, V2 and V3 is correspondingly associated to a heat exchanger E0, E1, E2 and E3, as a reboiler for the same column,
 - 35 - heat exchangers E0 and E3 are condensers for column V2;

- heat exchanger E2 is condenser for column V1.

and wherein:

- $P1 < 2$ barg; and

- Heat exchanger E1 is supplied by an external energy source.

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(2) Process according to embodiment 1, wherein the temperature in the coldest part of V2 is higher than the temperature in the warmest part of V3 and V0 and the temperature in the coldest part of V1 is higher than the temperature in the warmest part of V2.

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(3) Process according to the previous embodiments, wherein the temperature in the coldest part of V2 is preferably 4 °C higher than the temperature in the warmest part of V3 and V0 and the temperature in the coldest part of V1 is preferably 4 °C higher than the temperature in the warmest part of V2.

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(4) Process according to the previous embodiments wherein the difference between P1 and P0 is greater than or equal to 7.7 bar.

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(5) Process according to the previous embodiments, wherein P1 is higher than 9,7 bar(g), P2 is comprised between 6,9 and 13 bar(g).

(6) Process according to the previous embodiments, wherein P1 is preferably 17 bar(g), P2 is preferably 9 bar(g) and P3 is preferably 0,98 bar(g).

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(7) Process according to the previous embodiments, wherein the heat duty of E0 is at least 30% less than the duty of E1.

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(8) Process according to the previous embodiments, wherein B3 comprises the water removed from circulating streams and is recovered from the lower section of V3.

(9) Process according to the previous embodiments, wherein the crude product to be distilled is ethanol or other suitable product.

(10) Apparatus for distillation of methanol, comprising a stabilizing column V0, at pressure P0, connected in series with at least 3 distillation columns V1, V2 and V3 at correspondingly decreasing pressure P1, P2 and P3 wherein each column is associated to a heat exchanger E0, E1, E2 and E3, said heat exchanger being a reboiler for that column, wherein:

- a) heat exchangers E0 and E3 are condensers of column V2;
- b) heat exchanger E2 is condenser of column V1;.
- c) E1 has an incoming heat stream, external to said apparatus;
- d) $P1 < 2 \text{ barg}$.

(11) Apparatus according to embodiment 10, wherein the external heat stream to E1 is steam or a synthesis gas containing sensible heat.

(12) Apparatus according to embodiments 10 and 11, wherein the crude product to be distilled is ethanol or other suitable product.

(13) Plant for distillation of methanol according to embodiments 1 to 9, comprising at least one apparatus according to embodiments 10-11, wherein the amount of steam required for E1 is less than 1.3 kg/kg of product methanol.

(14) Use of apparatus according to embodiments 10-11 in a plant according to embodiment 13, for distillation of methanol according to embodiments 1-9.

(15) Use of the process, apparatus and plant according to embodiments 1-13 comprising N concentration columns V1, V2, V3 and up to Vn, with decreasing pressures $P1 > P2 > P3$ and down to Pn, connected to a stabilizing column V0 at pressure P0, wherein:

A: Feed of crude methanol;

B0 to Bn: Liquid streams comprising methanol, recovered from the lower section of columns V0 to Vn;

C1 to Cn: Product, such as liquid distilled methanol;

E0 to En: Energy streams, in particular heat exchangers;

T0 to Tn: Gaseous streams recovered from the upper section of columns V0 to Vn;

L: Light gaseous stream from Stabilizer;

H: Heavy side stream recovered from the final concentration column Vn;

S: Split of stream Tn-1 in two separate sub-streams, one sub-stream being condensed in heat exchanger E0, supplying energy to V0, and the other sub-stream being condensed in heat exchanger En, supplying energy to concentration column Vn,

V0: Stabilizing column;

5 V1 to Vn: Concentration columns,

Wherein

- Columns V1, V2 and up to Vn operate at decreasing pressures, such that $P1 > P2$ and down to Pn ,

10 - $P0 > 0$ barg and $P1 > 0$ barg

- each column V0, V1, V2 and up to Vn is correspondingly associated to a heat exchanger E0, E1, E2 and up to En, which a reboiler for the same column,

- heat exchangers E0 and En are condensers for column Vn-1;

- heat exchanger E2 is condenser for column V1.

15 and wherein:

- $P1 < 2$ barg; and

- Heat exchanger E1 is supplied by an external energy source.

Claims

1. Process for distillation of methanol, comprising:
 - (i) pre-treatment of a crude stream A of methanol in a stabilizing column V0 at pressure P0, for separation of volatile components, obtaining a stream of light gases L from the upper section of V0 and a liquid stream B0 comprising methanol from the lower section of V0,
 - (ii) B0 is then directed towards concentration column V1, at pressure P1,
 - (iii) gaseous stream T1 recovered from the upper section of V1 is condensed in heat exchanger E2, supplying energy to concentration column V2,
 - (iv) part of the condensed methanol obtained in step (iii) is sent to product C1, and the remaining part of the condensed methanol is added to the upper section of V1 and used as reflux flow,
 - (v) a liquid stream B1 comprising methanol is recovered from the lower section of V1 and passed on to V2, at pressure P2,
 - (vi) gaseous stream T2 recovered from the upper section of V2 is split (S) in two separate streams, one stream being condensed in a heat exchanger E0, supplying energy to V0, and the other stream being condensed in a heat exchanger E3, supplying energy to concentration column V3,
 - (vii) part of the condensed methanol obtained in step (vi) is sent to product, C2, and the remaining part of the condensed methanol is added to the upper section of V2 and used as reflux flow,
 - (viii) a liquid stream B2 comprising methanol is recovered from V2 and passed on to V3, at pressure P3,
 - (ix) gaseous stream T3, recovered from the upper section of V3, is condensed, part of the condensed methanol being sent to product, C3, and the remaining part being added to the upper section of V3 and used as reflux flow,
 - (x) one or more side streams H comprising higher alcohols and other minor biproducts is withdrawn from V3 and a liquid stream B3, is drawn from V3,
- wherein:
- Columns V1, V2 and V3 operate at decreasing pressures, such that $P1 > P2 > P3$
 - $P0 > 0$ barg and $P1 > 0$ barg
 - each column V0, V1, V2 and V3 is correspondingly associated to a heat exchanger E0, E1, E2 and E3, which is a reboiler for the same column,
 - heat exchangers E0 and E3 are condensers for column V2;
 - heat exchanger E2 is condenser for column V1.

characterized in that:

- P1<2 barg; and
- Heat exchanger E1 is supplied by an external energy source.

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2. Process according to claim 1, wherein the temperature in the coldest part of V2 is higher than the temperature in the warmest part of V3 and V0 and the temperature in the coldest part of V1 is higher than the temperature in the warmest part of V2.

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3. Process according to claims 1 and 2 wherein the temperature in the coldest part of V2 is preferably 4 °C higher than the temperature in the warmest part of V3 and V0 and the temperature in the coldest part of V1 is preferably 4 °C higher than the temperature in the warmest part of V2.

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4. Process according to the previous claims wherein the difference between P1 and P0 is greater than or equal to 7.7 bar.

5. Process according to the previous claims, wherein P1 is higher than 9,7 bar(g), P2 is comprised between 6,9 and 13 bar(g).

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6. Process according to the previous claims wherein P1 is preferably 17 bar(g), P2 is preferably 9 bar(g) and P3 is preferably 0,98 bar(g).

7. Process according to the previous claims wherein the heat duty of E0 is at least 30% less than the duty of E1.

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8. Process according to the previous claims wherein B3 comprises the water removed from circulating streams and is recovered from the lower section of V3.

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9. Apparatus for distillation of methanol, comprising a stabilizing column V0, at pressure P0, connected in series with at least 3 distillation columns V1, V2 and V3 at correspondingly decreasing pressure P1, P2 and P3 wherein each column is associated to a heat exchanger E0, E1, E2 and E3, said heat exchanger being a reboiler for that column, characterized in that,

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- a) heat exchangers E0 and E3 are condensers of column V2;

- b) heat exchanger E2 is condenser of column V1;
- c) E1 has an incoming heat stream, external to said apparatus;
- d) $P1 < 2$ barg.

5 10. Apparatus according to claim 9 wherein the external heat stream to E1 is steam or a synthesis gas containing sensible heat.

11. Plant for distillation of methanol according to claims 1 to 8 comprising at least one apparatus according to claims 9-10, wherein the amount of steam required for E1 is
10 less than 1.3 kg/kg of product methanol.

12. Use of apparatus according to claims 9-10 in a plant according to claim 11, for distillation of methanol according to claims 1-8.

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