

DESCRIPTION

TITLE OF INVENTION:

FLUX CORED WIRE FOR GAS SHIELD ARC WELDING AND WELDING
METAL

5

TECHNICAL FIELD

[0001]

The present invention relates to a flux-cored wire for gas-shielded arc welding that enables to obtain a weld metal having good low-temperature toughness, and the weld
10 metal.

BACKGROUND ART

[0002]

In recent years, energy development is expanding into colder regions and waters,
15 and a cryogenic steel has been used for a structure in such cold regions and cold waters. However, for the structure in these cold regions and cold waters, a structure design in consideration of weather conditions in the regions and waters where the structure operates has been executed in addition to the conventional requirement for low-temperature toughness, and a steel material having higher toughness is demanded. Furthermore, for
20 the purpose of achieving high efficiency and deskillling of welding, a requirement for application of a flux-cored wire to welding of this kind of cryogenic steel is increasing.

[0003]

Based on such background, Patent Literature 1 discloses a technique that the toughness at low temperatures is enhanced by controlling the chemical components and the
25 amount of solute Ti of the weld metal. In the technique described in Patent Literature 1, attention is focused on the formation of acicular ferrite inside prior γ grains.

[0004]

In addition, Patent Literature 2 discloses a flux-cored wire for gas-shielded arc welding for a high tensile steel having a tensile strength of 680 N/mm² class or more. In
30 the technique described in Patent Literature 2, strength corresponding to the base metal strength and good toughness are ensured in a wide range of use from small heat input to large heat input by specifying appropriate ranges for the contents of C, Si, Mn, P, S, Ni, Cr and Mo based on the total weight of wire and specifying the addition amount of Ta, and

furthermore, the weight ratio of metal powders in the flux is specified for enhancing the operating efficiency.

CITATION LIST

5 PATENT LITERATURE

[0005]

Patent Literature 1: JP-A-2000-263283

Patent Literature 2: JP-A-H03-294093

10 SUMMARY OF INVENTION

TECHNICAL PROBLEM

[0006]

However, in Patent Literature 1, toughness is enhanced by reducing formation of acicular ferrite inside the prior γ grains, but attention is not paid to the viewpoint of
15 alleviating stress concentration on inclusions or the viewpoint of reducing the brittle fracture rate of the weld metal. Accordingly, the toughness of the weld metal when welding a cryogenic steel is not sufficient.

[0007]

In Patent Literature 2, attention is not paid to the viewpoint of alleviating stress
20 concentration on inclusions or the viewpoint of reducing the brittle fracture rate of the weld metal. Accordingly, the toughness of the weld metal when welding a cryogenic steel is not sufficient.

[0008]

The present invention has been made in consideration of these problems, and an
25 object of the present invention is to provide a flux-cored wire enabling to obtain a weld metal having both good low-temperature toughness and high strength when assembling a structure by gas-shielded arc welding of a cryogenic steel and achieve good welding workability, and to provide the weld metal.

30 SOLUTION TO PROBLEM

[0009]

As described above, in Patent Literatures 1 and 2, the brittle fracture rate is not studied. Here, the brittle fracture rate indicates a percentage of brittle fracture occurring

when a load is applied in a Charpy impact test. In a region where brittle fracture occurred, the energy absorbed until reaching fracture by a steel material is extremely reduced, and the fracture easily proceeds. Accordingly, in particular for inhibiting the fracture at low temperatures, a requirement to not only improve an absorption energy at
5 low temperatures in a general Charpy impact test but also prevent the formation of a brittle fracture surface is considered to be very important.

[0010]

In addition, as described above, energy development is expanded into colder regions and waters and as for a structure in such cold regions and cold waters, the
10 low-temperature toughness is required to be improved, but it is important particularly for a structure used at low temperatures to avoid an unstable fracture involving the brittle fracture and more increase the safety of the structure used in a low-temperature environment. Here, in a low alloy steel weld metal formed by gas-shielded arc welding, a large amount of oxygen is contained, and most thereof is present as an oxide-based
15 inclusion in the weld metal. At the time of fracture of the weld metal, stress concentration occurs around the oxide-based inclusion, and particularly, in a low-temperature environment, the brittle fracture is expected to be promoted by stress concentration around the oxide-based inclusion. Therefore, in order to more increase the safety of a structure used at low temperatures, the brittle fracture needs to be avoided, and
20 it is considered to be important to alleviate stress concentration on an oxide-based inclusion.

[0011]

Based on these considerations, the present inventors have studied a technique for alleviating stress concentration on oxide-based inclusions. As a result, it has been newly
25 found that reducing the glass phase present in an oxide-based inclusion is effective. The oxide-based inclusion is a composite phase composed of a glass phase and other various crystal phases. Here, the Young's modulus of the glass phase is low compared with the base metal phase of the weld metal and since stress is likely to concentrate on the glass phase having a low Young's modulus, compared with the base metal phase, when many
30 glass phases are present in the oxide-based inclusions, the brittle fracture readily occurs.

[0012]

Accordingly, the present inventors have studied a means for reducing the glass phase in the oxide-based inclusion so as to reduce the brittle fracture. In addition, taking

note of the fact that the glass phase mainly includes SiO_2 , the present inventors have further studied reducing the amount of SiO_2 in the oxide-based inclusion of the weld metal and have conceived an idea of controlling a ratio between a deoxidizing element (Mn, Ti, Al, Ca) contained in the flux-cored wire and Si so as to reduce the amount of SiO_2 in the oxide-based inclusion. It has been found that according to the finding above, the brittle fracture rate at low temperatures as well as the absorption energy at low temperatures in a Charpy impact test of the weld metal can be improved, and then the invention is accomplished.

[0013]

10 More specifically, the present invention relates to a flux-cored wire for gas-shielded arc welding, containing, based on total mass of the wire:

C: from 0.03 to 0.12 mass%;

Si in terms of Si in Si alloy and Si compound: from 0.10 to 0.50 mass%;

Mn: from 1.0 to 4.0 mass%;

15 Ti in terms of Ti in Ti alloy and Ti compound: from 2.4 to 4.5 mass%;

Al: from 0.005 to 0.050 mass%;

at least one of Ni: from 0.30 to 3.50 mass% and B: from 0.0008 to 0.012 mass%;

and

Fe: 80 mass% or more, and

20 satisfying $(\text{Ti} + \text{Mn} + \text{Al}) / \text{Si} \geq 15$.

[0014]

The flux-cored wire for gas-shielded arc welding above may further contain, based on the total mass of the wire: ZrO_2 : from 0.02 to 0.50 mass%; and Al_2O_3 : from 0.02 to 0.80 mass%.

25 [0015]

The flux-cored wire for gas-shielded arc welding above may further contain at least one member selected from the group consisting of, based on the total mass of the wire: Cu: 0.40 mass% or less; Cr: 1.0 mass% or less; Mo: 0.35 mass% or less; Nb: 0.030 mass% or less; and V: 0.050 mass% or less.

30 [0016]

The flux-cored wire for gas-shielded arc welding above may further contain at least one member selected from the group consisting of, based on the total mass of the wire: a total of Li, Na and K: 1.0 mass%; and Ca: 1.0 mass% or less.

[0017]

The flux-cored wire for gas-shielded arc welding above may further contain, based on the total mass of the wire: Mg: 1.0 mass% or less.

[0018]

5 The flux-cored wire for gas-shielded arc welding above may further contain, based on the total mass of the wire: F: 1.0 mass% or less.

[0019]

One preferred embodiment of the flux-cored wire for gas-shielded arc welding above satisfies:

10 Si in terms of Si in Si alloy and Si compound: from 0.10 to 0.45 mass%
Mn: from 1.1 to 3.4 mass%, and
Ti in terms of Ti in Ti alloy and Ti compound: from 2.4 to 4.0 mass%
and contains both of Ni: from 1.00 to 3.50 mass% and B: from 0.0008 to 0.012 mass%.

15 [0020]

The invention also relates to a weld metal containing:

C: from 0.04 to 0.12 mass%;

Si: from 0.05 to 0.30 mass%;

Mn: from 0.80 to 3.00 mass%;

20 Ti: from 0.030 to 0.100 mass%;

Al: from 0.002 to 0.010 mass%;

O: from 0.030 to 0.070 mass%;

N: more than 0 and 0.01 mass% or less; and

at least one of Ni: from 0.30 to 3.50 mass% and B: from 0.0005 to 0.0070 mass%,

25 with the remainder consisting of Fe and inevitable impurities,

wherein an average composition of oxide-based inclusions having a minor

diameter of 1 μm or more contained in the weld metal satisfies, by mass%, the following requirements (1) and (2):

$$\text{Al}_2\text{O}_3 + \text{SiO}_2 + \text{MnO} + \text{TiO}_2 \geq 70\% \quad (1)$$

30 $(\text{TiO}_2 + \text{MnO} + \text{Al}_2\text{O}_3) / \text{SiO}_2 \geq 5 \quad (2)$

[0021]

The weld metal above may further contain at least one member selected from the group consisting of: Cu: 0.40 mass% or less; Cr: 1.0 mass% or less; Mo: 0.35 mass% or less; Nb: 0.020 mass% or less; and V: 0.050 mass% or less.

[0022]

- 5 One preferred embodiment of the weld metal above is one satisfying:
 Si: from 0.05 to 0.25 mass%;
 Mn: from 1.00 to 2.40 mass%; and
 Ti: from 0.030 to 0.090 mass%, and
 containing both of Ni: from 1.00 to 3.50 mass% and B: from 0.0005 to 0.0070
 10 mass%,
 wherein a rate of acicular ferrite formation defined by the following formula is
 15 15% or more:

Rate of acicular ferrite formation (%) = (number of inclusions acting as a start point of acicular ferrite/number of all inclusions)×100

15

ADVANTAGEOUS EFFECTS OF INVENTION

[0023]

- According to the invention, low-temperature toughness that has not been conventionally obtained as a weld metal can be obtained by controlling the composition of
 20 the weld metal and the composition of an oxide-based inclusion. The above-described weld metal having excellent toughness at low temperatures can be obtained by properly controlling the composition of the flux-cored wire. Therefore, according to the invention, the safety of a structure used in a low-temperature environment can be more increased.

25 DESCRIPTION OF EMBODIMENTS

[0024]

The embodiments for carrying out the present invention are described in detail below. However, the present invention is not limited to the following embodiments.

[0025]

30 [First Embodiment]

<Flux-Cored Wire for Gas-Shielded Arc Welding>

The flux-cored wire for gas-shielded arc welding (hereinafter, sometimes simply referred to as "flux-cored wire" or "wire") of this embodiment contains, based on total

mass of the wire: C: from 0.03 to 0.12 mass%; Si in terms of Si in Si alloy and Si compound: from 0.10 to 0.50 mass%; Mn: from 1.0 to 4.0 mass%; Ti in terms of Ti in Ti alloy and Ti compound: from 2.4 to 4.5 mass%; Al: from 0.005 to 0.050 mass%; at least one of Ni: from 0.30 to 3.50 mass% and B: from 0.0008 to 0.012 mass%; and Fe: 80 mass% or more, and satisfies $(\text{Ti}+\text{Mn}+\text{Al})/\text{Si} \geq 15$.

[0026]

The reason for numerical limitation on the amount of each component contained in the flux-cored wire for gas-shielded arc welding of this embodiment is described below. In the following, the amount of each component in the flux-cored wire for gas-shielded arc welding is a content based on the total mass of the flux-cored wire for gas-shielded arc welding, i.e., a content based on the total mass of the wire.

In addition, in the present description, the percentage on a mass basis (mass%) has the same meaning as the percentage on a weight basis (wt%). Furthermore, the numerical range expressed using "to" means to be equal to or more than the lower limit and equal to or less than the upper limit.

[0027]

(C: from 0.03 to 0.12 mass%)

C is an element effective in enhancing the strength of the weld metal. However, if the amount of C is excessive, the strength may increase excessively, causing deterioration of the toughness. On the other hand, if the amount of C is too small, a lack of strength may be caused and coarse grain boundary ferrite, which adversely affects the toughness, is formed.

From these viewpoints, the C amount in the wire is 0.12% or less, preferably 0.09% or less, more preferably 0.08% or less. In addition, the C amount in the wire is 0.03% or more, preferably 0.04% or more, more preferably 0.05% or more.

[0028]

(Si in terms of Si in Si alloy and Si compound: from 0.10 to 0.50 mass%)

Si is an element acting as a deoxidizer and is also important in controlling the glass phase of an oxide-based inclusion. However, if the amount of Si is excessive, the glass phase of an oxide-based inclusion may increase, leading to a reduction in the toughness. On the other hand, if the amount of Si is too small, a blowhole may be formed due to insufficient deoxidation.

From these viewpoints, the Si amount in the wire is, in terms of Si in an Si alloy and an Si compound, 0.50% or less, preferably 0.30% or less, more preferably 0.25% or less. In addition, the Si amount in the wire is, in terms of Si in an Si alloy and an Si compound, 0.10% or more, preferably 0.13% or more, more preferably 0.15% or more.

5 Here, examples of the Si source also include potash glass and soda glass, besides SiO_2 , K_2SiF_6 , etc.

[0029]

(Mn: from 1.0 to 4.0 mass%)

Mn acts as a deoxidizer and is an element affecting the strength and toughness.

10 However, if the amount of Mn is excessive, the strength may increase excessively and the hardenability during quenching may increase excessively, leading to a reduction in the toughness. On the other hand, if the amount of Mn is too small, a lack of strength may be caused and coarse grain boundary ferrite, which adversely affects the toughness, is formed.

From these viewpoints, the Mn amount in the wire is 4.0% or less, preferably 3.0% or less, more preferably 2.7% or less. In addition, the Mn amount in the wire is 1.0% or more, preferably 2.3% or more, more preferably 2.6% or more.

[0030]

(Ti in terms of Ti in Ti alloy and Ti compound: from 2.4 to 4.5 mass%)

20 Ti is an element acting as a deoxidizer, and an oxide-based inclusion thereof acts as a nucleus of acicular ferrite. However, if the amount of Ti is excessive, an excess of solute Ti may be formed and not only the strength may increase excessively but also the toughness may deteriorate. On the other hand, if the amount of Ti is too small, ferrite may be coarsened, causing deterioration of the toughness.

From these viewpoints, the Ti amount in the wire is, in terms of Ti in Ti alloy and 25 Ti compound, 4.5% or less, preferably 3.6% or less, more preferably 3.2% or less. In addition, the Ti amount in the wire is, in terms of Ti in Ti alloy and Ti compound, 2.4% or more, preferably 2.6% or more, more preferably 2.8% or more.

Here, examples of the Ti source include TiO_2 , etc.

[0031]

30 (Al: from 0.005 to 0.050 mass%)

Al is an element acting as a deoxidizer. However, if the amount of Al is excessive, nucleation of acicular ferrite may be prevented, causing deterioration of the

toughness. On the other hand, if the amount of Al is too small, a blowhole may be formed due to insufficient deoxidation.

From these viewpoints, the Al amount in the wire is 0.050% or less, preferably 0.048% or less, more preferably 0.045% or less. In addition, the Al amount in the wire is

[0032]

(At least one of Ni: from 0.30 to 3.50 mass% and B: from 0.0008 to 0.012 mass%)

Ni is an element having an action of enhancing the toughness of the weld metal and also has an action of promoting acicular ferrite formation by retarding the formation of a grain boundary bainite structure competing with acicular ferrite. However, if the amount of Ni is excessive, high-temperature cracking may occur. In addition, the amount of martensite formed may increase to raise the strength and in turn, the Charpy impact absorption energy may decrease. On the other hand, if the amount of Ni is too small, the toughness may deteriorate.

Similarly, B is an element having an action of enhancing the toughness of the weld metal and contributes to a reduction in the brittle fracture rate at low temperatures by reducing grain boundary ferrite, which adversely affects the toughness. However, if the amount of B is excessive, high-temperature cracking may occur. On the other hand, if the amount of B is too small, the toughness may deteriorate.

The wire of this embodiment contains at least one of Ni and B in a specific amount range.

More specifically, in the case of containing Ni, from the above-described viewpoint, the Ni amount in the wire is 3.50% or less, preferably 3.00% or less, more preferably 2.50% or less. In addition, the Ni amount in the wire is 0.30% or more, preferably 0.50% or more, more preferably 0.70% or more, still more preferably 1.50% or more.

In the case of containing B, from the above-described viewpoint, the B amount in the wire is 0.012% or less, preferably 0.010% or less, more preferably 0.007% or less. In addition, the B amount in the wire is 0.0008% or more, preferably 0.0010% or more, more preferably 0.0015% or more.

[0033]

$((\text{Ti}+\text{Mn}+\text{Al})/\text{Si})\geq 15$

(Ti+Mn+Al)/Si is a parameter indicative of the amount of the glass phase in an oxide-based inclusion of the weld metal. Since the glass phase in an oxide-based inclusion mainly consists of SiO₂, when the amount of SiO₂ in an oxide-based inclusion of the weld metal is reduced, the proportion of the glass phase having a low Young's modulus in an oxide-based inclusion can be reduced, and occurrence of brittle fracture can be prevented.

From these viewpoints, in this embodiment, the ratio ((Ti+Mn+Al)/Si) of the total amount of deoxidizing elements (Mn, Ti and Al) contained in the wire to the Si amount is 15 or more, preferably 20 or more, more preferably 30 or more. On the other hand, the upper limit of (Ti+Mn+Al)/Si is not particularly limited but the ratio is preferably 85.5 or less, more preferably 80 or less.

[0034]

(Fe and inevitable impurities)

The remainder of the flux-cored wire of this embodiment consists of Fe and inevitable impurities.

Fe of the remainder includes Fe constituting the outer shell, an iron powder added to the flux, and Fe of an alloy powder. The flux-cored wire of this embodiment contains Fe in an amount of 80 mass% or more, preferably 82 mass% or more, more preferably 84 mass% or more.

The upper limit of the amount of Fe is not particularly limited but the amount of Fe is, for example, 96 mass% or less in relation to other component composition.

Examples of the inevitable impurities of the remainder include P, S, Sn, Pb, Sb, etc.

Furthermore, in the flux-cored wire of this embodiment, an alloy element other than the above-described elements, a slag forming agent, an arc stabilizer, etc. may be added in addition to each of the components described above, as long as the effects of the present invention are not inhibited. In the case where each element is added as an oxide or a nitride, the remainder of the flux-cored wire of this embodiment contains O or N as well.

[0035]

Furthermore, in addition to each of the components described above, the flux-cored wire of this embodiment may further contain a predetermined amount of at least one of the following components.

[0036]

(Cu: 0.40 mass% or less)

Cu is an element effective in ensuring the strength of the weld metal. However, if the amount of Cu is excessive, the strength may increase excessively, causing deterioration of the toughness.

From these viewpoints, in the case of incorporating Cu into the wire, it is sufficient as long as the Cu amount in the wire is more than 0%, but the amount is preferably 0.01% or more, more preferably 0.05% or more, still more preferably 0.10% or more. In addition, the Cu amount in the wire is preferably 0.40% or less, more preferably 0.30% or less, still more preferably 0.25% or less.

[0037]

(Cr: 1.0 mass% or less)

Cr is an element effective in ensuring the strength of the weld metal. However, if the amount of Cr is excessive, the strength may increase excessively, causing deterioration of the toughness.

From these viewpoints, in the case of incorporating Cr into the wire, it is sufficient as long as the Cr amount in the wire is more than 0%, but the amount is preferably 0.01% or more, more preferably 0.05% or more, still more preferably 0.10% or more. In addition, the Cr amount in the wire is preferably 1.0% or less, more preferably 0.8% or less, still more preferably 0.6% or less.

[0038]

(Mo: 0.35 mass% or less)

Mo is an element effective in ensuring the strength of the weld metal. However, if the amount of Mo is excessive, the strength may increase excessively, causing deterioration of the toughness.

From these viewpoints, in the case of incorporating Mo into the wire, it is sufficient as long as the Mo amount in the wire is more than 0%, but the amount is preferably 0.01% or more, more preferably 0.05% or more, still more preferably 0.10% or more. In addition, the Mo amount in the wire is preferably 0.35% or less, more preferably 0.30% or less, still more preferably 0.25% or less, yet still more preferably 0.20% or less.

[0039]

(Nb: 0.030 mass% or less)

Nb is an element effective in ensuring the strength of the weld metal. However, if the amount of Nb is excessive, the strength may increase excessively, causing deterioration of the toughness.

From these viewpoints, in the case of incorporating Nb into the wire, it is sufficient as long as the Nb amount in the wire is more than 0%, but the amount is preferably 0.001% or more, more preferably 0.005% or more, still more preferably 0.008% or more. In addition, the Nb amount in the wire is preferably 0.030% or less, more preferably 0.020% or less, still more preferably 0.015% or less.

[0040]

10 (V: 0.050 mass% or less)

V is an element effective in ensuring the strength of the weld metal. However, if the amount of V is excessive, the strength may increase excessively, causing deterioration of the toughness.

From these viewpoints, in the case of incorporating V into the wire, it is sufficient as long as the V amount in the wire is more than 0%, but the amount is preferably 0.001% or more, more preferably 0.005% or more, still more preferably 0.008% or more. In addition, the V amount in the wire is preferably 0.050% or less, more preferably 0.020% or less, still more preferably 0.015% or less.

[0041]

20 (A total of Li, Na and K: 1.0 mass% or less)

Li, Na and K are elements having an effect of enhancing the arc stability and reducing spatter generation. However, if the amounts of these elements are excessive, the hygroscopicity resistance may deteriorate, causing a problem with low-temperature cracking resistance and porosity resistance.

From these viewpoints, in the case of incorporating one or more of Li, it is sufficient as long as the total amount of Li, Na and K in the wire is more than 0%, but the total amount is preferably 0.005% or more, more preferably 0.010% or more, still more preferably 0.020% or more. In addition, the total amount of Li, Na and K in the wire is preferably 1.0% or less, more preferably 0.50% or less, still more preferably 0.20% or less.

[0042]

30 (Ca: 1.0 mass% or less)

Ca is an element having an effect of enhancing the arc stability and reducing spatter generation. However, if the amount of Ca is excessive, the amount of spatter generation rather increases.

From these viewpoints, in the case of incorporating Ca into the wire, it is sufficient as long as the Ca amount in the wire is more than 0%, but the amount is preferably 0.005% or more, more preferably 0.050% or more, still more preferably 0.20% or more. In addition, the Ca amount in the wire is preferably 1.0% or less, more preferably 0.90% or less, still more preferably 0.70% or less.

[0043]

10 (Mg: 1.0 mass% or less)

Mg is an element having an effect of enhancing the arc stability and reducing spatter. However, if the amount of Mg is excessive, spatter generation rather increases.

From these viewpoints, in the case of incorporating Mg into the wire, it is sufficient as long as the Mg amount in the wire is more than 0%, but the amount is preferably 0.005% or more, more preferably 0.050% or more, still more preferably 0.20% or more. In addition, the Mg amount in the wire is preferably 1.0% or less, more preferably 0.90% or less, still more preferably 0.70% or less.

[0044]

20 In the case of incorporating both Mg and Ca, the total amount of Mg and Ca is preferably 1.0% or less, more preferably 0.90% or less, still more preferably 0.70% or less. In addition, the total amount of Mg and Ca is preferably 0.005% or more, more preferably 0.050% or more, still more preferably 0.20% or more.

[0045]

(F: 1.0 mass% or less)

25 F may be incorporated into the wire so as to adjust the arc spraying force (concentration) and reduce the amount of hydrogen diffused in the deposited metal. However, if the amount of F becomes excessive, the fume emission and spatter generated may increase.

30 From these viewpoints, in the case of incorporating F into the wire, it is sufficient as long as the F amount in the wire is more than 0%, but the amount is preferably 0.010% or more, more preferably 0.025% or more, still more preferably 0.050% or more. In addition, the F amount in the wire is preferably 1.0% or less, more preferably 0.60% or less, still more preferably 0.40% or less.

[0046]

(ZrO₂: from 0.02 to 0.50 mass%)

ZrO₂ is a component having an effect of enhancing the bead smoothness. However, if the amount of ZrO₂ is excessive, a convex bead shape may be formed in a vertical position. On the other hand, if the amount of ZrO₂ is too small, the bead smoothness may deteriorate.

From these viewpoints, in the case of incorporating ZrO₂ into the wire, the ZrO₂ amount in the wire is preferably 0.02% or more, more preferably 0.05% or more. In addition, the ZrO₂ amount in the wire is preferably 0.50% or less, more preferably 0.45% or less.

[0047]

(Al₂O₃: from 0.02 to 0.80 mass%)

Al₂O₃ is a component having an effect of enhancing the bead smoothness. However, if the amount of Al₂O₃ is excessive, the bead wettability may deteriorate or spatter may be generated. On the other hand, if the amount of Al₂O₃ is too small, the bead smoothness may deteriorate.

From these viewpoints, in the case of incorporating Al₂O₃ into the wire, the Al₂O₃ amount in the wire is preferably 0.02% or more, more preferably 0.05% or more. In addition, the Al₂O₃ amount in the wire is preferably 0.80% or less, more preferably 0.60% or less.

The amount of Al metal is not regarded as the amount of Al₂O₃.

[0048]

In one preferred embodiment, the flux-cored wire for gas-shielded arc welding of this embodiment satisfies Si in terms of Si in Si alloy and Si compound: from 0.10 to 0.45 mass%, Mn: from 1.1 to 3.4 mass%, and Ti in terms of Ti in Ti alloy and Ti compound: from 2.4 to 4.0 mass%, and contains both of Ni: from 1.00 to 3.50 mass% and B: from 0.0008 to 0.012 mass%.

[0049]

More specifically, the flux-cored wire for gas-shielded arc welding according to this one preferred embodiment is a core-fluxed wire for gas-shielded arc welding, containing, based on the total mass of the wire:

C: from 0.03 to 0.12 mass%;

Si in terms of Si in Si alloy and Si compound: from 0.10 to 0.45 mass%;

Mn: from 1.1 to 3.4 mass%;

Ti in terms of Ti in Ti alloy and Ti compound: from 2.4 to 4.0 mass%;

Al: from 0.005 to 0.050 mass%;

Ni: from 1.00 to 3.50 mass%;

5 B: from 0.0008 to 0.012 mass%; and

Fe: 80 mass% or more, and

satisfying $(\text{Ti}+\text{Mn}+\text{Al})/\text{Si} \geq 15$.

[0050]

According to the flux-cored wire for gas-shielded arc welding of this embodiment,
 10 for the above-described reasons, the glass phase having a low Young's modulus in an
 oxide-based inclusion of the weld metal can be reduced. In addition, both a specific
 amount of Ni and a specific amount of B are contained, and the Si amount, the Mn amount
 and the Ti amount are further controlled in respective specific ranges, so that while
 reducing formation of coarse grain boundary ferrite, which adversely affects the toughness,
 15 formation of grain boundary bainite competing with acicular ferrite can be inhibited,
 thereby enabling to increase a fine acicular ferrite (AF) structure formed starting from an
 inclusion, which is effective in improving the low-temperature toughness. Consequently,
 the low-temperature toughness can be further improved.

[0051]

20 The flux-cored wire of this embodiment is a wire obtained typically by filling a
 steel-made outer shell with a flux. More specifically, the flux-cored wire according to
 this embodiment is composed of a stainless steel- or soft steel-made outer shell taking on a
 tubular shape and a flux filling the interior (inner side) of the outer shell.

The flux-cored wire may be in either form of a seamless one having no seam on
 25 the outer shell or a seam one having a seam on the outer shell. Furthermore, in the
 flux-cored wire, the wire surface (outside of the outer shell) may or may not be subjected
 to plating, etc.

[0052]

Then, one embodiment of the method for producing the flux-cored wire of this
 30 embodiment is described.

In the production of the flux-cored wire of this embodiment, first, the interior of a
 steel-made outer shell is filled with a flux. On this occasion, a soft steel or low alloy steel
 having good wire drawability is preferably used for the outer shell. In addition, the

composition and filling rate of the flux can be appropriately adjusted depending on the composition, thickness, etc. of the outer shell such that the total wire composition falls in the above-described range.

The wire in which the interior of the outer shell is filled with a flux is then drawn using a pore die or a roller die to decrease in diameter, and a flux-cored wire having a predetermined outside diameter is thereby obtained.

[0053]

The outside diameter of the flux-cored wire of this embodiment is not particularly limited but in view of productivity of the wire, is preferably from 1.0 to 2.0 mm, more preferably from 1.2 to 1.6 mm.

The flux filling rate may be set to any value as long as each component in the wire falls within the range of the present invention, but in view of wire drawability and workability (e.g., feedability) during welding, the flux filling rate is preferably from 10 to 25 mass%, more preferably from 13 to 16 mass%, based on the total mass of the wire.

The flux filling rate is defined as the ratio of the mass of the flux filling the interior of the outer shell to the total mass of the wire (i.e., outer shell + flux).

[0054]

<Weld Metal>

The weld metal (low alloy steel weld metal) of this embodiment is a weld metal containing: C: from 0.04 to 0.12 mass%; Si: from 0.05 to 0.30 mass%; Mn: from 0.80 to 3.00 mass%; Ti: from 0.030 to 0.100 mass%; Al: from 0.002 to 0.010 mass%; O: from 0.030 to 0.070 mass%; N: more than 0 and 0.01 mass% or less; and at least one of Ni: from 0.30 to 3.50 mass% and B: from 0.0005 to 0.0070 mass%, with the remainder consisting of Fe and inevitable impurities,

wherein the average composition of oxide-based inclusions having a minor diameter of 1 μm or more contained in the weld metal satisfies, by mass%, the following requirements (1) and (2):

$$\text{Al}_2\text{O}_3 + \text{SiO}_2 + \text{MnO} + \text{TiO}_2 \geq 70\% \quad (1)$$

$$(\text{TiO}_2 + \text{MnO} + \text{Al}_2\text{O}_3) / \text{SiO}_2 \geq 5 \quad (2)$$

[0055]

The weld metal of this embodiment is, for example, a weld metal having excellent low-temperature toughness obtained by gas-shielded arc welding using the above-described flux-cored wire for gas-shielded arc welding.

[0056]

The reason for numerical limitation on the amount of each of components contained in the weld metal of this embodiment is described below. The amount of each component in the weld metal is a content based on the total mass of the weld metal, i.e., a content based on the total mass of the weld metal.

[0057]

(C: from 0.04 to 0.12 mass%)

The reason for numerical limitation on the C amount in the weld metal is the same as the reason for numerical limitation on the C amount in the wire above.

Accordingly, the C amount in the weld metal is 0.12% or less, preferably 0.10% or less, more preferably 0.08% or less. In addition, the C amount in the weld metal is 0.04% or more, preferably 0.05% or more, more preferably 0.06% or more.

[0058]

(Si: from 0.05 to 0.30 mass%)

The reason for numerical limitation on the Si amount in the weld metal is the same as the reason for numerical limitation on the C amount in the wire above.

Accordingly, the Si amount in the weld metal is 0.30% or less, preferably 0.25% or less, more preferably 0.20% or less, still more preferably 0.15% or less. In addition, the Si amount in the weld metal is 0.05% or more, preferably 0.07% or more, more preferably 0.09% or more.

[0059]

(Mn: from 0.80 to 3.00 mass%)

The reason for numerical limitation on the Mn amount in the weld metal is the same as the reason for numerical limitation on the Mn amount in the wire above.

Accordingly, the Mn amount in the weld metal is 3.00% or less, preferably 2.50% or less, more preferably 1.90% or less. In addition, the Mn amount in the weld metal is 0.80% or more, preferably 1.20% or more, more preferably 1.50% or more.

[0060]

(Ti: from 0.030 to 0.100 mass%)

The reason for numerical limitation on the Ti amount in the weld metal is the same as the reason for numerical limitation on the Ti amount in the wire above.

Accordingly, the Ti amount in the weld metal is 0.100% or less, preferably 0.080% or less, more preferably 0.070% or less. In addition, the Ti amount in the weld metal is 0.030% or more, preferably 0.040% or more, more preferably 0.050% or more.
[0061]

5 (Al: from 0.002 to 0.010 mass%)

The reason for numerical limitation on the Al amount in the weld metal is the same as the reason for numerical limitation on the Al amount in the wire above.

Accordingly, the Al amount in the weld metal is 0.010% or less, preferably 0.008% or less, more preferably 0.006% or less. In addition, the Al amount in the weld
10 metal is 0.002% or more, preferably 0.003% or more, more preferably 0.004% or more.
[0062]

(O: from 0.030 to 0.070 mass%)

O is an element contributing to the formation of slag ensuring the welding workability. If the amount of O is excessive, an oxide-based inclusion may increase,
15 causing deterioration of the toughness. On the other hand, if the amount of O is too small, the welding workability may seriously deteriorate.

From these viewpoints, the O amount in the weld metal is 0.070% or less, preferably 0.060% or less, more preferably 0.055% or less. In addition, the O amount in the weld metal is 0.030% or more, preferably 0.035% or more, more preferably 0.040% or
20 more.

[0063]

(N: more than 0 and 0.01 mass% or less)

If N is incorporated in an excessive amount, the strength may increase excessively, causing deterioration of the toughness, but it is industrially difficult to reduce
25 the N amount to 0%.

Accordingly, the N amount in the weld metal is controlled to be more than 0 and 0.01% or less. The N amount is preferably 0.007% or less, more preferably 0.006% or less.

[0064]

30 (At least one of Ni: from 0.30 to 3.50 mass% and B: from 0.0005 to 0.0070 mass%)

The reason for numerical limitation on the Ni amount in the weld metal is the same as the reason for numerical limitation on the Ni amount in the wire above.

In addition, the reason for numerical limitation on the B amount in the weld metal is the same as the reason for numerical limitation on the B amount in the wire above.

The weld metal of this embodiment contains at least one of Ni and B in a specific amount range.

5 In the case of incorporating Ni into the weld metal, the Ni amount in the weld metal is 3.50% or less, preferably 3.00% or less, more preferably 2.70% or less. In addition, the Ni amount in the wire is 0.30% or more, preferably 0.80% or more, more preferably 1.00% or more, still more preferably 2.00% or more.

10 In the case of incorporating B into the weld metal, the B amount in the weld metal is 0.0070% or less, preferably 0.0050% or less, more preferably 0.0030% or less. In addition, the B amount in the wire is 0.0005% or more, preferably 0.0010% or more, more preferably 0.0015% or more.

[0065]

(Fe and Inevitable impurities)

15 The remainder of the weld metal of this embodiment consists of Fe and inevitable impurities.

The amount of Fe of the remainder is, for example, 90 mass% or more, preferably 90.5 mass% or more, more preferably 91 mass% or more.

20 The upper limit of the amount of Fe is not particularly limited but the amount of Fe is, for example, 98.8 mass% or less in relation to other component composition.

The inevitable impurities of the remainder may be impurities in which a component (e.g., P, S, Sn, Pb, Sb) other than the above-described components, or the later-described components (e.g., Nb, V, Cu) that may be selectively contained are inevitably contained, and these components are allowed to be contained as long as the effects of the present invention are not inhibited.

[0066]

In the weld metal of this embodiment, the average composition of oxide-based inclusions having a minor diameter of 1 μm or more contained in the weld metal satisfies, by mass%, the following requirements (1) and (2):

30 $\text{Al}_2\text{O}_3 + \text{SiO}_2 + \text{MnO} + \text{TiO}_2 \geq 70\%$ (1)

$(\text{TiO}_2 + \text{MnO} + \text{Al}_2\text{O}_3) / \text{SiO}_2 \geq 5$ (2)

[0067]

$(\text{Al}_2\text{O}_3 + \text{SiO}_2 + \text{MnO} + \text{TiO}_2 \geq 70\%)$

$\text{Al}_2\text{O}_3+\text{SiO}_2+\text{MnO}+\text{TiO}_2$ is a parameter indicative of the composition of the oxide-based inclusion, and if it is less than 70%, a fine acicular ferrite structure formed starting from an inclusion may decrease, leading to a reduction in the low-temperature toughness.

5 Accordingly, in the weld metal of this embodiment, the average composition of oxide-based inclusions is controlled to satisfy, by mass%, $\text{Al}_2\text{O}_3+\text{SiO}_2+\text{MnO}+\text{TiO}_2$ of 70% or more, preferably 75% or more, more preferably 80% or more.

[0068]

$((\text{TiO}_2+\text{MnO}+\text{Al}_2\text{O}_3)/\text{SiO}_2 \geq 5)$

10 $(\text{TiO}_2+\text{MnO}+\text{Al}_2\text{O}_3)/\text{SiO}_2$ is a parameter indicative of the amount of the glass phase in an oxide-based inclusion, and if it is less than 5, the amount of the glass phase may increase, causing deterioration of the toughness.

Accordingly, in the weld metal of this embodiment, the average composition of oxide-based inclusions is controlled to satisfy $(\text{TiO}_2+\text{MnO}+\text{Al}_2\text{O}_3)/\text{SiO}_2$ of 5 or more, preferably 10 or more, more preferably 20 or more.

[0069]

The average composition of oxide-based inclusions having a minor diameter of 1 μm or more contained in the weld metal can be measured by the Electron Probe X-ray Micro Analyzer (EPMA) method. In addition, the oxide-based inclusion contains TiO_2 , MnO , Al_2O_3 , and SiO_2 , and the components of the remainder are inevitable oxides and inevitable fluorides. The inevitable oxide is an oxide unavoidably contained during welding, etc. and examples thereof includes, for example, ZrO_2 , Cr_2O_3 , Li_2O , Na_2O , MgO , CaO , FeO , Fe_3O_4 , and Fe_2O_3 . Examples of the inevitable fluoride include CaF_2 . The inevitable oxide or the inevitable fluoride may be contained as long as it does not adversely affect the properties described above and desired properties are obtained. The total mass percentage of inevitable oxide and inevitable fluoride based on the total mass of the oxide-based inclusion is, typically, preferably less than 30%, more preferably 20% or less. In addition, each of ZrO_2 , Cr_2O_3 , Li_2O , Na_2O , CaO , MgO , FeO , Fe_3O_4 , Fe_2O_3 and CaF_2 may be contained at a mass percentage of less than 10% based on the total mass of the oxide-based inclusion. Additionally, in order for oxide-based inclusions having a minor diameter of 1 μm or more contained in the weld metal to satisfy the requirements (1) and (2), the composition of the wire used, the composition of the base metal, various welding conditions, etc. are appropriately adjusted.

[0070]

In addition to each of the components described above, the weld metal of this embodiment may further contain at least one of the following components in a predetermined amount.

5 [0071]

(Cu: 0.40 mass% or less)

The reason for numerical limitation on the Cu amount in the weld metal is the same as the reason for numerical limitation on the Cu amount in the wire above.

Accordingly, in the case of incorporating Cu into the weld metal, it is sufficient as long as the Cu amount in the weld metal is more than 0%, but the amount is preferably 0.01% or more, more preferably 0.05% or more, still more preferably 0.10% or more. In addition, the Cu amount in the weld metal is preferably 0.40% or less, more preferably 0.30% or less, still more preferably 0.25% or less.

[0072]

15 (Cr: 1.0 mass% or less)

The reason for numerical limitation on the Cr amount in the weld metal is the same as the reason for numerical limitation on the Cr amount in the wire above.

Accordingly, in the case of incorporating Cr into the weld metal, it is sufficient as long as the Cr amount in the weld metal is more than 0%, but the amount is preferably 0.01% or more, more preferably 0.05% or more, still more preferably 0.10% or more. In addition, the Cr amount in the weld metal is preferably 1.0% or less, more preferably 0.8% or less, still more preferably 0.6% or less.

[0073]

(Mo: 0.35 mass% or less)

25 The reason for numerical limitation on the Mo amount in the weld metal is the same as the reason for numerical limitation on the Mo amount in the wire above.

Accordingly, in the case of incorporating Mo into the weld metal, it is sufficient as long as the Mo amount in the weld metal is more than 0%, but the amount is preferably 0.01% or more, more preferably 0.05% or more, still more preferably 0.10% or more. In addition, the Mo amount in the weld metal is preferably 0.35% or less, more preferably 0.30% or less, still more preferably 0.25% or less, yet still more preferably 0.20% or less.

[0074]

(Nb: 0.020 mass% or less)

The reason for numerical limitation on the Nb amount in the weld metal is the same as the reason for numerical limitation on the Nb amount in the wire above.

Accordingly, in the case of incorporating Nb into the weld metal, it is sufficient as long as the Nb amount in the weld metal is more than 0%, but the amount is preferably 0.001% or more, more preferably 0.005% or more, still more preferably 0.008% or more. In addition, the Nb amount in the weld metal is preferably 0.020% or less, more preferably 0.015% or less, still more preferably 0.012% or less.

[0075]

(V: 0.050 mass% or less)

The reason for numerical limitation on the V amount in the weld metal is the same as the reason for numerical limitation on the V amount in the wire above.

Accordingly, in the case of incorporating V into the weld metal, it is sufficient as long as the V amount in the weld metal is more than 0%, but the amount is preferably 0.001% or more, more preferably 0.005% or more, still more preferably 0.008% or more.

In addition, the V amount in the weld metal is preferably 0.050% or less, more preferably 0.020% or less, still more preferably 0.015% or less.

[0076]

One preferred embodiment of the weld metal above is a weld metal satisfying Si: from 0.05 to 0.25 mass%, Mn: from 1.00 to 2.40 mass%, and Ti: from 0.030 to 0.090

mass%, and

containing both of Ni: from 1.00 to 3.50 mass% and B: from 0.0005 to 0.0070 mass%,

wherein the rate of acicular ferrite formation defined by the following formula is 15% or more:

Rate of acicular ferrite formation (%) = (number of inclusions acting as a start point of acicular ferrite/number of all inclusions)×100

[0077]

More specifically, the weld metal according this one preferred embodiment is a weld metal containing:

C: from 0.04 to 0.12 mass%,

Si: from 0.05 to 0.25 mass%,

Mn: from 1.00 to 2.40 mass%,

Ti: from 0.030 to 0.090 mass%,

Al: from 0.002 to 0.010 mass%,

O: from 0.030 to 0.070 mass%,

N: more than 0 and 0.01 mass% or less,

Ni: from 1.00 to 3.50 mass%, and

5 B: from 0.0005 to 0.0070 mass%,

with the remainder consisting of Fe and inevitable impurities,

wherein the average composition of oxide-based inclusions having a minor diameter of 1 μm or more contained in the weld metal satisfies, by mass%, the following requirements (1) and (2):

$$10 \quad \text{Al}_2\text{O}_3 + \text{SiO}_2 + \text{MnO} + \text{TiO}_2 \geq 70\% \quad (1)$$

$$(\text{TiO}_2 + \text{MnO} + \text{Al}_2\text{O}_3) / \text{SiO}_2 \geq 5 \quad (2)$$

and

wherein the rate of acicular ferrite formation defined by the following formula is 15% or more:

$$15 \quad \text{Rate of acicular ferrite formation (\%)} = (\text{number of inclusions acting as a start point of acicular ferrite} / \text{number of all inclusions}) \times 100$$

[0078]

In the weld metal of this embodiment, for the above-described reasons, the glass phase having a low Young's modulus in an oxide-based inclusion of the weld metal is reduced. In addition, both a specific amount of Ni and a specific amount of B are contained and furthermore, each of the Si amount, the Mn amount and the Ti amount falls in a specific range, so that while reducing formation of coarse grain boundary ferrite, which adversely affects the toughness, formation of grain boundary bainite competing with acicular ferrite is inhibited and a fine acicular ferrite (AF) structure formed starting from an inclusion, which is effective in improving the low-temperature toughness, is thereby increased. Consequently, the low-temperature toughness can be further improved.

25 [0079]

Here, the rate of acicular ferrite (AF) formation (%) is a parameter indicative of a capability of forming fine acicular ferrite (AF) contributing to the improvement of low-temperature toughness and is defined by (number of inclusions acting as a start point of acicular ferrite/number of all inclusions) $\times$ 100.

30

From these viewpoints, the rate of acicular ferrite formation in the weld metal of this embodiment is 15% or more, preferably 18% or more, more preferably 20% or more.

[0080]

The rate of acicular ferrite formation can be measured as follows.

First, the weld metal is cut at a surface perpendicular to the welding direction and etched with nital (nitric acid:ethanol=5:95). Subsequently, a range of 165 μm ×219 μm of the unmodified portion of the final pass is photographed by an optical microscope at a magnification of 400 in four visual fields and out of inclusion particles on the photograph, those having an equivalent-circle diameter of 1.5 μm or more are selected. Then, a structure extending radially from an inclusion particle is defined as acicular ferrite, and the rate of acicular ferrite formation (%) is measured based on the following formula:

Rate of acicular ferrite formation (%) = (number of inclusions acting as a start point of acicular ferrite/number of all inclusions)×100

[0081]

Furthermore, in the deposited metal of this embodiment, the tensile strength in a tensile test in conformity with JIS Z2202 is preferably in excess of 490 MPa, more preferably in excess of 690 MPa, still more preferably in excess of 780 MPa.

[0082]

<Welding Conditions>

Preferable welding conditions when gas-shielded arc welding is performed using the above-described flux-cored wire for gas-shielded arc welding are described below.

[0083]

(Heat Input)

The heat input is not particularly limited but is preferably 2.5 kJ/mm or less. If the heat input exceeds 2.5 kJ/mm, the cooling rate during welding decreases, and this causes a tendency that a coarse structure is readily formed and the toughness is reduced.

[0084]

(Shielding Gas)

The shielding gas is not particularly limited, but a mixed gas containing 20 vol% or less of CO₂, with the remainder being Ar, is preferably used. If the CO₂ amount exceeds 20 vol%, there is a tendency that a coarse oxide is readily formed and the roughness is reduced.

[0085]

(Preheating-Interpass Temperature)

The preheating-interpass temperature is not particularly limited but is preferably from 50 to 200°C. If the temperature falls below 50°C, cracking during welding tends to be readily occur. In addition, if it exceeds 200°C, the cooling rate during welding decreases, and a coarse structure tends to be readily formed and the toughness tends to be reduced.

[0086]

The base metal is not particularly limited as long as the effects of the present invention are obtained, and the base metal may be appropriately selected in consideration of the composition of the flux-cored wire for gas-shielded arc welding, the welding conditions, etc.

EXAMPLES

[0087]

The effects of the present invention are specifically described below by referring to Examples and Comparative Examples, but the present invention is not limited thereto.

[0088]

(Examples 1 to 32)

Flux-cored wires of Examples 1 to 32 having the chemical component composition shown in Table 1 below were manufactured with a wire diameter: 1.2 mm, a flux filling rate of 13.5%. The remainder of each flux-cored wire consists of iron and inevitable impurities. Furthermore, in Table 1, amount in terms of Si indicates the amount in terms of Si in an Si alloy and an Si compound, and amount in terms of Ti indicates the amount in terms of Ti in a Ti alloy and a Ti compound.

[0089]

Table 1

No.	Composition of Wire (mass%)																		(Ti+Mn+Al)/ Si
	C	Amount in Terms of Si	Mn	Amount in Terms of Ti	Al	Ni	B	Cu	Cr	Mo	Nb	V	Li+Na+ K	Ca	Mg	F	ZrO ₂	Al ₂ O ₃	
1	0.14	0.21	2.6	3.0	0.023	2.2				0.13			0.09	0.02	0.49	0.12	0.53	0.54	26
2	0.05	0.58	3.8	4.5	0.049		0.0015			0.08			0.07	0.02	0.34	0.09	0.14	0.33	14
3	0.08	0.35	3.3	3.4	0.031	2.1				0.13			0.08	0.02	0.47	0.26	0.43	0.43	19
4	0.06	0.26	3.5	3.6	0.029	1.7				0.08			0.08	0.02	0.34	0.27	0.31	0.40	28
5	0.08	0.20	2.7	3.3	0.048		0.0027			0.13			0.05	0.25	0.24	0.17	0.22	0.54	31
6	0.07	0.14	2.6	2.7	0.046	2.3				0.12			0.08	0.02	0.62	0.10	0.26	0.53	39
7	0.07	0.12	2.6	3.0	0.038		0.0021			0.16			0.08	0.02	0.58	0.25	0.42	0.43	49
8	0.05	0.09	2.6	3.1	0.037		0.0036			0.14			0.06	0.44	0.13	0.20	0.25	0.83	63
9	0.05	0.14	4.1	3.0	0.034	2.1				0.16			0.05	0.07	0.45	0.11	0.44	0.01	51
10	0.07	0.22	2.7	4.6	0.038	2.4				0.11			0.07	0.07	0.25	0.15	0.06	0.41	33
11	0.07	0.20	2.7	1.7	0.025	2.0				0.12			0.06	0.07	0.32	0.21	0.43	0.42	22
12	0.06	0.20	2.6	2.7	0.057	2.1				0.15			0.07	0.02	0.35	0.24	0.01	0.59	27
13	0.05	0.18	2.6	3.0	0.004	2.2				0.13			0.08	0.02	0.36	0.26	0.44	0.34	31
14	0.08	0.17	2.7	2.6	0.046	3.6				0.15			0.07	0.04	0.52	0.27	0.11	0.15	31
15	0.08	0.19	2.6	2.7	0.022	0.2				0.09			0.05	0.04	0.43	0.21	0.13	0.36	28
16	0.05	0.18	2.7	2.9	0.026	2.1				0.31			0.06	0.02	0.35	0.13	0.11	0.48	31

Table 1 continued

No.		Composition of Wire (mass%)																	(Ti+Mn+Al)/ Si	
		C	Amount in Terms of Si	Mn	Amount in Terms of Ti	Al	Ni	B	Cu	Cr	Mo	Nb	V	Li+Na+ K	Ca	Mg	F	ZrO ₂		Al ₂ O ₃
17	0.05	0.17	2.6	2.7	0.028		0.0132				0.14			0.06	0.02	0.42	0.20	0.32	0.22	31
18	0.05	0.21	2.7	3.1	0.022		0.0005				0.17			0.07	0.02	0.48	0.10	0.38	0.30	27
19	0.05	0.14	2.6	2.8	0.029		0.0029				0.09			0.06	0.02	0.29	0.17	0.31	0.40	37
20	0.06	0.20	2.8	2.9	0.047	2.0					0.07			0.08	0.04	0.51	0.25	0.22	0.09	28
21	0.07	0.19	2.6	2.9	0.048	2.6					0.17			0.09	0.08	0.30	0.15	0.43	0.58	29
22	0.05	0.14	2.6	2.8	0.031	2.2								0.08	0.45	0.16	0.13	0.07	0.20	39
23	0.05	0.13	2.7	2.7	0.030		0.0038							0.08	0.15	0.37	0.19	0.31	0.27	42
24	0.05	0.21	2.6	3.1	0.038		0.0029				0.10			0.08	0.30	0.24	0.21	0.25	0.58	27
25	0.07	0.21	2.6	3.2	0.035	2.2					0.17			0.05	0.02	0.36	0.11	0.43	0.44	28
26	0.08	0.14	2.6	3.1	0.023	2.0					0.15			0.06	0.04	0.44	0.26	0.29	0.51	41
27	0.08	0.42	2.8	3.3	0.027	2.2					0.08			0.08	0.02	0.34	0.25	0.41	0.19	14
28	0.05	0.21	2.6	2.8	0.047	2.1					0.15			0.08	0.04	0.65	0.25	0.06	0.09	26
29	0.05	0.19	2.6	3.1	0.034		0.0049	0.13			0.13			0.08	0.08	0.45	0.12	0.08	0.42	30
30	0.05	0.18	2.6	3.4	0.030		0.0038		0.16	0.17				0.07	0.15	0.22	0.22	0.18	0.09	33
31	0.07	0.21	2.6	2.9	0.031	2.4					0.12	0.011		0.06	0.02	0.64	0.24	0.09	0.09	27
32	0.06	0.21	2.6	2.7	0.025	2.6					0.12		0.011	0.07	0.02	0.41	0.22	0.33	0.57	26

[0090]

A 20° V groove was formed in an SM490A steel sheet having a thickness of 20 mm, and gas-shielded arc welding was performed under the following conditions by using a flux-cored wire of each of Examples.

- 5 Shielding gas: 20% CO₂-80% Ar mixed gas
- Polarity: DCEP (direct current electrode positive)
- Current-voltage-speed: 280 A-29 V-35 cpm
- Heat input: 1.4 kJ/mm
- Preheating temperature: 100°C-110°C
- 10 Interpass temperature: 140°C-160°C
- Buildup procedure: 7 layers, 14 passes
- Welding position: flat

[0091]

- The chemical component composition of the obtained weld metal according to
- 15 each of Examples is shown in Table 2. The remainder of each weld metal consists of iron and inevitable impurities. In addition, the average composition of oxide-based inclusions having a minor diameter of 1 μm or more contained in the weld metal according to each of Examples and, with respect to the average composition, Al₂O₃+SiO₂+MnO+TiO₂ and (TiO₂+MnO+Al₂O₃)/SiO₂ are shown in Table 3. The remainder of the average
 - 20 composition of oxide-based inclusions having a minor diameter of 1 μm or more contained in the weld metal according to each of Examples consists of inevitable oxides and inevitable fluorides. Furthermore, the average composition of oxide-based inclusions having a minor diameter of 1 μm or more contained in the weld metal according to each of Examples was quantitatively analyzed by observing a polished surface of a micro sample,
 - 25 which was cut out from the weld metal, by means of an Electron Probe X-ray Micro Analyzer (EPMA, trade name: "JXA-8500F") manufactured by JEOL Datum Ltd. Details are as follows. The observation area at the polished surface of the micro sample was 100 mm², and the composition in the central part of an inclusion was quantitatively analyzed by characteristic X-ray wavelength dispersion spectrometry. Elements to be analyzed were
 - 30 Al, Si, Ti, Mg, Mn, Zr, Na, K, Cr and O (oxygen). After the relationship between the X-ray intensity of each element and the concentration of the element was previously determined as a calibration curve by using a known substance, the elements contained in each inclusion were quantitatively determined from the obtained X-ray intensity of the

above-described inclusion to be analyzed and the calibration curve, and the composition of the inclusion was determined by arithmetic averaging of the results. Out of inclusions quantitatively determined in this way, an inclusion having an oxygen (O) content of 5 mass% or more is defined as an oxide-based inclusion. At this time, when a plurality of elements are observed in one oxide-based inclusion, the oxide composition was calculated from the ratio of the X-ray intensities showing existence of those elements by performing conversion to a single oxide of each element. In the present invention, values converted to mass as the above-described single oxides were averaged to determine the oxide composition.

10 [0092]

Table 2

No.	Composition of Weld Metal (mass%)													
	C	Si	Mn	Ti	Al	O	N	Ni	B	Cu	Cr	Mo	Nb	V
1	0.13	0.13	1.65	0.054	0.004	0.053	0.004	2.55				0.12		
2	0.07	0.31	2.70	0.097	0.009	0.047	0.004		0.0015			0.10		
3	0.08	0.26	2.82	0.085	0.005	0.052	0.004	2.26				0.14		
4	0.07	0.22	2.30	0.075	0.005	0.047	0.003	2.16				0.11		
5	0.08	0.13	1.84	0.077	0.004	0.055	0.005		0.0016			0.14		
6	0.07	0.08	1.65	0.063	0.004	0.043	0.004	2.51				0.11		
7	0.07	0.06	1.71	0.058	0.006	0.050	0.004		0.0018			0.17		
8	0.06	0.04	1.77	0.065	0.006	0.044	0.004		0.0017			0.14		
9	0.07	0.10	3.05	0.060	0.006	0.040	0.006	2.35				0.18		
10	0.08	0.11	1.78	0.103	0.006	0.041	0.004	2.62				0.14		
11	0.07	0.14	1.75	0.027	0.004	0.042	0.005	2.40				0.14		
12	0.07	0.14	1.74	0.062	0.011	0.053	0.005	2.40				0.17		
13	0.06	0.11	1.73	0.053	0.001	0.049	0.005	2.65				0.15		
14	0.08	0.10	1.73	0.065	0.004	0.040	0.005	3.51				0.14		
15	0.08	0.10	1.65	0.057	0.004	0.053	0.004	0.27				0.10		
16	0.06	0.11	1.85	0.063	0.004	0.046	0.006	2.46				0.33		
17	0.06	0.10	1.62	0.051	0.005	0.044	0.005		0.0074			0.15		
18	0.07	0.12	1.73	0.052	0.004	0.046	0.004		0.0004			0.16		

Table 2 continued

No.	Composition of Weld Metal (mass%)													
	C	Si	Mn	Ti	Al	O	N	Ni	B	Cu	Cr	Mo	Nb	V
19	0.07	0.10	1.65	0.060	0.005	0.051	0.006		0.0018			0.10		
20	0.07	0.11	1.87	0.054	0.004	0.042	0.003	2.21				0.10		
21	0.08	0.10	1.66	0.063	0.006	0.052	0.006	2.61				0.16		
22	0.07	0.10	1.82	0.068	0.005	0.042	0.003	2.56						
23	0.06	0.10	1.73	0.059	0.005	0.049	0.004		0.0019					
24	0.06	0.12	1.76	0.059	0.006	0.047	0.003		0.0017			0.11		
25	0.08	0.13	1.65	0.063	0.006	0.044	0.004	2.58				0.17		
26	0.08	0.11	1.62	0.054	0.004	0.052	0.004	2.38				0.16		
27	0.08	0.26	2.50	0.078	0.005	0.044	0.004	2.47				0.11		
28	0.06	0.12	1.72	0.065	0.005	0.047	0.005	2.28				0.14		
29	0.06	0.11	1.72	0.063	0.006	0.042	0.004		0.0025	0.11		0.14		
30	0.07	0.10	1.61	0.064	0.005	0.040	0.005		0.0027		0.13	0.18		
31	0.08	0.13	1.68	0.057	0.005	0.053	0.004	2.56				0.14	0.009	
32	0.07	0.11	1.67	0.057	0.004	0.048	0.003	2.65				0.15		0.010

[0093]

Table 3

No.	Average Composition of Oxide-Based Inclusions with Minor Diameter of 1 μm or more in Weld Metal (mass%)				Requirements	
	Al_2O_3	SiO_2	MnO	TiO_2	$\text{Al}_2\text{O}_3+\text{SiO}_2+$ MnO+ TiO_2	($\text{TiO}_2+\text{MnO}+$ Al_2O_3)/ SiO_2
1	7	4	19	63	93	22
2	10	16	29	25	80	4
3	8	12	21	47	88	6
4	9	6	22	55	92	14
5	5	4	26	57	92	22
6	6	2	22	52	82	40
7	10	2	23	52	87	43
8	10	1	27	56	94	93
9	10	2	36	50	98	48
10	10	2	21	62	95	47
11	6	4	25	45	80	19
12	21	4	19	36	80	19
13	1	2	25	64	92	45
14	5	3	22	59	89	29
15	5	2	23	59	89	44

Table 3 continued

No.	Average Composition of Oxide-Based Inclusions with Minor Diameter of 1 μm or more in Weld Metal (mass%)				Requirements	
	Al_2O_3	SiO_2	MnO	TiO_2	$\text{Al}_2\text{O}_3+\text{SiO}_2+$ $\text{MnO}+\text{TiO}_2$	$(\text{TiO}_2+\text{MnO}+$ $\text{Al}_2\text{O}_3)/\text{SiO}_2$
16	7	2	24	54	87	43
17	9	3	24	58	94	30
18	6	3	22	54	85	27
19	8	2	20	61	91	45
20	5	3	28	56	92	30
21	10	3	21	52	86	28
22	6	2	23	58	89	44
23	8	2	25	60	95	47
24	10	2	22	55	89	44
25	8	4	19	58	89	21
26	5	3	22	62	92	30
27	9	15	18	40	82	4
28	9	3	25	56	93	30
29	9	3	21	64	97	31
30	9	3	20	62	94	30
31	6	5	20	54	85	16
32	7	3	24	51	85	27

[0094]

With respect to each of the obtained weld metals, various performances (strength, low-temperature toughness) were evaluated by the following evaluation tests. These evaluation results are shown in Table 4.

5 [0095]

(Strength)

A tensile test piece in conformity with JIS Z2202 was sampled from the central part of the weld metal in parallel to the weld line and subjected to a tensile test, and those having a tensile strength in excess of 490 MPa were judged to be passed.

10 [0096]

(Low-Temperature Toughness)

A Charpy impact test piece (JIS Z3111 No. 4 V-notched specimen) was sampled vertically to the weld line direction from a thickness central part of the weld metal, and the energy absorption and the brittle fracture rate at -40°C were measured in a manner

15 prescribed in JIS Z2242. Those having, as the average value of three measurements, an absorption energy at -40°C of 47 J or more and a brittle fracture rate of 20% or less were judged to have excellent low-temperature toughness.

[0097]

20 In addition, when formation of convex bead shape in vertical position, formation of blowhole, deterioration of bead wettability, generation of spatter, deterioration of bead smoothness, deterioration of porosity resistance, deterioration of welding workability, occurrence of high-temperature cracking, etc., took place, these are shown together as other properties in Table 4.

[0098]

25

Table 4

No.	Tensile Strength	Brittle Fracture Rate (-40°C)	Absorption Energy (-40°C)	Other Properties
1	880	52	25	formation of convex bead shape in vertical position
2	787	35	18	good
3	902	18	53	good
4	802	9	75	good
5	700	4	92	good
6	726	2	110	good
7	661	1	105	good
8	636	19	53	blowhole, deterioration of bead wettability, generation of spatter
9	903	80	31	deterioration of bead smoothness
10	828	47	15	good
11	663	33	30	formation of convex bead shape in vertical position, deterioration of porosity resistance
12	747	91	17	deterioration of bead smoothness
13	726	25	61	blowhole, deterioration of bead smoothness
14	807	17	58	occurrence of high-temperature cracking
15	659	31	36	good
16	762	19	52	good

Table 4 continued

No.	Tensile Strength	Brittle Fracture Rate (-40°C)	Absorption Energy (-40°C)	Other Properties
17	694	16	53	occurrence of high-temperature cracking
18	650	36	24	good
19	646	0	100	good
20	741	2	93	good
21	765	0	110	good
22	732	2	98	good
23	616	1	97	good
24	637	0	102	good
25	767	2	96	good
26	752	0	108	good
27	867	46	36	good
28	709	0	105	good
29	646	0	100	good
30	665	2	98	good
31	765	8	85	good
32	743	0	111	good

[0099]

Examples 3 to 7, 16, 19 to 26 and 28 to 32 are Examples, and Examples 1 to 2, 8 to 15, 17 to 18 and 27 are Comparative Examples.

5 In Example 1, the C amount in the wire was as high as 0.14%, the C amount in the weld metal was as high as 0.13% and therefore, the low-temperature toughness was poor. Furthermore, since the ZrO_2 amount in the wire was as high as 0.53%, formation of a convex bead shape in a vertical position was observed.

10 In Example 2, the amount in terms of Si in the wire was as high as 0.58%, $(\text{Ti}+\text{Mn}+\text{Al})/\text{Si}$ was as low as 14, the Si amount in the weld metal was as high as 0.31%, $(\text{TiO}_2+\text{MnO}+\text{Al}_2\text{O}_3)/\text{SiO}_2$ in the average composition of oxide-based inclusions having a minor diameter of 1 μm or more contained in the weld metal was as low as 4 and therefore, the low-temperature toughness was poor.

15 In Example 8, the amount in terms of Si in the wire was as low as 0.09%, the Si amount in the weld metal was as low as 0.04% and therefore, a blowhole was formed. Furthermore, since the Al_2O_3 amount in the wire was as high as 0.83%, bead wettability was deteriorated and spatter was generated.

20 In Example 9, the Mn amount in the wire was as high as 4.1%, the Mn amount in the weld metal was as high as 3.05 mass% and therefore, the low-temperature toughness was poor. Furthermore, since the Al_2O_3 amount in the wire was as low as 0.01%, bead smoothness was deteriorated.

In Example 10, the amount in terms of Ti in the wire was as high as 4.6%, the Ti amount in the weld metal was as high as 0.103% and therefore, the low-temperature toughness was poor.

25 In Example 11, since the amount in terms of Ti in the wire was as low as 1.7% and the Ti amount in the weld metal was as low as 0.027%, the low-temperature toughness was poor, formation of a convex bead shape in a vertical position was observed, and the porosity resistance was deteriorated.

30 In Example 12, the Al amount in the wire was as high as 0.057%, the Al amount in the weld metal was as high as 0.011% and therefore, the low-temperature toughness was poor. Furthermore, since the ZrO_2 amount in the wire was as high as 0.01%, the bead smoothness was deteriorated.

In Example 13, since the Al amount in the wire was as low as 0.004% and the Al amount in the weld metal was as low as 0.011%, a blowhole was formed and the bead smoothness was deteriorated.

5 In Example 14, the Ni amount in the wire was as high as 3.6%, the Ni amount in the weld metal was as high as 3.51% and therefore, high-temperature cracking occurred.

In Example 15, the Ni amount in the wire was as low as 0.2%, the Ni amount in the weld metal was as low as 0.27% and therefore, the low-temperature toughness was poor.

10 In Example 17, the B amount in the wire was as high as 0.0132%, the B amount in the weld metal was as high as 0.0074% and therefore, high-temperature cracking occurred.

In Example 18, the B amount in the wire was as low as 0.0005%, the B amount in the weld metal was as low as 0.0004% and therefore, the low-temperature toughness was poor.

15 In Example 27, $(\text{Ti}+\text{Mn}+\text{Al})/\text{Si}$ in the wire was as low as 14, $(\text{TiO}_2+\text{MnO}+\text{Al}_2\text{O}_3)/\text{SiO}_2$ in the average composition of oxide-based inclusions having a minor diameter of 1 μm or more contained in the weld metal was as low as 4 and therefore, the low-temperature toughness was poor.

20 On the other hand, the weld metals of Examples 3 to 7, 16, 19 to 26 and 28 to 32, which are within the range defined in the present invention, had excellent low-temperature toughness as well as good other properties.

[0100]

(Examples 33 to 51 and 53 to 61)

25 Flux-cored wires of Examples 33 to 51 and 53 to 61 having the chemical component composition shown in Table 5 below were manufactured with a wire diameter: 1.2 mm at a flux filling rate of 13.5%. In Table 5, amount in terms of Si indicates the amount in terms of Si in an Si alloy and an Si compound, and amount in terms of Ti indicates the amount in terms of Ti in a Ti alloy and a Ti compound.

[0101]

Table 5

No.	C	Amount in Terms of Si	Amount Mn in Terms of Ti	Al	Ni	B	Cu	Cr	Mo	Nb	V	ZrO ₂	Al ₂ O ₃	Li+K+Na	Ca	Mg	F	Fe and Impurities	(Ti+Mn+ Al)/Si
33	0.06	0.16	2.3 2.7	0.009	2.3	0.0022												92.5	31
34	0.10	0.13	1.8 2.7	0.012	2.2	0.0025						0.15						92.9	35
35	0.07	0.14	1.9 2.6	0.025	1.2	0.0072	0.01					0.16	0.40	0.06				93.4	32
36	0.08	0.25	2.2 2.7	0.019	1.6	0.0041	0.19					0.42	0.41	0.06	0.02	0.50		91.5	20
37	0.10	0.13	2.1 3.4	0.031	1.2	0.0060	0.01	0.44			0.011	0.15	0.43	0.08	0.02	0.12	0.21	91.6	43
38	0.07	0.17	2.6 3.4	0.010	2.3	0.0029	0.01	0.05	0.14		0.006	0.13	0.37	0.08	0.05	0.18	0.29	90.1	35
39	0.03	0.17	2.4 3.4	0.026	2.6	0.0024	0.03	0.18		0.003	0.011	0.16	0.15	0.12	0.02	0.57	0.15	90.0	34
40	0.04	0.10	2.9 3.3	0.050	2.2	0.0031	0.33	0.12		0.012	0.011	0.22	0.03	0.06	0.02	0.56	0.25	89.8	63
41	0.08	0.19	3.3 3.9	0.005	3.0	0.0022	0.01	0.60	0.26			0.42	0.55	0.21	0.11	0.40	0.15	86.8	38
42	0.07	0.26	2.4 2.4	0.010	3.4	0.0030	0.03	0.05	0.03		0.015	0.40	0.27	0.02	0.12	0.30	0.09	90.1	19
43	0.08	0.16	2.6 2.4	0.006	2.2	0.0034	0.01		0.03			0.41	0.68	0.03	0.11	0.33	0.20	90.8	31
44	0.06	0.16	2.0 3.0	0.024	1.0	0.0074	0.10	0.86	0.20	0.017	0.004	0.46	0.16	0.35	0.11	0.70	0.33	90.5	31
45	0.12	0.14	1.1 3.4	0.017	1.2	0.0106	0.01					0.23	0.22	0.07	0.02	0.03	0.27	93.2	32
46	0.06	0.27	1.9 3.4	0.016	1.1	0.0045	0.01			0.010	0.024	0.04	0.45	0.07	0.05	0.10	0.59	91.9	20
47	0.03	0.40	2.4 3.8	0.019	1.5	0.0075	0.03		0.10	0.011	0.026	0.20	0.46	0.07	0.47	0.03	0.25	90.2	16

Table 5 continued

No.	C	Amount in Terms of Si	Amount Mn in Terms of Ti	Al	Ni	B	Cu	Cr	Mo	Nb	V	ZrO ₂	Al ₂ O ₃	Li+K+Na	Ca	Mg	F	Fe and Impurities	(Ti+Mn+ Al)/Si
48	0.07	0.32	2.4 3.4	0.009	2.1	0.0019	0.01		0.16		0.007	0.37	0.38	0.05	0.50	0.13	0.51	89.6	18
49	0.08	0.31	2.4 3.1	0.009	2.3	0.0020	0.01		0.13		0.011	0.25	0.49	0.06	0.31	0.24	0.20	90.1	18
50	0.07	0.10	2.6 3.3	0.016	2.1	0.0020	0.03	0.03	0.11		0.012	0.33	0.33	0.06	0.08	0.25	0.20	90.4	59
51	0.02	0.16	2.5 3.4	0.014	0.8	0.0018						0.41	0.58	0.06	0.02	0.25	0.18	91.6	37
53	0.07	0.14	3.1 2.2	0.015	1.9	0.0022	0.01		0.08		0.006	0.41	0.46	0.09	0.02	0.53	0.26	90.7	38
54	0.07	0.45	1.2 2.4	0.006	1.9	0.0021	0.01		0.08		0.006	0.38	0.37	0.10	0.08	0.45	0.16	92.3	8
55	0.07	0.14	2.6 3.0	0.008	3.6	0.0027	0.01				0.008	0.22	0.28	0.08	0.11	0.21	0.29	89.4	40
56	0.08	0.17	2.6 3.0	0.056	1.6	0.0005	0.02				0.007	0.27	0.28	0.08	0.11	0.40	0.16	91.2	33
57	0.08	0.43	2.7 5.6	0.088	2.3	0.0024	0.01	0.03	0.14		0.010	0.31	0.30	0.07	0.02	0.37	0.15	87.4	20
58	0.08	0.67	2.7 4.5	0.024	1.9	0.0025	0.03	0.04	0.12		0.012	0.20	0.40	0.05	0.11	0.44	0.26	88.5	11
59	0.07	0.54	2.7 4.2	0.022	2.1	0.0027	0.01	0.04	0.12		0.006	0.30	0.45	0.03	0.11	0.37	0.21	88.7	13
60	0.06	0.18	2.0 3.4	0.022	0.9	0.0023	0.01				0.006	0.30	0.21	0.08	0.02	0.24	0.25	92.3	30
61	0.08	0.18	2.6 3.0	0.022	1.6	0.0005	0.02				0.007	0.30	0.25	0.08	0.02	0.38	0.24	91.2	31

[0102]

A 20° V groove was formed in an SM490A steel sheet having a thickness of 20 mm, and gas-shielded arc welding was performed under the following conditions by using a flux-cored wire of each of Examples.

- 5 Shielding gas: A 20% CO₂-80% Ar mixed gas
- Polarity: DCEP (direct current electrode positive)
- Current-voltage-speed: 280 A-29 V-35 cpm
- Heat input: 1.4 kJ/mm
- Preheating temperature: 100°C-110°C
- 10 Interpass temperature: 140°C-160°C
- Buildup procedure: 7 layers, 14 passes
- Welding position: flat

[0103]

- The chemical component composition of the obtained weld metal according to
- 15 each of Examples is shown in Table 6. The remainder of each weld metal consists of iron and inevitable impurities. In addition, with respect to the average composition of oxide-based inclusions having a minor diameter of 1 μm or more contained in the weld metal according to each of Examples, Al₂O₃+SiO₂+MnO+TiO₂ and (TiO₂+MnO+Al₂O₃)/SiO₂ are shown in Table 8. The remainder of the average
 - 20 composition of oxide-based inclusions having a minor diameter of 1 μm or more contained in the weld metal according to each of Examples consists of inevitable oxides and inevitable fluorides.

[0104]

- 25 In addition, the rate of acicular ferrite formation in the weld metal was measured as follows.

- First, the weld metal was cut at a surface perpendicular to the welding direction and etched with nital (nitric acid:ethanol=5:95). Subsequently, a range of 165 μm×219 μm of the unmodified portion of the final pass was photographed by an optical microscope at a magnification of 400 in four visual fields and out of inclusion particles on the
- 30 photograph, those having an equivalent-circle diameter of 1.5 μm or more were selected. Then, a structure extended radially from an inclusion particle was defined as acicular ferrite, and the rate of acicular ferrite formation (%) was measured based on the following formula:

Rate of acicular ferrite formation (%) = (number of inclusions acting as a start point of acicular ferrite/number of all inclusions)×100

[0105]

(Low-Temperature Toughness)

- 5 With respect to the obtained weld metal, the low-temperature toughness was evaluated by the following evaluation test.

- 10 More specifically, a Charpy impact test piece (JIS Z3111 No. 4 V-notched specimen) was sampled vertically to the weld line direction from a thickness central part of the weld metal and measured for the energy absorption at -60°C (vE_{-60}) and the brittle fracture rate in a manner prescribed in JIS Z2242. The evaluation results are shown in Table 6. Those having, as the average value of three measurements, an absorption energy at -60°C of 35 J or more and a brittle fracture rate of less than 33% were rated as having excellent low-temperature toughness.

[0106]

Table 6

No.	C	Si	Mn	Ti	Al	Ni	B	N	O	Cu	Cr	Mo	Nb	V	Oxides		Rate of AF	Low-Temperature Toughness	
															Al ₂ O ₃ +SiO ₂ +MnO+TiO ₂	(TiO ₂ +MnO+Al ₂ O ₃)/SiO ₂		vE ₋₆₀ (J)	Brittle Fracture Rate (%)
33	0.071	0.15	1.68	0.055	0.004	2.51	0.0014	0.0040	0.049						88	28	20	88	15
34	0.095	0.13	1.36	0.055	0.005	2.50	0.0014	0.0047	0.050						84	11	25	75	13
35	0.077	0.11	1.45	0.042	0.006	1.45	0.0041	0.0066	0.042	0.01					92	30	31	93	12
36	0.077	0.18	1.64	0.050	0.006	1.88	0.0027	0.0045	0.046	0.19					91	10	27	75	18
37	0.095	0.09	1.55	0.075	0.008	1.54	0.0035	0.0045	0.051	0.01	0.44			0.008	90	89	23	71	20
38	0.074	0.15	1.77	0.075	0.003	2.51	0.0017	0.0040	0.049	0.01	0.02	0.14		0.008	85	13	26	71	12
39	0.044	0.11	1.80	0.070	0.006	2.86	0.0018	0.0049	0.035	0.01	0.20		0.003	0.011	90	22	19	86	22
40	0.055	0.05	2.11	0.066	0.009	2.50	0.0018	0.0051	0.046	0.32	0.11		0.011	0.008	94	93	17	68	27
41	0.076	0.20	2.36	0.088	0.002	2.95	0.0016	0.0056	0.045	0.01	0.54	0.26			92	9	21	60	27
42	0.075	0.13	1.78	0.036	0.003	3.48	0.0020	0.0071	0.050	0.01	0.03	0.05		0.013	76	9	17	61	28
43	0.075	0.11	1.90	0.036	0.002	2.38	0.0021	0.0055	0.048	0.01		0.05			74	14	16	67	23
44	0.059	0.15	1.54	0.061	0.006	1.17	0.0041	0.0067	0.064	0.08	0.85	0.20	0.016	0.003	83	20	17	64	30
45	0.111	0.11	1.06	0.076	0.005	1.38	0.0061	0.0050	0.053	0.01					78	10	31	61	23
46	0.065	0.21	1.44	0.066	0.005	1.22	0.0027	0.0041	0.046	0.01			0.008	0.022	86	9	23	96	22
47	0.041	0.24	1.80	0.077	0.006	1.75	0.0042	0.0050	0.046	0.01		0.10	0.009	0.024	91	6	24	76	28

Table 6 continued

No.	C	Si	Mn	Ti	Al	Ni	B	N	O	Cu	Cr	Mo	Nb	V	Oxides		Rate of AF	Low-Temperature Toughness	
															Al ₂ O ₃ +SiO ₂ +MnO+TiO ₂	(TiO ₂ +MnO+Al ₂ O ₃)/SiO ₂		vE ₋₆₀ (J)	Brittle Fracture Rate (%)
48	0.072	0.22	1.80	0.069	0.003	2.28	0.0015	0.0045	0.048	0.01		0.15		0.007	91	8	30	76	22
49	0.075	0.16	1.83	0.061	0.004	2.42	0.0016	0.0039	0.046	0.01		0.14		0.010	90	9	27	71	22
50	0.075	0.05	1.84	0.068	0.004	2.36	0.0016	0.0037	0.047	0.01	0.02	0.13		0.009	89	88	33	78	5
51	0.025	0.17	1.83	0.066	0.004	0.95	0.0015	0.0044	0.045						85	11	12	61	45
53	0.076	0.11	2.24	0.028	0.005	2.17	0.0016	0.0057	0.043	0.01		0.10		0.008	68	13	7	46	35
54	0.076	0.21	1.15	0.031	0.002	2.15	0.0015	0.0057	0.043	0.01		0.09		0.008	69	4	7	65	33
55	0.077	0.12	1.83	0.060	0.003	3.61	0.0015	0.0050	0.042	0.01				0.008	91	22	22	56	27
56	0.076	0.15	1.86	0.060	0.011	1.90	0.0004	0.0049	0.071	0.01				0.008	91	12	9	58	40
57	0.078	0.22	1.95	0.120	0.021	2.51	0.0018	0.0035	0.053	0.01	0.02	0.14		0.009	94	9	9	13	75
58	0.076	0.51	1.91	0.094	0.006	2.23	0.0018	0.0036	0.048	0.01	0.02	0.13		0.010	89	4	13	55	33
59	0.074	0.36	1.92	0.100	0.005	2.41	0.0019	0.0034	0.045	0.01	0.02	0.14		0.008	97	3	8	30	57
60	0.066	0.16	1.45	0.055	0.005	0.95	0.0016	0.0045	0.048	0.01				0.008	83	13	13	54	47
61	0.075	0.16	1.90	0.058	0.004	1.92	0.0004	0.0052	0.050	0.01				0.008	83	16	18	56	37

[0107]

The weld metals of Examples 33 to 50 satisfying Si: from 0.05 to 0.25 mass%, Mn: from 1.00 to 2.40 mass% and Ti: from 0.030 to 0.090 mass% and containing both of Ni: from 1.00 to 3.50 mass% and B: from 0.0005 to 0.0070 mass%, in which the rate of acicular ferrite formation was 15% or more, were obtained by use of a wire satisfying amount in terms of Si: from 0.10 to 0.45 mass%, Mn: from 1.1 to 3.4 mass%, and amount in terms of Ti: from 2.4 to 4.0 mass% and containing both of Ni: from 1.00 to 3.50 mass% and B: from 0.0008 to 0.012 mass%, and had an absorption energy at -60°C and a brittle fracture rate, as the average value of three measurements, of 60 J or more and 30% or less, respectively, as well as particularly excellent low-temperature toughness.

[0108]

While the invention has been described in detail and with reference to specific embodiments thereof, it is apparent to one skilled in the art that various changes and modifications can be made therein without departing from the spirit and scope of the invention. This application is based on Japanese Patent Application (Patent Application No. 2016-174095) filed on September 6, 2016, the entirety of which is incorporated herein by way of reference. In addition, all references cited herein are incorporated in their entirety.

CLAIMS

[Claim 1]

A flux-cored wire for gas-shielded arc welding, containing, based on total mass of the wire:

- 5 C: from 0.03 to 0.12 mass%;
Si in terms of Si in Si alloy and Si compound: from 0.10 to 0.50 mass%;
Mn: from 1.0 to 4.0 mass%;
Ti in terms of Ti in Ti alloy and Ti compound: from 2.4 to 4.5 mass%;
Al: from 0.005 to 0.050 mass%;
10 at least one of Ni: from 0.30 to 3.50 mass% and B: from 0.0008 to 0.012 mass%;
and
Fe: 80 mass% or more, and
satisfying $(\text{Ti} + \text{Mn} + \text{Al})/\text{Si} \geq 15$.

15 [Claim 2]

The flux-cored wire for gas-shielded arc welding according to Claim 1, further containing, based on the total mass of the wire:

- ZrO₂: from 0.02 to 0.50 mass%; and
Al₂O₃: from 0.02 to 0.80 mass%.

20

[Claim 3]

The flux-cored wire for gas-shielded arc welding according to Claim 1, further containing at least one member selected from the group consisting of, based on the total mass of the wire:

- 25 Cu: 0.40 mass% or less;
Cr: 1.0 mass% or less;
Mo: 0.35 mass% or less;
Nb: 0.030 mass% or less; and
V: 0.050 mass% or less.

30

[Claim 4]

The flux-cored wire for gas-shielded arc welding according to Claim 1 further containing, at least one member selected from the group consisting of, based on the total mass of the wire:

a total of Li, Na and K: 1.0 mass% or less; and

5 Ca: 1.0 mass% or less.

[Claim 5]

The flux-cored wire for gas-shielded arc welding according to Claim 1, further containing, based on the total mass of the wire:

10 Mg: 1.0 mass% or less.

[Claim 6]

The flux-cored wire for gas-shielded arc welding according to Claim 1, further containing, based on the total mass of the wire:

15 F: 1.0 mass% or less.

[Claim 7]

The flux-cored wire for gas-shielded arc welding according to any one of Claims 1 to 6, satisfying:

20 Si in terms of Si in Si alloy and Si compound: from 0.10 to 0.45 mass%;
Mn: from 1.1 to 3.4 mass%; and
Ti in terms of Ti in Ti alloy and Ti compound: from 2.4 to 4.0 mass%, and
containing both of Ni: from 1.00 to 3.50 mass% and B: from 0.0008 to 0.012
mass%.

25

[Claim 8]

A weld metal containing:

C: from 0.04 to 0.12 mass%;

Si: from 0.05 to 0.30 mass%;

30 Mn: from 0.80 to 3.00 mass%;

Ti: from 0.030 to 0.100 mass%;

Al: from 0.002 to 0.010 mass%;

O: from 0.030 to 0.070 mass%;

N: more than 0 and 0.01 mass% or less; and
 at least one of Ni: from 0.30 to 3.50 mass% and B: from 0.0005 to 0.0070 mass%,
 with the remainder consisting of Fe and inevitable impurities,
 wherein an average composition of oxide-based inclusions having a minor

5 diameter of 1 μm or more contained in the weld metal satisfies, by mass%, the following requirements (1) and (2):

$$\text{Al}_2\text{O}_3 + \text{SiO}_2 + \text{MnO} + \text{TiO}_2 \geq 70\% \quad (1)$$

$$(\text{TiO}_2 + \text{MnO} + \text{Al}_2\text{O}_3) / \text{SiO}_2 \geq 5 \quad (2).$$

10 [Claim 9]

The weld metal according to Claim 8, further containing at least one member selected from the group consisting of:

Cu: 0.40 mass% or less;

Cr: 1.0 mass% or less;

15 Mo: 0.35 mass% or less;

Nb: 0.020 mass% or less; and

V: 0.050 mass% or less.

[Claim 10]

20 The weld metal according to Claim 8 or 9, satisfying:

Si: from 0.05 to 0.25 mass%;

Mn: from 1.00 to 2.40 mass%; and

Ti: from 0.030 to 0.090 mass%, and

25 containing both of Ni: from 1.00 to 3.50 mass% and B: from 0.0005 to 0.0070 mass%,

wherein a rate of acicular ferrite formation defined by the following formula is 15% or more:

Rate of acicular ferrite formation (%) = (number of inclusions acting as a start point of acicular ferrite/number of all inclusions) $\times$ 100.

30