

DESCRIPTION

PROCESS OF MAKING A SEMICONDUCTOR OPTICAL LENS AND A
SEMICONDUCTOR OPTICAL LENS FABRICATED THEREBY

TECHNICAL FIELD

The present invention is directed to a process for fabricating an optical lens from a body of semiconductor substrate, and a semiconductor optical lens fabricated by the same process.

BACKGROUND ART

Japanese patent publication No. 2000-263556 discloses a process of making a mold for a micro optical lens. The mold is fabricated by steps of preparing a semiconductor substrate, providing a dielectric mask on a top surface of the substrate, forming one or more openings in the mask, placing the substrate in an electrolytic solution, and anodizing a portion in the top surface not covered by the mask to convert the portion into a porous zone. Thereafter, the porous zone is removed to leave a rounded convex in the top surface of the substrate. An ultraviolet curable resin is placed in the convex and is cured therein to obtain a convex lens. Although the prior art discloses the formation of the porous zones, the process relies upon the mask with the opening so that the porous zone develops isotropically from the center of each opening. Accordingly, the resulting rounded convex is limited to have substantially a uniform radius of curvature. With this limitation, the process cannot be not adapted to fabricate optical lens having non-uniform radius of curvature or sophisticated surface profile.

Further, it is found that the rounded convex revealed by removal of the porous zone suffers from minute projections due to the fact that the porous zone

leaves a relatively irregular interface with the semiconductor substrate. This irregularity may detract from lens transmissivity and is desired to be smoothed out when fabricating the lens of good transmissivity.

DISCLOSURE OF THE INVENTION

In view of the above problem, the present invention has been accomplished to provide an improved process of fabricating an optical lens of various surface profiles and also of good transmissivity.

The process according to the present invention utilizes a semiconductor substrate having a flat top surface and a flat bottom surface opposed to each other, and includes the steps forming an anode on the bottom surface, placing the semiconductor substrate in an electrolyte solution. Then, the steps are followed by flowing a current between the anode and a cathode within the solution to convert the top surface of the substrate to a varying depth from portions to portions, leaving a resulting porous layer in the top surface, and removing the porous layer from the substrate to leave a curved surface on the top surface. The process is characterized by including a smoothing step of smoothening out minute projections remaining on the curved surface. Thus, the lens is finished to have a smoothly curved surface for improving transmissivity. In addition, since the anode can be configured to give the predetermined distribution of the electric field intensity varying from portions to portions of the substrate, it is easy to give continuously varying radius of curvature to the resulting curved surface. Further, because of that the anodization proceeds from the top surface of the substrate which is exposed entirely to the electrolyte solution, i.e., not covered or masked by a material restricting the anodization, and

that the surface profile of the curved surface is controlled principally by the electric field intensity distribution given by the anode pattern on the bottom surface of the substrate, it is easy to develop the porous layer of accurately controlled contour or profile and therefore give the correspondingly accurate surface profile to the resulting lens. Accordingly, the process can be best utilized to fabricate the optical lens, especially a non-spherical lens with precisely controlled surface profile and good transmissivity.

The process may rely upon an etching technique of immersing the semiconductor substrate in a suitable etching solution after removing the porous layer. With this result, the minute projections can be preferentially etched out to give a smoothed curved surface to the lens.

Alternatively, the process may utilize a thermal oxidation to form an oxidized layer in the top of the curved surface. Also in this instance, the oxidation proceeds preferentially in the minute projections to selectively oxidize the minute projections so that the oxidized layer extends the minute projections and not proceed deep into the semiconductor substrate. Therefore, etching out the oxidized layer can reveal the smoothed surface on the curved surface to give the lens of smoothed surface.

Further, it is equally possible to utilize a plasma etching or laser ablation process in either of which the minute projections can be preferentially removed to provide a smoothed finish to the lens.

The above smoothing can assure to give the curved surface having a root mean square surface roughness (RMS) of 200 nm or less, which enables to reduce transmissivity lowering due to the surface irregularity as less as 10% or below, and therefore satisfies good transmissivity of the lens.

Moreover, the present invention gives a good solution of facilitating the above smoothening process by minimizing the projections formed at the interface between the semiconductor substrate and the porous layer. For this purpose, it is made to change a parameter of anodizing the top surface of the substrate with time while forming the porous layer in order to lower the porosity of the porous layer at the interface with the substrate than at the other portion. With this consequence, a control can be made to develop the porous layer with relatively large porosity until the porous layer reaches to the intended interface with the substrate, and with less porosity at the interface, thereby enabling to form and remove the porous layer efficiently, yet minimizing the projections or surface irregularity in accordance with the less porosity.

The parameter may be a current density of the current which flows through the anode and the cathode and which is controlled to decrease in the final stage of developing the porous layer to such a thickness that influence the surface smoothness.

Alternatively or in combination with the control of the current density, the electrolyte solution may be controlled to increase its concentration in the final stage of the forming the porous layer.

These and still other advantageous features of the present invention will become more apparent from the following detailed explanation when taking in conjunction with the attached drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a perspective view of a plano-convex lens fabricated in accordance with a preferred embodiment of the present invention;

FIG. 2 is a sectional view of the lens;

FIG. 3A is a sectional view illustrating a device in which the above lens is utilized;

FIG. 3B is a top view of the above device;

FIG. 4 is an exploded perspective view of the above device;

FIG. 5 is a sectional view of an anodizing apparatus utilized for making the process of the present invention;

FIGS. 6A to 6E are sectional views illustrating the steps of forming the lens;

FIG. 7A and 7B are schematic views illustrating electric field intensity distribution developed in the process of forming the lens;

FIG. 8 is a plan view illustrating an anode pattern formed on the bottom surface of the semiconductor substrate;

FIG. 9A and 9B are graphs illustrating a control of developing the porous layer;

FIG. 10A and 10B are graphs illustrating another control of developing the porous layer;

FIG. 11A to 11D are sectional views illustrating a step of smoothening the lens surface;

FIG. 12 is a graph illustrating a relation between transmissivity and surface roughness of the lens; and

FIG. 13A to 13E are sectional views illustrating another step of smoothening the lens surface.

BEST MODE FOR CARRYING OUT THE INVENTION

Referring to FIGS. 1 to 5, the present invention is now explained for fabrication of a plano-convex lens as one particular representative of a semiconductor optical lens in accordance with a preferred embodiment of the present invention. As shown in FIGS. 1 to 3, the lens **L** is configured to have an

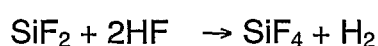
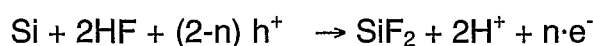
integral flange **F** which is utilized for mounting the lens in a device such as an optical sensor **200**, which is one typical application of the lens and is configured to have a sensing element such as a pyroelectric element **210** as well as an associated electronic circuit module **220** to receive the light through the lens, as shown in FIGS. 3 and 4. The pyroelectric element **210** is carried on the circuit module **220** which is mounted on a base **230** having a plurality of terminal pins **240**, while the lens **L** is supported by a cover **250**.

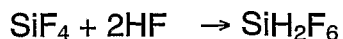
The lens is made from a semiconductor material such as, silicon (Si), germanium (Ge), silicon carbide (SiC), gallium arsenide (GaAs), gallium phosphide (GaP), and indium phosphide (InP). In this embodiment, the semiconductor substrate **10** of p-type Si is utilized to fabricate the plano-convex lens by selective anodization of the substrate **10**. The anodization is made by use of an anodizing apparatus **100** which, as shown in FIG. 5, is configured to place the substrate **10** within a volume of an electrolyte solution **140**, and which is configured to be equipped with a regulator **130** for regulation of an electric current flowing between an anodic electrode **120** and a cathode **110** immersed in the solution. The anodic electrode **120** is held in contact with the bottom surface of substrate **10** in order to advance the anodization to a varying extent in the top surface opposed to the cathode **110**. The anodic electrode **120** and cathodes **110** are both made of platinum or any other suitable metal.

In this embodiment, the substrate **10** is selected to have a low resistance of several ohm centimeters ($\Omega\cdot\text{cm}$) to several hundreds ohm centimeters ($\Omega\cdot\text{cm}$). For example, a 0.5 mm thick flat p-type Si substrate **10** of 80 $\Omega\cdot\text{cm}$ is shaped into the lens through the steps of FIGS. 6A to 6E. After being washed and cleaned, the substrate **10** is processed to have an electrically conductive layer **20** on the

entire bottom surface (FIG. 6B). The conductive layer **20** is made of aluminum, for example, and is deposited by sputtering or like technique on the substrate **10** to have a uniform thickness of 1 μm . Then, the conductive layer **20** is formed with a resist pattern by a photolithography, and is partially etched out by a wet-etching to leave a circular opening **22** of 2 mm diameters in match with a diameter of the lens to be fabricated to give a consolidated structure in which the conductive layer **20** defines an anode having an anode pattern integrated to the substrate **10** (FIG. 6C). The above etching is not limited to the wet-etching and may be made by a dry-etching. Hereinafter, the term "anode" is utilized in place of the conductive layer where it is deemed appropriate to explain the present invention. Subsequently, the substrate **10** is immersed within the electrolyte solution **140** in the anodizing apparatus **100** with the anode **20** in contact with the anodic electrode **120** and is followed by receiving an electric current flowing between the anode **20** and the cathode **110** so as to anodize the top surface of the semiconductor substrate **10** selectively in correspondence to the anode pattern, thereby developing a porous layer **30** in the top surface of the substrate **10** (FIG. 6D). The electric current is regulated by the regulator **130** to have a predetermined current density of 30 mA/cm^2 , for example, and continue for a predetermined period of 120 minutes for example. Thereafter, the porous layer **30** and the anode **20** are etched out to obtain the lens (FIG. 6E).

The electrolyte solution utilized is an aqueous solution of hydrogen fluoride (HF) and ethanol mixed in a suitable ratio. In the anodization process, the following chemical reactions take place:





where h^+ denotes a hole and e^- denotes an electron.

As soon as the Si substrate is anodically oxidized, the oxidized portion is removed by reaction with the electrolyte solution so as to leave the porous layer **30** in the surface of the substrate **10**. Accordingly, the anodization proceeds without being retarded by the oxidized portion, which makes it possible to develop the porous layer **30** having a greater depth, and therefore enable to fabricate the lens of relatively great thickness.

As schematically shown in FIG. 7A, an in-plane electric field strength or current density is variably distributed in coincidence with the anode pattern. In the figure, the lines with black arrows indicate paths of the positive current flowing through the substrate **10**, while the lines with white arrows indicate the paths of the electrons flowing through the substrate **10**. Since the in-plane current density becomes denser towards the periphery of the opening **22** than at the center of the opening, the resulting porous layer **30** has a continuously varying depth which is greater towards the periphery of opening **22** than at the center of the opening. Consequently, the plano-convex lens is obtained by removal of the porous layer **30** and optionally by removal of the anode **20**. The distribution of the in-plane electric field strength will be determined primarily by the anode pattern, and secondarily by the resistivity and the thickness of the substrate **10**, resistance of the electrolyte solution **140**, a distance between the substrate **10** and the cathode **110**, and a planar configuration of the cathode **110** (i.e. cathode arrangement in a plane parallel to the substrate). Accordingly, it is readily possible to give any desired lens profile by suitably selecting these parameters in combination with the anode pattern. It should be noted here that

since the anodization proceeds to develop the porous layer continuously without being retarded by otherwise appearing oxidized portions in the substrate, the thick lens can be easily fabricated in a single anodization process, which enhances flexibility of the lens design.

The resistance of the electrolytic solution **140** can be adjusted by the concentration of the aqueous solution of hydrogen fluoride (HF) and/or by a mixing ratio of HF to ethanol. The cathode **110** may be designed to have a pattern in exact coincident with the anode pattern as shown in FIG. 7A, or to have a pattern in which the opposing cathode elements **112** are offset slightly towards the center of the opening **22** of the anode pattern in a plane parallel to the substrate **10**, as shown in FIG. 7B. The offset amount can be adjusted in relation with the current density as well as the distance to the substrate **10**.

In the anodization process, the regulator **130** acts to keep the current density basically at a constant level. However, it is preferred to decrease the current density gradually in a final stage of the anodization process in order to correspondingly decrease the rate of developing the porous layer **30**. With this technique, the porosity of the porous layer can be lowered by lowering the current density during the anodization, which minimizes surface irregularity on the curved surface revealed by removal of the porous layer, and therefore gives a more smooth surface finish to the resulting lens. The regulation of the current density is made by monitoring the current level or voltage level.

The removal of the porous layer **30** and the conductive layer **20** can be made by use of an alkali solution such as KOH, NaOH and TMAH (tetramethyl ammonium hydroxide) or HF solution.

FIG. 9A and 9B show controls of decreasing the current density in the final stage of the anodization process, respectively by continuously lowering the current density from I1 (for example, 30 mA/cm²) to I2 (for example, 5 mA/cm²), or lowering the current density stepwise from I1 to I2. With this consequence, the anodization proceeds at a lowered rate to lessen the porosity at the interface with the substrate than at the other portions, as schematically shown in FIG. 11A, thereby leaving only minute projections on the resulting curved surface of the substrate **10** after the porous layer **30** is removed. It is noted that FIG. 11A illustrates the varying porosity in an exaggerated format only for the purpose of explaining the anodization process, and the size and distribution of pores does not reflect the actual ones. In view of that the porous layer is developed at a lower rate when lowering the current density to correspondingly lower the porosity, it is preferred to give the less porosity only at the final stage of developing the porous layer **30**. In order to satisfy the requirement of rapidly etching out the porous layer **30** and at the same time of minimizing the projections on the curved surface of the substrate, T1 for anodization at a large current density I1 and time T2 for anodization at a reduced current density I2 are suitably selected. For instance, T1 and T2 are selected to be 30 minutes and 10 minutes, respectively.

Alternatively or in combination with the control of the current density, it may be possible to control a concentration of the electrolytic solution, for example, HF concentration, to increase in the final stage of the anodization process, as shown in FIGS. 10A and 10B, by increasing the concentration either by stepwise from M1 to M2 or continuously from M1 to M2. The higher the concentration of the electrolytic solution, the more minute pores are developed with

correspondingly lowered porosity to leave more minute projections on the surface of the substrate **10**. Also, time T1 and T2 are suitable selected to facilitate the formation and removal of the porous layer, yet leaving only minute projections at the interface between the porous layer **30** and the substrate **10**.

As shown in FIG. 11B, the minute projections **12** left on the substrate **10** are generally dimensioned to have an average height of 1 μm and spaced from each other at a distance of several μm . The surface irregularity is removed by a smoothing process following the removal of the porous layer **30**. In the present embodiment, the substrate **10** removed of the porous layer **30** (shown in FIG. 11B) is immersed in a dry etching solution such as KOH, NaOH and TMAH (tetramethyl ammonium hydroxide) or HF-based solution. In this process, the minute projections **12** on the substrate surface are selectively etched out as indicated by dotted lines in FIG. 11C, thereby leaving a smoothed surface on the substrate **10**, as shown in FIG. 11D.

EXAMPLE

A 100 mm diameter p-type Si substrate **10** of 0.5 mm thick and 80 $\Omega\cdot\text{cm}$ resistivity was formed on its bottom surface with a 1 μm thick aluminum conductive layer **20** by sputtering. After sintering the conductive layer **20** at 420°C for 20 minutes, the layer **20** was masked by photolithography with a resist pattern having a plurality of windows of 2 mm diameters. Then, the unmasked portion of the conductive layer **20** was etched out by dry-etching to form a plurality of 2 mm diameter openings **22** in the conductive layer, as shown in FIG. 8. After being removed of the resist pattern, the substrate **10** was placed in the anodizing apparatus of FIG. 5 containing the electrolytic solution comprised of an

1:1 ratio mixture of a 50% aqueous solution of hydrogen fluoride (HF) and ethanol. Then, the substrate was anodized at current density of 30 mA/cm² for 3 hours. The resulting porous layer **30** was found to have a 0.3 mm thick at the portion corresponding to the conductive layer **20** and to have a decreasing thickness towards the center of the opening **22** in a plane parallel to the substrate. The porous layer **30** and the conductive layer **20** were then etched out by a 10% aqueous solution of KOH over a period of 15 minutes, thereby forming a plurality of plano-convex lenses. Thereafter, the substrate **10** was immersed in an aqueous solution of HF for 1 hour to selectively etch out the minute projections **12** remaining on the surface of the substrate **10**. The substrate **10** was then cut out into a plurality of the lens. The etching rate of removing the porous layer **30** was more than 10 times than that of removing the minute projections on the substrate **10**. Thus formed lens were each configured to have a lens thickness of 0.195 mm and a root mean square surface roughness (RMS) of 50 nm

FIG. 12 illustrates a relation between the root mean square surface roughness (RMS) and the transmissivity (%) of the infrared ray having a wavelength of 5 μ m which represents one of radiation having a range of 5 μ m to 10 μ m wavelength emitted from a human and selected in view of that the infrared sensor is used for detection of human presence. In the graph of FIG. 12, black dots indicate measured roughness and the transmissivity, while a curve indicates a theoretical relation as expressed by the following equation.

$$T = \exp\left[-\left(\frac{4\pi\sigma}{\lambda^2}\right)^2\right]$$

where σ is a surface roughness

From the graph, the measured transmissivity is lowered with the increased surface roughness in line with the theoretical relation. For practical use, it is

preferred to reduce the lowering of transmissivity due to scattering on the surface irregularity as less as 10% or less. In this respect, the lens is required to have a transmissivity of 42 % or more with the surface roughness (RMS) of 200 nm or less. In this sense, the lens fabricated in the above example to have the surface roughness (RMS) of 50 nm can well satisfy the requirement, and the lens fabricated in the above process to have the surface roughness (RMS) of 200 nm or less is sufficient for practical use.

Alternatively, the smoothening of the lens surface can be made by another process of thermally oxidizing the surface of the substrate followed by etching out the resulting oxidized layer, as shown in FIG. 13A to 13E. Firstly, as shown in FIG. 13A, the porous layer **30** is formed in the top surface of the substrate **10** to give a curved interface between the porous layer **30** and the remaining substrate **10** in correspondence with the opening of the anode **20**, i.e., the anode pattern in a manner as explained hereinbefore. The porous layer **30** is etched out to give the structure of FIG. 13B in which minute projections **12** remains in the top surface of the substrate **10**. Subsequently, the substrate **10** is placed in an oxidation furnace and is heated so as to develop the oxidized layer **14** in the top surface of the substrate **10**, as shown in FIG. 13C. In order to make the thermal oxidization, steam is introduced to the furnace to treat the substrate at a temperature of 1000 °C for 200 minutes to develop an oxidation layer of 0.4 μm thickness. During the thermal oxidation, oxidation of Si into SiO_2 proceeds uniformly in a direction normal to the surface of the substrate such that the oxidization proceeds preferentially at the projections **12** than the other portion to smooth the top surface of the substrate, as shown in FIG. 13D. Thus, the thermal oxidization can be easily controlled to form the oxidized layer **14** which

includes the entire projections **12** but not the remaining substrate **10**. Thereafter, the oxidized layer **14** is etched out to give a smooth top surface of the substrate **10**, as shown in FIG. 13E.

Further, it is equally possible to utilize a plasma etching in order to remove the minute projections **12** from the top surface of the substrate **10**. In this process, the substrate **10** removed of the porous layer **30** is exposed to a plasma stream to selectively and preferentially etch out the projections remaining on the top surface of the substrate. A sputtering etching is made when using argon gas, while a reactive ion etching is made when using CF_4 gas, or a mixture gas of CF_4 and O_2 .

Still further, the smoothening may be made by a laser ablation in which a laser beam is irradiated to the top surface of the substrate to selectively and preferentially remove the minute projections.

It should be noted that the anodization process of varying the current density or concentration of the electrolyte solution is preferred, but the present invention is not limited thereto and may equally utilize the anodization without the control of varying these parameters.

Further, the present invention should be interpreted to be not limited to the use of the silicon substrate but to allow the use of other semiconductor materials in combination with specific electrolyte solution as shown in the table below.

Semiconductor material	Electrolytic solution	Masking material
Si	HF:C ₂ H ₅ OH	SiN
Ge	HCl: C ₂ H ₅ OH	SiO ₂ , SiN, SiC
SiC	HF: C ₂ H ₅ OH	SiN
GaAs	HCl	SiO ₂ , SiN, SiC
GaP	H ₂ SO ₄	SiO ₂ , SiN, SiC
InP	HCl	SiO ₂ , SiN, SiC

In the above table, the mask material available in combination of the semiconductor material and the electrolytic solution are listed.

CLAIMS

1. A process of fabricating a semiconductor optical lens, said process comprising the steps of:

preparing a semiconductor substrate having a flat top surface and a flat bottom surface opposed to each other;
forming an anode on said bottom surface,
placing said semiconductor substrate in an electrolyte solution;
flowing a current between said anode and a cathode within said solution to anodize the top surface of said substrate to a varying depth from portions to portions, leaving a porous layer in said top surface; and
removing said porous layer from said substrate to leave a curved surface on said top surface,
said process being characterized by including a smoothing step of smoothening out minute projections remaining on said curved surface.

2. The process as set forth in claim 1, wherein said smoothing step follows the step of removing said porous layer and comprises:
immersing said semiconductor substrate in an etching solution to etch out said minute projections.

3. The process as set forth in claim 1, wherein said smoothing step follows the step of removing said porous layer and comprises sub-steps of:
forming an oxidized layer by thermal oxidation in the top of said curved surface,
and
etching out said oxidized layer to remove said minute projections.

4. The process as set forth in claim 1, wherein said smoothing step follows the step of removing said porous layer and comprises exposing said curved surface to a plasma to remove said minute projections.

5. The process as set forth in claim 1, wherein said smoothing step follows the step of removing said porous layer and comprises irradiating a laser beam to said curved surface to remove said minute projections.
6. The process as set forth in anyone of claims 2 to 5, wherein said smoothing step is made to finish said curved surface having a root mean square surface roughness (RMS) of 200 nm or less.
7. The process as set forth in claim 1, wherein the step of forming said porous layer including to change a parameter of anodizing the top surface of said substrate with time in order to lower the porosity of the porous layer at the interface with the substrate than at the other portion.
8. The process as set forth in claim 7, wherein said parameter is a current density of the current flowing through said anode and said cathode, said current density being controlled to decrease in a final stage of forming said porous layer.
9. The process as set forth in claim 1, wherein said parameter is a concentration of said electrolyte solution, said concentration being controlled to increase in a final stage of forming said porous layer.
10. A semiconductor optical lens fabricated in accordance with any one of claims 2 to 5, wherein said smoothing step is made to finish said curved surface having a root mean square surface roughness (RMS) of 200 nm or less.