

Description

The invention relates to a bridge amplifier, comprising between two connection terminals for connecting an asymmetrical supply voltage :

— a voltage divider having a tap for taking off substantially half the supply voltage

— a first amplifier for amplifying an input signal, comprising a first non-inverting input which is coupled to the tap on the voltage divider, a first inverting input and an output for connecting a first connection terminal of a load, said output being fed back by a resistor to the first inverting input, and

— a second amplifier for amplifying the input signal, comprising a first non-inverting input which is coupled to the tap on the voltage divider, a first inverting input and an output for connecting a second connection terminal of the load, said output being fed back by a resistor to the first inverting input.

A bridge amplifier of this type is suitable for amplifying audio signals and may be particularly used in car radios.

A bridge amplifier of this type is known from the Philips Data Handbook Integrated Circuits Part 1, March 1984, "Bipolar IC's for radio and audio equipment", page 310. The first amplifier is a non-inverting negative feedback amplifier in which the input voltage to be amplified is applied to the non-inverting input and in which a fraction of the output voltage is fed back to the inverting input via a voltage divider arranged between the output and ground. Furthermore, the non-inverting input is connected to the tap on a voltage divider arranged between the supply connection points and is therefore at half the supply voltage with respect to the d.c. voltage. The inverting input and the output are also at this half supply voltage because the amplifier is completely negatively fed back with respect to the d.c. voltage by a capacitor incorporated in the voltage divider between the output and ground. The second amplifier constitutes an inverting amplifier in which a fraction of the output voltage of the first amplifier is applied to the inverting input of the second amplifier. Otherwise, the second amplifier is formed similarly as the first amplifier, whilst the capacitor for the direct voltage negative feedback is combined with that of the first amplifier to form a common capacitor. This capacitor is a non-integratable electrolytic capacitor. The tap on the voltage divider arranged between the supply terminals is connected to ground via a likewise nonintegratable electrolytic capacitor in order to suppress the hum voltage of the supply voltage. In principle this capacitor may be omitted because in that case the amplified hum voltage appears at the output of both the first and the second amplifier and consequently does not cause a signal current through the load. In principle it is also possible to omit the capacitor for the direct voltage negative feedback and to connect the ends of the

voltage dividers for the signal negative feedback to the tap on the voltage divider arranged between the supply terminals. In that case the capacitor connected to this tap cannot be omitted, because otherwise the negative feedback factor and hence the amplification is no longer accurately fixed.

Therefore, the known bridge amplifier requires at least one non-integratable capacitor. It is therefore an object of the invention to provide a bridge amplifier which is fully integratable and thus does not require any external components. According to the invention, a bridge amplifier of the type described in the opening paragraph is characterized in that at least the first inverting input of the first amplifier and the first inverting input of the second amplifier are coupled to an output of a buffer amplifier, an input of which is coupled to the tap on the voltage divider. As is known per se, a buffer amplifier has a voltage gain which is substantially equal to one and its output impedance is substantially equal to zero so that the output of the buffer amplifier is at half the supply voltage with respect to the direct voltage, whilst this output constitutes a virtual earth point with respect to the signal. Consequently, the ends of the voltage dividers used for the negative feedback can be connected via the buffer amplifier to the tap on the voltage divider arranged between the supply terminals without this tap having to be connected to ground via a capacitor. The bridge amplifier according to the invention is thereby fully integratable.

The first non-inverting inputs of the first and the second amplifier may be connected directly or via the buffer amplifier to the tap on the voltage divider arranged between the supply terminals.

An embodiment of a bridge amplifier according to the invention is characterized in that the first non-inverting input of the first amplifier constitutes the input for supplying the input signal. This embodiment may be further characterized in that the first inverting input of the second amplifier is coupled to a tap on a voltage divider arranged across the output of the first amplifier. In addition it is also possible to apply the input voltage directly to the first non-inverting input of the second amplifier via a voltage inverter circuit.

A further embodiment of a bridge amplifier according to the invention is characterized in that the first amplifier comprises :

— a first input stage having a first input constituting the first non-inverting input of the amplifier, a second input constituting the first inverting input of the amplifier, and an output connected to the input of an output stage having an output constituting the output of the first amplifier, and

— a second input stage having a first input constituting a second non-inverting input of the first amplifier, a second input constituting a second inverting input of the first amplifier, and an output connected to the input of the output stage, and in that the second

amplifier comprises

— a third input stage having a first input constituting the first non-inverting input of the second amplifier, a second input constituting the first inverting input of the second amplifier, and an output connected to the input of an output stage having an output constituting the output of the second amplifier,

— a fourth input stage having a first input constituting a second non-inverting input of the second amplifier, a second input constituting a second inverting input of the second amplifier, and an output connected to the input of the output stage, and in that

— the second non-inverting input of the first amplifier and the second inverting input of the second amplifier are coupled to a connection point for applying an input signal, and in that

— the second inverting input and the second noninverting input of both the first and the second amplifier are coupled to a connection point for carrying a reference potential. By causing the negative feedback of the first and the second amplifier to be effected via separate input stages, the input voltage cannot only be applied directly to the second non-inverting input of the first amplifier, but also directly to the second inverting input of the second amplifier. This prevents the output signal from being distorted as in the case when the input voltage is applied via a voltage inverter circuit to the first non-inverting input or in the case when the input voltage is applied via a voltage divider connected to the output of the first amplifier to the first inverting input of the second amplifier.

In the case when the first, second, third and fourth input stages are each constituted by a differential amplifier having a differential-to-single-ended converter, this embodiment may be further characterized in that the first and the second input stage comprise a common differential-to-single-ended converter and the third and the fourth input stage comprise a common differential-to-single-ended converter.

The invention will be further described with reference to the accompanying drawing in which

Fig. 1 shows a first embodiment of a bridge amplifier according to the invention.

Fig. 2 shows an embodiment of a buffer amplifier for the circuit of Fig. 1,

Fig. 3 shows a second embodiment of a bridge amplifier according to the invention, and.

Fig. 4 shows an embodiment of an amplifier for the circuit of Fig. 3.

Fig. 1 shows a first embodiment of a bridge amplifier according to the invention. The bridge amplifier comprises a first amplifier 1 having a non-inverting input 2, an inverting input 3 and an output 4. The non-inverting input 2 is connected by an input resistor R_1 to the tap 14 on a voltage divider having mutually equal resistors R_2 and R_3 arranged between the positive supply voltage terminal 15 and the ground

terminal 16. Consequently, the non-inverting input 2 is at substantially half the supply voltage. The inverting input 3 is connected to the junction point on a voltage divider constituted by the resistors R_5 and R_6 and being arranged between the output 4 and the output 12 of a buffer amplifier 9. The non-inverting input 10 of this buffer amplifier 9 is connected to the tap 14 on the voltage divider R_2 , R_3 . The inverting input 11 is connected to the output 12 so that amplifier 9 is fully negatively fed back and thus constitutes a voltage follower. The voltage at the output 12 and consequently the voltage at the inverting input 3 of amplifier 1 is therefore substantially equal to half the supply voltage.

With respect to d.c. voltage the non-inverting input 2, the inverting input 3 and hence also the output 4 are thus at half the supply voltage. With respect to the signals the first amplifier constitutes a non-inverting amplifier because the input voltage to be amplified is applied to an input terminal 13 which is connected to the non-inverting input 3. Due to the full negative feedback, the output impedance of the buffer amplifier 9 is substantially equal to zero so that the output 12 constitutes a virtual earth point with respect to the signals. The negative feedback voltage and consequently the voltage gain of the non-inverting first amplifier 1 is therefore substantially entirely determined by the resistors R_5 and R_6 .

Furthermore, the bridge amplifier comprises a second amplifier 5 which is equal to the first amplifier and has a non-inverting input 6, and inverting input 7 and an output 8. Similarly as in the first amplifier the non-inverting input 6 is connected via a decoupling resistor R_7 to the tap on the voltage divider R_2 , R_3 and the inverting input 7 is connected to a tap on a voltage divider constituted by the resistors R_9 and R_8 and arranged between the output 8 of amplifier 5 and the output 12 of buffer amplifier 9. The non-inverting input 6 and the inverting input 7 are thus likewise at half the supply voltage with respect to the d.c. voltage. With respect to the signals amplifier 5 constitutes an inverting amplifier because the voltage to be amplified is applied to the inverting input 7. Due to the negative feedback with resistors R_8 and R_9 , the inverting input 7 has a low impedance so that the input voltage cannot be applied directly to this input. Therefore, a fraction of the output voltage of the first amplifier 1 obtained with the aid of a voltage divider comprising resistors R_{10} and R_{11} is applied to the inverting input via a resistor R_{12} . The load R_L is incorporated between the outputs 4 and 8 of the first and the second amplifier 1 and 5, respectively.

It is to be noted that the non-inverting input 2 of the first amplifier 1 via the resistor R_1 and the non-inverting input 6 of the second amplifier 5 via the resistor R_7 can also be connected directly to the output 12 of the buffer amplifier 9, as is shown in broken lines in the Figure, instead of to the tap 14 on the voltage

divider R_2 , R_3 . Furthermore it is to be noted that instead of applying the voltage to be amplified to the inverting input 7 of the second amplifier, it is alternatively possible to apply the input voltage directly to the non-inverting input 6 via a voltage inverter circuit.

The bridge amplifier of Fig. 1 does not require any electrolytic capacitors for d.c. biasing as does the known bridge amplifier and can therefore be fully integrated.

Fig. 2 shows an embodiment of a buffer amplifier for the circuit of Fig. 1 in which the same components have the same reference numerals. The buffer amplifier 9 is formed by two npn transistors T_1 and T_2 arranged as a differential pair whose common emitter connection is connected to ground via a current source I_1 . The base of transistor T_1 constitutes the non-inverting input 10 and the base of transistor T_2 constitutes the inverting input 11 of the buffer amplifier. The collector of transistor T_1 is connected to the collector of transistor T_2 by a current mirror with pnp transistors T_3 and T_4 . Furthermore, this collector is connected to the base of an npn transistor T_5 which is arranged as an emitter follower with a current source 12 whose output 12 is connected to the inverting input 11.

It is to be noted that instead of the buffer amplifier shown any other buffer amplifier may be used provided that its voltage gain is substantially equal to one and that the output impedance is substantially equal to zero.

Fig. 3 shows a second embodiment of a bridge amplifier according to the invention in which the same components have the same reference numerals as those in Fig. 1. In this embodiment the first amplifier 1 is provided with a first input stage 20 having a first input constituting the first non-inverting input 2 of the first amplifier 1, a second input constituting the first inverting input 3 of the first amplifier 1, and an output 23 connected to the input 26 of the output stage 25 whose output 4 is connected by a resistor R_5 to the first inverting input 3 which is furthermore connected by a resistor R_6 to the output 12 of buffer amplifier 9 which, similarly as in Fig. 1, is connected to the tap 14 on the voltage divider R_2 , R_3 . The non-inverting input 2 is connected directly to the output 12 of this buffer amplifier 9. The non-inverting input 2, the inverting input 3 and, as a consequence of the feedback with resistor R_5 , also the output 4 are therefore at half the supply voltage with respect to the d.c. voltage. The first amplifier 1 also comprises a second input stage 29 which is equal to the first and which has a first input constituting the second non-inverting input 28 of the first amplifier, a second input constituting the second inverting input 27 of the first amplifier, and an output 30 which is connected to the input 26 of the output stage 25. The inverting input 27 is connected by a resistor R_{15} to a terminal 60 carrying a reference voltage V_{ref} . The non-inverting input 28 is connected by

the series arrangement of a resistor R_{16} , which is equal to the resistor R_{15} , and a resistor R_{18} to this terminal 60. The inverting input 27 and the non-inverting input 28 are at the reference voltage V_{ref} with respect to the d.c. voltage. This voltage may differ from half the supply voltage at the non-inverting input 2 and the inverting input 3 of the first input stage 20. Furthermore the inverting input 28 is connected via the resistor R_{18} to the connection terminal 13 to which the input voltage V_i is applied. The resistor 18 has a resistance which is large relative to that of the resistors R_{15} and R_{16} and consequently functions as an input resistor for the input voltage V_{in} to the non-inverting input 28. The input voltage V_{in} is amplified in a non-inverting manner via the input stage 29 and the output stage 25. Since the output 12 of the buffer amplifier 9 constitutes a virtual ground connection, a fraction of the voltage at output 4 determined by the resistors R_5 and R_6 is feedback to the inverting input 3. This feedback voltage is amplified in an inverting manner via the input stage 20 and the output stage 25. Thus, the amplifier 1 functions as a conventional non-inverting negative feedback amplifier whose gain is substantially fully determined by the resistors R_5 and R_6 .

Furthermore the bridge amplifier comprises a second amplifier 5 which is equal to the first amplifier 1 and which is provided with a third input stage 40 having a first input constituting the first non-inverting input 6 of the amplifier 5, a second input constituting the first inverting input 7 of the amplifier 5, and an output 43 which is connected to the input 46 of an output stage 45 whose output constitutes the output 8 of the amplifier 5, which output is connected via a resistor R_8 equal to resistor R_5 to the inverting input 7. This inverting input 7 is also connected via a resistor R_9 , which is equal to resistor R_6 , and the non-inverting input 6 is connected directly to the output 12 of the buffer amplifier 9. The inputs 6 and 7 and also the output 8 are therefore at half the supply voltage with respect to the d.c. voltage. The second amplifier 5 is also provided with a fourth input stage 50 having a first input constituting the second non-inverting input 49 of amplifier 5, a second input constituting the second inverting input 48 of the amplifier 5, and an output 51 which is connected to the input 46 of the output stage 45. The second non-inverting input 49 is connected via a resistor R_{20} , and the second inverting input 48 is connected via the resistors R_{19} and R_{21} to the terminal 60 carrying the reference voltage V_{ref} .

The resistors R_{19} , R_{20} and R_{21} are equal to the resistors R_{15} , R_{16} and R_{18} , respectively. Furthermore, the second inverting input 48 is connected via the resistor R_{19} to the connection terminal 13 for applying the input voltage V_{in} . The resistor R_{21} then serves as an input resistor for this voltage to the second inverting input 48. The input voltage V_{in} is amplified in an inverting manner via the input stage 50 and the output stage 45. A fraction of the output voltage determined

by the resistors R_8 and R_9 is fed back to the first inverting input 7 and is subsequently amplified once more in an inverting manner via the input stage 40 and the output stage 46. Consequently, the amplifier 5 functions as a conventional inverting negative feedback amplifier, whose gain is substantially fully determined by the resistors R_8 and R_9 .

With respect to the embodiment of Fig. 1, this embodiment has the following advantage. In the embodiment of Fig. 1 the input signal only traverses the first amplifier in the case of a non-inverting amplification, whereas the input signal traverses both the first and the second amplifier in the case of inverting amplification. Consequently phase differences occur, which may give rise to distortion of the output signal. Since in the embodiment of Fig. 3 the negative feedback of the first and second amplifiers 1 and 5 is effected through separate input stages, the input voltage V_{in} cannot only be applied directly to the non-inverting amplifier 1, but also directly to the inverting amplifier 5. Consequently no phase difference occurs between the output signal at the output 4 of the first amplifier 1 and the output signal at the output 8 of the second amplifier 5 so that the output signal across the load R_L cannot be distorted. The same advantage occurs with respect to the embodiment in which the input voltage is applied via a voltage inverter circuit to the non-inverting input of the second amplifier.

Fig. 4 shows a simplified diagram of a possible embodiment of the first amplifier 1 for the bridge amplifier of Fig. 3. The second amplifier 5 is constructed in a similar manner. The first input stage 20 comprises two transistors T_{10} and T_{11} whose emitters are connected via resistors R_{30} and R_{31} to the output of a current source I_1 , which is connected to the positive supply voltage terminal 15. The collector of transistor T_{10} is connected directly and the collector of transistor T_{11} is connected by a current mirror including transistors T_{14} and T_{15} to the output 23 of the input stage 20. With the aid of Line current mirror T_{14} , T_{15} the differential collector currents flowing in the transistors T_{10} , T_{11} due to the feedback voltage are converted into a single-ended output current which appears at output 23. The second input stage 29 is equal to the input stage 20 and comprises two transistors T_{12} and T_{13} whose emitters are connected via resistors R_{32} and R_{33} to the output of a current source I_2 . The collectors of the transistors T_{12} and T_{13} are connected to the collectors of transistors T_{10} and T_{11} , respectively. Consequently, the current mirror T_{14} , T_{15} also serves for converting the differential collector currents flowing in the transistors T_{12} and T_{13} due to the input voltage V_i into a single-ended output current to the output 23. This output 23 is connected to the input 26 of the output stage 25 which is provided with a so-called Miller stage comprising a transistor T_{18} whose collector is connected via a level shifting diode D_1 to a load current source I_3 . A frequency compensation capacitor C_1 is

arranged between the output 60 and the input 26 of this Miller stage. This output 60 is connected to the base of a first output transistor T_{18} which is arranged in series with a second output transistor T_{19} between the positive supply voltage terminal 15 and ground terminal 16. The emitter of transistor T_{18} and the collector of transistor T_{19} are connected to the output 4 of the output stage 25. This output stage 25 also comprises a voltage current converter 70 which is formed by two transistors T_{20} and T_{21} whose emitters are connected via resistors R_{34} and R_{35} to the output of a current source $I_4 = 2I_1$. The base of transistor T_{20} is connected to the output 60 of the Miller stage, while the base of transistor T_{21} is connected via a diode D_2 to the output 4 and via a current source I_7 to the positive supply voltage terminal 15. The collector of transistor T_{20} is connected via a current source $I_5 = 2I_1$ to the positive supply voltage terminal 15 and also to the emitter of a current follower transistor T_{22} whose base carries a reference voltage V_6 and whose collector is connected via a current source $I_6 = I_1$ to ground terminal 16 and also to the base of output transistor T_{19} . The current source I_7 and diode D_2 ensure that a small quiescent current flows through the transistors T_{18} and T_{19} so that these transistors are set in class-AB. The change of the base emitter voltage of transistor T_{18} occurring upon driving by the Miller stage is converted by the voltage current converter 70 into a drive current with which transistor T_{19} is driven in phase opposition with transistor T_{18} .

In addition to the embodiment shown in Fig. 4, the first and the second amplifier may be formed in any manner other than the one shown, provided that they have an inverting input which gets a low impedance due to negative feedback, and a push-pull output stage.

The invention is not limited to the embodiments shown, but many variations within the scope of the invention are feasible to those skilled in the art.

Claims

1. A bridge amplifier comprising between two connection terminals for connecting an asymmetrical supply voltage :

— a voltage divider having a tap for taking off substantially half the supply voltage,

— a first amplifier for amplifying an input signal, comprising a first non-inverting input which is coupled to the tap on the voltage divider, a first inverting input and an output for connecting a first connection terminal of a load, said output being fed back by a resistor to the first inverting input, and

— a second amplifier for amplifying the input signal, comprising a first non-inverting input which is coupled to the tap on the voltage divider, a first inverting input and an output for connecting a second con-

by the resistors R_8 and R_9 is fed back to the first inverting input 7 and is subsequently amplified once more in an inverting manner via the input stage 40 and the output stage 46. Consequently, the amplifier 5 functions as a conventional inverting negative feedback amplifier, whose gain is substantially fully determined by the resistors R_8 and R_9 .

With respect to the embodiment of Fig. 1, this embodiment has the following advantage. In the embodiment of Fig. 1 the input signal only traverses the first amplifier in the case of a non-inverting amplification, whereas the input signal traverses both the first and the second amplifier in the case of inverting amplification. Consequently phase differences occur, which may give rise to distortion of the output signal. Since in the embodiment of Fig. 3 the negative feedback of the first and second amplifiers 1 and 5 is effected through separate input stages, the input voltage V_{in} cannot only be applied directly to the non-inverting amplifier 1, but also directly to the inverting amplifier 5. Consequently no phase difference occurs between the output signal at the output 4 of the first amplifier 1 and the output signal at the output 8 of the second amplifier 5 so that the output signal across the load R_L cannot be distorted. The same advantage occurs with respect to the embodiment in which the input voltage is applied via a voltage inverter circuit to the non-inverting input of the second amplifier.

Fig. 4 shows a simplified diagram of a possible embodiment of the first amplifier 1 for the bridge amplifier of Fig. 3. The second amplifier 5 is constructed in a similar manner. The first input stage 20 comprises two transistors T_{10} and T_{11} whose emitters are connected via resistors R_{30} and R_{31} to the output of a current source I_1 which is connected to the positive supply voltage terminal 15. The collector of transistor T_{10} is connected directly and the collector of transistor T_{11} is connected by a current mirror including transistors T_{14} and T_{15} to the output 23 of the input stage 20. With the aid of Line current mirror T_{14} , T_{15} the differential collector currents flowing in the transistors T_{10} , T_{11} due to the feedback voltage are converted into a single-ended output current which appears at output 23. The second input stage 29 is equal to the input stage 20 and comprises two transistors T_{12} and T_{13} whose emitters are connected via resistors R_{32} and R_{33} to the output of a current source I_2 . The collectors of the transistors T_{12} and T_{13} are connected to the collectors of transistors T_{10} and T_{11} , respectively. Consequently, the current mirror T_{14} , T_{15} also serves for converting the differential collector currents flowing in the transistors T_{12} and T_{13} due to the input voltage V_i into a single-ended output current to the output 23. This output 23 is connected to the input 26 of the output stage 25 which is provided with a so-called Miller stage comprising a transistor T_{18} whose collector is connected via a level shifting diode D_2 to a load current source I_3 . A frequency compensation capacitor C_1 is

arranged between the output 60 and the input 26 of this Miller stage. This output 60 is connected to the base of a first output transistor T_{18} which is arranged in series with a second output transistor T_{19} between the positive supply voltage terminal 15 and ground terminal 16. The emitter of transistor T_{18} and the collector of transistor T_{19} are connected to the output 4 of the output stage 25. This output stage 25 also comprises a voltage current converter 70 which is formed by two transistors T_{20} and T_{21} whose emitters are connected via resistors R_{34} and R_{35} to the output of a current source $I_4 = 2I_1$. The base of transistor T_{20} is connected to the output 60 of the Miller stage, while the base of transistor T_{21} is connected via a diode D_2 to the output 4 and via a current source I_7 to the positive supply voltage terminal 15. The collector of transistor T_{20} is connected via a current source $I_5 = 2I_1$ to the positive supply voltage terminal 15 and also to the emitter of a current follower transistor T_{22} whose base carries a reference voltage V_c and whose collector is connected via a current source $I_6 = I_1$ to ground terminal 16 and also to the base of output transistor T_{19} . The current source I_7 and diode D_2 ensure that a small quiescent current flows through the transistors T_{18} and T_{19} so that these transistors are set in class-AB. The change of the base emitter voltage of transistor T_{18} occurring upon driving by the Miller stage is converted by the voltage current converter 70 into a drive current with which transistor T_{19} is driven in phase-opposition with transistor T_{18} .

In addition to the embodiment shown in Fig. 4, the first and the second amplifier may be formed in any manner other than the one shown, provided that they have an inverting input which gets a low impedance due to negative feedback, and a push-pull output stage.

The invention is not limited to the embodiments shown, but many variations within the scope of the invention are feasible to those skilled in the art.

Claims

1. A bridge amplifier comprising between two connection terminals for connecting an asymmetrical supply voltage :

– a voltage divider having a tap for taking off substantially half the supply voltage,

– a first amplifier for amplifying an input signal, comprising a first non-inverting input which is coupled to the tap on the voltage divider, a first inverting input and an output for connecting a first connection terminal of a load, said output being fed back by a resistor to the first inverting input, and

– a second amplifier for amplifying the input signal, comprising a first non-inverting input which is coupled to the tap on the voltage divider, a first inverting input and an output for connecting a second con-



nection terminal of the load, said output being fed back by a resistor to the first inverting input, characterized in that at least

– the first inverting input of the first amplifier and the first inverting input of the second amplifier are coupled to an output of a buffer amplifier, an input of which is coupled to the tap on the voltage divider.

2. A bridge amplifier as claimed in Claim 1, characterized in that the first non-inverting input of the first amplifier and the first non-inverting input of the second amplifier are also coupled to the output of the buffer amplifier.

3. A bridge amplifier as claimed in Claim 1 or 2, characterized in that the first non-inverting input of the first amplifier constitutes the input for supplying the input signal.

4. A bridge amplifier as claimed in Claim 3, characterized in that the first inverting input of the second amplifier is coupled to a tap on a voltage divider arranged across the output of the first amplifier.

5. A bridge amplifier as claimed in Claim 1 or 2, characterized in that the first amplifier comprises :

– a first input stage having a first input constituting the first input constituting the first non-inverting input of the amplifier, a second input constituting the first inverting input of the amplifier, and an output connected to the input of an output stage having an output constituting the output of the first amplifier, and

– a second input stage having a first input constituting a second non-inverting input of the first amplifier, a second input constituting a second inverting input of the first amplifier, and an output connected to the input of the output stage, and in that the second amplifier comprises :

– a third input stage having a first input constituting the first non-inverting input of the second amplifier, a second input constituting the first inverting input of the second amplifier, and an output connected to the input of an output stage having an output constituting the output of the second amplifier,

– a fourth input stage having a first input constituting a second non-inverting input of the second amplifier, a second input constituting a second inverting input of the second amplifier, and an output connected to the input of the output stage, and in that

– the second non-inverting input of the first amplifier and the second inverting input of the second amplifier are coupled to a connection point for applying an input signal, and in that

– the second inverting input and the second non-inverting input of both the first and the second amplifier are coupled to a connection point for carrying a reference potential.

6. A bridge amplifier as claimed in Claim 5, characterized in that the first, second, third and fourth input stages are each constituted by a differential amplifier having a differential-to-single-ended converter.

7. A bridge amplifier as claimed in Claim 6, characterized in that the first and the second input stage comprise a common differential-to-single-ended converter and in that the third and the fourth input stage comprise a common differential-to-single-ended converter.

Revendications

1. Amplificateur en pont comportant entre deux bornes de connexion pour la connexion d'une tension d'alimentation asymétrique :

– un diviseur de tension muni d'une prise pour le prélèvement de pratiquement la moitié de la tension d'alimentation,

– un premier amplificateur pour amplifier un signal d'entrée muni d'une première entrée non inverseuse qui est couplée à la prise du diviseur de tension, d'une première entrée inverseuse et d'une sortie pour la connexion d'une première borne de connexion d'une charge, ladite sortie étant couplée à réaction par une résistance à la première entrée inverseuse et

– un deuxième amplificateur pour amplifier le signal d'entrée muni d'une première entrée non inverseuse qui est couplée à la prise du diviseur de tension, d'une première entrée inverseuse et d'une sortie pour la connexion d'une deuxième borne de connexion de la charge, laquelle sortie étant couplée à réaction par une résistance à la première entrée inverseuse, caractérisé en ce qu'au moins la première entrée inverseuse du premier amplificateur et la première entrée inverseuse du deuxième amplificateur sont couplées à une sortie de l'amplificateur tampon dont une entrée est couplée à la prise du diviseur de tension.

2. Amplificateur en pont selon la revendication 1, caractérisé en ce que la première entrée non inverseuse du premier amplificateur et la première entrée non inverseuse du deuxième amplificateur sont également couplées à la sortie de l'amplificateur tampon.

3. Amplificateur en pont selon la revendication 1 ou 2, caractérisé en ce que la première entrée non inverseuse du premier amplificateur constitue l'entrée pour la fourniture du signal d'entrée.

4. Amplificateur en pont selon la revendication 3, caractérisé en ce que la première entrée inverseuse du deuxième amplificateur est couplée à une prise du diviseur de tension disposé aux extrémités de la sortie du premier amplificateur.

5. Amplificateur en pont selon la revendication 1 ou 2, caractérisé en ce que le premier amplificateur comporte :

– un premier étage d'entrée présentant une première entrée constituant la première entrée non inverseuse de l'amplificateur, une deuxième entrée constituant la première entrée inverseuse de l'amplificateur et une sortie connectée à l'entrée d'un étage

de sortie présentant une sortie qui constitue la sortie du premier amplificateur et

– un deuxième étage d'entrée présentant une première entrée constituant une deuxième entrée non inverseuse du premier amplificateur, une deuxième entrée constituant une deuxième entrée inverseuse du premier amplificateur et une sortie connectée à l'entrée de l'étage de sortie, et en ce que le deuxième amplificateur comporte

– un troisième étage d'entrée présentant une première entrée constituant la première entrée non inverseuse du deuxième amplificateur, une deuxième entrée constituant la première entrée inverseuse du deuxième amplificateur et une sortie connectée à l'entrée de l'étage de sortie présentant une sortie qui constitue la sortie du deuxième amplificateur,

– un quatrième étage d'entrée présentant une première entrée constituant une deuxième entrée non inverseuse du deuxième amplificateur, une deuxième entrée constituant une deuxième entrée inverseuse du deuxième amplificateur et une sortie connectée à l'entrée de l'étage de sortie, et en ce que

– la deuxième entrée non inverseuse du premier amplificateur et la deuxième entrée inverseuse du deuxième amplificateur sont couplées à un point de connexion pour l'application d'un signal d'entrée, et en ce que

– la deuxième entrée inverseuse et la deuxième entrée non inverseuse des premier et deuxième amplificateurs sont couplées à un point de connexion pour appliquer un potentiel de référence

6. Amplificateur en pont selon la revendication 5, caractérisé en ce que les premier, deuxième, troisième et quatrième étages d'entrée sont constitués chacun par un amplificateur différentiel présentant un convertisseur différentiel à sortie unique.

7. Amplificateur en pont selon la revendication 6, caractérisé en ce que les premier et deuxième étages d'entrée comportent un convertisseur différentiel à sortie unique commun et en ce que les troisième et quatrième étages d'entrée comportent un convertisseur différentiel à sortie unique commun

Ansprüche

1. Brückenverstärker, der zum Anlegen einer asymmetrischen Speisespannung zwischen zwei Anschlußklemmen folgende Elemente enthält

– einen Spannungsteiler mit einem Abzweig zum Ableiten von im wesentlichen der Hälfte der Speisespannung,

– einen ersten Verstärker zum Verstärken eines Eingangssignals, mit einem ersten nicht invertierenden Eingang, der mit dem Abzweig auf dem Spannungsteiler verbunden ist, mit einem ersten invertierenden Eingang und mit einem Ausgang zum Anschließen einer ersten Anschlußklemme einer

Belastung, wobei dieser Ausgang über einen Widerstand zum ersten invertierenden Eingang rückgekoppelt wird, und

– einen zweiten Verstärker zum Verstärken des Eingangssignals, mit einem ersten nicht invertierenden Eingang, der mit dem Abzweig auf dem Spannungsteiler verbunden ist, mit einem ersten invertierenden Eingang und mit einem Ausgang zum Anschließen einer zweiten Anschlußklemme der Belastung, wobei dieser Ausgang über einen Widerstand zum ersten invertierenden Eingang rückgekoppelt wird, dadurch gekennzeichnet, daß wenigstens

– der erste invertierende Eingang des ersten Verstärkers und der erste invertierende Eingang des zweiten Verstärkers an einen Ausgang eines pufferverstärkers angeschlossen sind, von dem ein Ausgang mit dem Abzweig auf dem Spannungsteiler verbunden ist.

2. Brückenverstärker nach Anspruch 1, dadurch gekennzeichnet, daß der erste nicht invertierende Eingang des ersten Verstärkers und der erste nicht invertierende Eingang des zweiten Verstärkers ebenfalls mit dem Ausgang des Pufferverstärkers verbunden sind.

3. Brückenverstärker nach Anspruch 1 oder 2, dadurch gekennzeichnet, daß der erste nicht invertierende Eingang des ersten Verstärkers den Eingang zum Zuleiten des Eingangssignals darstellt.

4. Brückenverstärker nach Anspruch 3, dadurch gekennzeichnet, daß der erste invertierende Eingang des zweiten Verstärkers an einen Abzweig eines Spannungsteilers angeschlossen ist, der über den Ausgang des ersten Verstärkers angeordnet ist.

5. Brückenverstärker nach Anspruch 1 oder 2, dadurch gekennzeichnet, daß der erste Verstärker folgende Elemente enthält :

– eine erste Eingangsstufe mit einem ersten Eingang, der den ersten nicht invertierenden Eingang des Verstärkers darstellt, mit einem zweiten Eingang, der den ersten invertierenden Eingang des Verstärkers darstellt, und mit einem Ausgang, der an den Eingang einer Ausgangsstufe angeschlossen ist, von der ein Ausgang den Ausgang des ersten Verstärkers darstellt, und

– eine zweite Eingangsstufe mit einem ersten Eingang, der einen zweiten nicht invertierenden Eingang des ersten Verstärkers darstellt, mit einem zweiten Eingang, der einen zweiten invertierenden Eingang des ersten Verstärkers darstellt, und mit einem Ausgang, der an den Eingang der Ausgangsstufe angeschlossen ist, und daß der zweite Verstärker folgende Elemente enthält :

– eine dritte Eingangsstufe mit einem ersten Eingang, der den ersten nicht invertierenden Eingang des zweiten Verstärkers darstellt, mit einem zweiten Eingang, der den ersten invertierenden Eingang des zweiten Verstärkers darstellt, und mit einem Ausgang, der an den Eingang einer Ausgangsstufe mit ei-



nem Ausgang angeschlossen ist, der den Ausgang des zweiten Verstärkers darstellt,

– eine vierte Eingangsstufe mit einem ersten Eingang, der einen zweiten nicht invertierenden Eingang des zweiten Verstärkers darstellt, mit einem zweiten Eingang, der einen zweiten invertierenden Eingang des zweiten Verstärkers darstellt, und mit einem Ausgang, der an den Eingang der Ausgangsstufe angeschlossen ist, und daß

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– der zweite nicht invertierende Eingang des ersten Verstärkers und der zweite invertierende Eingang des zweiten Verstärkers an einen Anschlußpunkt zum Zuführen eines Eingangssignals angeschlossen sind, und daß

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– der zweite invertierende Eingang und der zweite nicht invertierende Eingang sowohl des ersten als auch des zweiten Verstärkers an einen Anschlußpunkt zur Führung eines Bezugspotentials angeschlossen sind

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6. Brückenverstärker nach Anspruch 5, dadurch gekennzeichnet, daß die ersten, zweiten, dritten und vierten Eingangsstufen durch je einen Differenzverstärker mit einem Differenz-zu-Eintakt-Wandler dargestellt werden.

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7. Brückenverstärker nach Anspruch 6, dadurch gekennzeichnet, daß die erste und die zweite Eingangsstufe einen gemeinsamen Differenz-zu-Eintakt-Wandler enthalten, und daß die dritte und die vierte Eingangsstufe einen gemeinsamen Differenz-zu-Eintakt-Wandler enthalten.

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