

SHEARING INTERFEROMETER WITH DYNAMIC PUPIL FILL

BACKGROUND OF THE INVENTION

Field of the Invention

[0001] The present invention is generally related to photolithography systems, and more particularly, to measuring wavefront parameters in a photolithographic system.

Related Art

[0002] Lithography is a process used to create features on the surface of substrates. Such substrates can include those used in the manufacture of flat panel displays, circuit boards, various integrated circuits, and the like. A frequently used substrate for such applications is a semiconductor wafer. One skilled in the relevant art would recognize that the description herein would also apply to other types of substrates.

[0003] During lithography, a wafer, which is disposed on a wafer stage (WS), is exposed to an image projected onto the surface of the wafer by an exposure system located within a lithography system. The exposure system includes a reticle (also called a mask) for projecting the image onto the wafer.

[0004] The reticle is usually mounted on a reticle stage (RS) and generally located between the wafer and a light source. In photolithography, the reticle is used as a photo mask for printing a circuit on the wafer, for example. Lithography light shines through the mask and then through a series of optical lenses that shrink the image. This small image is then projected onto the wafer. The process is similar to how a camera bends light to form an image on film. The light plays an integral role in the lithographic process. For example, in the manufacture of microprocessors (also known as computer chips), the key to creating more powerful microprocessors is the size of the light's wavelength. The shorter the wavelength, the more transistors can be

formed on the wafer. A wafer with many transistors results in a more powerful, faster microprocessor.

[0005] As chip manufacturers have been able to use shorter wavelengths of light, they have encountered a problem of the shorter wavelength light becoming absorbed by the glass lenses that are intended to focus the light. Due to the absorption of the shorter wavelength light, the light fails to reach the silicon wafer. As a result, no circuit pattern is created on the silicon wafer. In an attempt to overcome this problem, chip manufacturers developed a lithography process known as Extreme Ultraviolet Lithography (EUVL). In this process, a glass lens can be replaced by a mirror.

[0006] The problem of measuring the undesirable perturbations of the wavefront (often referred to as wavefront aberrations) is a persistent one for the lithographic applications. These wavefront aberrations result from various physical causes, such as changes in refractive or reflective properties of the optical elements (lenses or mirrors) occurring as a result of mechanical displacements or deformations, or changes in the optical properties of the optical elements caused by heating, or light-induced compaction. In particular, it is desirable to be able to measure wavefront quality in the photolithographic tool during wafer production and exposure, rather than having to take the tool offline in order to do so, which increases cost of ownership, reduces through-put or introduces some other type of inefficiency.

SUMMARY OF THE INVENTION

[0007] The present invention is directed to a scanning interferometer with dynamic pupil fill that substantially obviates one or more of the problems and disadvantages of the related art.

[0008] An embodiment of the present invention includes a wavefront measurement system including a source of electromagnetic radiation. An illumination system delivers the electromagnetic radiation to an object plane. An object generates a diffraction pattern and is located in the object plane. A projection optical system projects an image of the object onto an image plane.

A detector receives a fringe pattern from the image plane. The diffraction pattern is scanned across a pupil of the projection optical system.

[0009] Another embodiment of the present invention includes a wavefront measurement system with an illumination system that delivers electromagnetic radiation at an object plane. A source of a beam of the electromagnetic radiation is in the object plane. A projection optical system focuses the beam onto an image plane. A detector receives a fringe pattern of the beam from the image plane. The beam is scanned across a pupil of the projection optical system.

[0010] Another embodiment of the present invention includes a method of measuring a wavefront of an optical system including generating electromagnetic radiation at a source; delivering the electromagnetic radiation at an object plane of the optical system; generating a diffraction pattern at the object plane; scanning the diffraction pattern across a pupil of the optical system; receiving an image of the source while scanning the diffraction pattern; and determining wavefront parameters from the image.

[0011] Additional features and advantages of the invention will be set forth in the description that follows, and in part will be apparent from the description, or may be learned by practice of the invention. The advantages of the invention will be realized and attained by the structure and particularly pointed out in the written description and claims hereof as well as the appended drawings.

[0012] It is to be understood that both the foregoing general description and the following detailed description are exemplary and explanatory and are intended to provide further explanation of the invention as claimed.

BRIEF DESCRIPTION OF THE DRAWINGS

[0013] The accompanying drawings, which are included to illustrate exemplary embodiments of the invention and are incorporated in and constitute a part of this specification, illustrate embodiments of the invention

and together with the description serve to explain the principles of the invention. In the drawings:

- [0014] **FIG. 1** shows a portion of an exemplary photolithographic system of the present invention.
- [0015] **FIGs. 2 and 3** illustrate the use of an interferometer to produce shear wavefronts.
- [0016] **FIG. 4** illustrates an example of interference fringes as they appear at the focal plane with the use of the present invention.
- [0017] **FIG. 5** illustrates the rationale for the present invention, showing the optical exposure system in a stylized, schematic form.
- [0018] **FIG. 6** shows how magnitudes of the diffraction orders and change in an interferogram with an extended object in the object plane.
- [0019] **FIG. 7** illustrates an effect of modulating the extended object by a Ronchi grating.
- [0020] **FIG. 8** is another illustration of the arrangement of the optical elements that may be used in the present invention.
- [0021] **FIG. 9** is an illustration of dynamic pupil fill using a tilting reflective Ronchi grating.

DETAILED DESCRIPTION OF EMBODIMENTS OF THE INVENTION

- [0022] Reference will now be made in detail to the embodiments of the present invention, examples of which are illustrated in the accompanying drawings.
- [0023] It is convenient to characterize field-dependent aberrations of a projections optics (PO) by an aberration of a wavefront of a spherical wave emitted from a corresponding field point in the object plane. Various interferometry techniques can be used to measure aberration of this spherical wave. Shearing interferometry based on an extended incoherent source in the object plane superimposed with an object-plane grating matching the shearing grating is described in J. Braat and A. J.E.M. Janssen, *Improved Ronchi test with Extended Source*, J. Opt. Soc. Am. A, Vol. 16, No.1, pp.131-140, January

1999, incorporated by reference herein. Also, the paper by Naulleau *et al.*, *Static Microfield Printing at the ALS with the ETS-2 Set Optic*, Proc. SPIE 4688, 64-71 (2002)

([http://goldberg.lbl.gov/papers/Naulleau_SPIE_4688\(2002\).pdf](http://goldberg.lbl.gov/papers/Naulleau_SPIE_4688(2002).pdf)), incorporated by reference herein describes the dynamic pupil fill illumination system for EUV implemented in order to control partial coherence during printing at a synchrotron light source where illumination is coherent.

[0024] **FIG. 1** illustrates a photolithographic system **100** according to the present invention. The system **100** includes an illumination source **105**, a condenser lens **102**, an extended object **103** (located in the object plane), projection optics **104** with a pupil **105**, an image plane shearing grating **106**, a detector lens **107** and a CCD detector **108**, arranged as shown in the figure. These elements will be discussed further below.

[0025] The grating **106** includes both transmissive and opaque regions. The opaque regions can be formed of materials that absorb the radiation (for example, for 13.5 nm exposure wavelength in the case of EUV lithography, or optical radiation in the case of lithographic systems using longer wavelengths), such as nickel, chromium or other metals.

[0026] It will also be appreciated that although the present invention is applicable to lithographic systems that use refractive optical elements (such as the projection optics **104**, and the imaging optics), the invention is also applicable to systems using other wavelengths, with appropriate transmissive/refractive components used in place of reflective ones, as needed.

[0027] The grating **106** also can include reflective (or opaque) regions. These reflective regions can be formed of materials that absorb the radiation (for example, for 13.5 nm EUV exposure wavelength), such as nickel, chromium or other metals.

[0028] The pitch of the grating **106** is chosen to provide an appropriate shear ratio, where the CCD detector **108** is in the fringe plane (i.e., below the focal, or image, plane of the system), and "sees" a pattern of fringes (an interferogram) or a number of overlapping circles, as will be discussed further

below. The shear ratio is a measure of the overlap of two circles, where a shear ratio of zero represents perfect overlap. Note also that it is desirable for the CCD detector **108** to "see" only the zeroth order and the + and - 1st order diffraction images, and to eliminate the + and - 2nd order diffraction images. Furthermore, the extended object **103** is constructed to aid in eliminating unwanted orders. It is important, however, that whichever pattern of transmission and reflection areas is used, that it be a regular pattern.

[0029] The pitch of the source module grating **203** is also preferably chosen to match the pitch of the shearing grating so as to redistribute the light in the pupil to those locations that will mutually overlap as a result of shearing.

[0030] **FIGs. 2 and 3** illustrate reference wavefronts and shear in a lateral shearing interferometer **210**. The lateral shearing interferometer **210** interferes a wavefront with itself, or, phrased another way, it interferes a shifted copy of the wavefront with itself. As shown in **FIGs. 2 and 3**, the grating **106**, positioned in the image plane, acts as a shearing interferometer, and generates a transmitted waves **204** with a wavefront **211A**, and a diffracted reference wave **205** with a wavefront **211B**. Thus, the lateral shearing interferometer **210** creates one or more apparent sources, whose wavefronts **211A, 311B** interfere to produce fringes **212**.

[0031] **FIG. 4** illustrates the wavefront fringes (**212A, 212B** in **FIG. 2**) as seen by the CCD detector **108**. As shown in **FIG. 4**, in the upper right-hand photograph, sheared fringes for a single object space slit are shown, where the slit is positioned in front of an incoherent, diffuse source that fills the maximum numerical aperture and smoothes any wavefront inhomogeneities. The bottom right-hand figure shows a fringe visibility function **401**, with zeroth order pattern **502** and first order diffraction patterns **403**. The 50% duty cycle on the grating **106** makes all even orders of the diffraction pattern invisible. At the bottom left of **FIG. 4**, the image space shearing grating **106** is shown, with a shear ratio of 0.5.

[0032] In practice, a source point (**101**) is replaced by the "extended object **103**" to increase the optical throughput. The minimal dimensions of the

extended object **103** are dictated by the available illumination power and the sensitivity of the detector device used to measure the interferograms. Depending on the object-side numerical aperture (NA) of the projection optics **104** and the optical throughput requirements, it is often the case that the angular width of the diffraction pattern from the extended object **103** is small compared to the object-side NA of the PO **104**. In that case, most of the light from this object ends up concentrated within a small area of the PO **104** pupil **105**. Even for the highest pupil fills of the projection optics **104**, the pupil **105** is still not completely filled, as is preferred for a complete aberration measurement. In this situation, the wavefront measurement methods will have very little sensitivity to the PO **104** aberrations occurring outside a relatively small illuminated area of the pupil **105**. It is therefore preferred to fill the pupil **105** of the PO **104** more or less uniformly.

[0033] Thus, the problem of measuring wavefront aberrations has to balance two competing interests: filling the entire pupil **105** (but at the cost of very low intensity), or having sufficient intensity, but only on a small portion of the pupil **105**.

[0034] The following methods can be used to ensure the desired pupil fill in shearing interferometry:

[0035] (1) introducing a transmissive pattern inside the extended object **103** that matches the shearing grating (e.g., a Ronchi grating) and providing a fully incoherent illumination of the extended object **103** [see Baselmans, *supra*]; and

[0036] (2) placing an extended incoherent source into an object plane (by using a critical illumination or a diffuser in the object plane) and superimposing it with a Ronchi grating that matches the shearing grating [see Bratt et al., *supra*].

[0037] These methods have several problems:

[0038] (1) speckle disturbance of the measured interferograms occurs due to the remaining coherence of the effective source (this applies to methods 1 and 2) or due to a finite size of the object plane diffuser elements (this applies

to method 2). The speckle disturbance adds high-frequency intensity fluctuations to the measured interferograms, resulting in wavefront measurement errors;

[0039] (2) the need to switch to a special illumination mode (this applies to methods 1 and 2) during the measurement complicates the wavefront measurement process; and

[0040] (3) a significant portion of light is diffracted from the extended object 103 away from the pupil 105 and does not participate in a formation of the sheared interferogram.

[0041] The present invention thus applies to the situation when the size of the extended object 103 needed to ensure the required optical throughput is such that the characteristic width of the diffraction pattern is much less than the object side NA of the PO 104, i.e., $\lambda / \text{extended object size} \ll \text{NA object}$.

[0042] The pupil fill by the extended object 103 can be achieved dynamically. During the measurement of the interferogram, the extended object 103 can be dynamically modified, so that the diffraction pattern from this object scans across the whole entrance pupil 105. The CCD detector 108 that measures the sheared interferogram integrates (or sums) the momentary interferograms occurring in the process of measurement.

[0043] The dynamic modification of an extended object 103 can be performed by using a reflective element, such as a tilting mirror, or by using a refractive object with varying slope and/or other characteristics (e.g., a parabolic or spherical lens) moved against an aperture.

[0044] The reflected and transmissive extended objects described above use dynamic phase variation of light induced by linearly varying complex reflectivity/transmittance within or across the extended object 103. However, arbitrary (non-linear) phase variation effect can be also used to fill the pupil 105 dynamically. Many physical arrangements well known to those skilled in the art are possible for realizing such arbitrary non-linear phase variations. For instance, they can be achieved by using an extended movable object with its structure changing within or across it, and/or dynamically deformed, and/or

otherwise dynamically modified (e.g., using spatial light modulators). Other possible realizations of dynamically introduced phase variation can include a diffusor pattern formed on a transmissive or reflective flexible substrate that can be physically deformed, including plastics, piezoelectric materials, and stress-birefringent materials whose stresses are induced by actuators, etc.

[0045] Unless very small shears are utilized, in either of the above methods, the extended object 103 must have a transmittance pattern (an object plane Ronchi grating matching the shearing grating) superimposed on it to provide additional redistribution of light in the pupil 105, as described in Bratt et al. and Baselmans, cited above.

[0046] The dynamic modification is performed so that the transmittance function within the extended object has a time-dependent linear variation of the phase that ensures that the diffraction pattern from the extended object is shifted within the pupil 105, dynamically sweeping the pupil 105 during the act of measurement.

[0047] The measurement of the interferogram is performed by the CCD detector 108 that records energy distribution across the CCD detector 108 plane. The CCD detector 108 is capable of integrating the time-varying intensity at every point in the detector 108 plane to collect a sufficient number of photons during the act of measurement. The CCD arrays used in present-day wavefront sensors (like the CCD detector 108) satisfy this requirement.

[0048] As noted above, the dynamic modification of the extended object 103 can be achieved by any number of mechanisms. For instance, a reflective extended object 103 may be used. Examples of such reflective objects include:

[0049] (1) A tilting flat mirror can be used in a combination with an aperture, or having only a small flat portion of a large tilting object to be reflective. A relatively large tilting mirror is easier to control (e.g., to tilt and rotate) compared to a micro-mirror. The extended object 103 in this case coincides with the tilting flat mirror, as shown in FIG. 9.

[0050] (2) A tilting micro-mirror, such as a mirror from a spatial light modulator (SLM) array, can be used as the entire extended object 103 (see FIG. 9). In order to sweep the pupil 105, the micro-mirror has to tilt in two axes in the object plane. If the micro-mirror can only tilt in one axis, it can be rotated around the axis perpendicular to the object plane, thus allowing a conical sweep of the 2D pupil 105. In practice, such a case is rare.

[0051] (3) A reflective object with a varying slope of a reflective surface, such as a parabolic or spherical mirror, which is moved linearly behind a small aperture, can be used as the entire extended object 103.

[0052] Note that in the case of reflective elements used to scan the diffraction pattern across the pupil 105, they need not always be located at the object plane. For example, a flat tilting mirror could be located between the object plane and the pupil 105 of the PO 104 (also acting to fold the optical axis of the system).

[0053] The extended object 103 can also be transmissive. In that case, the dynamic pupil fill can be achieved by moving a refractive element with a varying slope of one of its surfaces (e.g., a spherical or parabolic lens) against a small aperture, as shown in FIG. 8. A transmissive grating can also be used, such that various regions on the grating have different grating pitch, and the grating is moved linearly in its plane (i.e., perpendicular to the direction of the propagation of the electromagnetic radiation) so as to vary the direction of the beam (i.e., to scan it across the pupil 105). It is also important to realize that, depending on the particular type of extended object 103 used, the size of the pupil 105 and the scanning approach, maintaining proper focus in the image plane may become a problem, as the diffraction pattern is being scanned across the pupil 105. However, it is currently believed that although it is preferred to maintain focus, some de-focusing is acceptable.

[0054] Unless very small shears are utilized, in any of the above implementations, the extended object 103 must have a transmittance pattern (an object plane Ronchi grating matching the shearing grating) superimposed on it to provide additional redistribution of light in the pupil 105, as described

in Bratt et al. and Baselmans. In addition, any of the above objects are preferably translatable in two lateral dimensions to accomplish the phase shift readout of fringes preferred in the shearing interferometer measurement.

[0055] The final sheared interferogram measured by the CCD detector 108 is a result of integration in time of the momentary sheared interferograms resulting from most of the light concentrated within a small portion of the pupil 105. The momentary sheared interferograms may have high contrast interference fringes only within a relatively small portion of the pupil image in the detector plane formed by the interfering diffraction orders. Their time integral measured by the CCD detector 108 has well-defined interference fringes across the whole pupil 105 that can be used (typically in conjunction with phase-stepping) to compute the wavefront aberration.

[0056] This is due to the fact that dynamic pupil fill described above is equivalent to the use of a stationary source corresponding to an actual source convolved with the dynamic movement (source scanning). Thus, regardless of the degree of coherence of illumination from the actual source, the effective source provides fully incoherent illumination.

[0057] **FIG. 5** illustrates the rationale for the present invention, showing the optical exposure system in a somewhat stylized, schematic form. This figure relates to the use of a pinhole in the object plane in order to generate the spherical wave that fills the pupil 105 and whose aberration is measured by the shearing interferometer. As shown in **FIG. 5**, going from top to bottom in the figure, light from a light source goes through a condenser lens 102, and then through an object plane with a pinhole. The magnitude of the field at the pupil 105 of the projection optics 104 is shown by diagram A, where the pupil 105 coordinate is given as "f". Light then is focused onto an image plane 605, then passes through optional detector projection optics 107, and is detected by the detector 108 in the detector plane. Graph B shows magnitudes of the -1 and +1 diffraction orders formed by the shearing grating, which is located in the image plane 605. Graph C shows an interferogram resulting from the diffraction orders from the shearing grating. Note the visible image variation

that is due to the aberrations (phase variations) that are present in the resulting interferogram.

[0058] **FIG. 6** shows how the magnitudes of the diffraction orders and change in the interferogram, when an extended object **103** is placed in the object plane that fills only a small portion of the pupil **105**, resulting in interferogram fringes of very small (negligible) contrast observed in the detector plane within the non-overlapping peaks corresponding to the sheared diffraction pattern of the extended object **103**. As in **FIG. 5**, Graph A in **FIG. 6** shows the magnitude of the field in the pupil **105** of the projection optics **104**, with the pupil coordinate "f". Graph B shows the magnitudes of the 0th, -1, and +1 diffraction orders formed by the shearing grating **106**, when an extended object **103** is present in the object plane. Graph C shows the interferograms resulting from the diffraction orders from the shearing grating. Because the diffraction orders do not overlap sufficiently, the resulting interferogram only weakly depends on the wavefront aberrations.

[0059] **FIG. 7** illustrates the effect of modulating the extended object **103** by a Ronchi grating, that redistributes the light in the pupil **105** to those locations that will mutually overlap as a result of shearing. As with **FIGs. 5** and **6**, Graph A shows the magnitude of the field in the pupil **105** of the projection optics **104**. Graph B shows magnitudes of the 0th, +1 and -1 diffraction orders formed by the shearing grating, and Graph C shows the resulting interferogram from the diffraction orders from the shearing grating and the matching Ronchi grating. As a result of the overlap between the 0th, +1 and -1 diffraction orders, the interferogram in the overlap region (inside the peaks) strongly depends on the wavefront aberrations.

[0060] **FIG. 8** is another illustration of the arrangement of the optical elements that may be used in the present invention, namely a dynamic pupil fill using a moving refractive object. The illustration of **FIG. 8** is primarily applicable to a transmissive extended object **103**. For example, as shown in **FIG. 8**, a transmissive Ronchi grating **801** can be used, with a refractive object having a varying slope that is moved against the object plane. The graphs on

the lower right of **FIG. 8** illustrate the interferograms resulting with this arrangement. Note that the refractive object, as noted above, may be, for instance, a spherical or a parabolic lens that is being moved against a small aperture.

[0061] **FIG. 9** is another illustration of dynamic pupil fill using a tilting reflective Ronchi grating **901**, with the beam patterns not shown. As shown in **FIG. 9**, a beam splitter **902** may also be necessary. The reflective extended object **103** (in this case, the Ronchi grating **901**) is placed on a tilting mirror. The diagrams at bottom right illustrate the resulting interferogram patterns. The large tilting mirror can be used in combination with an aperture, or can have only a small, flat part portion, or can be a small flat portion of a large tilting object, which is made reflecting. A relatively large mirror, or a larger object, is easier to handle (in other words, to tilt and rotate) compared to a micromirror. The extended object **103** in this case would coincide with the large tilting mirror, as shown in **FIG. 9**.

[0062] Also, a tilting micromirror (such as a mirror in a spatial light-modulator array) may be used as the entire extended object **103**.

[0063] The present invention has a number of advantages over conventional systems. For example, the dynamic pupil fill eliminates the need for a diffuser in the object plane (e.g., in EUV wavefront sensors), thus resulting in elimination or reduction of speckle-induced wavefront measurement errors.

[0064] The dynamic pupil fill also eliminates the need to switch to a special illumination mode during the wavefront measurement. The same illumination mode used during the exposure can be used to perform the wavefront measurement. (However, one still has to properly position a reticle stage with the tilting mirror on it.)

[0065] The dynamic pupil fill also allows to fill the PO pupil **105** "tightly," thus significantly reducing the loss of light that occurs with other methods. If necessary or desirable, the dynamic pupil fill allows sampling only the portions of the PO pupil that are of interest.

[0066] It will be understood by those skilled in the art that various changes in form and details may be made therein without departing from the spirit and scope of the invention as defined in the appended claims. Thus, the breadth and scope of the present invention should not be limited by any of the above-described exemplary embodiments, but should be defined only in accordance with the following claims and their equivalents.

WHAT IS CLAIMED IS:

1. A wavefront measurement system comprising:
a source of electromagnetic radiation;
an illumination system that directs said electromagnetic radiation to an object plane;
an object in the object plane producing a diffraction pattern;
a projection optical system that projects an image of said object onto an image plane; and
a detector that receives a fringe pattern from said image plane,
wherein the diffraction pattern is scanned across a pupil of said projection optical system.
2. The system of claim 1, wherein the object includes a tiltable mirror for scanning the diffraction pattern across the pupil.
3. The system of claim 1, wherein the object includes a diffraction grating with variable pitch for scanning the diffraction pattern across the pupil.
4. The system of claim 1, wherein the object includes a refractive prism with a varying wedge angle for scanning the diffraction pattern across the pupil.
5. The system of claim 1, wherein the object includes a spatial light modulator for scanning the diffraction pattern across the pupil.
6. The system of claim 1, wherein the object generates a non-linear phase variation across to scan the diffraction pattern across the pupil.
7. The system of claim 1, wherein the object comprises a stress-birefringent material to scan the diffraction pattern across the pupil.

8. The system of claim 1, further comprising reflective optics for scanning the diffraction pattern across the pupil.

9. The system of claim 1, further comprising refractive optics for scanning the diffraction pattern across the pupil.

10. The system of claim 1, wherein the object includes a movable mirror with a variable surface slope for scanning the diffraction pattern across the pupil.

11. The system of claim 1, wherein the diffraction pattern is dynamically scanned across a pupil of said projection optical system.

12. The system of claim 1, wherein the detector is located in a plane that is optically conjugate with the pupil.

13. The system of claim 1, further comprising a grating in the image plane to generate the fringe pattern.

14. A wavefront measurement system comprising:
an illumination system that delivers electromagnetic radiation to an object plane;
an object in the object plane that generates a beam of the electromagnetic radiation;
a projection optical system that projects the beam onto an image plane;
and
a detector that receives a fringe pattern of the beam from the image plane,
wherein the beam is scanned across a pupil of the projection optical system.

15. The system of claim 14, wherein the object includes a tiltable mirror for scanning the beam across the pupil.

16. The system of claim 14, wherein the object includes a diffraction grating with variable pitch for scanning the beam across the pupil.

17. The system of claim 14, wherein the object includes a refractive prism with a varying wedge for scanning the beam across the pupil.

18. The system of claim 14, wherein the object includes a spatial light modulator for scanning the beam across the pupil.

19. The system of claim 14, wherein the source of the diffraction pattern generates a non-linear phase variation across to scan the diffraction pattern across the pupil.

20. The system of claim 14, wherein the source of the diffraction pattern includes a stress-birefringent material for scanning the beam across the pupil.

21. The system of claim 14, further comprising reflective optics for scanning the beam across the pupil.

21. The system of claim 14, further comprising refractive optics for scanning the beam across the pupil.

22. The system of claim 14, wherein the object includes a movable mirror with a variable surface slope for scanning the beam across the pupil.

23. The system of claim **14**, wherein the detector is located in a plane that is optically conjugate with the pupil.

24. The system of claim **14**, further comprising a grating in the image plane to generate the fringe pattern.

25. A method of measuring a wavefront of an optical system comprising:

generating electromagnetic radiation at a source;

delivering said electromagnetic radiation to an object plane of said optical system;

generating a diffraction pattern at said object plane;

scanning the diffraction pattern across a pupil of said optical system;

receiving an image of said source while scanning the diffraction pattern; and

determining wavefront parameters from said image.

26. The method of claim **25**, wherein the scanning step includes tilting a mirror to direct the diffraction pattern across the pupil.

27. The method of claim **25**, wherein the scanning step includes moving a diffraction grating with variable pitch to direct the diffraction pattern across the pupil.

28. The method of claim **25**, wherein the scanning step includes adjusting a refractive prism with a varying wedge angle to direct the diffraction pattern across the pupil.

29. The method of claim **25**, wherein the scanning step includes adjusting a spatial light modulator to direct the diffraction pattern across the pupil.

30. The method of claim **25**, wherein the scanning step uses reflective optics to scan the diffraction pattern across the pupil.

31. The method of claim **25**, wherein the scanning step uses refractive optics to scan the diffraction pattern across the pupil.

32. A method of measuring a wavefront of a projection optical system comprising:

- (1) delivering electromagnetic radiation at an object plane of the projection optical system so as to generate a beam directed at the projection optical system;
- (2) positioning a detector below an image plane of the projection optical system;
- (3) receiving a fringe pattern of the beam at the detector while simultaneously scanning the beam across a pupil of the optical system; and
- (4) calculating wavefront aberrations from the fringe pattern.

33. A wavefront measurement system comprising:
means for generating electromagnetic radiation;
means for delivering said electromagnetic radiation to an object plane of a projection optical system;
means for generating a diffraction pattern in the object plane;
the projection optical system that projects an image of said diffraction pattern onto an image plane; and
means for detecting a fringe pattern from said image plane,
means for scanning the diffraction pattern across a pupil of said projection optical system.