A METHOD AND A SYSTEM FOR MULTI-PIXEL RANGING OF A SCENE

Field of the Invention

The present invention relates to a method and a system for multi-pixel ranging of a scene, using a single detector/receiver associated with a time-delay arrangement and is specifically concerned with such methods and systems in which the time delay is constituted by multi-length optic fibers.

Background of the Invention

As far as passive, two-dimensional scanning is concerned, especially in the visible region of the spectrum, present-day technology has provided a satisfactory answer in the form of various detector arrays and matrices, such as, e.g., CCD devices. The problem becomes more complex when the scene to be scanned requires active illumination. Some of the known devices use the direct scanning solution, in which the illuminator beam is passed through a scanning device and impinges upon the scene. The reflected light, after being steered by the same scanner, produces an image on a detector. The moving parts and the required synchronization constitute serious drawbacks.

At the other end of the spectrum of scanning devices is the detector array. The light source illuminates the entire scene, which is "seen" in full by an array of detectors.

The practical value of these solutions depends on various parameters, associated partly with the device itself and partly with the scene and the atmospheric conditions, in conjunction with the demands of the overall system. Sometimes a hybrid solution is indicated, in which a detector array having a partial field of view only, and an accordingly shaped illuminator beam, partially scan the scene. Such complex solutions should be selected when three-dimensional profiling imaging is

required, especially in the infrared region of the spectrum, and more particularly when eye-safe illumination is to be used.

The heart of advanced, modern, non-eye-safe three-dimensional imagers is the high-powered laser, illuminating the scene or part of it, and an array of avalanche photodiodes (APDs) with the associated range-measuring and image-creating electronics. The most serious disadvantage of these devices is the demand for arrays of detectors that must be both sensitive and have a very rapid response to the short pulses of the laser illuminators.

It is these illuminators and the corresponding detectors that are used in military range finders. The light radiated is not eye-safe and the APD detectors with their range-imaging electronics are very complex and expensive, in comparison with the conventional detector arrays used in video cameras.

Lately, due to the growing demand for eye-safe devices and due to the latest developments and availability of solid-state, eye-safe laser illuminators, a similar demand is felt for appropriate APD detector arrays for eye-safe, three-dimensional profiling imaging. This means a low-cost array, or at least a sub-array, of APDs, sensitive to the wavelength of eye-safe laser light (1.5 to 1.6 μm). Until recently, no such array has been available. Detectors to be used with laser range finders operating at such a wavelength are too difficult to produce as multi-element arrays. Despite efforts reported in the literature, so far only partial success has been achieved in developing a prototype of such an APD having a quasi-array of a few elements, which suffers from enormous electronic complexity and is very expensive, making it impractical for world market demands.

U.S. Patent 3,991,318 (Duguay) discloses an optical detection system utilizing an organ array of optical fibers, each cut to different lengths, one end of each of the fibers being arranged in a grid under a planar writing surface. Detection means are coupled to the other end of each of the fibers. The utilization of a detector for each of the fibers renders the system cumbersome and costly.

Disclosure of the Invention

It is therefore a broad object of the present invention to ameliorate the problems and disadvantages of the above-described methods and systems for the ranging of a scene.

It is a further object of the present invention to provide a method and system for multi-pixel, ranging of a scene using a single detector/receiver associated with time-delay arrangement, based on multi-length optical fibers.

According to the present invention, the above objects are achieved by a method for multi-pixel ranging of a scene, comprising the steps of providing a single detector associated with a time-delay arrangement; producing a time-arrival distribution of pulse echoes of at least part of a remote scene in a defined ranging plane; receiving said distribution as produced on said ranging plane and conveying it, echo pulse by echo pulse through a plurality of echo pulse conveying means to a single detector while introducing a time delay, whereby said echo pulses arrive at said single detector in a sequential order, and using an electronic logic to reconstruct said time-arrival distribution from said time-delayed echo pulses received by said detector.

The invention still further provides a system for ranging of a scene, comprising optical means to create a replicate of a remote scene range distribution on a defined ranging plane; time-ordered echo pulses conveying means receiving said echo pulses from said ranging plane, each of said conveying means constituting an optical path of different length, introducing time delays; a single detector/receiver for detecting the echo pulses time of arrival in a sequential order produced by said time delays, and an electronic logic fed by said single detector to reconstruct said scene by the ranged distribution of echo pulses.

Brief Description of the Drawings

The invention will now be described in connection with certain preferred embodiments with reference to the following illustrative figures so that it may be more fully understood.

With specific reference now to the figures in detail, it is stressed that the particulars shown are by way of example and for purposes of illustrative discussion of the preferred embodiments of the present invention only, and are presented in the cause of providing what is believed to be the most useful and readily understood description of the principles and conceptual aspects of the invention. In this regard, no attempt is made to show structural details of the invention in more detail than is necessary for a fundamental understanding of the invention, the description taken with the drawings making apparent to those skilled in the art how the several forms of the invention may be embodied in practice.

In the drawings:

Fig. 1 is a block diagram of the system according to the present invention;

Fig. 2 is an enlarged, more detailed, schematic view of the fiber/detector unit of the system of Fig. 1;

Fig. 3 represents a two-dimensional scanning configuration;

Fig. 4 shows a one-dimensional scanning configuration;

Fig. 5 shows a non-scanning, staring configuration;

Fig. 6 depicts an example of a combined fiber architecture;

Fig. 7 illustrates a practical, compact version of the architecture of Fig. 6;

Fig. 8 shows the use of a sub-bundle of fibers;

Fig. 9 illustrates the use of a sub-bundle of fibers for use with a light-intensity detector/receiver;

Fig. 10 illustrates the use of a mediator arrangement;

Fig. 11 shows a first method of coupling a relatively narrow fiber to a much larger detector/receiver;

Fig. 12 illustrates a mediator arrangement for the same purpose as shown in Fig. 11, and

Fig. 13 is a detailed block diagram of an embodiment of the electronics associated with the single detector/receiver of the system according to the present invention.

Detailed Description of Preferred Embodiments

Referring now to the drawings, there is seen in Figs. 1 and 2 a block diagram of the system of the present invention, comprising imaging means 2 such as, e.g., a lens, a bundle 4 of optical fibers 1 to $1^{n'}$, a single detector/receiver 6 and signal addressing logic 8. The fiber-detector sub-unit is denoted by numeral 10, and the entire system by numeral 12. In Fig. 2 there are seen details of the sub-unit 10 of Fig. 1 also illustrating the working principle of the invention, according to which the whole array of detectors required by conventional range imagers is replaced by a single detector/receiver 6.

It is assumed that an illuminator (not shown) illuminates the scene by appropriate pulses of light and that a multi-pixel optical image of the scene is produced by imaging means in the ranging plane 14 in which the front end of the fiber bundle 4 is located. The plane 14 collects the echoes of the illuminator light from the various parts of the scene, each having its own range and conveys it to detector/receiver 6. The stratagem, provided by the invention, whereby each range pixel of an instantaneous, multi-range pixel scene is channeled into a single detector/ receiver while still retaining its individuality, is clearly perceived from Fig. 2 and consists in introducing a time delay between the arrival at the single detector/receiver of each of the fiber-transmitted range pixels. This is realized by providing each of the fibers of bundle 4 with a different optical path length, i.e., a different physical length, as clearly seen in Fig. 2. There is shown a fiber bundle 4 having *n* fibers extending between ranging plane 14 and the single detector/receiver 6. It is seen that each fiber 1 is longer than its neighbor by a length symbolized by loop 16 and

predetermined in accordance with the pixel position and the signal addressing logic 8 of system 12. Given the limited range imager space available and weight permissible on the one hand, and the velocity of light on the other, it is obvious that these delays are of an order of magnitude of nanoseconds, but are still within the power of resolution of logic 8.

In this way, the sequential, time-ordered electronic pulses outputting from the single detector/receiver 6 and fed to the signal addressing logic 8 will each carry its own range and artificially added time-delay address, to be individually recognized and processed by the signal addressing logic 8.

The present invention allows for several fiber bundle configurations, depending on the light distribution created in ranging plane 14, which, in turn, is defined by the overall illuminator-detection system chosen. In principle, there are three configurations available: a configuration requiring two-dimensional scanning (Fig. 3), a configuration allowing one-dimensional scanning (Fig. 4) and a non-scanning configuration (Fig. 5).

The two-dimensional scanning configuration of Fig. 4 shows a bundle 4 of, in this example, four fibers, the ends of which are located in ranging plane 14 and over which the image is scanned by any of the *per se* known two-dimensional scanners. In conformity with the above-given explanations concerning the time-delay principle, each one of the four fibers is of a different length. Arrow *A* indicates the light from the imaging means 2 (Fig. 1).

A one-dimensional scanning configuration is shown in Fig. 4. Here, bundle 4 (at its range plane end) is flat, and of a linear extent that covers the largest horizontal dimension of ranging plane 14, in this case, its diameter. In this embodiment, too, the fibers of flat bundle 4 are each of a different length. It will be appreciated that while the image-side end of bundle 4 must be flat, the rest of its length may assume any shape. The shape of the detector-side end will be discussed further below. The

advantage of this configuration is the reduced complexity of the required scanning mechanism.

Fig. 5 illustrates a non-scanning, so-called staring configuration, in which bundle 4 is of such a size as to fill the entire ranging plane 14. The fact that this configuration requires no scanning at all is a definite advantage. On the other hand, the total weight, length and bulkiness of such a bundle might present difficulties for some applications, for which possible solutions will be proposed further below.

An additional parameter influencing the fiber bundle configuration is the filling factor of the scene-to-fiber transfer. While it is most convenient to provide one fiber for each range pixel in ranging plane 14, the circular cross-section of commercially available fibers, when packed to form a bundle, produces blind spots between adjacent fibers. With fibers of a diameter of, e.g., 100 μm, the extent of these blind spots is liable to become significant, inasmuch as important information may be missed. In such cases, it is advantageous to use a number (n^2) of fibers of a small diameter (e.g., 10 μm), to jointly collect the range pixels previously collected by a single, 100 μm diameter fiber, resulting in a pronounced reduction of the blind spot areas. Depending on the fiber architecture selected (see below), the n^2 fibers may be directly coupled to detector/receiver 6, or may be merged into a single, larger fiber before reaching detector/receiver 6.

The term "fiber bundle architecture" refers, in general, to the way the light is conveyed from the ranging plane to the detector/receiver, using a bundle of fibers. In direct architecture, one end of each fiber is located in ranging plane 14, the other end being coupled to detector/receiver 6. This architecture is convenient when the number of pixels, multiplied by the diameter of the fiber, is close to the detector/ receiver diameter, thus ensuring that most of the detector/receiver surface will be illuminated. As an example, when 10 fibers are needed, each of a diameter of 100 μm, and the detector/receiver diameter is 1.5 to 2 mm, the direct architecture will be a good choice.

The combined architecture is used when the number of needed fibers is large and/or when there are severe restrictions on the volume and weight of the detection system. It should be kept in mind that, due to the increasing length of the fibers (one with respect to the other) in the bundle, the total length and weight, in the direct architecture, may be too great. The combined architecture resolves this problem in a very elegant way the fibers used in ranging plane 14 are chosen to be of small diameter (for example, 10 μm). Some distance way from the ranging plane, the fibers are inserted into a main, thick fiber (in this example, 300 μm), each fiber at a different distance, to produce a different optical path for each fiber, as required by the invention. In such a configuration, the total fiber length is mainly the length of the main, thick fiber, which is much less than the total lengths of all the fibers used in the direct architecture. When necessary matching between the main fiber diameters and the detector diameter requires a thicker main fiber, several main fibers may be used, with only a part of the ranging-plane fibers entering each main fiber, or a thicker main fiber may be used. Schematically, this architecture is seen in Fig. 6, showing ranging plane 14, detector/receiver 6, main fiber 18 and thin ranging-plane fibers 1, 1', 1" to $1^{n'}$.

Fig. 7 shows a practical, compact version of the architecture of Fig. 6, showing a coil 20 on which main fiber 18 is wound, as well as parts of the thin, ranging-plane fibers 1 to $1^{n'}$.

The former architecture may present difficulties when the ranging plane thin fibers are of extremely small diameters (e.g., 10 μm). This is so because of the severe mechanical adjustment needed between the exact fiber position and the ranging pixel position. As illustrated in Fig. 8, the solution to this problem is found in the previously mentioned replacement of each ranging plane fiber by $m \times m$ thin fibers 1 to $1^{n'}$ packed in sub-bundles 21, each sub-bundle replacing a single fiber 1 to $1^{n'}$. If, for example, $3 \times 3 = 9$, 10 μm replacement fibers are used, the focal length of the ranging means is changed to such an extent that the ranging pixel is enlarged to fit a

sub-bundle diameter of 3 x 10 = 30 μm. These fibers are commercial, and the problem of mechanical tolerance is eliminated. Furthermore, the $m \times m$ thin fiber model offers additional advantages and can be used to resolve additional problems and fulfill other functions. One of the $m \times m$ fibers can be used to measure properties other than the properties in the fibers of sub-bundle 21, e.g., true ranging polarization and the like.

This modification of the fiber architecture, namely, the reference probe, can be used to solve additional problems in the multi-pixel ranging. It is accomplished by splitting out one fiber 1 from each $m \times m$ fiber sub-bundle 21, forming a parallel bundle 22 of non-delaying equal length fibers and coupling it to an additional detector (not shown), designed to measure the other specific light echo properties.

Thus, if sub-bundles 21 are used to measure the distances to the target pixels using the delay solution according to the present invention, bundle 22 may be used to measure the genuine, undelayed ranges, thus enabling the system to distinguish between proper target induced light echoes and ghost echoes that are caused by the presence of irrelevant, additional obstacles positioned in front of the main target (i.e., birds, poles). The signal addressing logic 8, when given pixel-related delayed ranges, together with correct non-pixel-related delayed ranges can calculate correct pixel-related ranges. Such additional information, when correctly used, will prevent the inclusion of these obstacles in the final target ranging, thus reducing system false alarms. This additional information will enable the logic unit to determine the correct range pixel identification of light echoes when the scene depth, i.e., the range difference between the nearest and furthest object in the scene is similar to the system- induced delays.

Another use of the additional sub-bundle illustrated in Fig. 9 is when it is connected to a light-intensity measuring detector 23. This application uses a bundle 22 as a reference probe to prevent the main detector electronics and logic 8 from being blinded by high-intensity light echoes. The signal from the undelayed bundle

22 arrives at its detector 23 early enough to let main detector electronics 8, by means of control circuit 24, to reduce its amplification (voltages) automatically to the required value.

In principle, the fiber-to-detector coupling should not pose any difficulty, being a conventional coupling that transfers light energy to standard detectors. In spite of this, the fact should be kept in mind that various fiber architectures may require different couplings.

When the direct configuration is used, depending on the number of fibers in the bundle, the total diameter of bundle 4 may be smaller or larger than the detector/ receiver diameter. For example, a total number of 20 fibers, each of a diameter of 30 μm, results in a bundle diameter of 600 μm = 0.6 mm. A diode of an effective diameter of 2 mm may accept such a bundle directly, without the need for a mediator. When, on the other hand, the fibers are of diameters of 200 μm each, the total bundle diameter will be 4 mm, a value which exceeds the effective diameter of the detector. This requires the use of a mediator, such as that shown in Fig. 10, comprising a mounting 26 accommodating the end of bundle 4, as well as a short focal length lens 28 that concentrates the light from bundle 4 onto detector/receiver 6.

The above-mentioned combined fiber architecture ends in the shape of a single main fiber, of a diameter that may be from 100-500 μm. When detector/receiver 6 is of a diameter of 0.1-1 mm, it can accept the fiber as is. But in the extreme case of a thin fiber (100 μm) and a large-aperture detector (2-4 mm), in spite of the fact that the direct approach may be adequate, it is advised that the light be diffused over the entire detector aperture, in order not to be dependent on the detector surface homogeneity. In this case, a main fiber may be used that flares at its end to match the detector diameter, as seen in Fig. 11. Alternatively, a mediating lens 28 may be used in an arrangement similar to that of Fig. 10 (see also Fig. 12).

By way of example, Fig. 13 represents a detailed block diagram of the electronics associated with the single detector/receiver 6 coupled to fiber bundle 4 in an arrangement used to produce range measurements. Seen are detector/receiver 6, feeding a preamplifier 30, a TPG amplifier 32, an A/D converter 34 leading to a memory 36, and decoding and processing unit 38. The unit 38 is operationally interconnected with the preamplifier 30, the amplifier 32, the A/D converter 34 and the memory 36. Advantageously, there is also provided a voltage control unit 40, and a range output at 42.

It will be evident to those skilled in the art that the invention is not limited to the details of the foregoing illustrated embodiments and that the present invention may be embodied in other specific forms without departing from the spirit or essential attributes thereof. The present embodiments are therefore to be considered in all respects as illustrative and not restrictive, the scope of the invention being indicated by the appended claims rather than by the foregoing description, and all changes which come within the meaning and range of equivalency of the claims are therefore intended to be embraced therein.

WHAT IS CLAIMED IS:

1. A method for non-scanning multi-pixel ranging of a scene, comprising the steps of:

providing a single detector/receiver associated with a time-delay arrangement;

producing a time-arrival distribution of pulse echoes of at least part of a remote scene in a defined ranging plane;

receiving said distribution as produced on said ranging plane and conveying it, echo pulse by echo pulse through a plurality of echo pulse conveying means to said single detector/receiver, while introducing a time delay, whereby said echo pulses arrive at said single detector/receiver in a sequential order, and

reconstructing said time-arrival distribution from said time-delayed echo pulses received by said detector/receiver, and

providing an output exhibiting ranging of said scene.

2. The method as claimed in claim 1, wherein said echo pulses conveying means is a bundle of optical fibers and further comprising the step of providing each of said echo pulses-conveying means with a different length, thereby producing said time-delay.

3. A system for ranging of a scene, comprising:

optical means to create a replicate of a remote scene range distribution on a defined ranging plane;

time-ordered echo pulses conveying means receiving said echo pulses from said ranging plane, each of said conveying means constituting an optical path of different length, introducing time delays;

a single detector/receiver for detecting the echo pulses time of arrival in a sequential order produced by said time delays, and

an electronic logic fed by said single detector to reconstruct said time-arrival distribution from said time-delayed echo pulses, to produce an output exhibiting ranging of said scene.

4. The system as claimed in claim 3, wherein said echo pulses conveying means is a bundle of optical fibers leading from said ranging plane to said single detector/ receiver.

5. The system as claimed in claim 3, wherein said echo pulses conveying means is a bundle of optical fibers of different lengths.

6. The system as claimed in claim 3, wherein said single detector is an avalanche photo diode.

7. The system as claimed in claim 5, wherein said bundle of optical fibers is of a configuration requiring two-dimensional scanning.

8. The system as claimed in claim 5, wherein said bundle of optical fibers is of a configuration requiring one-dimensional scanning.

9. The system as claimed in claim 5, wherein said bundle of optical fibers is of the staring, non-scanning type.

10. The system as claimed in claim 4, wherein the ranging plane and portion of said fiber bundle consist of a single, substantially linear array of fibers.

11. The system as claimed in claim 4, wherein said bundle of optical fibers is constituted by a length of a main fiber of an enlarged diameter and a plurality of smaller diameter fibers commencing from said ranging plane and entering said main fiber along its length.

12. The system as claimed in claim 3, further comprising an echo pulse intensity measuring and controlling unit interposed in circuit between the ranging plane and

said detector/receiver for preventing saturation of said detector/receiver by high intensity echo pulses.

13. The system as claimed in claim 12, wherein said measuring and controlling unit is fed by a non-time-delaying secondary function bunch of fibers.

14. The system as claimed in claim 13, wherein said detector/receiver is defined by a light-detecting aperture and said system further comprises a light diffuser affixed between at least some of the optical fibers and said detector/receiver for diffusing echo pulses over substantially the entire detector aperture.

15. The system as claimed in claim 14, wherein said light diffuser is an optical fiber section flaring at its end to substantially match the detector/receiver's aperture.

16. The system as claimed in claim 15, wherein said light diffuser is a mediating lens.

17. The system as claimed in claim 5, further comprising a sub-bundle of optical fibers for detecting objects located between the scene to be ranged and said ranging plane.